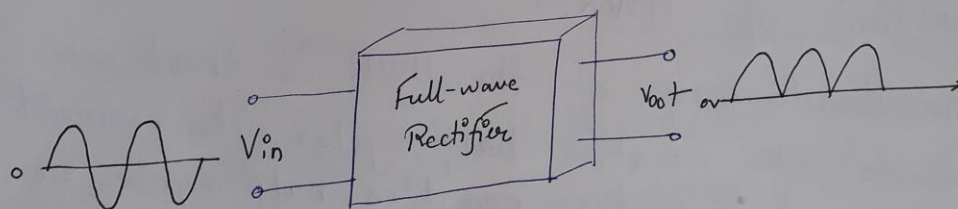


## Full-Wave Rectification:-

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- A full-wave rectifier allows uni-directional (one-way) current through the load during the entire  $360^\circ$  of the input cycle.
- The result of full-wave rectification is an output voltage with a frequency twice the input frequency and that pulsates every half-cycle of the input, as shown in fig (1.a)



- Two circuits commonly used for full-wave rectification are:

1. Center-tap Full-Wave Rectifier.
2. Full-wave Bridge Rectifier.

## Center-Tapped Full-wave Rectifier :-

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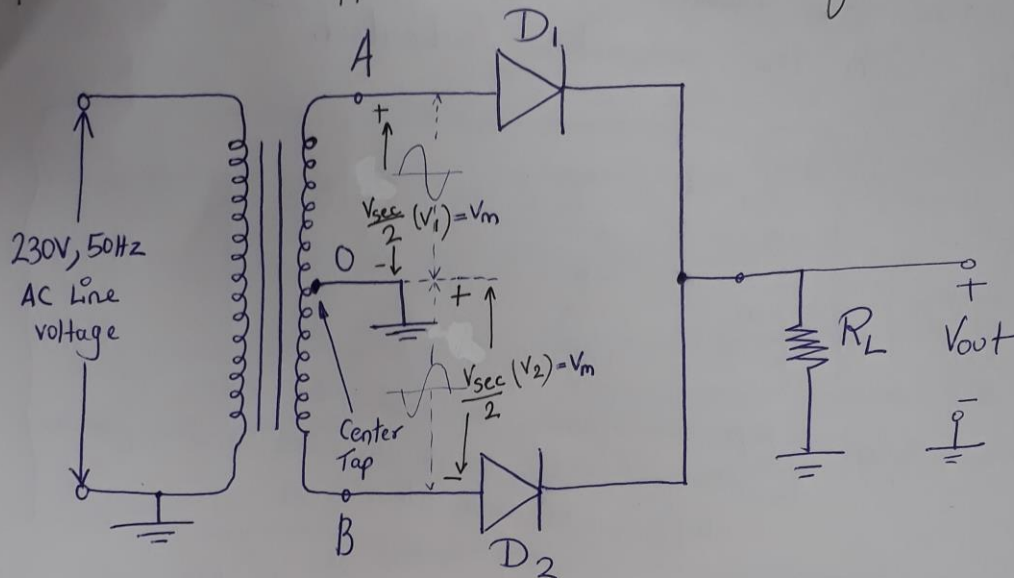


