

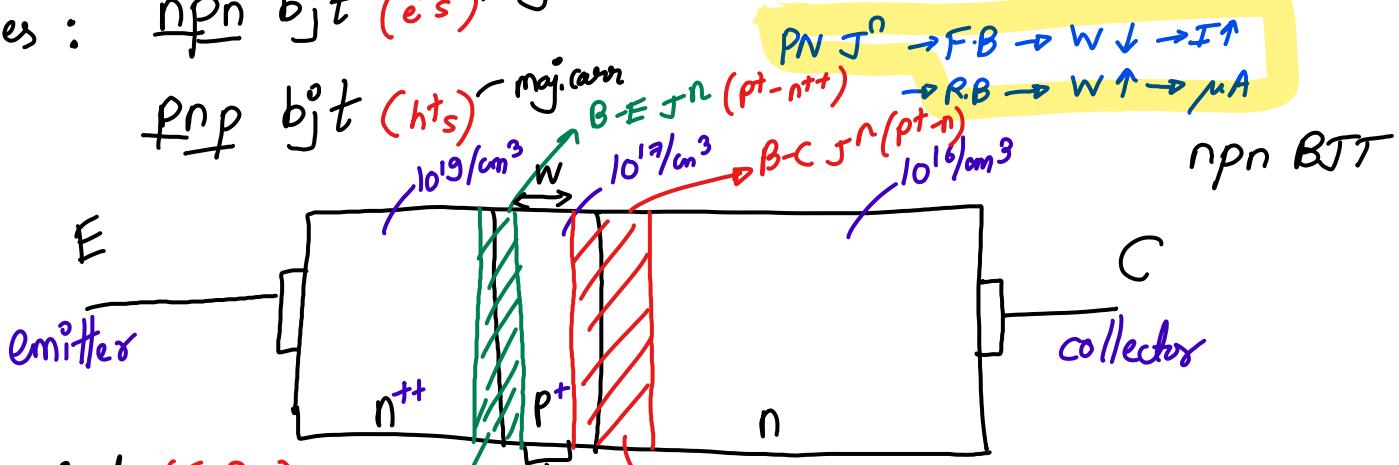
Module 5: [BJT operation, CE, CB, CC configuration of BJTs]
 [BJT as a switch, & voltage amplifier]

Applications

BJT: Bipolar junction transistor (1948, Bell labs)

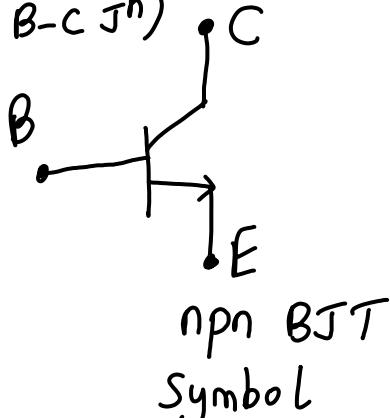
Types: npn bjt (e-s) ^{maj. curr}

pnp bjt (h-s) ^{maj. curr}

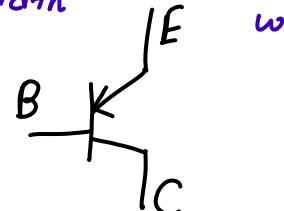


3 terminals (E, B, C)

two junctions (B-E Jⁿ)
 (B-C Jⁿ)



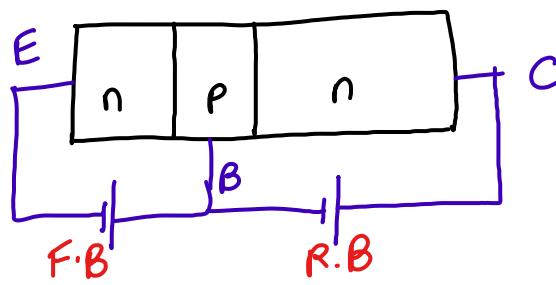
Emitter: heavily doped
 Base: moderately doped
 Collector: lightly doped



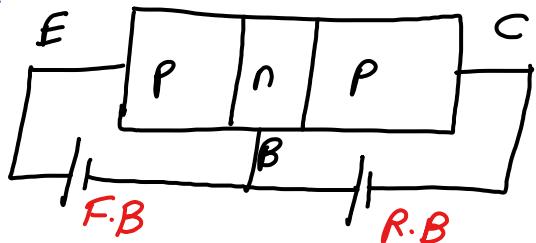
Different regions of operation

- ① Active region
- ② Cut-off region (OFF)
- ③ Saturation region (ON)
- ④ Inverse-active region
 ↴ Avoided (not used)

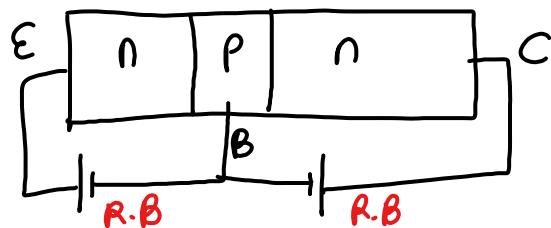
	B-E J ⁿ	B-C J ⁿ	
① Active region	F.B	R.B	(BJT as amplif)
② Cut-off region (OFF)	R.B	R.B	F.B → forward bias
③ Saturation region (ON)	F.B	F.B	(BJT as switch)
④ Inverse-active region ↴ Avoided (not used)	R.B	F.B	R.B → reverse bias



