

Polynomial Chaos based hurricane loss estimation model

A.B.Khajwal^a, A.Noshadravan^a

^a*Department of Civil Engineering, Texas AM University, College Staion, TX, USA*

Abstract

Hurricane hazard is one of the major causes for the loss of life and property and has recently led to an enormous economic loss and social disruption specifically in the coastal regions. Monetary loss of damage to the built infrastructure represents a significant portion of overall hurricane-induced damage. A detailed simulation of hurricane damage at regional scale requires large amount of specific information, which can be poorly understood or is not available with sufficient level of certainty for a large spatial extent. The existing wind damage models often assume a prescribed mathematical structure to describe the dependency between aggregated loss and the hazard intensity in an average sense. The effect of uncertainty is then introduced by treating model parameters as random variables. In the present study, a new approach to tackle this problem is introduced, which relies on a more rigorous and reliable quantification of the involved uncertainties. In particular, the damage induced by wind is modeled as a non-stationary stochastic process for which a probabilistic representation is constructed using polynomial expansion. As a case study, the economic damage data collected by an insurance company is used to calibrate and test the predictive capability of the proposed stochastic loss model. This representation has the advantage of being based on minimal prior assumptions and constraints, in addition to being computationally less demanding since it generates the vulnerability at a coarser regional level. The loss model is used to evaluate the storm risk curve or loss-exceedance model for the region.

Keywords: Polynomial-Chaos, Hurricane loss, Karhunen-Loeve, Loss model, storm-risk model

1. Introduction

Hurricanes have been one of the major causes of loss to life and property worldwide. In United States itself, the distribution of damage caused by disaster events from 1980 to 2018 is largely dominated by tropical cyclone losses, outpacing other natural hazards with the maximum damage (\$919.7 billion, CPI-adjusted), the highest average event cost (\$21.9 billion per event, CPI adjusted) and also being responsible for the highest number of deaths (6,487) [1]. As per the report published by Munich Re [2], 2017 marked the year of highest ever hurricane losses in a single year. The hurricane trio of Harvey, Irma and Maria making landfall within a span of four weeks led to the overall losses of around US\$ 220bn and insured losses of almost US\$ 90bn, which is higher than in the previous record year of 2005 that included hurricanes Katrina, Rita and Wilma (overall losses US\$ 163bn, insured losses US\$ 83bn). The statistics revealed by the same group for 2018 [3] suggest that tropical storms and hurricanes continued to dominate the losses in 2018 and resulted in high losses of US\$ 31bn, of which US\$ 15bn was insured, with Hurricanes Michael and Florence were responsible for the bulk of the burden. In order to mitigate the damages due to such events, a reliable prediction of such damages and losses based on environmental and structural variables is required by engineers and community planners. The environmental phenomenon associated with hurricane damage include high winds, storm surges, high water velocities, and large wave heights [4]. While the threat to life and property as a result of storm surge and storm tides produced by hurricanes is restricted to coastal communities, the associated high windstorms can cause havoc well inland, resulting in a widespread damage. This underscores the need to model and predict the damage caused by various environmental hazards associated with the hurricane event. These damage or vulnerability models can be obtained either empirically based on the claim data from insurance companies or from engineering-based methods [5]. The engineering-based models, however require a large amount of detailed statistical information on the structural behavior of buildings at the component, sub-system and the entire building level, which has limited their wide scale use [6]. On the other hand, there has been an extensive research in developing robust data-driven empirical vulnerability models, specifically in US owing to the availability of relatively large amount of data from hurricane losses [6]. However, owing to their data-driven nature, the degree of reliability associated with these empirical models is often questioned and there

