

## Tutorial- 11 (Solutions)

**Q.1.** For finding the equivalent inductance at  $ab$  terminals, let us assume a voltage  $v$  and currents  $i, i_1$  and  $i_2$  as shown in Fig. S1. We can use KVL for loop1 and loop2:

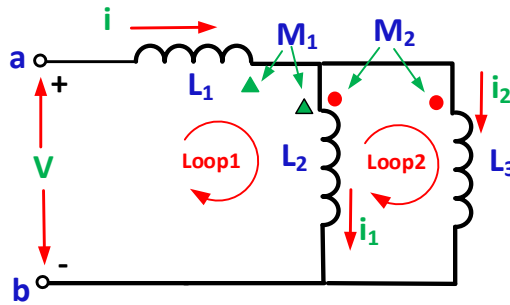


Fig. S1

$$i = i_1 + i_2$$

For loop1, applying the KVL,  $v = L_1 \frac{di}{dt} + L_2 \frac{di_1}{dt} - M_1 \frac{di_1}{dt} - M_1 \frac{di}{dt} + M_2 \frac{di_2}{dt}$

Similarly applying KVS in loop2,  $L_2 \frac{di_1}{dt} - L_3 \frac{di_2}{dt} + M_2 \frac{di_2}{dt} - M_1 \frac{di}{dt} - M_2 \frac{di_1}{dt} = 0$

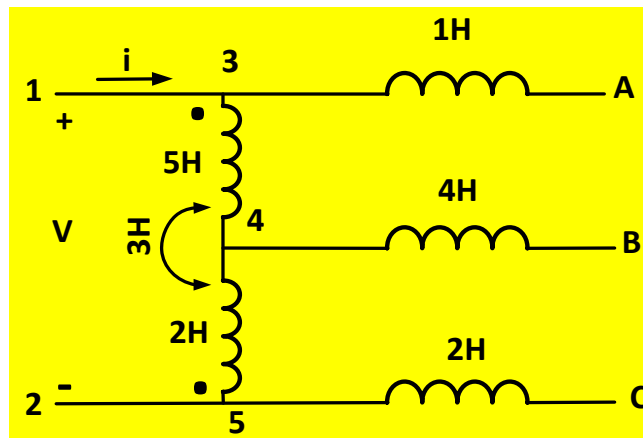
Solving the three equations and finding the relation between  $v$  and  $i$ , one can find the equivalent inductance at  $ab$  terminal.

**Q.2.** Voltage induced in a coil due to a current in the second coil will have its +ve polarity at the dotted terminal, if the current enters into the dotted terminal at the second coil. Similarly, the induced voltage will have -ve polarity if the current leaves the dotted terminal.

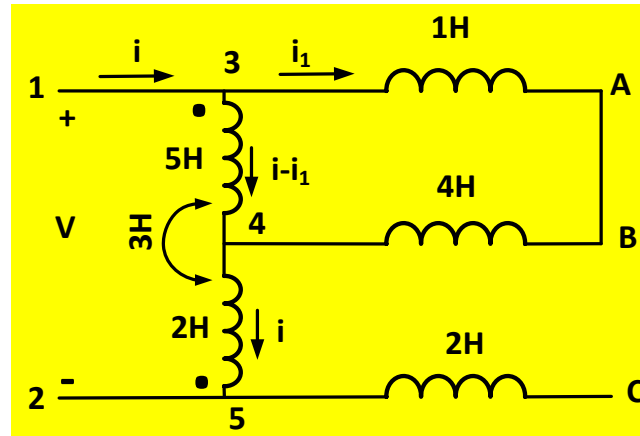
**(a)** Applying KVL in the loop 134521,

$$v - 5 \frac{di}{dt} + 3 \frac{di}{dt} - 2 \frac{di}{dt} + 3 \frac{di}{dt} = 0 \Rightarrow v - \frac{di}{dt} = 0$$

Leq = 1 H



(b)