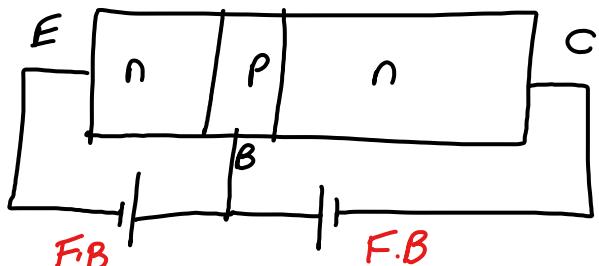
Active region



Cut-off region



Saturation region



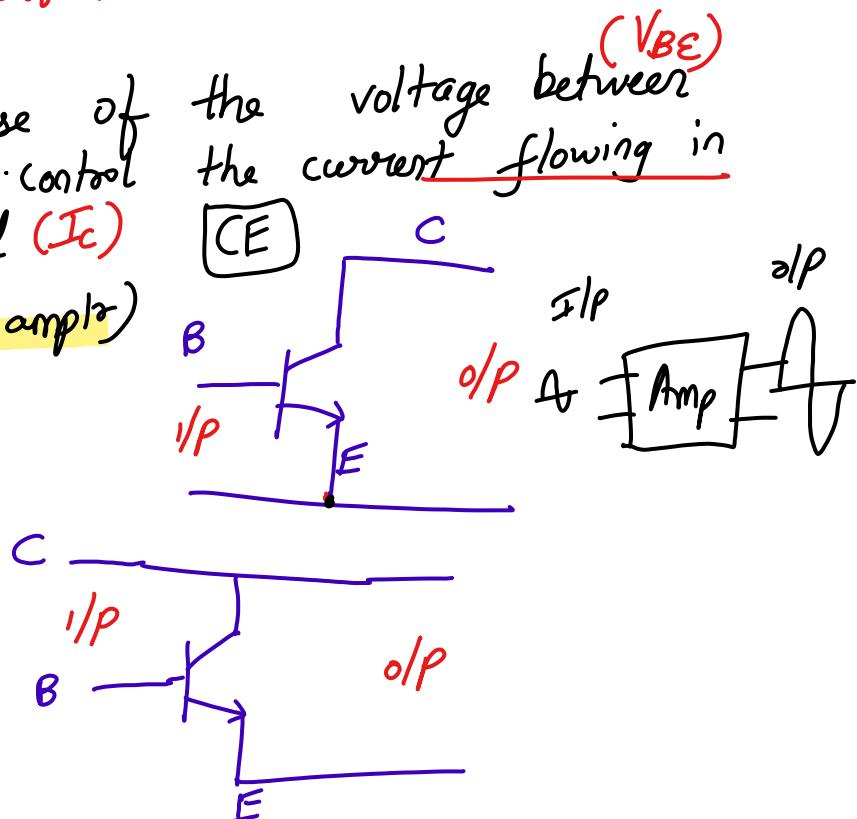
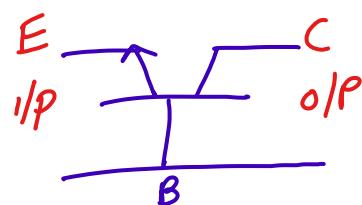
"
Bipolar"

charge carriers of both polarities
(e⁻s & holes) → take part in current conduction process

Principle of BJT : It involves the use of two terminals to control the 3rd terminal (I_c)

BJT configuration (BJT as amp)

- ① Common emitter (CE)
- ② Common base (CB)
- ③ Common collector (CC)