38 have been a number of studies focused to improve the predictability of such
 39 models.
 40 Over years, there has been a huge development in the field of estimation
 41 of wind damage to buildings, the initial major developments being mainly
 42 based on empirical vulnerability models obtained by comparing the building
 43 insurance claims for major wind events with the estimated wind speeds ex-
 44 perience by the buildings. Pioneering work in this regard was carried out
 45 by Don Friedman in 1964 who fitted a power law model to Florida hurricane
 46 data from previous 78 years [5][7]. Some of the other early models include
 47 Ishizaki (1965)[8], Friedman (1975)[9], Howard et al. (1972)[10], Leicester
 48 and Reardon (1976)[11]. Sparks and Brindarwala (1993)[12] developed a de-
 49 terministic vulnerability model for typical single family residences based on
 50 the detailed records of insurance losses in Hurricane Andrew. Rootzn and
 51 Tajvidi (1997)[13] and Katz (2002)[14] developed full stochastic models as-
 52 suming that occurrence of storm events can be modelled by extreme value
 53 functions and the economic damage be modelled as compound Poisson pro-
 54 cess respectively. Khanduri and Morrow (2003)[15] discusses the assessment
 55 of vulnerability of buildings to windstorms and also develops a methodology
 56 for the disaggregation of a generic vulnerability curve into several curves cov-
 57 ering different building classes. Heneka and Ruck (2008)[16] proposed a full
 58 probabilistic mathematical damage model, based on a set of logical assump-
 59 tions outlined by Sill and Kozlowski (1997)[17]. Wang et al. (2017)[18] high-
 60 lighted the impact of vulnerability model uncertainties on hurricane damage
 61 costs while assessing the hurricane damage costs in presence of vulnerability
 62 model uncertainty. An extensive review of different loss/vulnerability mod-
 63 els developed over years is provided in Walker 2011[6], Watson and Johnson
 64 (2014)[19] and Pita et al. (2014).[20]
 65 However most of the existing models rely on a prescribed mathematical struc-
 66 ture to model the relationship between damage and the hazard intensity.
 67 While this may give us fair idea to the damage, its reliability is being ques-
 68 tioned based on the importance of accounting for the associated uncertainties.
 69 Unlike the simpler models wherein only the variation of overall mean damage
 70 loss ratio is modelled, most of the current wind vulnerability models are based
 71 on empirically fitting probability distributions to recorded data and assum-
 72 ing certain stochastic distributions to account for the model uncertainties,
 73 thus not exploiting the entire information provided by the data. Since the
 74 empirical vulnerability functions are mostly based on the analysis of loss data
 75 collected by insurance companies, the uncertainties associated with the eval-

uation of hurricane damage costs not only include the inherent uncertainty in the occurrence of the hurricane event but also the uncertainty associated with the available data. Thus accounting for the uncertainties in the vulnerability model in a reliable and proper way is very important. Assuming a certain probability distribution for the damage or loss may be justified when the data available is less but with the increasing information and hurricane damage data, it is practical to relax the assumptions and extract more information from the available data. Moreover, most of the available data-driven models do not provide a well-defined flexible mathematical structure. The present study proposes a new approach to overcome these limitations by relying on a well-defined, more rigorous and reliable mathematical quantification of the model along with the involved uncertainties. The proposed model characterizes the damage curve as a non-stationary stochastic process indexed over the hazard intensity (wind velocity in the present case). Instead of assuming or pre-defining a certain distribution to account for the uncertainties, the probabilistic representation is constructed using polynomial expansion. Polynomial chaos (PC) expansion in tandem with Karhunen-Loeve (KL) representation is used to model the probabilistic structure of the damage model. This representation not only has the advantage of being based on minimal prior assumptions and is efficient in terms of the use of the information available in the damage data. Another advantage is that this representation can also provide a stochastic prior model that can be integrated in the Bayesian framework for model updating as new information and more data becomes available.

