Show all of your work on this assignment and answer each question fully in the given context.

## Please staple your assignment!

1. Chapter 4, Exercise 12, page 208(skip part d) [5 pts each part, 15 pts total]

(a) is the sum of the R<sup>2</sup> values from the two one-variable linear equations.

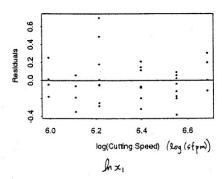
$$\ln y = 18.750 - 5.1209 \ln x_1 - 3.7379 \ln x_2,$$

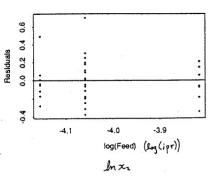
with an  $R^2$  of .960. The relationship  $yx_1^{\alpha_1}x_2^{\alpha_2}=C$  implies that

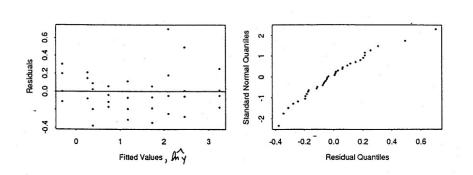
$$\ln y = \ln C - \alpha_1 \ln x_1 - \alpha_2 \ln x_2,$$

so 
$$\hat{\alpha}_1 = -b_1 = 5.1209$$
,  $\hat{\alpha}_2 = -b_2 = 3.7379$ , and  $\hat{C} = e^{b_0} = 1.39 \times 10^8$ .

(b)







The plot of Residuals versus  $\ln y$  shows a slight amount of curvature, but the pattern is not strong. The plot of Residuals versus  $\ln x_1$  shows that there is more spread in the response when  $\ln x_1 = 6.2146$  ( $x_1 = 500$ ), and the plot of Residuals versus  $\ln x_2$  shows that there is more spread in the response when  $\ln x_2 = -4.05994$  ( $x_2 = .01725$ ). The normal plot of residuals is fairly linear, indicating that the residuals are bell-shaped. Overall, the residual plots do not reveal any major problems with the fitted model.

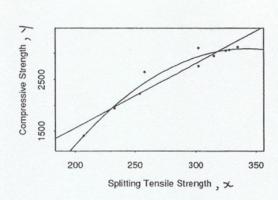
(c) For 
$$x_1 = 550$$
 and  $x_2 = .01650$ , 
$$\ln y = \ln \hat{C} - \hat{\alpha}_1 \ln(550) - \hat{\alpha}_2 \ln(.01650) = 1.7789,$$

so  $\hat{y} = e^{1.7789} = 5.92$  minutes.

(d)

## 2. Chapter 4, Exercise 16 [a-g][5 pts each part, 35 pts total]





The relationship is not quite linear.

(b) The calculations are given below:

| i  | $x_i$ | $x_i^2$ | $y_i$ | $y_i^2$  | $\frac{x_i y_i}{293940}$ |  |
|----|-------|---------|-------|----------|--------------------------|--|
| 1  | 207   | 42849   | 1420  | 2016400  |                          |  |
| 2  | 233   | 54289   | 1950  | 3802500  | 454350                   |  |
| 3  | 254   | 64516   | 2230  | 4972900  | 566420                   |  |
| 4  | 328   | 107584  | 3070  | 9424900  | 1006960                  |  |
| 5  | 325   | 105625  | 3060  | 9363600  | 994500                   |  |
| 6  | 302   | 91204   | 3110  | 9672100  | 939220                   |  |
| 7  | 258   | 66564   | 2650  | 7022500  | 683700                   |  |
| 8  | 335   | 112225  | 3130  | 9796900  | 1048550                  |  |
| 9  | 315   | 99225   | 2960  | 8761600  | 932400                   |  |
| 10 | 302   | 91204   | 2760  | 7617600  | 833520                   |  |
|    | 2859  | 835285  | 26340 | 72451000 | 7753560                  |  |

$$r = \frac{\sum x_i y_i - \frac{(\sum x_i)(\sum y_i)}{n}}{\sqrt{\left(\sum x_i^2 - \frac{(\sum x_i)^2}{n}\right) \left(\sum y_i^2 - \frac{(\sum y_i)^2}{n}\right)}}$$

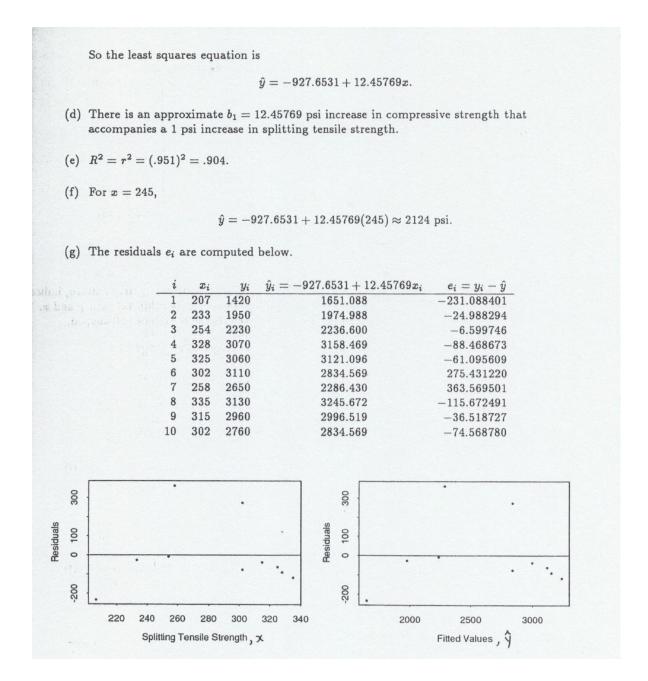
$$= \frac{7753560 - \frac{(2859)(26340)}{10}}{\sqrt{\left(835285 - \frac{(2859)^2}{10}\right) \left(72451000 - \frac{(26340)^2}{10}\right)}} = .951.$$