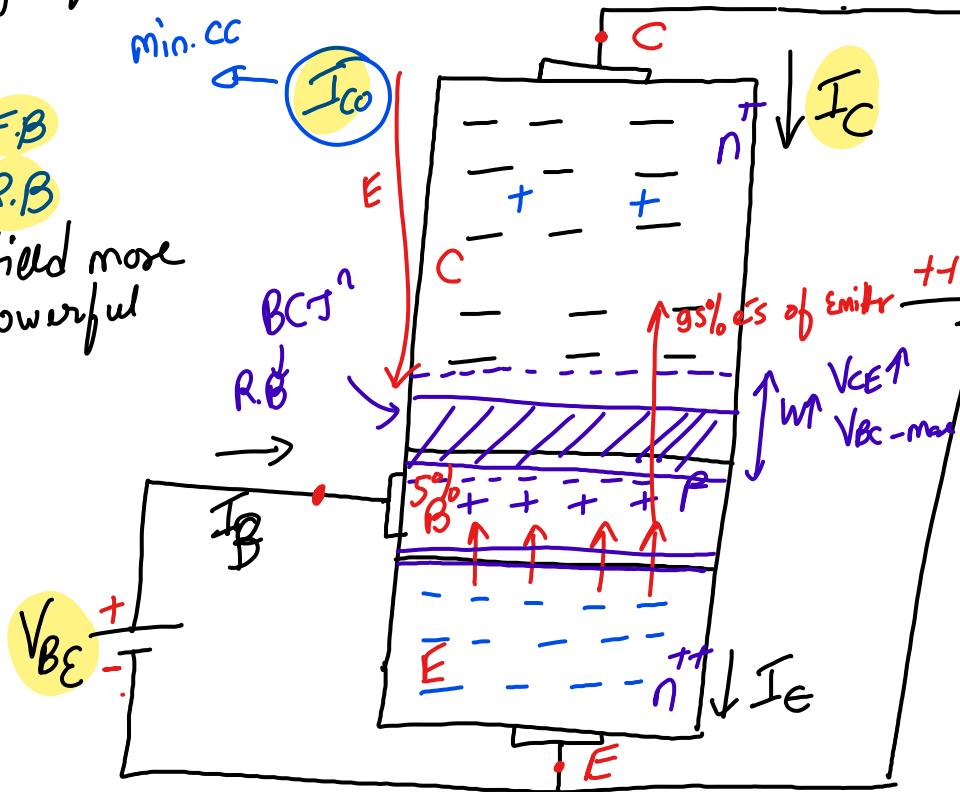


Working of npn BJT in active region (CE configuration)

Active:
region

$B_E J \rightarrow F_B$
 $B_C J \rightarrow R.B$

$\rightarrow E$ -field more
powerful



$$V_{BE} = V_B - V_E$$

$$V_{CE} = V_C - V_E$$

O/P
current
 I_C

Terminal current $I_C \gg I_B$

current:

$$I_C, I_E, I_B$$

MA MA

MA

↓ control I_B
control " I_C "

$$I_E = I_C + I_B$$

$$I_E = I_C + I_B$$

current gain

$\alpha < 1$

$$I_E = (1 + \beta) I_B$$

$$I_C = \alpha I_E$$

$$\frac{I_B + I_C}{I_B} = \frac{I_E}{I_B}$$

$$\frac{I_B + \alpha I_E}{I_B} = \frac{I_E}{I_B}$$

$$I_B = I_E (1 - \alpha)$$

$$I_B = \frac{I_C}{\alpha} (1 - \alpha)$$

$$\rightarrow I_C = \left(\frac{\alpha}{1 - \alpha} \right) I_B$$

$$I_C = \beta I_B$$

Current gain
(50-400)

BJT: Current controlled
device

V_{BE} → I_B → I_C
IP IP
Voltage Current O/P

EEEEE BJT CB configuration

22/11/23

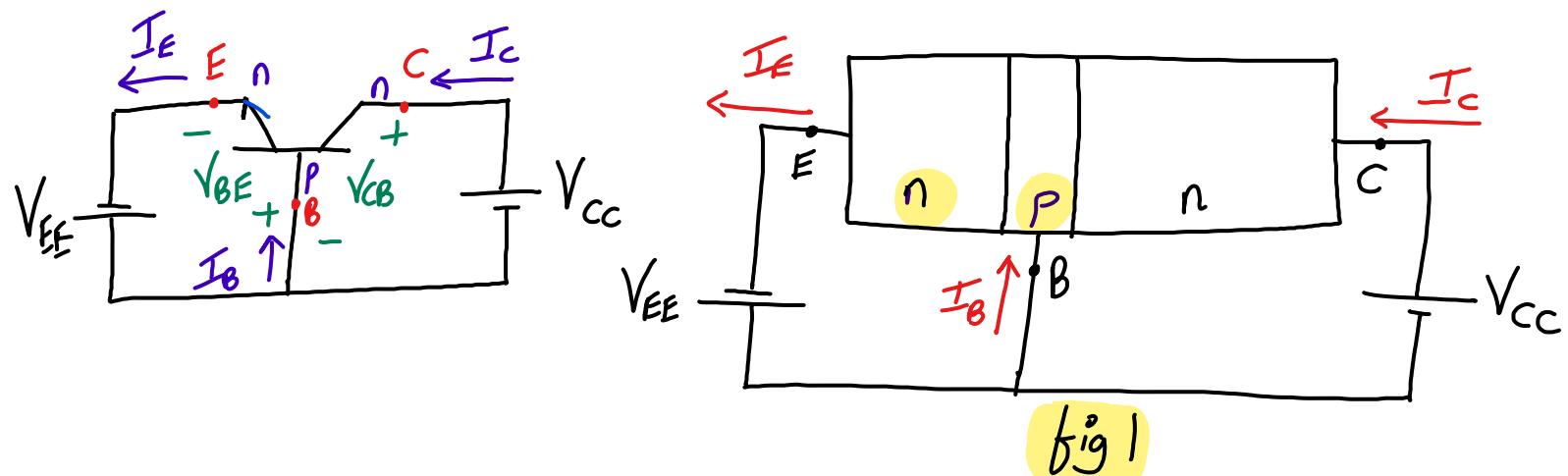


fig 1

- In common base (CB) configuration, input is applied between 'B' and 'E' and output is taken between 'C' and 'B'
- For BJT to be used as an amplifier \rightarrow npn bjt should be operated in active region

i.e B-E junction \rightarrow forward bias
and B-C junction \rightarrow reverse bias

- Terminal current in bjt,

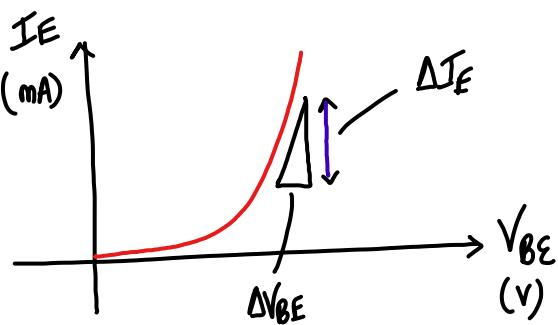
$$I_E = I_C + I_B$$

- Behavior of bjt in CB mode can be described by two characteristics :
 - Input characteristics
 - Output characteristics

