

→ Meaning of Impulse Invariant in IIT :

i. After transformation

$$(s+p_i) \rightarrow (-e^{j\omega T} z^{-1})$$

$$\left( \frac{1}{s-p_i} \right) \xrightarrow{\text{Converts s to } z} \left( \frac{1}{1 - e^{j\omega T} z^{-1}} \right)$$

i.e.,

after transformation of analog filter

into digital filter, shape of impulse

response (shape of o/p for impulse i/p)

remain same i.e., impulse response becomes invariant.

Justification of Above Statement

$$\text{i/p } x_a(t) = s(t) \xrightarrow{\text{H}_a(s) = \sum_{i=1}^N \frac{A_i}{s-p_i}} \text{o/p } y_a(t)$$

Analog filter

$$x_a(t) = s(t) \xrightarrow{\text{L.T}} X(s) = 1.$$

$$y(t) \xrightarrow{\text{L.T}} Y(s)$$

$$\text{Since } Y(s) = X(s) \cdot H_a(s)$$

$$\Rightarrow Y(s) = 1 \cdot \sum_{i=1}^N \frac{A_i}{s-p_i} \quad \left\{ \text{since } X(s) = 1 \right\}$$

$$\Rightarrow y(t) = \text{Inverse L.T of } Y(s)$$

$$y_a(t) = \sum_{i=1}^N A_i e^{p_i t} u(t).$$

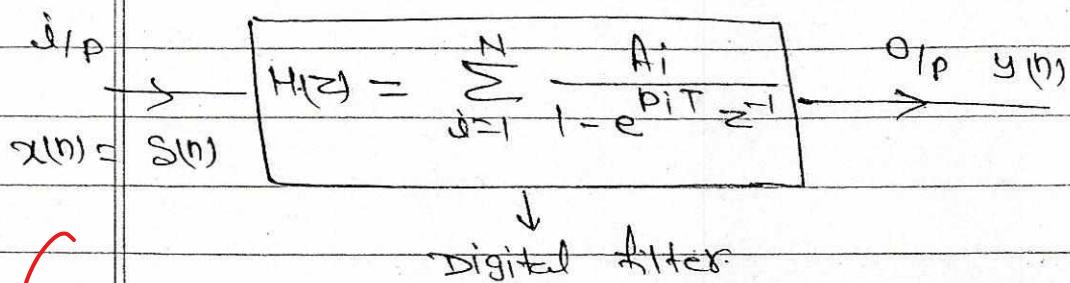
$$\text{So, sampled o/p} = y_a(t) \mid \text{at } t=nT$$

$$\text{Sampled o/p} = \sum_{i=1}^N A_i e^{p_i nT} u(nT) \quad \text{--- (1)}$$

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Now find O/P of [REDACTED] digital filter  
when I/P is [REDACTED] impulse  $x(n) = s(n)$



$$x(n) = s(n) \xrightarrow{z \cdot T} X(z) = 1$$

$$y(n) \xrightarrow{z \cdot T} Y(z)$$

$$\text{So, } Y(z) = X(z) H(z)$$

$$\Rightarrow Y(z) = 1 \cdot \sum_{i=1}^N \frac{A_i}{1 - e^{B_i T} z^{-1}}$$

$y(n)$  = inverse  $z \cdot T$  of  $Y(z)$ .

$$y(n) = \sum_{i=1}^N A_i \cdot e^{B_i T n} u(n).$$

$$\Rightarrow \left( \begin{array}{l} \text{O/P of digital filter} \\ \text{when I/P = impulse } s(n) \end{array} \right) = \sum_{i=1}^N A_i e^{B_i T n} u(n) \quad \text{--- (1)}$$

using eqn (1) & (11)

$$\left( \begin{array}{l} \text{sampled O/P of} \\ \text{analog filter when} \\ \text{I/P is impulse} \end{array} \right) = \left( \begin{array}{l} \text{digital O/P of digital filter} \\ \text{when I/P is impulse.} \end{array} \right)$$

Impulse response is invariant after transformation of

$$\frac{1}{s - p_i} \xrightarrow{\text{info}} \frac{1}{1 - e^{B_i T} z^{-1}}$$

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Why not step invariant?

X

$$\xrightarrow{\text{I/P}} \boxed{x(t) = u(t) \quad H_0(s) = \sum_{i=1}^N \frac{A_i}{s-p_i} \quad \xrightarrow{\text{O/P}} y_a(t)}$$

$$x(t) = u(t) \xrightarrow{\text{L.T.}} X(s) = \frac{1}{s}$$

$$y_a(t) \xrightarrow{\text{L.T.}} Y(s)$$

$$\text{So, } Y(s) = X(s) \cdot H_0(s).$$

$$Y(s) = \frac{1}{s} \cdot \sum_{i=1}^N \frac{A_i}{s-p_i}$$

$$Y(s) = \sum_{i=1}^N \frac{A_i}{s(s-p_i)}$$

After partial fraction.

$$Y(s) = \sum_{i=1}^N \frac{A_i}{p_i} \left( \frac{1}{s-p_i} - \frac{1}{s} \right)$$

$y_a(t)$  = inverse L.T of  $Y(s)$

$$y_a(t) = \sum_{i=1}^N \frac{A_i}{p_i} \left( e^{p_i t} u(t) - u(t) \right)$$

Sampled O/P =  $y_a(t)$  at  $t = nT$ .

$$\text{(sampled O/P)} = \sum_{i=1}^N \frac{A_i}{p_i} (e^{p_i nT} - 1) u(nT). \quad 1$$

Now find digital O/P when itp.