2. Methodology

2.1. Polynomial chaos representation of damage

Gust wind speed is used as the main measure of storm intensity for damage modeling. The uncertainty in the estimated or observed damage in a region subjected to a hurricane with a certain recorded wind velocity can be represented using polynomial chaos formalism for uncertainty quantification Xiu and Karniadakis [21][22]. Let us represent Γ_i as the one-dimensional Hermite polynomials expressed in terms of standard Gaussian random variable ξ . The observed damage corresponding to a given wind speed can be modelled as a second order random variable D and hence admits the PC representation of the form:

$$D_v = \sum_{i=0} k_i \Gamma_i(\xi) \quad (1)$$

111 where k_i are the generalized Fourier coefficients. This representation is
 112 convergent in the mean square sense to the marginal distribution of the
 113 random variable D and owing to the orthogonality of the approximating
 114 polynomials with respect to the Gaussian measure, the coefficients of in the
 115 above expansion can be evaluated as per the following expression

$$k_i = \frac{E[D \cdot \Gamma_i(\xi)]}{E[\Gamma_i^2]} \quad (2)$$

116 The numerator in the above expression represents the ensemble average
 117 and can be evaluated using Monte-Carlo simulation, numerical quadrature
 118 or least square minimization techniques. The denominator represents the
 119 normalization factors which are constant for each Hermite polynomial.

120 2.2. Representation of vulnerability model as a random process

121 The polynomial representation of damage as a random variable given
 122 in the previous section can be easily extended to stochastic process $D(v)$,
 123 representing the distribution of damage indexed by the varying wind velocity
 124 v .

$$D(v) = \sum_{i=0} k_i(v) \Gamma_i(\gamma(v)) \quad (3)$$

125 where the coefficients $k_i(v)$ are now the functions of v , $D(v)$ denotes
 126 the second-order stochastic process representing the damage expressed as a
 127 polynomial in terms of the underlying centered, normalized Gaussian process
 128 $\gamma(v)$ called germ. The correlation structure of this stochastic process can be
 129 captured by suitably specifying the correlation structure of the underlying
 130 Gaussian process $\gamma(v)$ [23]. This can be achieved based on the dependence
 131 of the correlation structure of the mutually orthogonal Hermite polynomials
 132 described above on the underlying Gaussian correlation. Assuming γ_1 and
 133 γ_2 denote the two standard Gaussian random variables at wind velocities v_1
 134 and v_2 , this relation can be written as

$$\langle \Gamma_i(\gamma_1), \Gamma_j(\gamma_2) \rangle = i! \langle \gamma_1, \gamma_2 \rangle^i \delta_{ij} \quad (4)$$

135 δ_{ij} denotes the Kronecker delta function. The immediate consequence of
 136 the equation (4) is an expression for correlation of the damage $D(v)$ in terms
 137 of the correlation of the underlying Gaussian process $\gamma(v)$ as follows

$$C_{ij}^D = \langle \tilde{D}(v_i), \tilde{D}(v_j) \rangle = \sum_{n=1} k_n^i k_n^j n! (c_{ij}^\gamma)^n \quad (5)$$

138 where \tilde{D} denote the centered Gaussian random variable and c_{ij}^D , c_{ij}^γ de-
 139 note the i^{th} and j^{th} components of the covariance structure of $D(v)$ and
 140 $\gamma(v)$ respectively. Equation (5) can be solved using non-linear optimization
 141 or by solving the resulting non-linear algebraic equation numerically. Solving
 142 Equation (5) for c_{ij}^D will result in the covariance structure of the underlying
 143 Gaussian process.