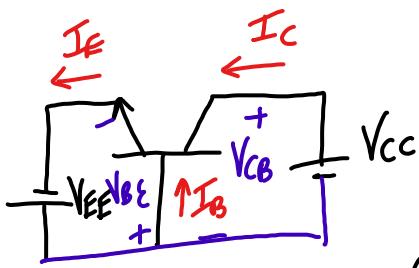
⑨ From input characteristics, we can find the input impedance of the device

$$R_{in}^o = \frac{\Delta V_{BE}}{\Delta I_E}$$

small changes
V_{CB} constant
huge changes

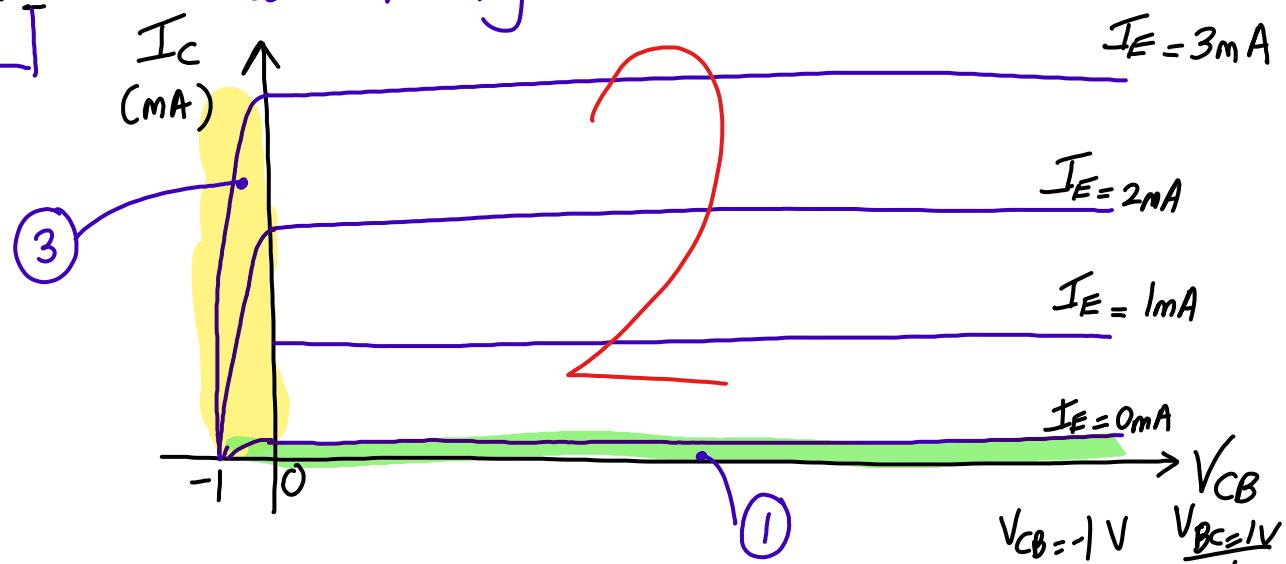


Thus, R_{in}^o is very low (in ohms) for npn BJT in CB configuration



I_c : O/p current

V_{CB} : O/p voltage



Region 1 : Cut-off

Region 2 : Active

Region 3 : Saturation

fig 3 : Output characteristics of npn bjt in CB configuration

V_{CB} Vs I_c | I_E constant

O/p resistance

$$R_{out} = \frac{\Delta V_{CB}}{\Delta I_c}$$

I_E constant

$\uparrow I_c (mA)$

ΔI_c

$\rightarrow V_{CB}$

v. high for CB configuration

EEEEE BJT CE configuration

- most famous configuration for BJT as amplifier

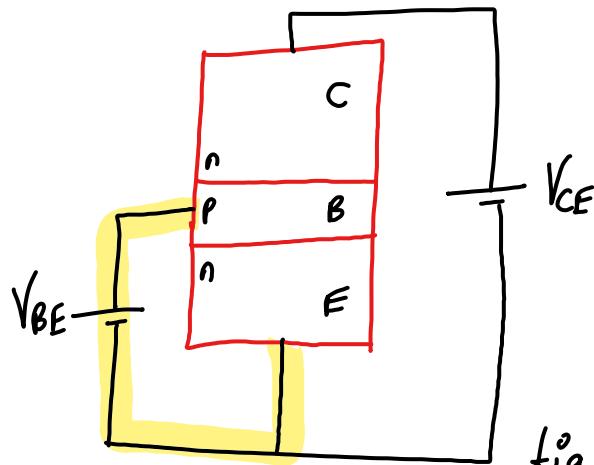
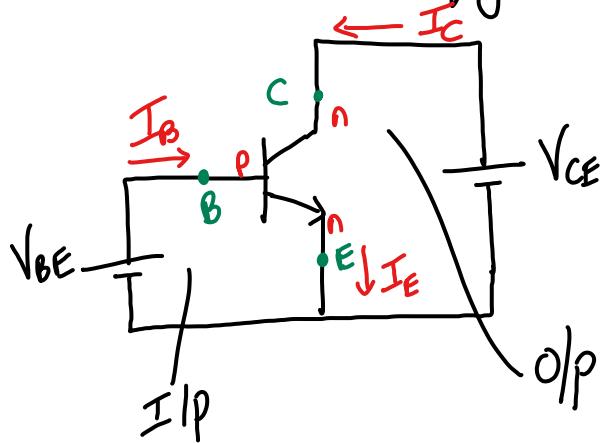
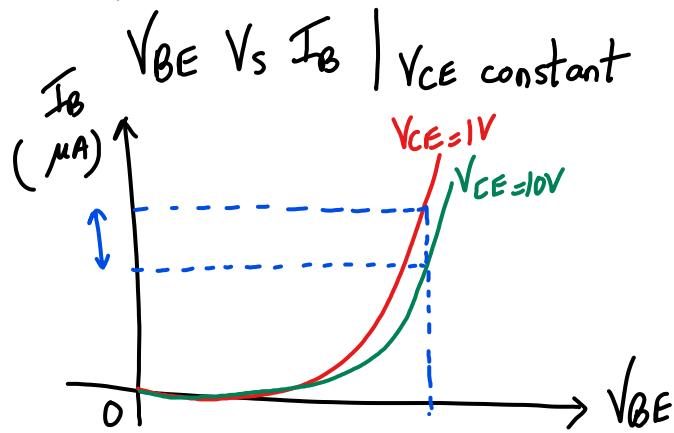


