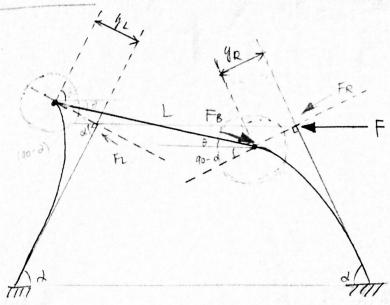
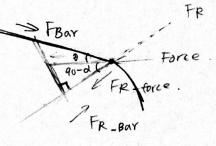
The 1st module

FBD :



$$F_R = F \cdot \cos(q_0 - d) - F_B \cdot \cos(q_0 - d + \theta)$$
 = FBar



pisplacement (9.4):

$$y_R = \frac{FL^3}{3k} = \frac{FR \cdot L^3}{3k}$$

. Force @ left hand side:

Pisplacement (YL):

FL-Bar Force

Far Force

France

$$\theta = \sin^{-1} \left[\frac{(4\rho \cdot \omega sd + 4\iota \cdot \cos d)}{L} \right] - 0$$

$$F_{R} = f(F, d, F_{B}, \theta)$$

$$Q_{R} = f(F_{R}) = f(F, d, F_{B}, \theta)$$

$$\theta = f(Q_{R}, \theta_{L}) = f(F, d, F_{B}, \theta)$$

The displacement on the bar:

$$g_L \cdot \sin(d+\theta) = g_R \cdot \sin(d-\theta)$$
 — 3

Arranging equations 10 to 6), since we have known that external force (F), initial angle (d), and bar-length (L). But, we don't know the force acting on the right and left, which dive FR, FL, and reacting force to the bar (FB). Also, we don't know the angle theta showing in the figure, and displacement at both RHS and LHS (GR and GL)

knows: F, d, L unknows: Fr, FL, Fr, O, gr, gl

$$F_{R} = F \cdot sin(d) - F_{B} \cdot sin(d-\theta)$$

$$y_{R} = \frac{F_{R} \cdot L^{3}}{3k}$$

$$F_{L} = F \cdot sin(d) - F_{B} \cdot sin(d+\theta)$$

$$y_{L} = \frac{F_{L} \cdot L^{3}}{3k}$$

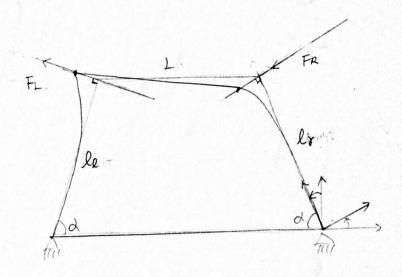
$$y_{L} = \frac{F_{L} \cdot L^{3}}{3k}$$

$$y_{L} \cdot sin(d+\theta) = y_{R} \cdot sin(d-\theta)$$

$$\theta = sin^{-1} \left[\frac{y_{R} \cdot cosd + y_{L} \cdot cosd}{L} \right]$$

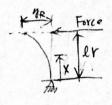
$$\theta = sin^{-1} \left[\frac{y_{R} \cdot cosd + y_{L} \cdot cosd}{L} \right]$$

Since we have six unknows, we use six equations to solve the unknows.



From elastic curve equation, we known that

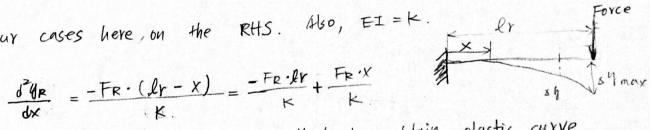
$$\frac{\delta^2 q}{\delta x^2} = \frac{M(x)}{\delta I}$$



 $\frac{\delta^2 q}{dx^2} = \frac{M(x)}{EI}.$ $\frac{\delta^2 q}{dx^2} = \frac{M(x)}{EI}.$ $\frac{\delta^2 q}{dx^2} = \frac{M(x)}{EI}.$

For our cases here on the RHS. Also, EI=K.

$$\frac{d^2 y_R}{dx} = -F_R \cdot (l_r - x) = \frac{-F_R \cdot l_r}{K} + \frac{F_R \cdot x}{K}$$



we use double integration method to obtain elastic curve. Now

$$\frac{dy_R}{dx} = -\left(\frac{F_R \cdot l_r}{k}\right) X + \left(\frac{F_R}{2K}\right) X^2 + C,$$

The initial B.Cs are y=0, y=0, then $0=0-0+C_1 \Rightarrow C_1=0$

The second time intergral =

$$y_R = -\left(\frac{F_R \cdot l_r}{2k}\right) x^2 + \left(\frac{F_R}{3 \cdot 2k}\right) x^3 + C_2$$

Applying initial B.Cs (x=0, y=0), then C2=0.

Therefore, we have displacement equation

$$V_R = -\left(\frac{F_R \cdot l_r}{2k}\right) x^2 + \left(\frac{F_R \cdot k}{6k}\right) x^3 = \frac{F_R x^2}{6k} \left[x - 3l_r\right] \cdot 0 \le x \le L$$

Similarly, for the curvature on the LHS. we can obtain the displacement equation as well.

$$\psi_{L} = -\left(\frac{F_{L} \cdot l_{e}}{2k}\right) x^{2} + \left(\frac{F_{L}}{6k}\right) x^{3} = \frac{F_{L} x^{2}}{6k} \left[x - 3l_{e}\right] \quad 0 \le x \le L.$$

Since we have rotated the cantilever beam, we need to multiply the rotation matrix to obtain our final position for displacement equation.

$$R = \begin{bmatrix} \cos(q_0 - \alpha) & -\sin(q_0 - \alpha) \\ \sin(q_0 - \alpha) & \cos(q_0 - \alpha) \end{bmatrix}$$