$x(n)$  is step if  $x(n) = \infty$  when  $x(n) = u(n)$

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$$\text{i/p} \rightarrow H(z) = \frac{\sum A_i}{1 - e^{P_i T} z^{-1}} \rightarrow \text{o/p}$$

~~X(n)~~  
~~U(n)~~

$$x(n) = u(n) \Rightarrow X(z) = \frac{1}{1 - z^{-1}}.$$

$$\text{So, } Y(z) = X(z) \cdot H(z).$$

$$= \left( \frac{1}{1 - z^{-1}} \right) \sum_{i=1}^N \frac{A_i}{1 - e^{P_i T} z^{-1}}$$

~~X~~ After partial fraction and inverse Z-T.

$$y(n) = \sum_{i=1}^N \frac{A_i}{1 - e^{P_i T}} \left( 1 - e^{P_i (n+1)T} \right) u(n).$$

~~X~~  $\Rightarrow$  digital O/P of  
 digital filter.  
 when i/p is step

$$= \sum_{i=1}^N \left( \frac{A_i}{1 - e^{P_i T}} \right) \left( 1 - e^{P_i (n+1)T} \right) u(n)$$

ii)

~~X~~ using equation (i) and (ii)

~~X~~ Sampled O/P of  
 analog filter for step i/p    // O/P of digital filter  
 when i/p is step

~~X~~ So step response has changed  
 $\Rightarrow$  step response is not invariant

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## ✓ Mapping of S plane into Z plane For Impulse-Invariant Transformation (IIT)

For impulse invariant transformation

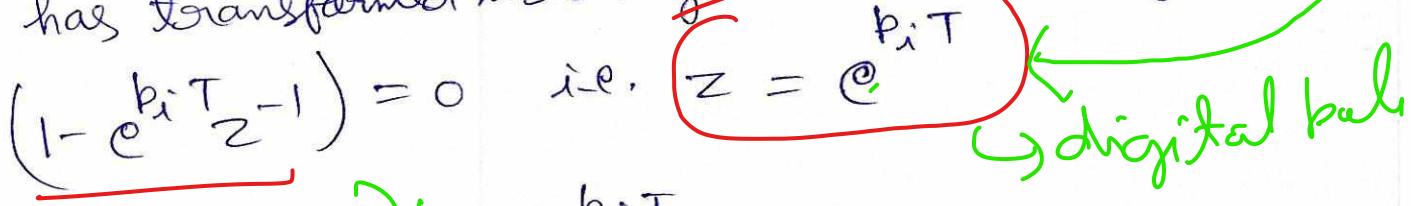
$$\left( \frac{1}{s - p_i} \right) \xrightarrow{\text{has transformed into}} \left( \frac{1}{1 - e^{p_i T} z^{-1}} \right)$$



Analog pole given by  $(s - p_i) = 0$  i.e.  $s = p_i$

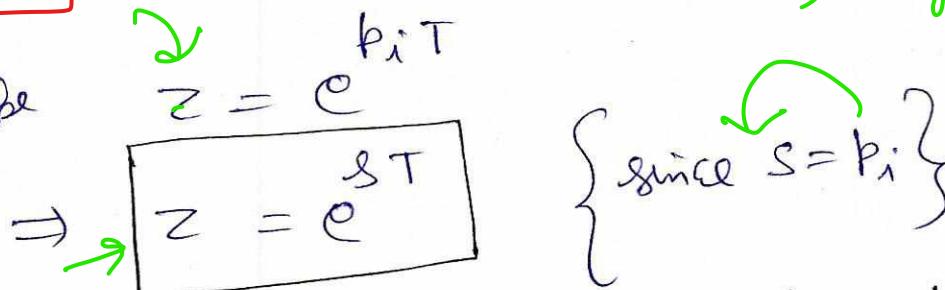
has transformed into digital pole given by

$$\left( 1 - e^{p_i T} z^{-1} \right) = 0 \quad \text{i.e. } z = e^{p_i T}$$



New pole

$$z = e^{\frac{sT}{p_i T}}$$

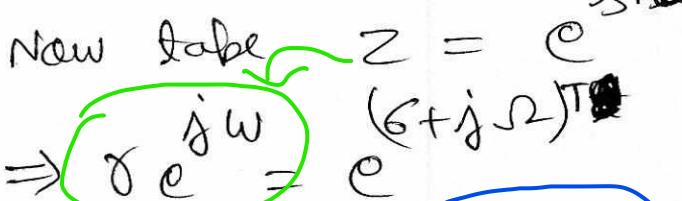


Relation between digital pole and analog pole.

$$\gamma = G + j\omega$$

$$\gamma = \gamma e^{j\omega}$$

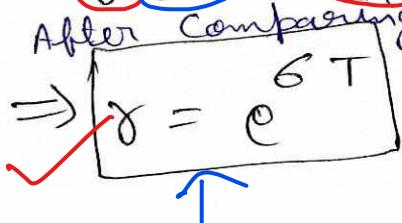
$$\text{New pole } z = e^{\frac{sT}{(G+j\omega)T}}$$



$$\Rightarrow \gamma e^{\frac{j\omega}{G+j\omega}} = e^{\frac{G \cdot T}{G+j\omega}}$$

After Comparing real and imaginary part, we get

$$\Rightarrow \gamma = e^{\frac{G \cdot T}{G+j\omega}}$$



$$\text{and } W = -\omega T$$

Relation between digital frequency  $\omega$  and analog frequency  $\omega$ .

Now take

$$\gamma = e^{j\theta T}$$

Case I

$$\text{when } \theta > 0 \Rightarrow (\gamma > 1)$$



region in the right-hand side of jw-axis on S plane

$$\begin{aligned} \gamma &= e^{j\theta T} \\ \gamma &= e^{j\theta} \\ \gamma &= e^{j\theta} \\ \gamma &> 1 \end{aligned}$$

$\gamma > 1$  is region outside unit circle

So region on the right hand side of S plane has been mapped into region outside unit circle

For an unstable analog filter, we will get an unstable digital filter.

