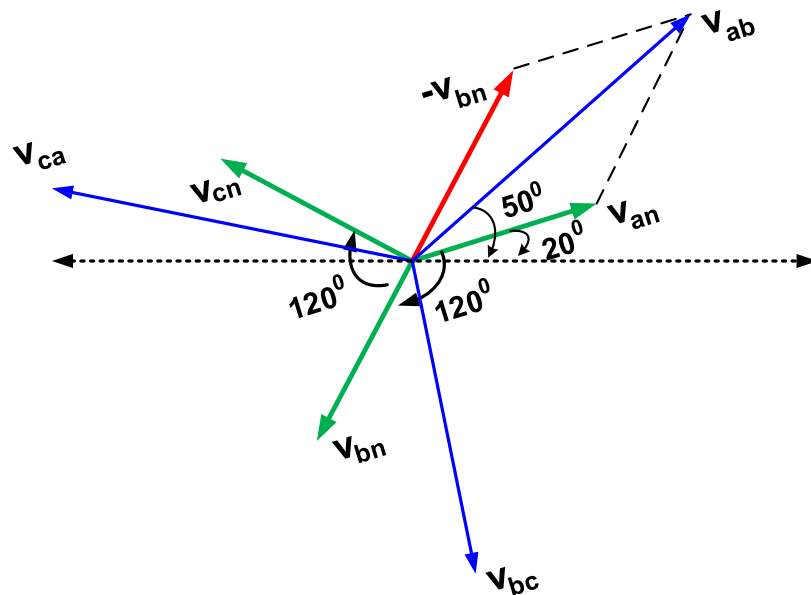


## Tutorial 7: Solutions

- Single phase motors are not able to start by themselves. This requires a polyphase source. 3-phase generators, motors and transformers are simpler, cheaper and more efficient. 3-phase transmission lines deliver more power for a given cost or for a given weight of conductor. Voltage regulation of a 3-phase system is inherently better. In case of star-connected source, the line voltage is  $\sqrt{3}$  times the phase voltage. This helps in transmitting and distributing power with a higher voltage. The number of conductors required for transmission and distribution is reduced thus helps reducing the cost in case of a balanced three-phase system.

$$\begin{aligned}
 v_{ab} &= v_{an} - v_{bn} \\
 &= V_p \angle 20^\circ - V_p \angle -100^\circ \\
 &= V_p \sin(\omega t + 20^\circ) - V_p \sin(\omega t - 100^\circ) \\
 &= V_p \times 2 \sin\left(\frac{\omega t + 20^\circ - \omega t + 100^\circ}{2}\right) \cos\frac{\omega t + 20^\circ + \omega t - 100^\circ}{2} \\
 &= V_p \times 2 \sin(60^\circ) \cos(\omega t - 40^\circ) \\
 &= \sqrt{3}V_p \cos(\omega t - 40^\circ) \\
 &= \sqrt{3}V_p \cos(90^\circ - (\omega t + 50^\circ)) \\
 &= \sqrt{3}V_p \sin(\omega t + 50^\circ)
 \end{aligned}$$

$$\begin{aligned}
 v_{ab} &= \sqrt{3}V_p \sin(\omega t + 50^\circ) = V_L \angle 50^\circ \\
 v_{bc} &= \sqrt{3}V_p \sin(\omega t - 70^\circ) = V_L \angle -70^\circ \\
 v_{ca} &= \sqrt{3}V_p \sin(\omega t - 190^\circ) = V_L \angle -190^\circ
 \end{aligned}$$



**Fig.S1**

2.

a.

