

COMMUNICATION THEORY ASSIGNMENT-4

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①

(i) $\theta_i(t) = kt^2$ $H(s) = 1$

$$\theta_e(t) = \theta_i(t) - \theta_o(t)$$

$$H_e(s) = \frac{\theta_i(s) - \theta_o(s)}{\theta_i(s)}$$

$$= \left(\frac{s}{s + KH(s)} \right)$$

$$\theta_i(s) = \mathcal{L}\{kt^2\} = \boxed{\frac{2k}{s^3}}$$

\therefore let us find the value of $\theta_e(t)$ as $t \rightarrow \infty$.
if it converges, we can track the signal
almost upto a constant phase or exactly (if phase = 0)

$$\Rightarrow \lim_{t \rightarrow \infty} \theta_e(t) = \lim_{s \rightarrow 0} \theta_e(s) \cdot s \quad \left(\begin{array}{l} \text{Final value} \\ \text{Theorem property} \\ \text{of LT} \end{array} \right)$$

$$= \lim_{s \rightarrow 0} s \cdot H_e(s) \cdot \theta_i(s)$$

$$= \lim_{s \rightarrow 0} s \cdot \left(\frac{s}{s + KH(s)} \right) \times \frac{2k}{s^3} \quad (H(s) = 1)$$

$$= \lim_{s \rightarrow 0} \left(\frac{2k}{(s + K)s} \right) = \boxed{\infty}$$

$\Rightarrow \theta_e(t)$ as $t \rightarrow \infty$ diverges.

\Rightarrow The incoming signal ~~can~~ not be tracked.

(ii) If $H(s) = \frac{s+a}{s}$,
|||ly, $\lim_{t \rightarrow \infty} \theta_e(t) = ?$

$$\lim_{t \rightarrow \infty} \theta_e(t) = \lim_{s \rightarrow 0} s \theta_e(s) = \lim_{s \rightarrow 0} s \cdot H_e(s) \cdot \theta_i(s)$$

$$= \lim_{s \rightarrow 0} s \cdot \left(\frac{s}{s + K(H(s))} \right) \cdot \frac{2k}{s^3}$$

$$= \lim_{s \rightarrow 0} s \left(\frac{s \cdot s}{s + \frac{K(s+a)}{s} \cdot s} \right) \left(\frac{2k}{s^3} \right)$$

$$= \lim_{s \rightarrow 0} \frac{s^3}{s^2 + K(s+a)} \left(\frac{2k}{s^3} \right)$$

$$= \frac{2k}{0^2 + K(0+a)} = \boxed{\frac{2k}{Ka}}$$

Thus, $\theta_e(t) \rightarrow \frac{2k}{Ka}$ where $t \rightarrow \infty$

\Rightarrow constant-phase difference tracking is possible.

$$(iii) \quad \text{If } H(s) = \frac{s^2 + as + b}{s^2},$$

$$\lim_{t \rightarrow \infty} \theta_e(t) = \lim_{s \rightarrow 0} s \cdot H_e(s) \cdot \Theta_i(s)$$

$$= \lim_{s \rightarrow 0} s \cdot \left(\frac{s}{s + K(H(s))} \right) \cdot \left(\frac{2k}{s^3} \right)$$

$$= \lim_{s \rightarrow 0} s \cdot \left(\frac{s}{s + K \left(\frac{s^2 + as + b}{s^2} \right)} \right) \cdot \frac{2k}{s^3}$$

$$= \lim_{s \rightarrow 0} \frac{\cancel{s}^4 \cancel{s}}{\cancel{s}^3 + K\cancel{s}^2 + Kas + Kb} \cdot \frac{2k}{\cancel{s}^3}$$

$$= \boxed{0}$$

\Rightarrow No phase error = 0 phase error tracking of the incoming signal.

(2)

(a)

Central freq = 1800.5 MHz

\therefore for $f_{IF} = 250 \text{ MHz}$, we have 2 possible f_{LO} .

(i) $f_{LO} = f_{RF} - f_{IF} = 1549.5 \text{ MHz}$
or

(ii) $f_{LO} = f_{RF} + f_{IF} = 2050.5 \text{ MHz}$

The f_{LO} obtained in (i) is within the tunable range of freq synth.

but (ii) does not as it is above the range and also cannot be obtained by ~~frequency division~~ frequency division by integer from tunable range.

\therefore we let $f_{LO} = 1549.5 \text{ MHz}$

$$f_{RF} = f_{LO} - f_{IF} = 1800.5 \text{ MHz and}$$

$$f_{IM} (\text{Image freq}) = f_{LO} + f_{IF} = \boxed{2300.5 \text{ MHz}}$$

RF filter must be centred ~~at~~ at 1800.5 MHz
thereby passing signals in the range 1800-1801 MHz
and reflecting frequency of Image at 2300.5 MHz.

A bandwidth of 50 MHz also comfortably allows for
this. The IF at 250 MHz should pass message at
249.5 MHz and quickly cut off after that range.

(b) ~~Centre freq~~ = 900.5 MHz $f_{IF} = 250 \text{ MHz}$

1/1 by 2 choices for f_{LO} :

i) $f_{LO} = f_{RF} + f_{IF} = 1150.5 \text{ MHz}$

ii) $f_{LO} = f_{RF} - f_{IF} = 649.5 \text{ MHz}$

Both are outside tunable range, but f_{LO} in ii)
can be obtained by dividing 1948.5 MHz by 3
and $(1948.5) \text{ MHz}$ falls inside Tunable range.

\Rightarrow We let $f_{LO} = 649.5 \text{ MHz}$.

$$\Rightarrow f_{RF} = f_{LO} + f_{IF} = \underline{\underline{900.5 \text{ MHz}}}$$

$$f_{IM} (\text{Image freq}) = f_{LO} - f_{IF} = \underline{\underline{399.5 \text{ MHz}}}$$

RF centered at 900.5 MHz
passes frequencies at 900 - 901 MHz
rejects 399.5 MHz.

~~20~~ 20 MHz bandwidth works.

IF filter at 250 MHz must pass
message at 249.5 MHz and
sharply cut off thereafter