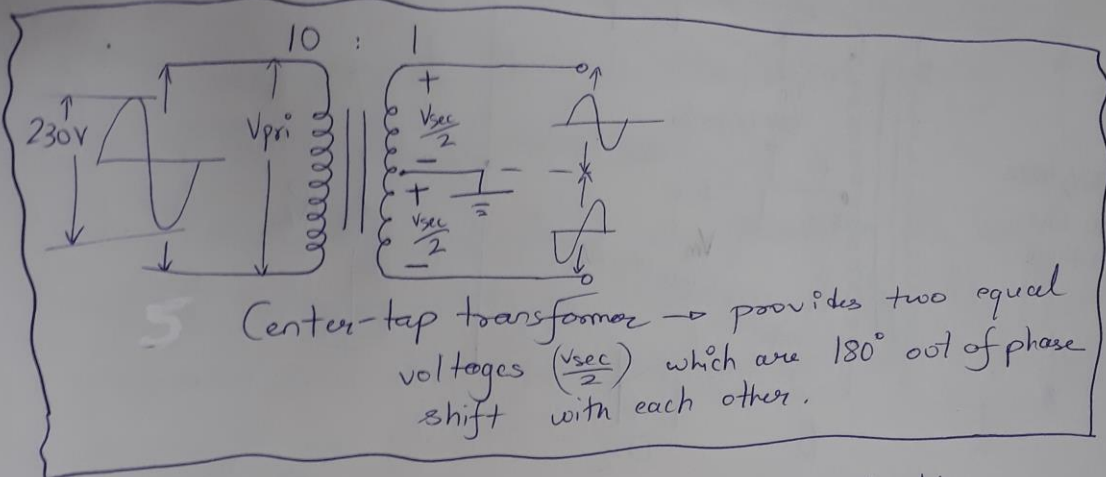
fig 1.b : Center-tapped Full-wave rectifier

### Description:-

- This circuit in fig(1.b) uses two diodes  $D_1$  &  $D_2$  connected to the secondary of a center-tapped transformer.
- The input to the rectifier consists of a center-tapped transformer, in which the input is normally a 230V, 50Hz ac line voltage.
- Here, the transformer secondary winding is center-tapped to provide two equal voltages  $\frac{V_{sec}}{2}$

- across the two halves of the secondary winding with the polarities indicated.

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- The input voltage is coupled through the transformer to the center-tapped secondary.
- Half of the total secondary voltage appears between the center-tap and each end of the secondary winding as shown in fig (1.b).
- The transformer also provides electrical isolation between the power line circuit and the electronic circuits to be biased by the rectifier circuit. This isolation reduces the risk of electrical shock.



• Working :-

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1. During the positive half cycle of AC input, point A is positive and point B is negative, thus the polarities of the secondary voltages are as shown in fig 1.c

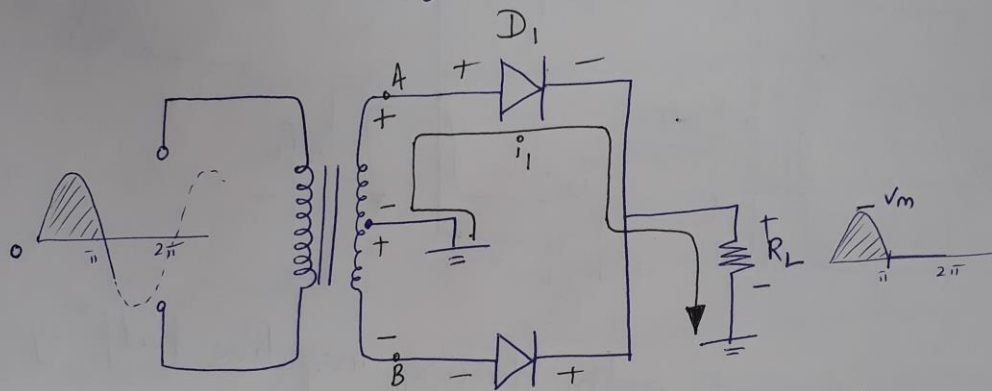


fig 1.c : Current path during positive half-cycles

- This condition forward-biases diode  $D_1$  and reverse-biases diode  $D_2$ .
- Thus,  $D_1$  conducts and the current  $i_1$  flows through  $D_1$  and the load resistor  $R_L$ , as indicated, which produces a positive O/P voltage across  $R_L$ .

2. During the negative half-cycle of the input voltage, point A is negative and point B is positive, thus the voltage polarities on the secondary are as shown in fig (1.d).