$$I_{AN} = \frac{120\angle 0^\circ}{10} = 12\angle 0^\circ \text{ A}$$

$$I_{NB} = \frac{120\angle 0^\circ}{10} = 12\angle 0^\circ \text{ A}$$

$$I_1 = \frac{120\angle 0^\circ + 120\angle 0^\circ}{16 + j12} = 12\angle -36.87^\circ \text{ A}$$

$$I_{aA} = I_1 + I_{AN} = 12\angle -36.87^\circ + 12\angle 0^\circ = 9.6 - j7.2 + 12 = 22.77\angle -18.43^\circ \text{ A}$$

$$I_{nN} = I_{NB} - I_{AN} = 0 \text{ A}$$

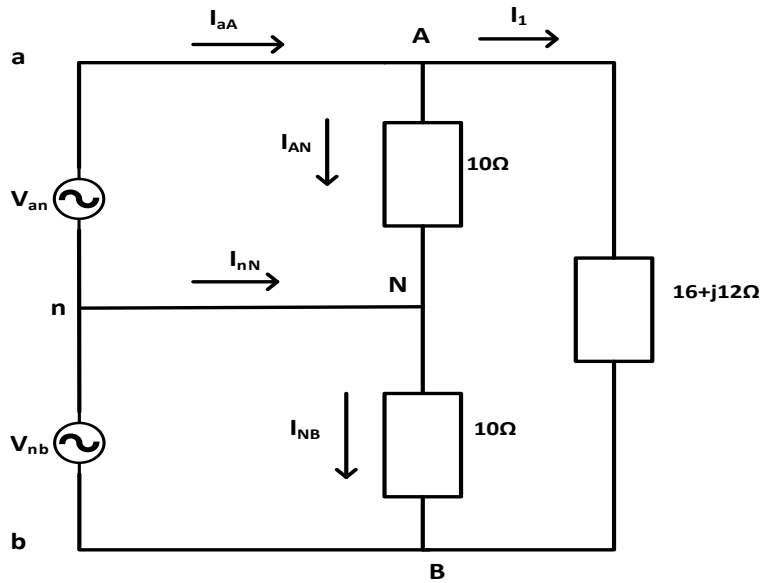


Fig.S2

b. When  $10 \Omega$  is connected in parallel with  $Z_{AN}$ ,

$$\text{new } Z_{AN} = 5\Omega, I_{AN} = \frac{120\angle 0^\circ}{5} = 24\angle 0^\circ \text{ A}$$

$$I_{aA} = I_1 + I_{AN} = 12\angle -36.87^\circ + 24\angle 0^\circ = 9.6 - j7.2 + 24 = 34.36\angle -12.09^\circ \text{ A}$$

$$I_{nN} = I_{NB} - I_{AN} = 12\angle 0^\circ - 24\angle 0^\circ = -12\angle 0^\circ \text{ A}$$

$$I_{bB} = -(I_{NB} + I_1) = -22.77\angle -18.43^\circ \text{ A}$$

3. Converting delta connected load to star connected load-

$$Z'_2 = \frac{Z_2^2}{3Z_2} = \frac{Z_2}{3} = 10 - j53.1 \Omega$$

$$\text{Total impedance per phase} = \frac{Z_1 Z'_2}{Z_1 + Z'_2} = \frac{(20 + j37.7)(10 - j53.1)}{30 - j15.4} = 68.38\angle 9.89^\circ \Omega$$

a. Line current  $= \frac{398}{\sqrt{3}} \times \frac{1}{68.38\angle 9.89^\circ} = 3.36\angle -9.89^\circ \text{ A}$

b. P.F.  $= \cos 9.89^\circ = 0.985$  lagging

c. Total power  $= \sqrt{3} \times V_L I_L^* = \sqrt{3} \times 398 \times 3.36\angle 9.89^\circ \text{ VA}$

Reactive power  $= 397.83 \text{ VAR}$

4. A The resistance value of the thermistor is

$$R_{\text{Therm}} = 10k\Omega - 120\Omega/^{\circ}C \times (T - 25^{\circ}C) \quad (1)$$

$$= \begin{cases} 10k\Omega & \text{at } 25^{\circ}C \\ 1k\Omega & \text{at } 100^{\circ}C \end{cases} \quad (2)$$

where  $T$  is the temperature in  $^{\circ}C$ . A simple circuit to convert the  $\Delta T \rightarrow \Delta R \rightarrow \Delta V$  is shown in Fig.S4(a). As the temperature changes from  $25^{\circ}C$  to  $100^{\circ}C$ ,  $V_{OUT}$  increases from 4.5V to 8.1818V ( $=V_{REF}$ ). We can compare the  $V_{OUT}$  value to 8.1818V to enable the alarm as shown in Fig.S4(b). One can generate the  $V_{REF}$  from the 9V battery using a resistive divider of  $10k\Omega$  and a  $1k\Omega$ .