fig 1

npn BJT in
active region → BE Jⁿ F.B
BC Jⁿ R.B

① Input characteristics:



② I/p characteristics is similar

to PN Jⁿ characteristics since
BE Jⁿ is forward-biased

i.e As V_{BE} ↑, I_B ↑ is exponentially
for constant V_{CE} value
(i.e BC Jⁿ is R.B)

③ As V_{CE} ↑ is → I_B is reducing? Why?

a) $V_{CE} = V_{CB} + V_{BE}$ ($V_{CB} = V_{CE} - V_{BE}$)

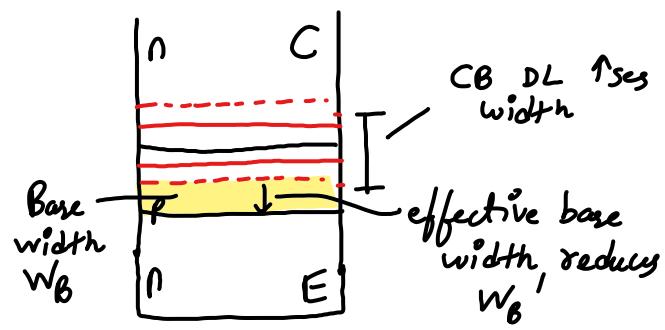
∴ with V_{BE} constant, if V_{CE} ↑ → V_{CB} ↑ is common
emitter terminal

b) As V_{CB} ↑ is, CB Jⁿ is more R.B



c) i.e. CB depletion region width \uparrow V_{CE}

i.e. effective base width reduces from W_B to W_B'



d) i.e. possibility of e-holes recombination in base region will reduce

e) i.e. Most of e's travelling from emitter to base gets collected at collector.

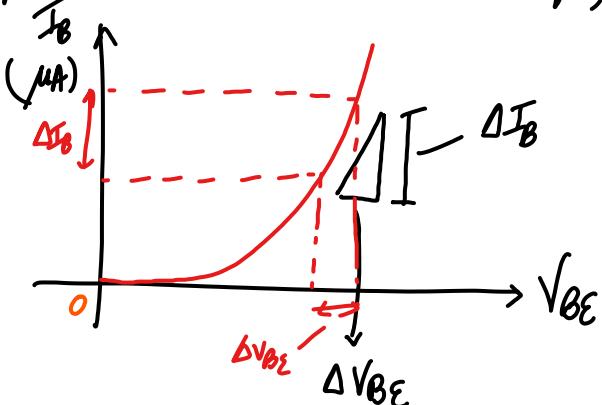
i.e. I_B reduces

\therefore As $V_{CE} \uparrow$ $\rightarrow I_B \downarrow$ i.e. curve shifts left hand side

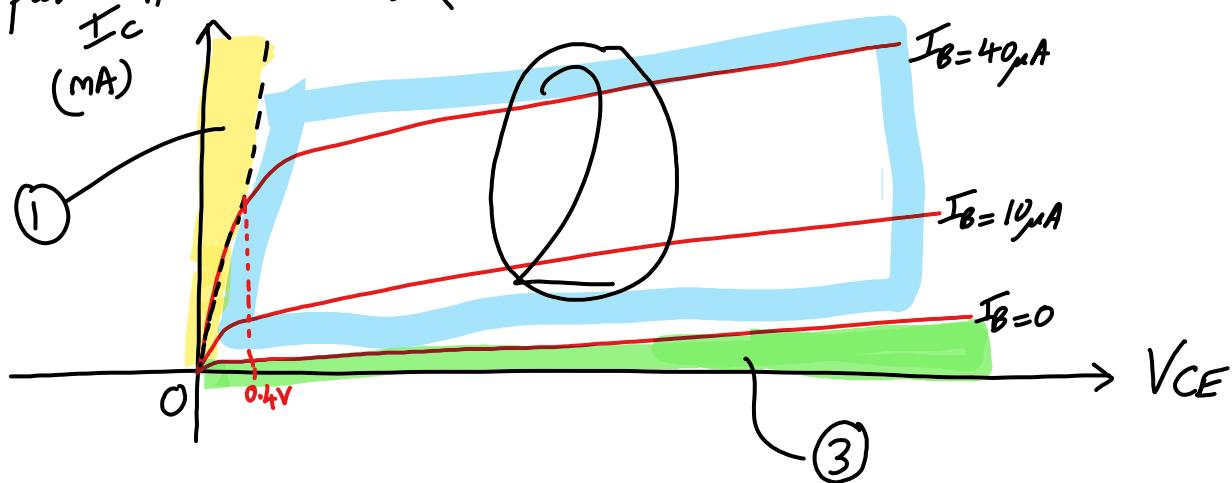
④ Input resistance from input characteristics (CE config)