Case II

$$\text{when } \theta < 0 \Rightarrow \gamma < 1$$

$$\gamma = e^{j\theta T}$$

$$e^{-4} = \frac{1}{e^{\theta T}} < 1$$

region in the left hand side of jw-axis on S plane

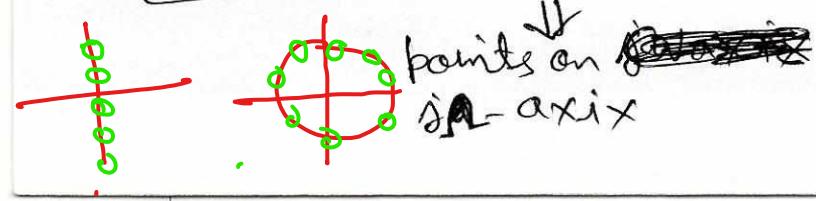
region inside unit circle.

So region on the left hand side of S plane has been mapped into region inside unit circle.

For an stable analog filter, we will get stable digital filter

Case III

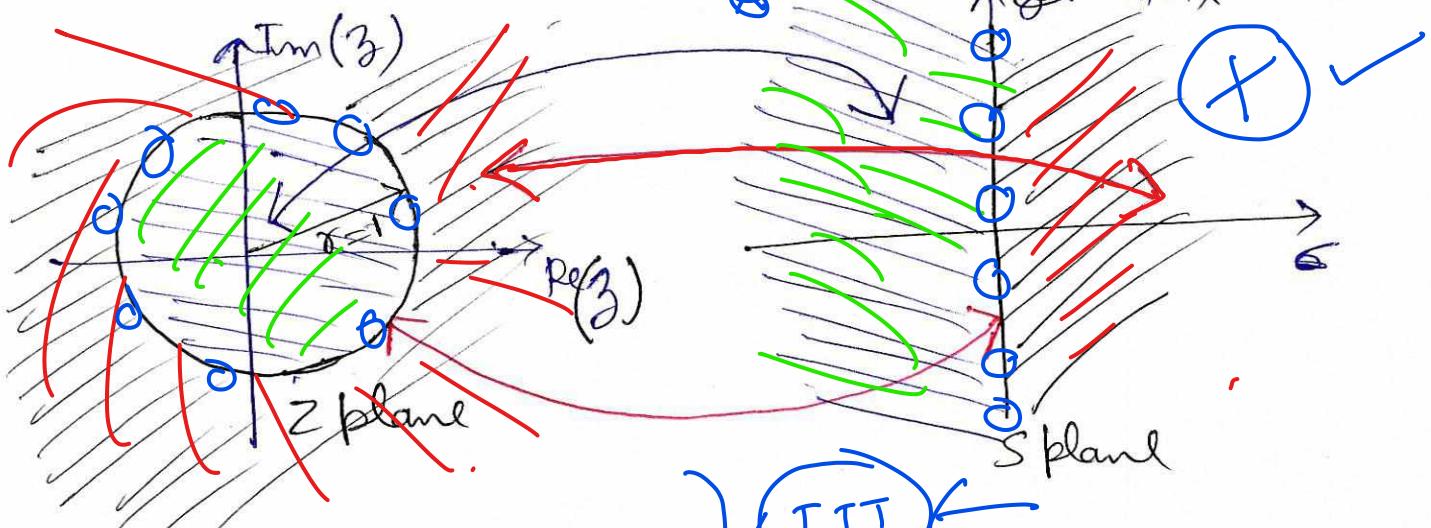
$$\text{when } \theta = 0 \text{ then } \gamma = 1$$



$$\begin{aligned} \gamma &= e^{j\theta T} \\ \gamma &= e^{j0} \\ \gamma &= e^0 \\ \gamma &= 1 \end{aligned}$$

points on unit circle.

So points on  $j\omega$ -axis has been mapped onto points on unit circle.



Mapping of S plane into Z-plane.

Mapping of S-plane into Z-plane For Bilinear Transformation (BLT)

For Bilinear transformation (BLT),  $\delta = \frac{2}{T} \left( \frac{z-1}{z+1} \right)$

Now since  $\delta = \sigma + j\omega$  and  $z = e^{j\omega}$

$$\text{So } \sigma + j\omega = \frac{2}{T} \left( \frac{e^{j\omega} - 1}{e^{j\omega} + 1} \right)$$

$$\Rightarrow \sigma + j\omega = \frac{2}{T} \left\{ \frac{\gamma (\cos \omega + j \sin \omega) - 1}{\gamma (\cos \omega + j \sin \omega) + 1} \right\}$$

After separating real and imaginary part of RHS

$$\sigma + j\omega = \frac{2}{T} \left( \frac{\gamma^2 - 1}{1 + \gamma^2 + 2\gamma \cos \omega} \right) + j \left( \frac{2\gamma \sin \omega}{1 + \gamma^2 + 2\gamma \cos \omega} \right)$$

After Comparing real and imaginary part on both side,  
we get

$$\sigma = \frac{2}{T} \left( \frac{\gamma^2 - 1}{1 + \gamma^2 + 2\gamma \cos \omega} \right)$$

$$\omega = \frac{2}{T} \left( \frac{2\gamma \sin \omega}{1 + \gamma^2 + 2\gamma \cos \omega} \right)$$

Now take  $\sigma = \frac{2}{T} \left( \frac{\gamma^2 - 1}{1 + \gamma^2 + 2\gamma \cos \omega} \right)$

$$\begin{aligned} \gamma^2 - 1 &= 0 \\ \gamma &= 1 \Rightarrow \sigma = 0 \\ (\gamma^2 - 1) &> 0 \end{aligned}$$

**Case I** when  $\gamma > 1$

$$\sigma > 0 \quad \gamma^2 > 1 \quad \gamma > 1$$

~~region in the right hand side of  $j\omega$ -axis on S-plane.~~

~~region in the right hand side (RHS) of  $j\omega$ -axis on S-plane.~~

$$(\gamma^2 - 1) > 0 \Rightarrow (\gamma^2 - 1) = +$$

~~region outside unit circle~~

So region on the right hand side of S-plane has been mapped into region outside unit circle.