Applying KVL in the loop 134521,

$$V - 5 \frac{d(i-i_1)}{dt} + 3 \frac{di}{dt} - 2 \frac{di}{dt} + 3 \frac{d(i-i_1)}{dt} = 0 \Rightarrow V - \frac{di}{dt} + 2 \frac{di_1}{dt} = 0 \quad (1)$$

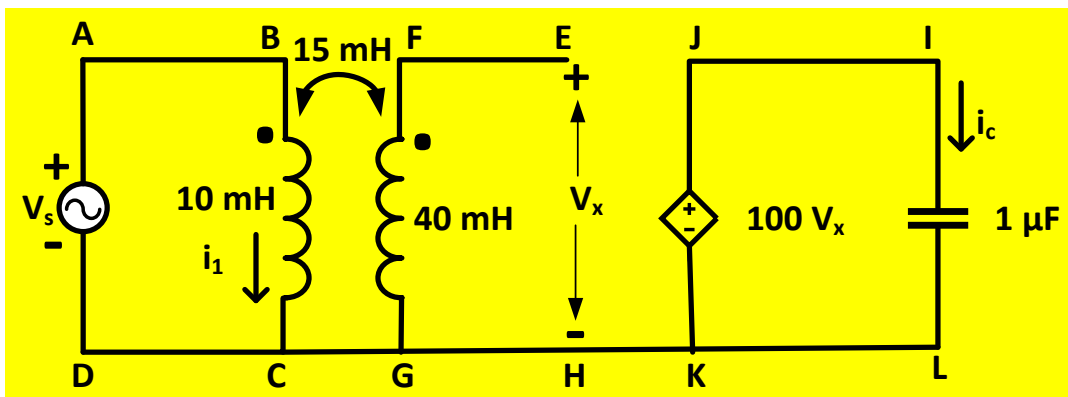
Applying KVL in the loop 3AB43,

$$- \frac{di_1}{dt} - 4 \frac{di_1}{dt} + 5 \frac{d(i-i_1)}{dt} - 3 \frac{di}{dt} = 0 \Rightarrow \frac{di_1}{dt} = \frac{1}{5} \frac{di}{dt} \quad \text{-----}(2)$$

Replacing the value of  $\frac{di_1}{dt}$  from (2) in equation (1)

$$V - \frac{di}{dt} \left(1 - \frac{2}{5}\right) = 0 \Rightarrow L_{eq} = \frac{3}{5} H$$

Q.3.



Applying KVL in the loop ABCDA

$$\frac{10t^2}{t^2 + 0.01} = 10 \times 10^{-3} \frac{di_1}{dt}$$

$$\Rightarrow \frac{di_1}{dt} = \frac{1000t^2}{t^2 + 0.01}$$

There will be an induced voltage in 40 mH coil due to the current  $i_1$  in 10 mH coil. Applying KVL in the loop EFGHE

$$15 \times 10^{-3} \frac{di_1}{dt} = V_x$$

$$\Rightarrow V_x = \frac{15t^2}{t^2 + 0.01}$$

Applying KVL in the loop LKJIL

$$100V_x - \frac{\int i_c dt}{C} = 0$$

$$\Rightarrow i_c = 100C \times \frac{dV_x}{dt} = \frac{0.03t}{(t^2 + 0.01)^2} \text{ mA}$$

# EE101: Basic Electronics

## Theme: Micro-electronics

Tutorial-11, Nov. 7, 2018

### Tutorial Problems

#### Solutions

Q4.

1. The diode equation can be rewritten in the following form:  $V_D = V_T \ln\left(\frac{I_D}{I_s}\right)$ .
2. From Fig. 1 and using the above equation, we can write the following expressions for output voltages.

$$V_1 = V_T \ln\left(\frac{nI_0}{I_s}\right) \quad (1)$$

$$V_2 = V_T \ln\left(\frac{I_0}{I_s}\right) \quad (2)$$

$$V_{OUT} = V_1 - V_2 = V_T \ln(n) \quad (3)$$

3. Recall that  $V_T = \frac{kT}{q}$  is the thermal voltage. Here  $k$  is the Boltzmann constant,  $T$  is the absolute temperature in Kelvin and  $q$  is the magnitude of the electron charge.
4.  $\frac{\partial V_{OUT}}{\partial T} = \frac{k}{q} \ln(n)$  is a positive constant!