$$R_{in} = \frac{\Delta V_{BE}}{\Delta I_B} \quad | \quad V_{CE} \text{ constant}$$

large value (in $M\Omega$)



⑤ Output characteristics (V_{CE} Vs I_C at constant I_B value)



Region 1 - Saturation

Region 2 - Active

Region 3 - Cut-off

⑥ In active region \rightarrow As $I_B \uparrow_{\text{ses}} \rightarrow I_C \uparrow_{\text{ses}}$ ($I_C = \beta I_B$)

\rightarrow As $V_{CE} \uparrow_{\text{ses}} \rightarrow I_C$ also \uparrow_{ses} slightly

a) Since $V_{CE} = V_{CB} + V_{BE}$



b) V_{BE} being constant (I_B constant) \rightarrow As $V_{CE} \uparrow \rightarrow V_{CB} \uparrow_{\text{ses}}$



c) As $V_{CB} \uparrow_{\text{ses}}$, CB depletion layer width \uparrow_{ses}



d) \therefore Effective base width will reduce



e) i.e. I_B contribution will reduce (as less of electrons will recombine with holes in base region)

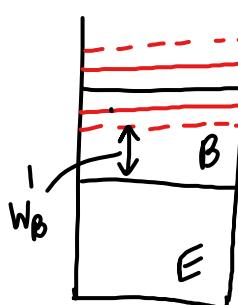


f) i.e. most of es travelling via base will be collected by collector

i.e. $I_C \uparrow_{\text{ses}}$

\therefore As $V_{CE} \uparrow_{\text{ses}} \rightarrow I_C \uparrow_{\text{ses}}$ with it slightly

(BJT is used as an amplifier in active region of bjt)



⑦ Since, I_B - I/p current , $I_C = \beta I_B$
 ↓ o/p current

$$\boxed{\beta_{dc} = \frac{I_C}{I_B}}$$

"DC"
 CE current gain

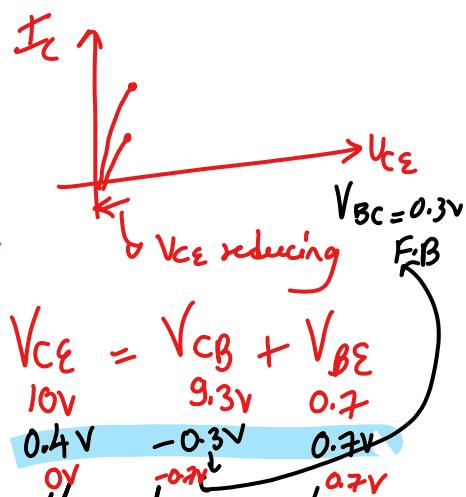
$$\boxed{\beta_{AC} = \frac{\Delta I_C}{\Delta I_B}}$$

β_{dc} almost same as β_{AC}

⑧ In saturation region, as the value of V_{CE} reduces

a) $V_{CE} = V_{CB} + V_{BE}$

i.e As $V_{CE} \downarrow$ → $V_{CB} \downarrow$ constant
 \downarrow $V_{CB} = -9.3V$

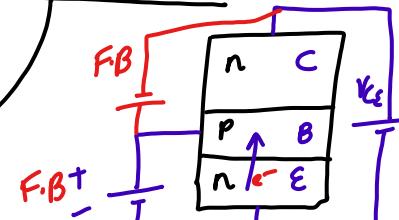


b) CB becomes lesser R.B & finally at very low value of V_{CE} → $CB J^n$ becomes F.B

c) $BE J^n$ is already F.B

d) As $CB J^n$ becomes F.B → e^- will not reach collector & ∴ I_C reduces to zero as V_{CE} is reduced to lower value

e) i.e BJT operates in saturation region



(g) npn bjt operates in cut-off region when $I_B = 0$

but here $I_C \neq 0$?