**Case II**

when  $\gamma < 1$

$$\sigma < 0$$

$\downarrow$

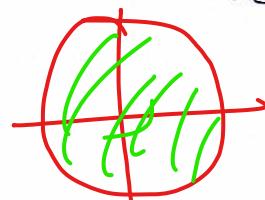
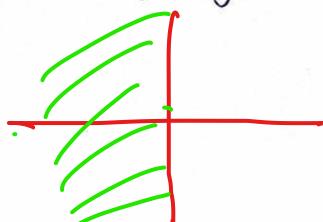
~~region on the left hand side (LHS) of  $j\omega$ -axis on S-plane.~~

$$(\gamma^2 - 1) < 0 \Rightarrow (-)$$

~~region inside unit circle~~

$$\gamma < 1 \rightarrow$$

So region on the left hand side of S-plane has been mapped into region inside unit circle.

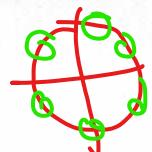


**Case III**

when  $\gamma = 1$

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$\delta = 0$

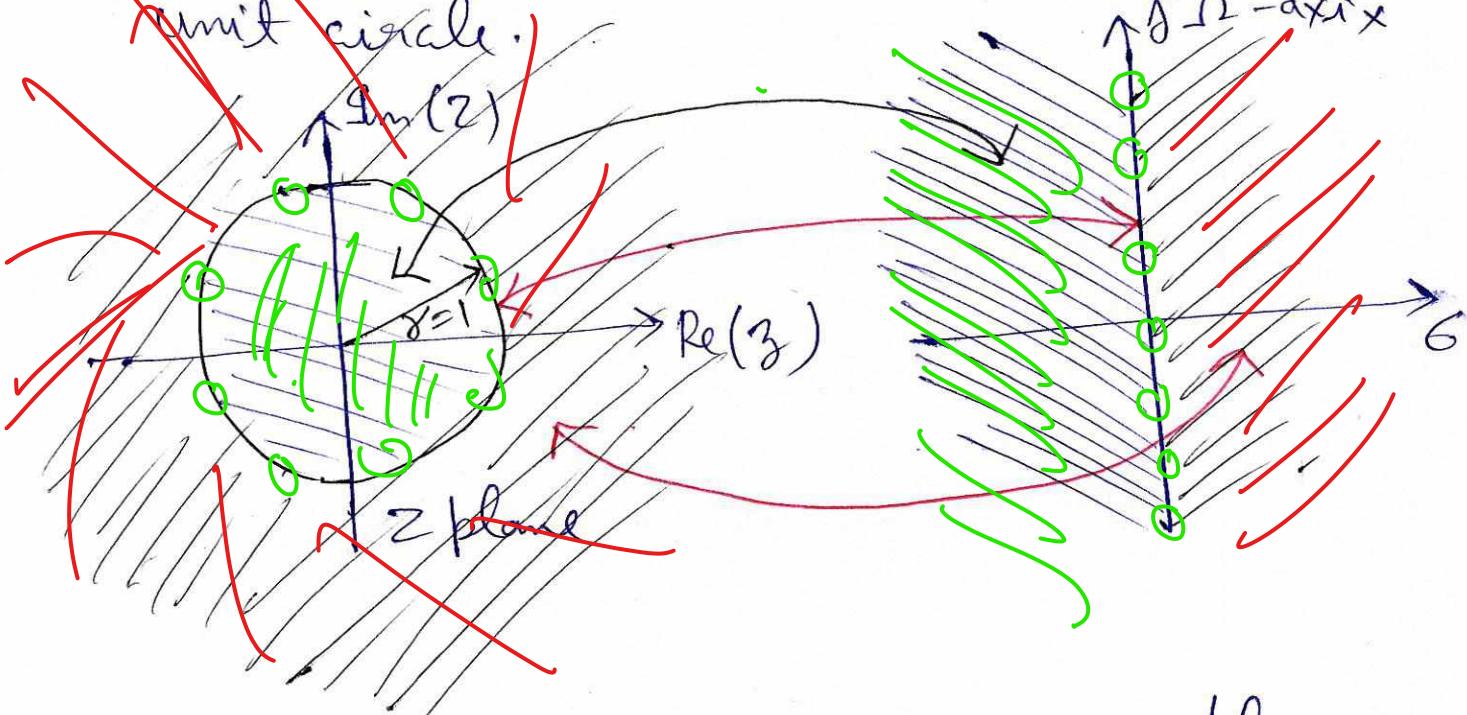


points on the unit circle.

points on the  $j\Omega$ -axis

so points on  $j\Omega$ -axis has been mapped onto

unit circle.



Mapping of S plane into Z plane.

Relation Between  $\Omega$  and  $w$  for Bilinear Transformation (BLT)

we know that for Bilinear Transformation,

$$\Omega = \frac{2}{T} \frac{2\gamma \sin w}{1 + \gamma^2 + 2\gamma \cos w}$$

when  $\gamma = 1$  then

$$\Omega = \frac{2}{T} \left( \frac{2 \sin w}{1 + 2 \cos w} \right)$$

$$\cos \theta = \left( 2 \cos^2 \frac{\theta}{2} - 1 \right) \quad (10)$$

$$\Rightarrow \Omega = \frac{2}{T} \frac{2 \sin w}{2 + 2 \cos w} = \frac{2}{T} \left( \frac{2 \sin w}{2(1 + \cos w)} \right)$$

$$\Rightarrow \Omega = \frac{2}{T} \left( \frac{\sin w}{1 + \cos w} \right) = \frac{2}{T} \cdot \left( \frac{\frac{2 \sin w}{2} \cos \frac{w}{2}}{1 + 2 \cos^2 \frac{w}{2} - 1} \right)$$