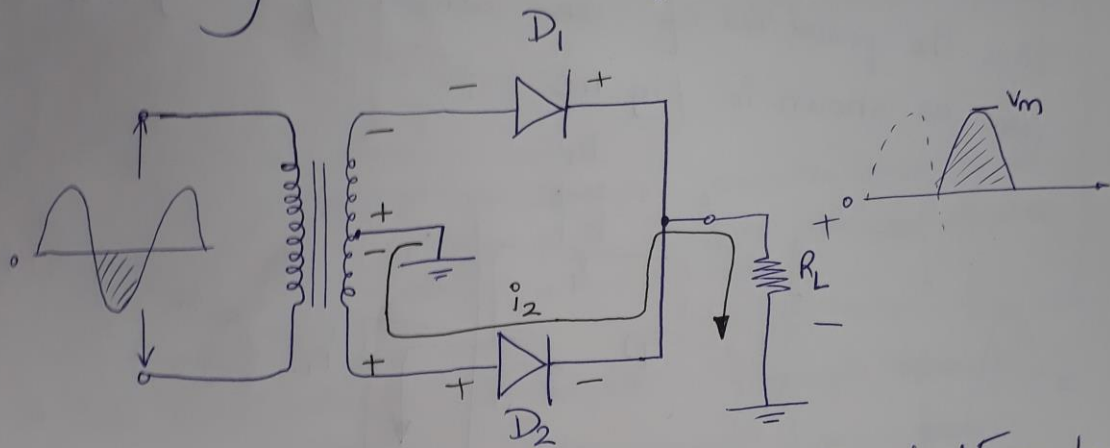
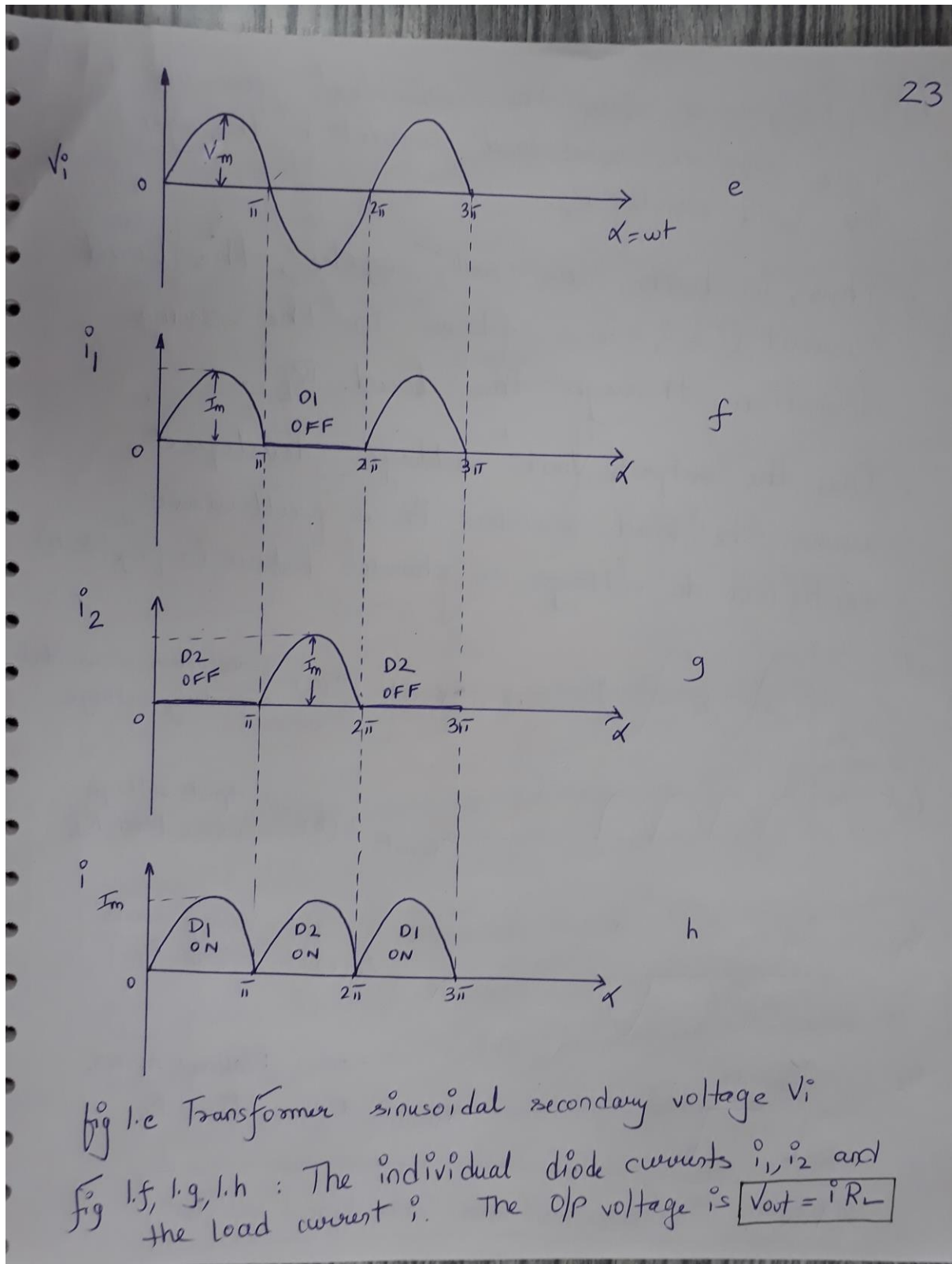