$$I_C = \beta I_B + \text{leakage}$$

a) When $I_E = 0 \rightarrow$ leakage current $I_C = \underline{\underline{I_{CBO}}}$

$$\therefore I_C = \alpha I_E + I_{CBO} - \textcircled{1}$$

$$\text{but } I_E = I_C + I_B$$

$$\therefore I_C = \alpha (I_C + I_B) + I_{CBO}$$

$$(1-\alpha) I_C = \alpha I_B + I_{CBO}$$

$$\therefore I_C = \frac{\alpha}{1-\alpha} I_B + \left(\frac{1}{1-\alpha} \right) I_{CBO}$$

$$\therefore I_C = \beta I_B + \left(\frac{1}{1-\alpha} \right) I_{CBO}$$

In cut-off region $\rightarrow I_B = 0$

$$\therefore I_C \approx \left(\frac{1}{1-\alpha} \right) I_{CBO} \quad \frac{1}{1-\alpha} - \text{large value}$$

$$\therefore I_C \approx (\beta + 1) I_{CBO} \quad \beta = \frac{\alpha}{1-\alpha}$$

$$1+\beta = \frac{1}{1-\alpha}$$

value of leakage
current at $I_B = 0$

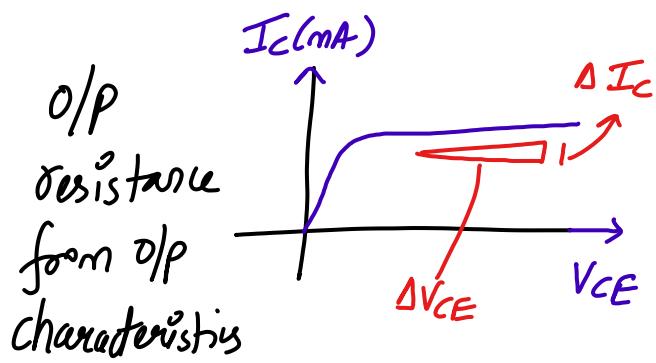
Called as " I_{CEO} "

$$\text{i.e. } I_{CEO} = (1+\beta) I_{CBO}$$

Collector to emitter
leakage current with base
open

⑩ Properties of CE configurations: .

- a) Moderate current gain
- b) Moderate voltage gain
- c) Moderate R_{in} & R_{out}
- d) High power gain

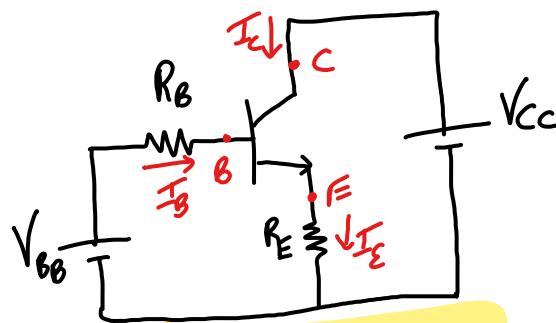
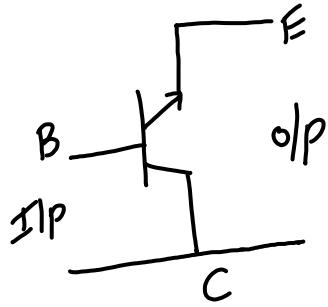


$$R_{out} = \frac{\Delta V_{CE}}{\Delta I_C} \quad | \quad I_B \text{ constant}$$

large value (in $k\Omega$)

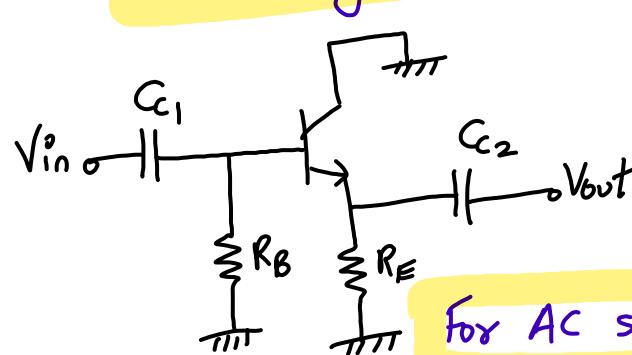
_____ x _____

EEEEE Common Collector configuration



B-E Jⁿ is F.B
B-C Jⁿ is R.B

IIP side	O/P side
I_B	I_E
V_{CB}	V_{CE}
I_{IP} ch ^r	O/P ch ^r
V_{CB} vs I_B	V_{CE} vs I_E



① Input characteristics (V_{CB} vs I_B)
@ V_{CE} constant

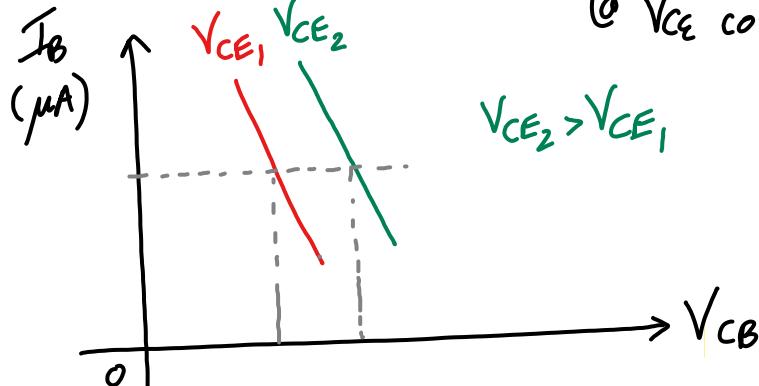
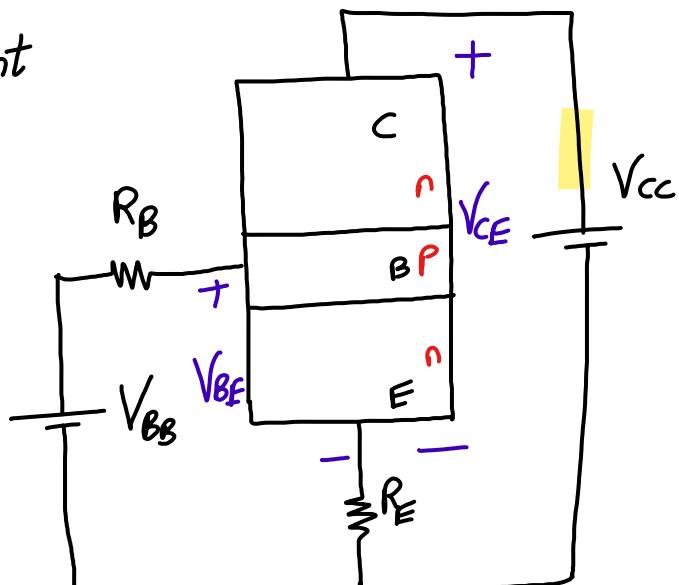