144 In order to cast the stochastic representation of the damage in terms of uncor-
 145 related standard Gaussian germs which can be easily simulated, Karhunen-
 146 Loeve expansion is employed to represent the N_D -dimensional standard Gaus-
 147 sian random vector $\gamma(v)$ with the covariance structure obtained previously
 148 in terms of uncorrelated independent standard Gaussian random variables.

$$\gamma(v) = \sum_{i=0}^{N_D} \sqrt{\lambda_i} f_i(v) \xi_i \quad (6)$$

149 where $\{\lambda_i\}_{i=1}^{N_D}$ and $\{f_i\}_{i=1}^{N_D}$ denote the eigenvalues and the corresponding
 150 eigen vectors of the covariance matrix of the underlying Gaussian process
 151 and ξ_i is a set of underlying uncorrelated Gaussian standard random vari-
 152 ables. Using Equation (6), Equation (3) can be rewritten in terms of uncorre-
 153 lated standard Gaussian random variables, which can be easily synthesized.
 154 The underlying correlation structure is now captured by the eigenvalues and
 155 eigenvectors of the correlation matrix of the underlying Gaussian process.

$$D(v) = \sum_{i=0}^{N_O} k_i(v) \Gamma_i \left(\sum_{k=1}^{N_D} \sqrt{\lambda_k} f_k(v) \xi_k \right) \quad (7)$$

156 N_O and N_D in the above expression represent the order of the polynomial
 157 expansion and dimension of the random vector respectively. The dimension-
 158 ality can be reduced by truncating the bracketed term in Equation (7) by
 159 only including the terms corresponding to the dominant eigen-values. Hav-
 160 ing represented the random variable $D(v)$ in terms of a set of uncorrelated

161 standard Gaussian random variables $\{\xi_i\}_{i=1}^{N_D}$, Equation (7) can be recast in
 162 the following multi-dimensional polynomial form

$$D(v) = \sum_{i=0}^{N_O} a_i(v) \Psi_i(\{\xi_i\}_{i=1}^{N_D}) \quad (8)$$

163 where Ψ_i is the i^{th} N_D dimensional Hermite polynomial, and a_i are the
 164 multi-dimensional PC coefficients which can be computed using Monte Carlo
 165 simulation or a numerical integration technique. However, equating the rep-
 166 resentations given by Equation (8) and Equation (3), the coefficients $a_i(v)$
 167 can also be obtained analytically from the following expression by Sakamoto
 168 and Ghanem [23]:

$$a_i(v) = \frac{p!}{\langle \Psi_i^2 \rangle} k_p(v) \prod_{j=1}^p \sqrt{\lambda_{m(j)}} f_{m(j)}(v) \quad (9)$$

169 where $\prod_{j=1}^p \sqrt{\lambda_{m(j)}} f_{m(j)}(v)$ denotes the product of the $\sqrt{\lambda_k} f_k(v)$ with m
 170 as the index on at least one of the underlying i making up Ψ_i , p is the order
 171 of the polynomial. Once the coefficients are evaluated, realizations of dam-
 172 age at different wind velocities can be simulated to generate the stochastic
 173 damage model using Monte Carlo simulation. The simulated damage model
 174 using Equation 8 will approximate the underlying data in terms of marginal
 175 distributions as well as preserve the correlation structure of the data.

176 2.3. Evaluation of loss-exceedance curve

177 The loss model developed in the previous section forms a basis for de-
 178 veloping several subsequent models which can represent the manifestation of
 179 the predicted damage in forms that can be more reasonable and informa-
 180 tive in order to facilitate decision making and proper planning towards the
 181 realization of a community resilient to the damage due to natural hazards.
 182 In the present study, loss-exceedance curve is generated from the hurricane
 183 storm hazard data and the hurricane loss model developed in the previous
 184 section. Having obtained the distribution of storm/wind hazard from the
 185 historic data, the probability of exceedance of a given threshold economic
 186 loss can be obtained as:

$$P(D > D_{th}) = \sum P(v_i) \cdot P(D(v_i) \geq D_{th}) \quad (10)$$

187 The probability of exceedance of the threshold loss can be calculated for
188 a range of threshold values giving us an estimation of the varying probability
189 of exceedance of a range of threshold losses. The loss exceedance curve for
190 a region can be of pivotal importance in evaluating post-hurricane resilience
191 and recovery strategies given the target degree of safety.