This is close to 1, so there is a fairly strong positive linear relationship between y and x.

(c)

$$b_1 = \frac{\sum x_i y_i - \frac{(\sum x_i)(\sum y_i)}{n}}{\sum x_i^2 - \frac{(\sum x_i)^2}{n}} = \frac{7753560 - \frac{(2859)(26340)}{10}}{835285 - \frac{(2859)^2}{10}} = 12.45769$$

$$b_0 = \bar{y} - b_1 \bar{x} = \frac{26340}{10} - (12.45769) \frac{2859}{10} = -927.6531$$



## 3. This is the rest of the problem 5 in HW 4.

The major cause of axel failure in freight trucks is when shippers exceed the recommended weight limits that can be handled by the axels. Issues resulting from these failures have been becoming more frequent as shippers try to cut corners, leading members of the state's Department of Transportation to ask one of their civil engineers to look into the available data and better advise them on the relationship between excessive weight and axel failure.

A company manufacturing axels provides the engineer with data gathered from conducting experiments loading axels with excessive weight and simulating traveling conditions. The data consists of two columns, excessive weight (in tonnes) is the amount of weight over the limit that was placed on the axel, and distance to failure (in tens of thousands of miles) is the simulated distance to the axel's failure.

Here are some summaries of the data:

$$\sum_{i=1}^{50} x_i = 64$$

$$\sum_{i=1}^{50} x_i^2 = 107$$

$$\sum_{i=1}^{50} y_i = 2025$$

$$\sum_{i=1}^{50} x_i y_i = 2028$$

The JMP output below comes from fitting a quadratic model using x and  $x^2$ .

| Respons                | esponse Distance to Failure |            |           |       |       |         |         |  |  |  |  |  |
|------------------------|-----------------------------|------------|-----------|-------|-------|---------|---------|--|--|--|--|--|
| Summa                  | ry of l                     | Fit        |           |       |       |         |         |  |  |  |  |  |
| RSquare                | REDACTED                    |            |           |       |       |         |         |  |  |  |  |  |
| RSquare A              | REDACTED                    |            |           |       |       |         |         |  |  |  |  |  |
| Root Mear              | n Squar                     | 5.281589   |           |       |       |         |         |  |  |  |  |  |
| Mean of R              | espons                      | 0.16       |           |       |       |         |         |  |  |  |  |  |
| Observation            | ons (or                     | 50         |           |       |       |         |         |  |  |  |  |  |
| Analysis of Variance   |                             |            |           |       |       |         |         |  |  |  |  |  |
| Sum of                 |                             |            |           |       |       |         |         |  |  |  |  |  |
| Source                 | DF                          | Square     | s Mean Sq | uare  | FF    | Ratio   |         |  |  |  |  |  |
| Model                  | 2                           | 13229.64   | 7 661     | 4.82  | 237.  | 1314    |         |  |  |  |  |  |
| Error                  | 47                          | 1311.07    | 3 2       | 7.90  | Prob  | ) > F   |         |  |  |  |  |  |
| C. Total               | 49                          | 14540.72   | 0         |       | <.0   | 001*    |         |  |  |  |  |  |
| Parameter Estimates    |                             |            |           |       |       |         |         |  |  |  |  |  |
| Term                   |                             |            | Estimate  | Std I | Error | t Ratio | Prob> t |  |  |  |  |  |
| Intercept              |                             |            | 16.27602  | 2.33  | 3507  | 6.97    | <.0001* |  |  |  |  |  |
| Weight Exceeding Limit |                             |            | 4.6604349 | 4.22  | 1593  | 1.10    | 0.2752  |  |  |  |  |  |
| (Weight Ex             | ceedin                      | a Limit)^2 | -10.2775  | 1.60  | 4983  | -6.40   | <.0001* |  |  |  |  |  |

(a) Write the equation of the fitted quadratic relationship. [5 pts]

$$\hat{y} = 16.27602 + 4.6604349x - 10.2775x^2$$

(b) Find and interpret the value of  $R^2$  for the fitted quadratic relationship.[5 pts]

$$R^2 = 1 - SSE/SSTO = 1 - (1311.073/14540.720) = 0.909834382341452$$

In other words, 90.98% of the variability in travel distance to failure can be explained by the linear relationship with weight exceeding guidelines.

Homework # 5

$$\hat{y} = 16.27602 + 4.6604349(3.4) - 10.2775(3.4)^2 = -86.68640134$$

Total: 65 pts