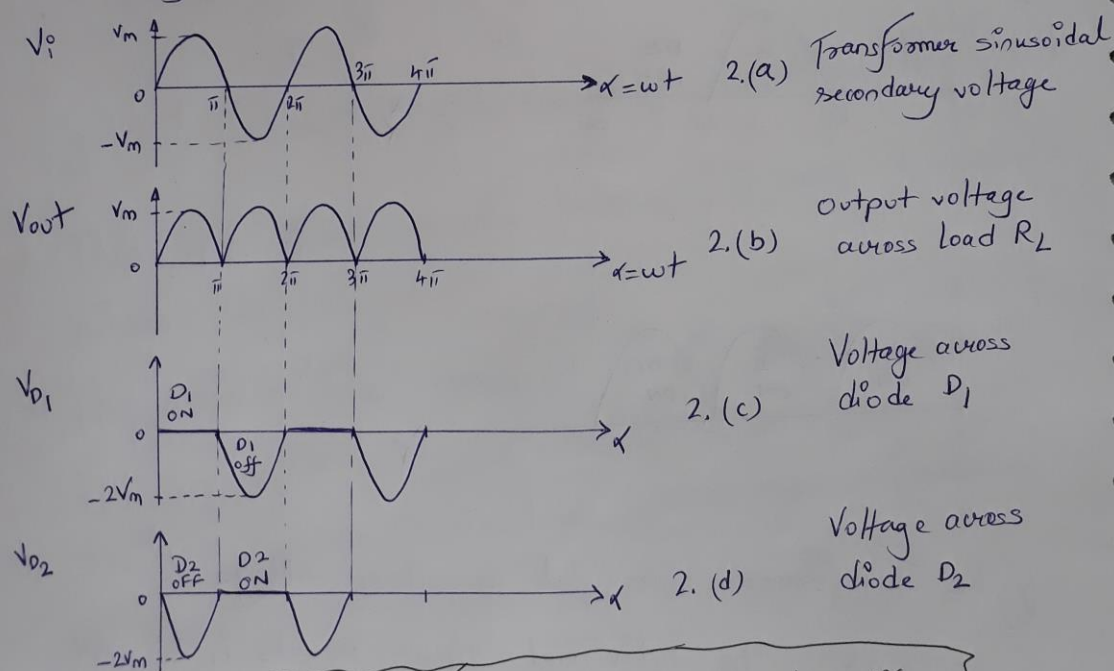
fig 1.d : Current path during negative half-cycle

- This condition reverse-biases  $D_1$  and forward-biases  $D_2$ .
- Thus, diode  $D_2$  conducts and the current  $i_2$  flows through diode  $D_2$  and load resistor  $R_L$  as indicated, which again produces a positive o/p voltage across  $R_L$ .