192 3. Case Study

193 3.1. Database

194 For the purpose of demonstrating the proposed methodology for the de-
195 velopment of the vulnerability model, the storm damage database obtained
196 from ICAT (<https://www.icat.com>), an insurance company dealing with pro-
197 viding hurricane and earthquake insurance to homeowners and businesses in
198 US, is used. The database consists of the total economic damages produced
199 by 248 storms that struck the east coast of US from 1900 to 2018. This data
200 is extracted from the storm and weather review reports produced by Na-
201 tional Hurricane Center (NHC). The total economic damage reported for
202 each storm in the year of its landfall is normalized to the economic damage
203 for the year 2019 by accounting for the changes in inflation, population and
204 wealth as per the approach outlined by Pielke et al. [24]. Normalizing the
205 economic damage to the current value brings all the damage values to the
206 same scale and enables the comparison of all storms equally as if they all
207 had their landfall in the current year. Figure 1 shows the scatter plot of the
208 data depicting the normalized total economic damage plotted against the
209 maximum wind speed observed during the storm.

210 3.2. Implementation and results

211 The stochastic vulnerability model here is characterized and simulated as
212 discrete random process indexed by wind velocity. In order to do so, the range
213 of wind velocities over which the damage is observed is discretized and the
214 observations of corresponding damage data are assigned to these discretized
215 values (Fig. 2). This is done such that there is sufficiently enough number
216 of data points at each wind speed to construct the proposed model. This
217 discretized economic damage data is treated as the input for developing the
218 predictive model using the proposed methodology. However, owing to a wide
219 range of damage values, $\ln(D)$ instead of D is used as the random variable
220 in the implementation of the presented methodology. The output is later

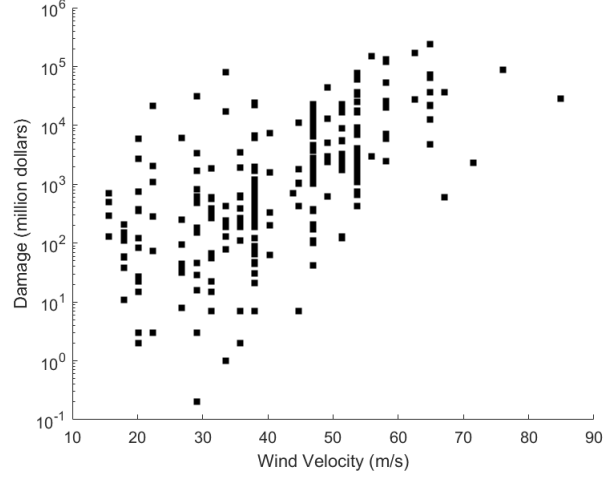


Figure 1: Scatter plot of the normalized total normalized economic damage plotted against maximum wind speed. (Data collected from: <http://www.icatdamageestimator.com>)

221 expressed back in terms of D for comparison with the data. The summary
 222 of the implementation algorithm is illustrated in figure 3

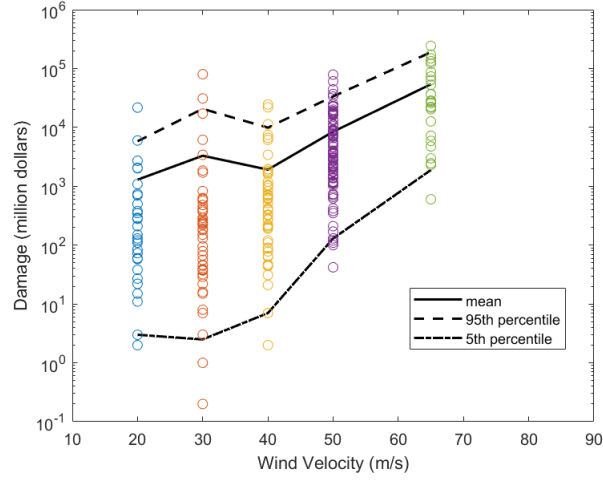


Figure 2: Discretized damage data. Solid line shows the mean; dashed and dotted lines show the 95th and 5th percentiles of the data respectively