$$\Rightarrow \Omega = \frac{2}{T} \frac{2 \sin \frac{w}{2} \cos \frac{w}{2}}{2 \cos^2 \frac{w}{2}}$$

$$\Rightarrow \Omega = \frac{2}{T} \left( \frac{\sin \frac{w}{2}}{\cos \frac{w}{2}} \right) \Rightarrow \boxed{\Omega = \frac{2}{T} \tan \frac{w}{2}}$$

$$\Rightarrow \frac{\Omega T}{2} = \tan \frac{w}{2} \Rightarrow \frac{w}{2} = \tan^{-1} \left( \frac{\Omega T}{2} \right)$$

$$\Rightarrow w = 2 \tan^{-1} \left( \frac{\Omega T}{2} \right)$$

since range of  $\tan^{-1}( )$  is from  $-\frac{\pi}{2}$  to  $\frac{\pi}{2}$

so range of  $2 \tan^{-1}( )$  will be from  $-\pi$  to  $\pi$ .

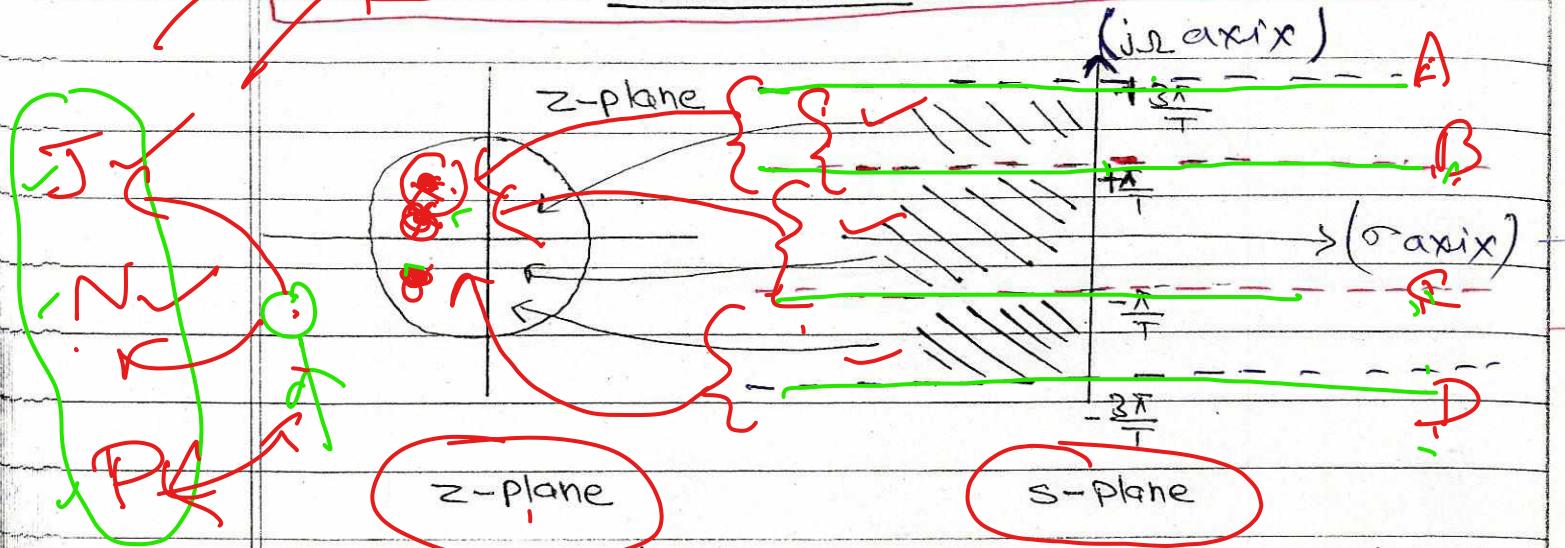
$$\tan^{-1}( ) \rightarrow \left[ -\frac{\pi}{2}, \frac{\pi}{2} \right]$$

$$2 \tan^{-1}( ) \rightarrow [-\pi, \pi]$$

# Disadvantage (ii) of IIT

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Aliasing      Problem In Impulse Transformation :-      Invariant



In case of Impulse Invariant transformation  
 $\omega = \Omega T$

So when  $-\frac{\pi}{T} < \sigma < +\frac{\pi}{T}$   $\omega = \Omega T$

then  $-\pi \leq \omega \leq +\pi$

when  $+\frac{\pi}{T} < \sigma < +\frac{3\pi}{T}$

then  $+\pi \leq \omega \leq +3\pi$

$-\pi \leq \omega \leq +\pi$  (How)

Similarly

when  $-\frac{3\pi}{T} < \sigma < -\frac{\pi}{T}$

then  $-3\pi \leq \omega \leq -\pi$

$-\pi \leq \omega \leq +\pi$  (How)