## Working of Full wave center tapped rectifier with waveforms

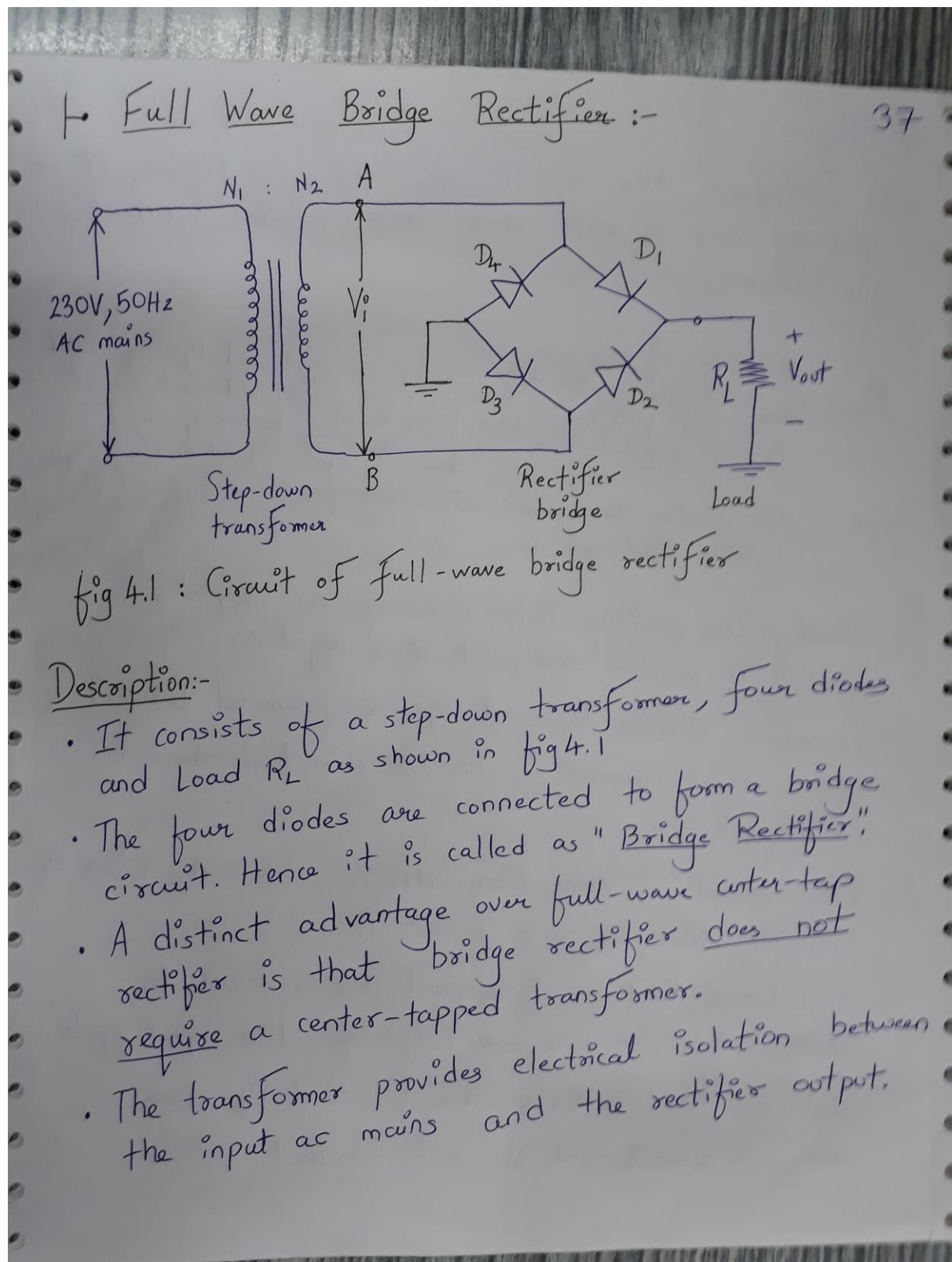


- Fig 1.f, 1.g and 1.h show the individual currents  $i_1, i_2$  and the total load current  $i$  through the load resistor  $R_L$ .
- Thus, in both the half cycles, the Load current ( $i = i_1 + i_2$ ) flows in the same direction through the load  $R_L$ .
- Thus, the output 'Vout' voltage developed across the load resistor is a full-wave rectified dc voltage as shown below in fig (2.b)



→ Next: Analysis of Full-wave Center-tapped rectifier







Working:-

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- To understand the action of bridge rectifier, it is necessary only to note that two diodes conduct simultaneously.