fig 2: Input characteristics of npn bjt in CC configuration



② As $V_{CB} \uparrow$ ses $\rightarrow I_B \downarrow$ ses ? why ?

a) $V_{CE} = V_{CB} + \frac{V_{BE}}{I_{fixed}}$

DL - Depletion layer

b) As $V_{CE} \uparrow$ ses $\rightarrow V_{CB} \uparrow$ ses

c) As $V_{CB} \uparrow$ ses \rightarrow width of BC DL \uparrow ses \rightarrow effective base width reduces

d) i.e. Probability of recombination of EHP in base reduces
↓ ↓
 (e⁻-hole pair)

e) i.e. $I_B \downarrow$ ses

i.e. As $V_{CB} \uparrow$ ses $\rightarrow I_B \downarrow$ ses

③ For fixed value of V_{CB} ; $V_{CE} = V_{CB} + V_{BE}$
↓ ↓
 fixed

i.e. As $V_{CE} \uparrow$ ses $\rightarrow V_{BE} \uparrow$ \rightarrow more e⁻'s pushed towards base region by emitter

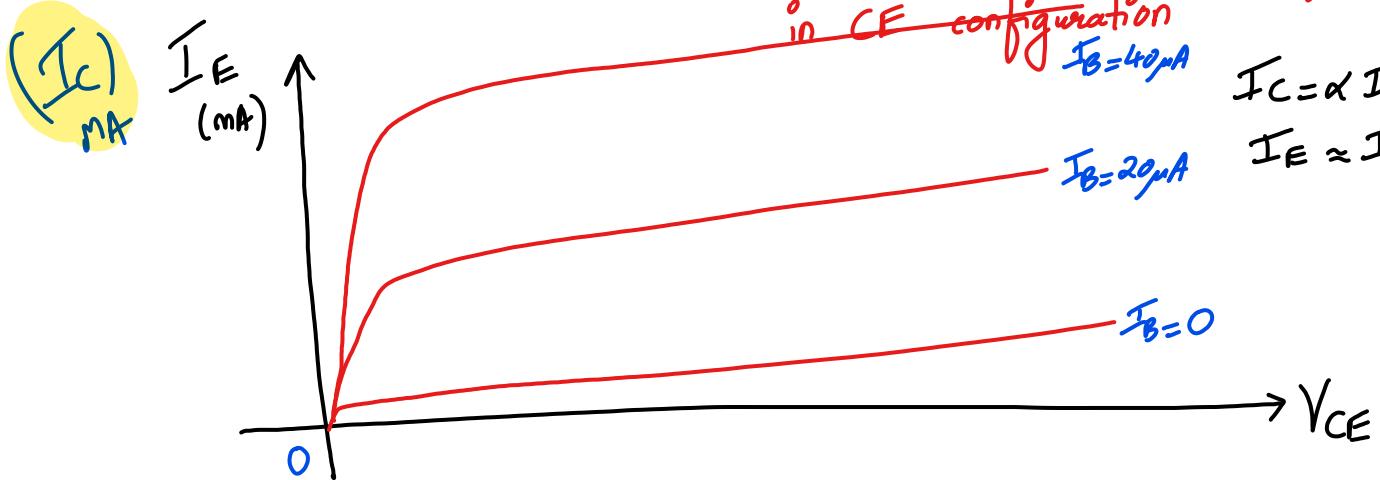
i.e. $I_B \uparrow$ ses

④
$$\frac{I_E}{I_B} = \gamma \rightarrow \text{gamma}$$

 I_E — o/p current
 I_B — I/p current

⑤ O/p characteristics (I_C vs V_{CE} | I_B constant)

It is similar to o/p characteristics of npn bjt
in CE configuration



$$I_C = \alpha I_E$$
$$I_E \approx I_C$$

⑥ $I_E = I_C + I_B$; $\gamma = \frac{I_E}{I_B}$; $I_C = \beta I_B$

$$\gamma = \frac{I_C + I_B}{I_B}$$

$$\text{i.e. } \gamma = \frac{I_C}{I_B} + 1 \approx \beta + 1$$

$$\text{i.e. } \boxed{\gamma = 1 + \beta} \quad \text{Also, } \gamma = \frac{\alpha}{1-\alpha} + 1 = \frac{1}{1-\alpha}$$

$$\text{i.e. } \gamma = 1 + \beta = \frac{1}{1-\alpha}$$

⑦ Common collector properties:

- ① High input resistance
- ② low output resistance
- ③ High current gain ($= 1 + \beta$)
- ④ Low voltage gain (≈ 1)
- ⑤ Low power gain

— x —