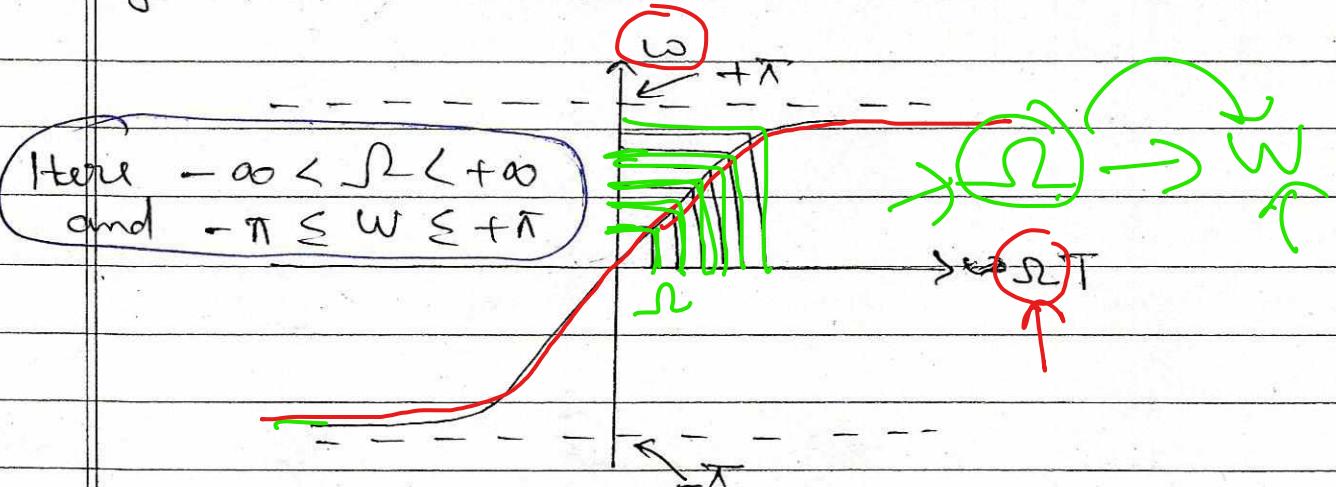
So mapping of analog frequency  $\omega$  to variable  $\omega$  in digital domain is many to one which reflects effect of aliasing

So because of many to one mapping, there is effect of aliasing in TST method.

### Absence of Aliasing In Bilinear Transformation :-

In case of Bilinear Transformation

Since  $\omega = \frac{\pi}{T} \tan^2 \frac{j\omega}{2}$ , so its graph is given as below:



Entire range of  $\omega$  is mapped into range  $\rightarrow -\pi \leq w \leq +\pi$

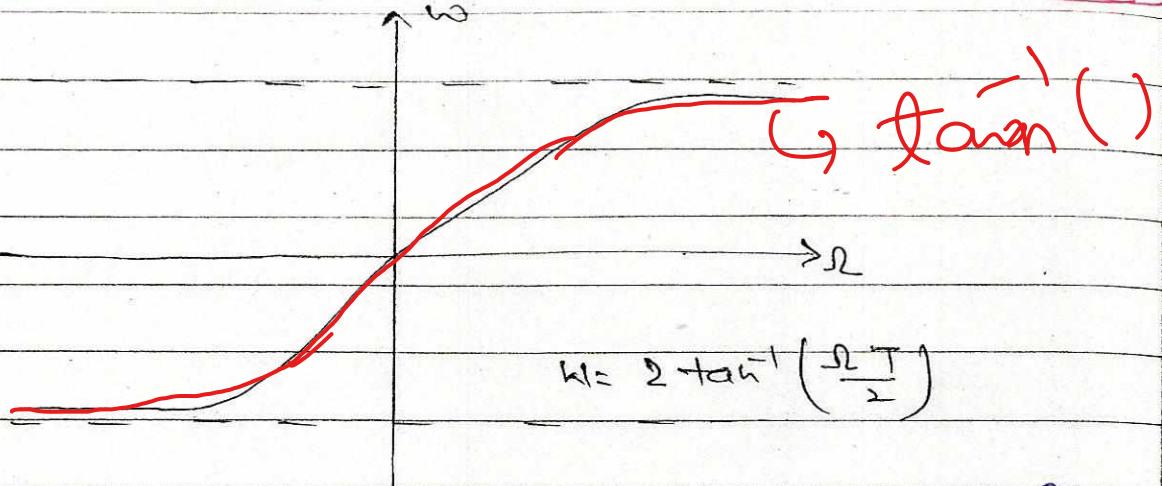
$$S = \frac{2}{T} \left( \frac{z-1}{z+1} \right)$$

$$\Rightarrow s+j\omega = \frac{2}{T} \left( \frac{e^{jw}-1}{e^{jw}+1} \right)$$

so for one value of  $w$ , there is only one value of  $s$ : so there is one to one mapping  $\Rightarrow$  No effect of aliasing

## Effect of Warping In Bilinear Transformation

**Wood Door**



Warping  $\Rightarrow$  something in twisted form.

**WARNING**

Here mapping is highly non-linear because of  $\tan^{-1}$  function.

So there is warping due to nature of non-linearity in  $\tan^{-1}$  function.

## Matched Z-transform

If  $z_1, z_2, \dots, z_m$  are zeroes of analog filter and  $p_1, p_2, \dots, p_N$  are poles of analog filter then.

$$H_a(s) = \frac{(s-z_1)(s-z_2) \dots (s-z_m)}{(s-p_1)(s-p_2) \dots (s-p_N)}$$

$$H_a(s) = \frac{\prod_{i=0}^M (s-z_i)}{\prod_{j=0}^N (s-p_j)}$$

soln

To matched  $z$ -transform replace  $\frac{1}{s-p_i}$   
 by  $\frac{1}{(-e^{p_i T} z^{-1})}$  and  $\frac{(s-p_i)}{(1-e^{p_i T} z^{-1})}$ .

~~Ques:~~

$$H(s) = \frac{2(s+3)}{(s+1)(s+2)}$$

Convert it into transfer function of  
 digital filter  $H(z)$ , using matched  
 $z$ -transform. Take  $T=1\text{ sec}$ .