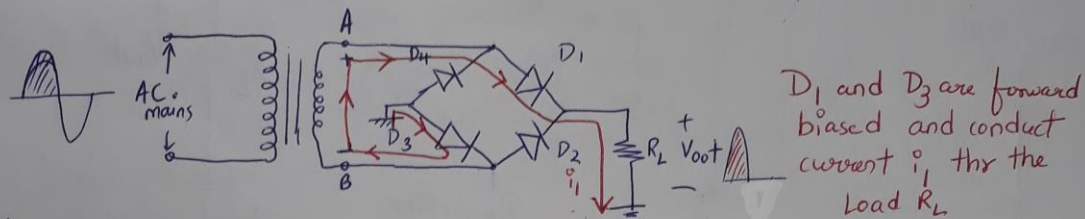


fig 4.2 ckt showing the current direction for a positive input cycle

- During the positive half cycle of ac input, point A is positive and point B is negative. Therefore, diodes  $D_1$  and  $D_3$  are forward-biased and conduct current  $i_L$  in the direction shown in fig 4.2.
- The current  $i_L$  conduction path is Point A, Diode  $D_1$ , Load  $R_L$ , diode  $D_3$  and point B.
- A voltage  $V_{out}$  is developed across load  $R_L$  that looks like the +ve half of the input cycle. During this cycle, diodes  $D_2$  and  $D_4$  are reverse-biased and do not conduct.