**Inference:** Even though the individual voltages  $V_1$  and  $V_2$  have negative temperature coefficients ( $-2\text{mV}/^\circ\text{C}$ ), the differential voltage ( $V_1 - V_2$ ) has a positive constant temperature coefficient. Moreover, the voltage  $V_{OUT}$  is proportional to the absolute temperature. This circuit can be used as a temperature sensor.

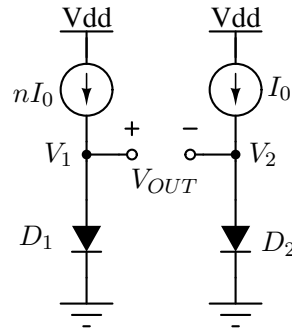


Figure 1: Diode circuits

Q5.

1.  $V_1$  (or  $V_2$ ) has a negative temperature coefficient and  $V_{OUT}$  has a positive temperature coefficient.

2. If we can generate a voltage  $V_{OUT,0T} = A_1 V_1 + A_2 V_{OUT}$ , then

$$\frac{\partial V_{OUT,0T}}{\partial T} = A_1(-2mV/^{\circ}C) + A_2\left(\frac{k}{q} \ln(n)\right) \approx [-2A_1 + 0.087 \times A_2 \ln(n)] \text{ mV}/^{\circ}C.$$

3. If we choose  $0.087 \times A_2 \ln(n) = 2A_1$ , then  $\frac{\partial V_{OUT,0T}}{\partial T} = 0$  and the voltage  $V_{OUT,0T}$  becomes independent of temperature.

4.  $V_{OUT,0T} = A_1 V_1 + A_2 V_{OUT} = (A_1 + A_2)V_1 - A_2 V_2$ .

5. Notes on realization:

- We need to sense the voltages  $V_1$  and  $V_2$  without drawing any current from the diode circuit.
- Since  $V_1$  and  $V_2$  require two different scaling factors  $(A_1 + A_2)$  and  $A_2$  respectively, the 3-opamp realization shown in Fig. 2 can be used<sup>1</sup>.

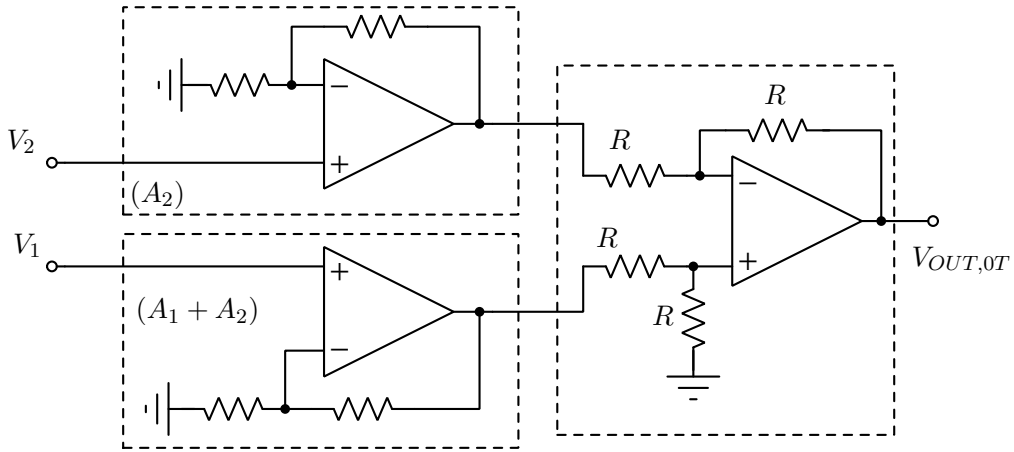


Figure 2:

<sup>1</sup>Important: This realization will not work in practice as the characteristics of opamps, resistors, and current sources change with temperature.