~~soln:~~

replace  $\frac{1}{s+1}$  by  $\frac{1}{1-e^{-1} z^{-1}}$

$\frac{1}{s+2}$  by  $\frac{1}{1-e^{-2} z^{-1}}$

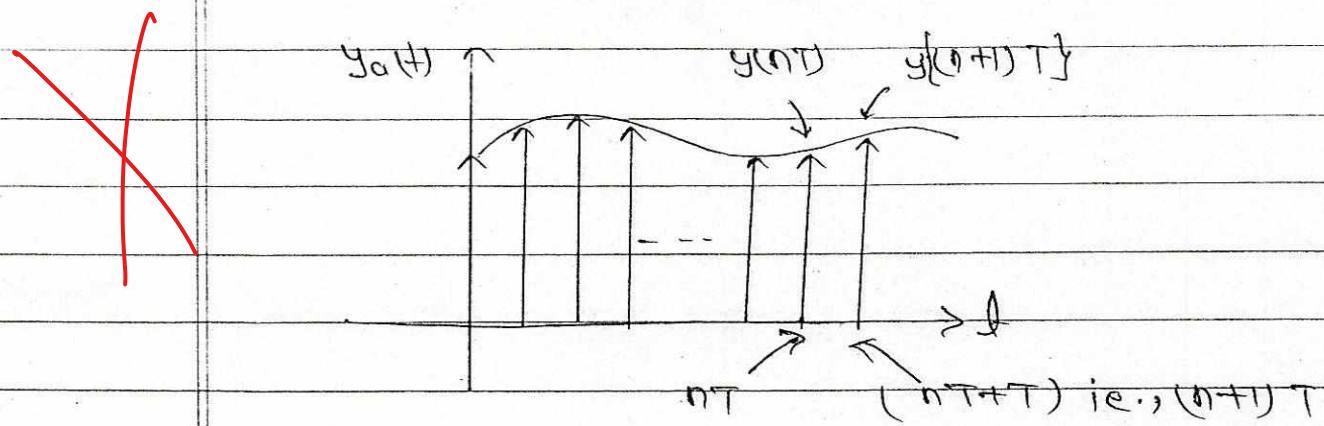
$s+3$  by  $1-e^{-3} z^{-1}$

and calculate  $H(z)$ .

$$\text{so } H(z) = \frac{2(1-e^{-3} z^{-1})}{\left(\frac{1}{1-e^{-1} z^{-1}}\right)\left(\frac{1}{1-e^{-2} z^{-1}}\right)}$$

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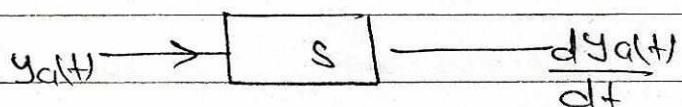
→ Approximation of derivative using forward difference Method :-



using forward difference method.

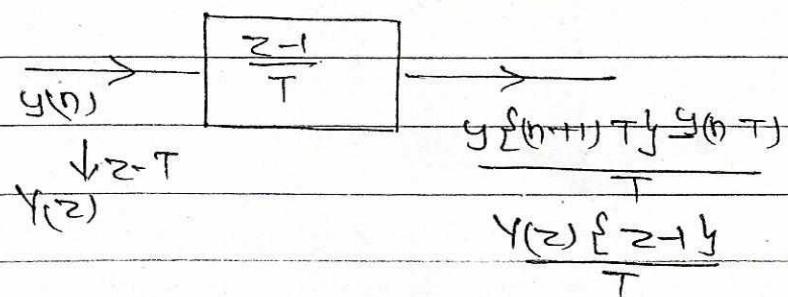
$$\frac{dy_{0T}}{dt} = \frac{y_{(n+1)T} - y_{nT}}{T}$$

can be obtained using following block



$\frac{y_{(n+1)T} - y_{nT}}{T}$  can be obtained using

following block.



So, Transfer function of digital block.

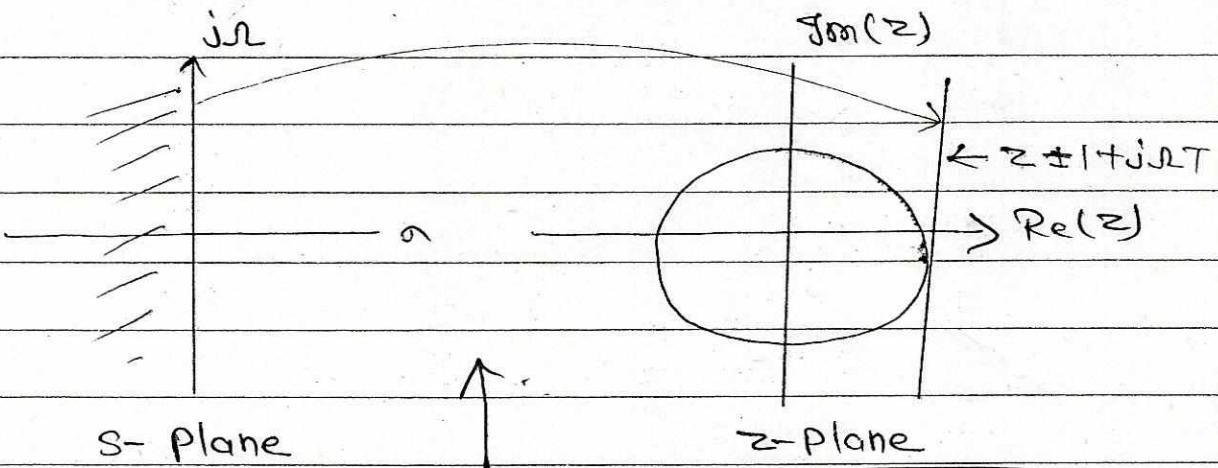
$$= \frac{Y(z) \{ (z-1)/T \}}{Y(z)}$$

So, put  $s = \frac{z-1}{T}$  in  $H(s)$  to convert

it into  $H(z)$  using forward difference method in approximation of derivative method.