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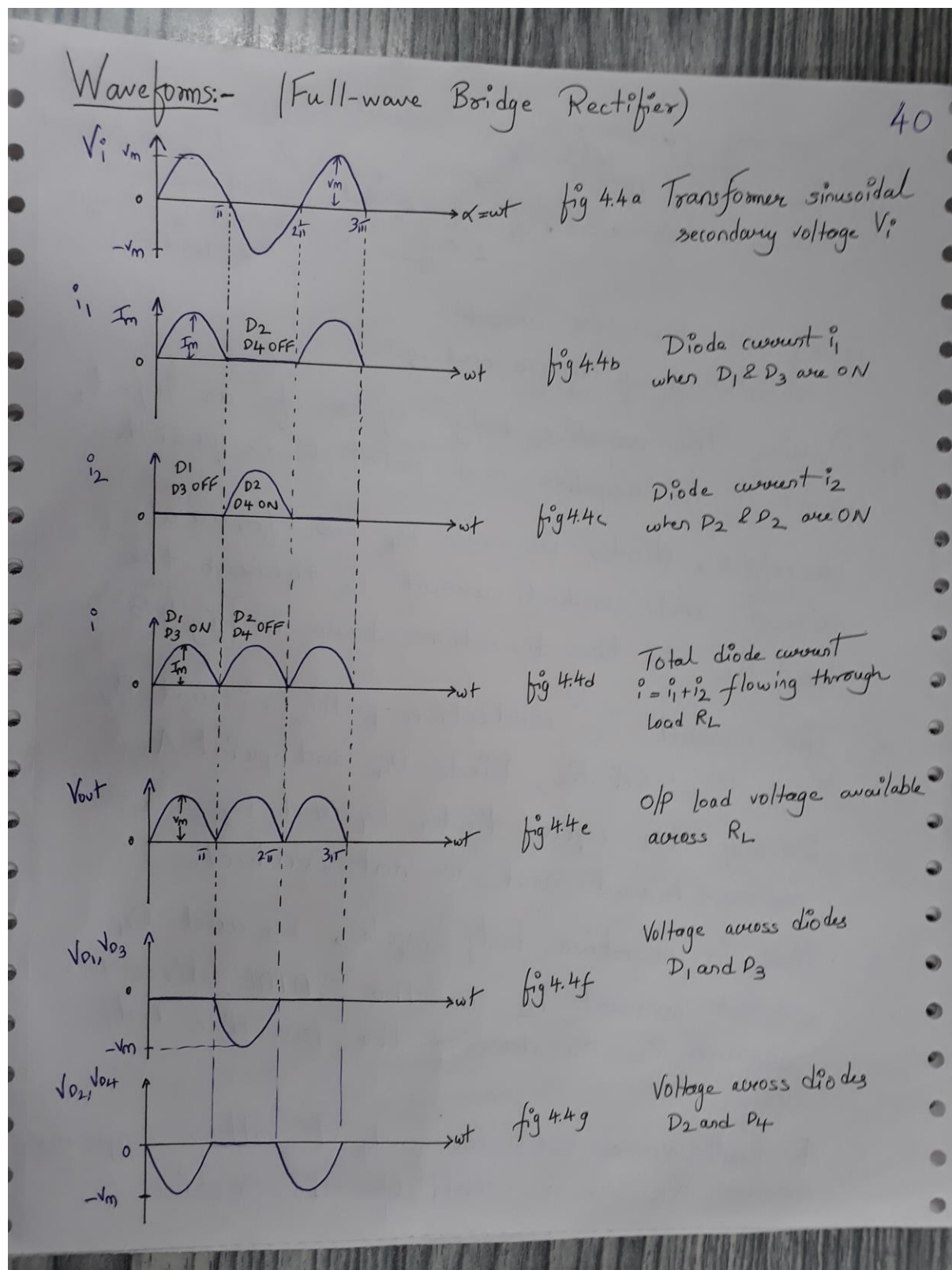
fig 4.3 ckt showing the current direction for a negative input cycle

4. During the negative half cycle of ac input, point A is negative and point B is positive. Therefore, diodes  $D_2$  and  $D_4$  are forward biased and conduct current  $i_2$  through the load  $R_L$  in the direction shown in fig 4.3.

5. The current  $i_2$  conduction path is Point B, Diode  $D_2$ , load  $R_L$ , Diode  $D_4$  and point A. During this cycle, diodes  $D_1$  and  $D_3$  are reverse-biased and do not conduct.

6. Thus, in negative half cycle,  $D_2$  and  $D_4$  conduct current  $i_2$  in the SAME direction through  $R_L$  as during the positive half cycle.

7. A full-wave rectified output voltage appears across  $R_L$  as a result of this action.





## Bridge output voltage :

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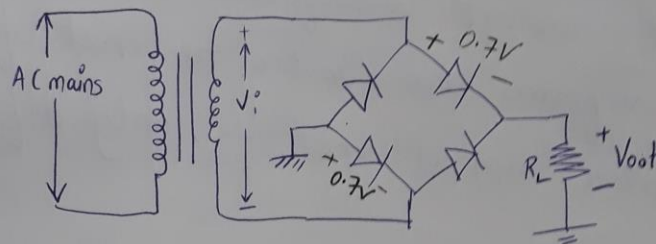


fig 4.5 Bridge operation during +ve h.c of primary and secondary voltages (Diode drops included)

- Fig shows the sinusoidal transformer secondary voltage  $V_i$  and the rectified output voltage  $V_{out}$ .
- Because two diodes are in series in the conduction path, the magnitude of  $V_{out}$  is two diode drops less than the magnitude of  $V_i$ .