223 The accuracy of this implementation is specified in terms of the order
 224 (N_O) of the polynomials Γ_i used in the PC expansion and the number of

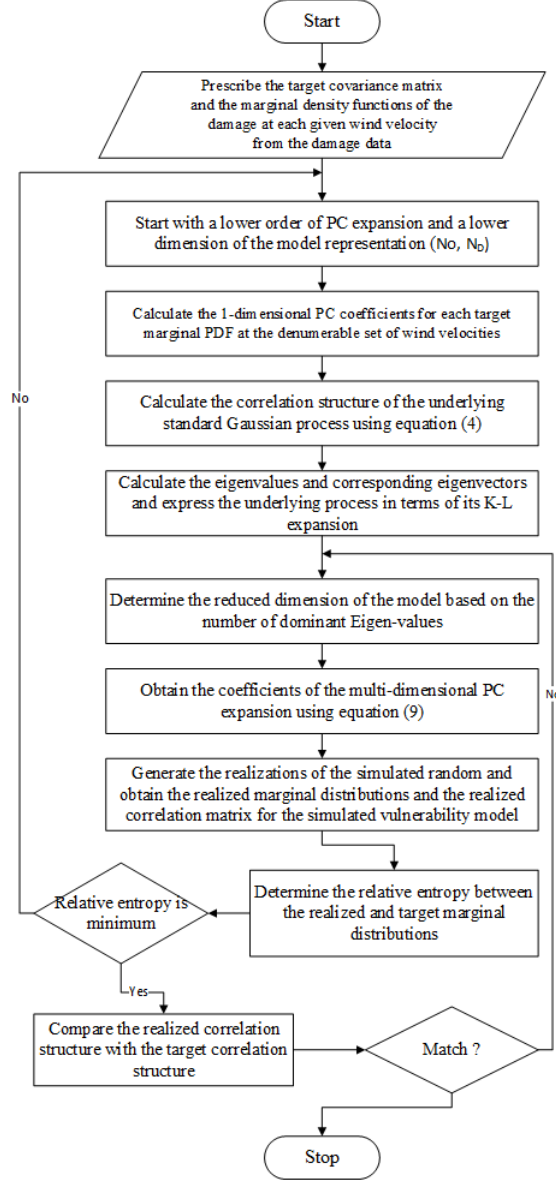


Figure 3: Algorithm outlining the implementation of polynomial chaos expansion for simulation of loss model.

225 dimensions (N_D) used in the K-L representation of the damage. While N_O
 226 dictates the precision of the synthesized marginal probability density func-
 227 tions, N_D dictates how well the correlation structure of the data is captured.

228 Suitable values of ND and NO are determined by examining the error in
 229 simulating the target marginals and correlation structure of the available
 230 data respectively. In order to specify the order, relative entropy between the
 231 target and the simulated marginal distributions is calculated for varying PC
 232 order, as shown in Figure 4, following which PC order 5 is chosen, without
 233 compromising too much on precision. The trend is observed to be similar for
 234 other marginals as well. Figure 5 shows the comparison between the target
 235 and simulated pdf of the damage corresponding to the selected order. The
 236 dimension ND used in the multi-dimensional PC representations is decided
 237 based on the number of significant eigen-values of the covariance structure of
 238 the data and the comparison of the target and the realized covariance matrix.
 239 Based on the observations, N_D is selected to be same as the number of nodes
 240 (N_N) in the data without any reduction in the dimensionality. However, the
 241 proposed model allows the reduction in dimensionality if permitted by the
 242 correlation structure of the data.