Since  $s = \frac{z-1}{T} \Rightarrow z = 1 + sT$

when  $\theta = j\omega$   $z = 1 + j\omega T$ .



mapping of S plane into z-plane  
for approximation of derivative  
using forward difference method

Ques:  $H(z) = \frac{3 + 4z}{(z - \frac{1}{2})(z - \frac{1}{4})}$

Is it

a) IIR or FIR Filter.

b) Find the difference equation.

c) Direct form-I structure using difference eqn

d) Make DF2 using DF1

Sol'n:  $H(z) = \frac{3(z - \frac{1}{2})(z - \frac{1}{4}) + 4z(z - \frac{1}{4}) - 2(z - \frac{1}{2})}{(z - \frac{1}{2})(z - \frac{1}{4})}$

$$= \left( 3z - \frac{3}{2} \right) (z - \frac{1}{4}) + 4z^2 - z - 2z + 1$$

$$(z - \frac{1}{2})(z - \frac{1}{4})$$

$$= 3z^2 - \frac{3z}{4} - \frac{3z}{2} + \frac{3}{8} + 4z^2 - z - 2z + 1$$

$$z^2 - \frac{1}{4}z - \frac{1}{2}z + \frac{1}{8}$$

$$H(z) = \frac{7z^2 - \frac{21z}{4} + \frac{11}{8}}{z^2 - \frac{1}{4}z - \frac{1}{2}z + \frac{1}{8}}$$

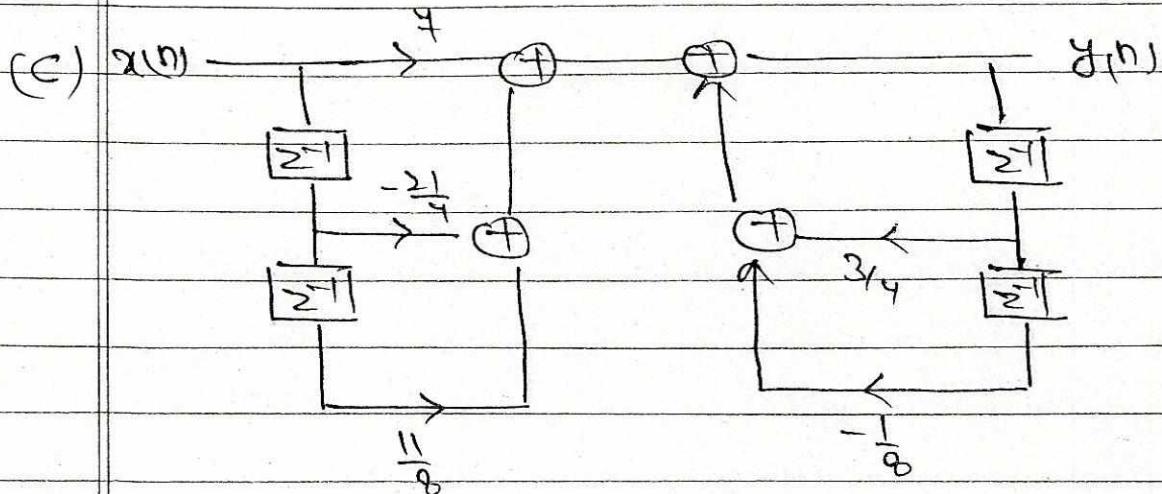
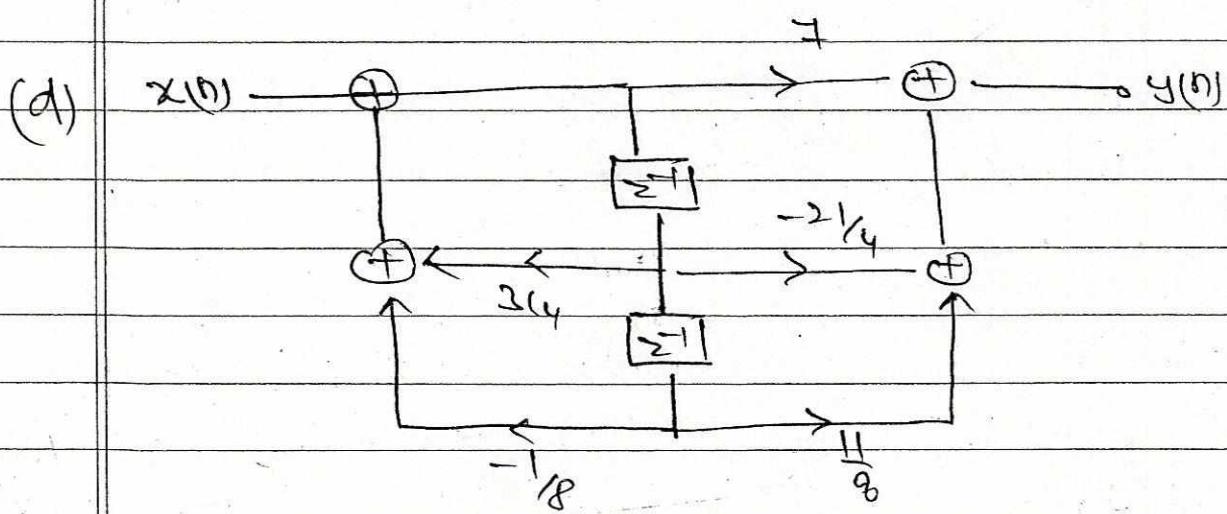
a) IIR.

$$\frac{Y(z)}{X(z)} = \frac{7z^2 - \frac{21z}{4} + \frac{11}{8}}{z^2 - \frac{3}{4}z + \frac{1}{8}} = \frac{7 - \frac{21}{4}z^{-1} + \frac{11}{8}z^{-2}}{1 - \frac{3}{4}z^{-1} + \frac{1}{8}z^{-2}}$$

$$Y(z) = -\frac{3}{4}z^{-1}Y(z) + \frac{1}{8}z^{-2}Y(z) = 7X(z) - \frac{21}{4}z^{-1}X(z) + \frac{11}{8}z^{-2}X(z)$$

$$y(n) = -\frac{3}{4}y(n-1) + \frac{1}{8}y(n-2) = 7x(n) - \frac{21}{4}x(n-1) + \frac{11}{8}x(n-2)$$

$$y(n) = \frac{3}{4}y(n-1) - \frac{1}{8}y(n-2) + 7x(n) = \frac{21}{4}x(n-1) + \frac{11}{8}x(n-2)$$

DF-1DF-2