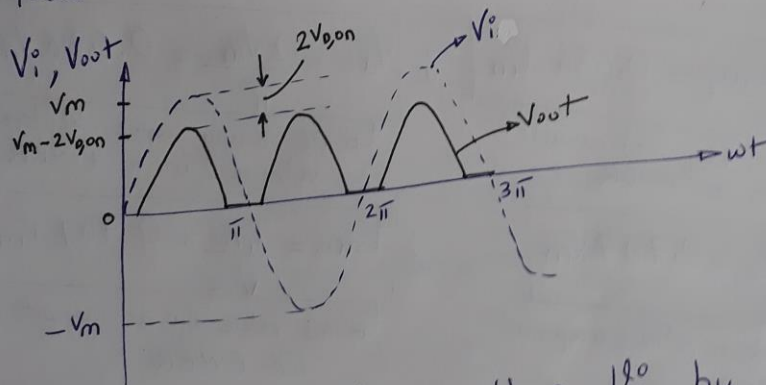


fig 4.6 Input  $V_i$  and o/p  $V_{out}$  waveforms (considering diode drops)

- Since  $V_{out}$  is lower than  $V_i$  by two diode drops (ie  $2V_{D(on)}$ ), it is somewhat a disadvantage of the bridge rectifier.



## Analysis of Full-wave Bridge Rectifier:-

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- Since the o/p current waveforms and rectified o/p voltage waveforms are similar to that of full-wave center-tapped rectifier, only difference being as follows:-

- Considering diode drop's  $V_{on}$  for diodes.

$$V_{out_{FWCT}} = V_m - V_{on} \quad ; \quad V_{out_{FWBR}} = V_m - 2V_{on} \rightarrow (4.1)$$

- Now since magnitude of  $V_m$  is very large compared to  $V_{on}$ , we have ignored it in our analysis.

- The expressions for  $I_{dc}$ ,  $V_{dc}$ ,  $I_{rms}$  and  $V_{rms}$  will be consistent with that of Full-wave center-tap rectifier

$$I_{dc} = \frac{2I_m}{\pi} = 0.636 I_m \quad ; \quad V_{dc} = \frac{2V_m}{\pi} = 0.636 V_m$$

$\hookrightarrow$  DC or avg value of load current in a FWBR       $\hookrightarrow$  DC or avg value of load o/p voltage in a FWBR

$$V_{rms} = \frac{V_m}{\sqrt{2}} = 0.707 V_m \quad ; \quad I_{rms} = \frac{I_m}{\sqrt{2}} = 0.707 I_m$$

$\hookrightarrow$  rms value of ac voltage component for FWBR       $\hookrightarrow$  rms value of ac current component for FWBR

$$P_{dc} = I_{dc}^2 R_L = \left(\frac{2I_m}{\pi}\right)^2 R_L \quad ; \quad P_{ac} = \frac{I_{rms}^2}{2} (R_f + R_L) = \frac{I_m^2}{2} (R_f + R_L)$$

$$\eta_{FWBR} = \frac{P_{dc}}{P_{ac}} \times 100 = 81.06\% \quad \text{----- Full-wave bridge rectifier} \quad (4.2)$$

From (4.2), we can say that efficiency wise there is no difference between full-wave center-tap and full-wave bridge rectifier. 43

• Ripple in a Full-wave bridge rectifier:-

$$\gamma = \frac{I_{ac}}{I_{dc}} = \sqrt{\frac{I_{rms}^2}{I_{dc}^2} - 1}$$

$$\gamma = \sqrt{\frac{I_m^2/2}{4I_m^2/\pi^2} - 1} = \sqrt{\frac{\pi^2}{8} - 1}$$

$$\boxed{\gamma = 0.483} \quad \text{--- For a F.W. Bridge Rectifier}$$

Observation:-

- In the bridge rectifier, the secondary winding of the bridge ckt is not directly grounded.
- Whereas in a center-tapped rectifier, the center tap of the secondary winding was at ground potential.