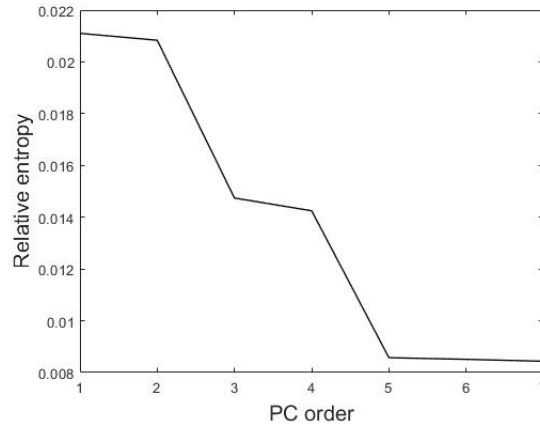


Figure 4: Relative entropy between PC predictions against the data distribution as the order of the expansion increases.

243 The number of dimensions in the multi-dimensional PC representations
 244 is decided based on the number of significant eigen-values of the covariance
 245 structure of the data and the comparison of the target and the realized co-
 246 variance matrix. Based on the observations, N_D is selected to be same as the
 247 number of nodes (N_N) in the data without any reduction in the dimension-
 248 ality. However, the proposed model allows the reduction in dimensionality
 249 if permitted by the correlation structure of the data. Having specified the

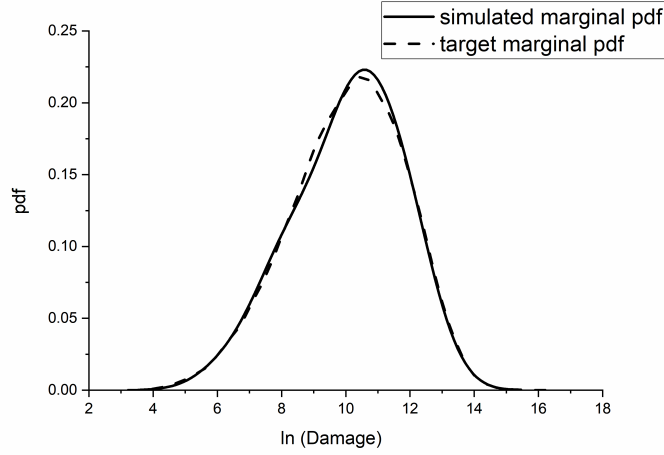


Figure 5: Comparison of the target marginal pdf and the simulated marginal pdf at $v=65\text{m/s}$.

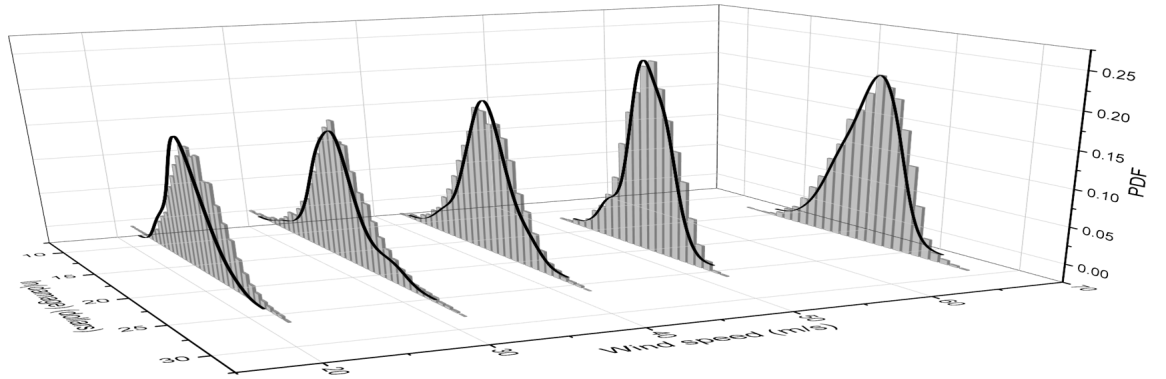


Figure 6: The predicted marginal distributions estimated from the pro-posed model at different wind speeds..