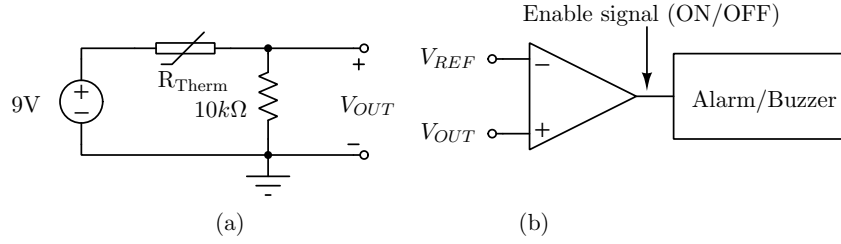


Fig.S4(a) A thermistor based temperature-to-voltage conversion (b) A comparator enabled alarm system.

5. The temperature-to-voltage conversion circuit shown in Fig.S4(a) can also be used here.

- Divide the temperature range into 16 levels and assign a 4-bit code to each level as shown in Fig.S5(a).
- Compute the  $V_{OUT}$  corresponding to each level as shown in Fig.S5(a).
- We need 16  $V_{REF}$  values to know the exact temperature<sup>1</sup>.
- A priority encoder can be used to encode the outputs of the 16 comparators into 4-bits. A 16-to-4 bit priority encoder outputs the 4-bit binary code corresponding to the highest priority input which is set to high (maximum decimal).

<sup>1</sup>In a typical implementation, voltage levels (instead of temperature) are equally divided so that the 16  $V_{REF}$  values can be generated from a single resistive divider loop

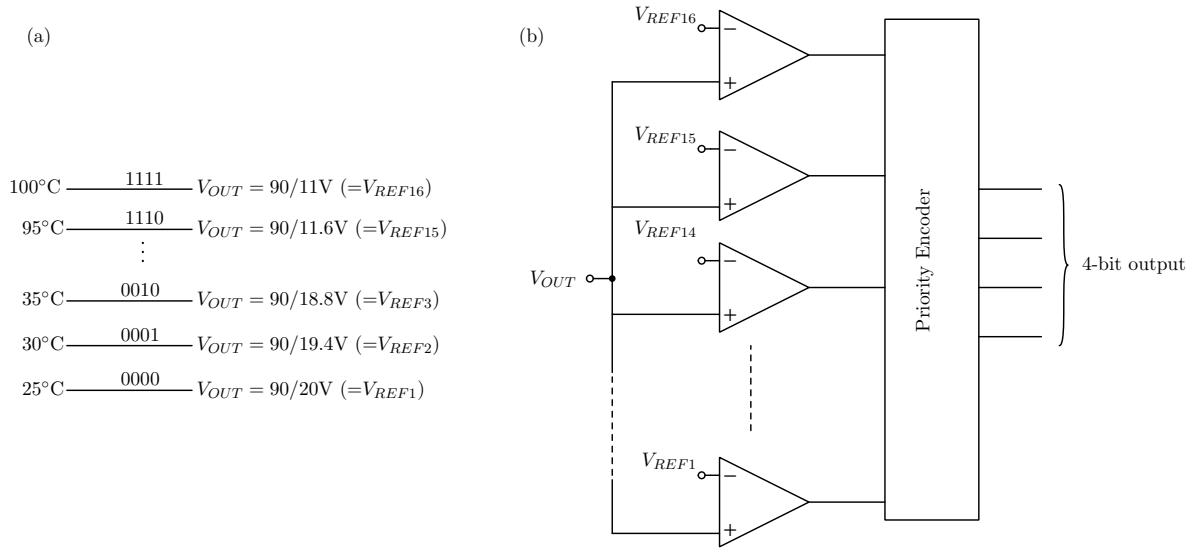


Fig.S5(a) 16 temperature levels and the corresponding  $V_{OUT}$  values. (b) A comparator enabled alarm system.