250 dimension and the order, the numerical simulation is performed to generate
 251 the set of marginal distributions, which is observed to follow the same corre-
 252 lation as present in the data. Figure 6 shows the distribution of the damage
 253 predicted using the proposed model plotted in the logarithmic scale. The
 254 predicted distribution is observed to capture the stochastic characteristics of
 255 the marginal distributions as well as the correlation structure of the underly-

ing data with significant accuracy. The comparison of the simulated marginal distributions at different wind velocities using the proposed model with the target distributions verifies the applicability of the proposed model for the stochastic prediction of dam-age or loss during the events of high windstorms (Fig. 6). Providing a well-defined mathematical framework for the simulation of the damage model, this methodology can not only be used to provide an estimate of the vulnerabilities to the hurricane hazard at a regional level but can also be easily integrated in the larger framework of regional hazard risk assessment as well as in developing post-disaster recovery and resilience quantification models.

Using the obtained PC-based loss model, a hazard-based evaluation based on the extreme value hazard events can be performed to evaluate storm risk curves for the area under study. The expected loss in the given region is set against the probability of exceedance. Hence a 10 year storm is expected to cause a total loss of around 30 billion USD and a 50-year storm of more than 100 billion USD. The approach adopted consists of two parts: first the wind hazard is estimated from the extreme value analysis of the storm events observed during last 118 years and then the risk associated with the exceedance of threshold losses is evaluated in terms of the probability of exceedance. The wind speeds are observed to accord well with Weibull extreme value distribution which is illustrated in the probability plot (7). The parameters of the two-parametric Weibull distribution estimated by the maximum likelihood method are $\lambda = 46.08$ and $k = 3.49$ for the wind speed data. Using 10 the loss-exceedance curve is evaluated as shown in figure 8.

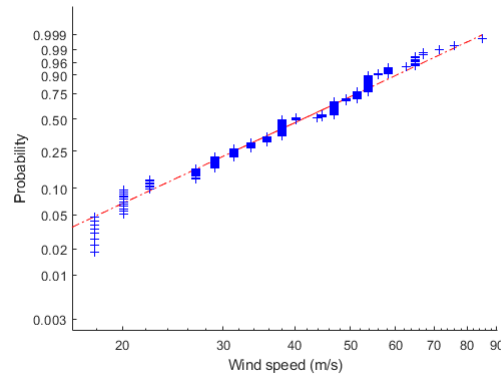


Figure 7: Weibull probability plots for wind velocity data

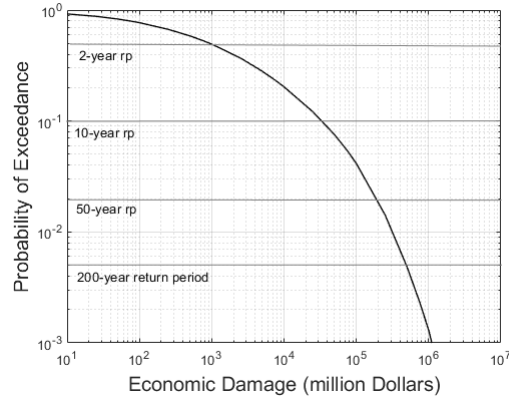


Figure 8: Loss exceedance curve for the region under study

280 4. Conclusion

281 The proposed methodology represents the hurricane wind-induced damage
 282 age model as an expansion of multi-dimensional Hermite polynomials in a set
 283 of uncorrelated standard normal Gaussian variables. This model in spite of
 284 relying on minimal prior assumptions and constraints, presents a well-defined
 285 and flexible stochastic model for prediction of hazard-induced damage and
 286 can provide a reliable input to regional risk and reliability assessment models
 287 for proper risk-informed decision making and prioritization of efforts to
 288 mitigate the overall damages due to future hurricane events.

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