

**COURSEWORK ASSIGNMENT**

<b>Module Title:</b> Mixed-Mode and VLSI Technologies	<b>Module Code:</b> 7ENT1008
<b>Assignment Title:</b> Design and Simulation of CMOS OTA-C Filters	<b>Individual Assignment</b>
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17019396	

<b>Marks Awarded %:</b>	<b>Marks Awarded after Lateness Penalty applied %:</b>
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Lab Answer Sheet on

**Design and Simulation of CMOS OTA-C Filters**

ID number: 17019396

(a) Determine the minimum value of bias voltage  $V_b$ , showing the workings. Choose bias voltage  $V_b = -1.6V$  and compute OTA transconductance,  $g_m$ , using the formula and parameter values given in the lab sheet.

(20%)

For the minimum value of  $V_b$  we should equal the  $g_m$  to 0 in the equation,

$$g_m = \mu_n C_{ox} \sqrt{\frac{1}{2} \left(\frac{W}{L}\right)_{1,2} \left(\frac{W}{L}\right)_9} (V_b - V_{ss} - V_{Tn}) \quad g_m = 0$$

$$0 = (V_b - V_{ss} - V_{Tn}) \text{ where } V_{ss} = -2.5V \text{ and } V_{Tn} = 0.8V$$

So minimum value of  $V_b = -1.7V$

With  $V_b$  given finding  $g_m$ ,

$$g_m = \mu_n C_{ox} \sqrt{\frac{1}{2} \left(\frac{W}{L}\right)_{1,2} \left(\frac{W}{L}\right)_9} (V_b - V_{ss} - V_{Tn})$$

Parameter values given in the lab sheet;

$$\mu_n = 700 \text{ cm}^2/V_s, C_{ox} = 3.45 \text{ fF}/\mu\text{m}^2, V_{Tn} = 0.8V, V_{ss} = -2.5V$$

$$g_m = (0.07) * (3.45) * \frac{10^{-15}}{10^{-12}} * \sqrt{\frac{1}{2} \left(\frac{50}{5}\right)_{1,2} \left(\frac{25}{5}\right)_9} * (-1.6 + 2.5 - 0.8)$$

$$= (0.07) \times (3.45) \times 10^{-3} \times 5 \times 10^{-1}$$

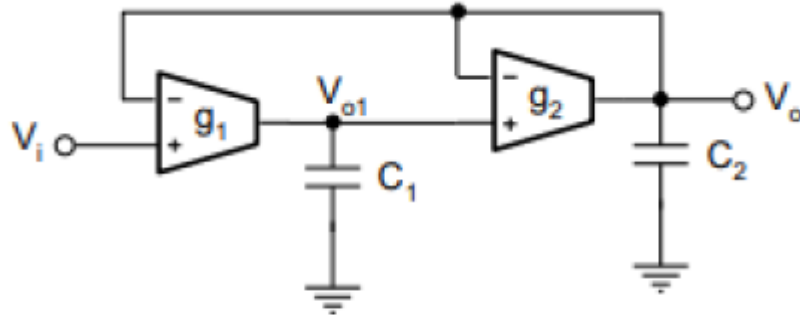
$$= 1.20175 \times 10^{-4}$$

$$= 12.0175 \times 10^{-5} \text{ siemens}$$

(b) For the OTA-C filter, at  $V_b = -1.6V$ , assuming  $g_1 = g_2 = g_m$ , calculate  $C_1$  and  $C_2$  for the given filter specifications  $f_0 = 10MHz$  and  $Q = 1$ . Give the formulas used and the process.

(20%)

$K_{LP} = 1$



$$H_{lp}(s) = \frac{g_1 g_2 / C_1 C_2}{s^2 + s(g_2 / C_2) + g_1 g_2 / C_1 C_2} = \frac{K_{LP} W_0^2}{s^2 + s(W_0 / Q) + W_0^2}$$

$$Q = \sqrt{\frac{g_1 * C_2}{g_2 * C_1}}$$

where

$Q = 1$  and assuming  $g_1 = g_2 = g_m$

from here  $C_1 = C_2 = C$

$$w_0 = \sqrt{\frac{g_1 * g_2}{C_1 * C_2}}$$

from here

$$w_0 = \frac{g_m}{C}$$

It is known that  $w_0 = 2\pi f_0$  and  $f_0 = 10MHz$

$$\begin{aligned} &= 2 \times 3.14 \times 10 \times 10^6 \\ &= 62.8 \times 10^6 \text{ Hz} \end{aligned}$$

$$C = \frac{gm}{\omega_o} = \frac{12.0175 \times 10^{-5}}{62.8 \times 10^{-6}} = 0.191 \times 10^{-11}$$

$$= 1.91 \times 10^{-12} F$$

$$= 1.91 pF$$

(c) Give the transistor level schematic of the whole CMOS OTA-C filter with  $V_b = -1.6V$  you actually used in your lab simulation. Give the simulated amplitude and phase frequency responses of the filter at  $V_b = -1.6V$  only, which were obtained in the lab experiment.

(20%)

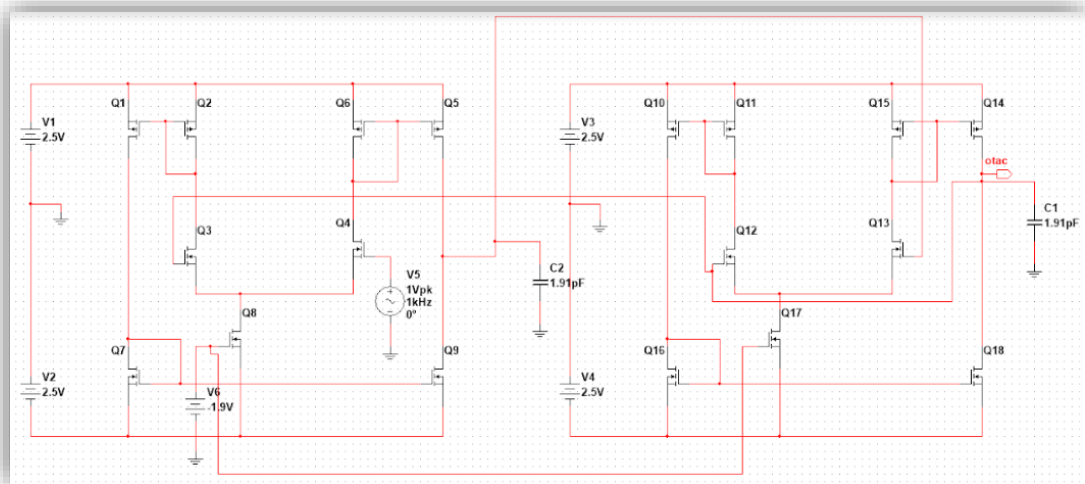


Figure 1 Schematic of the whole CMOS OTA-C filter

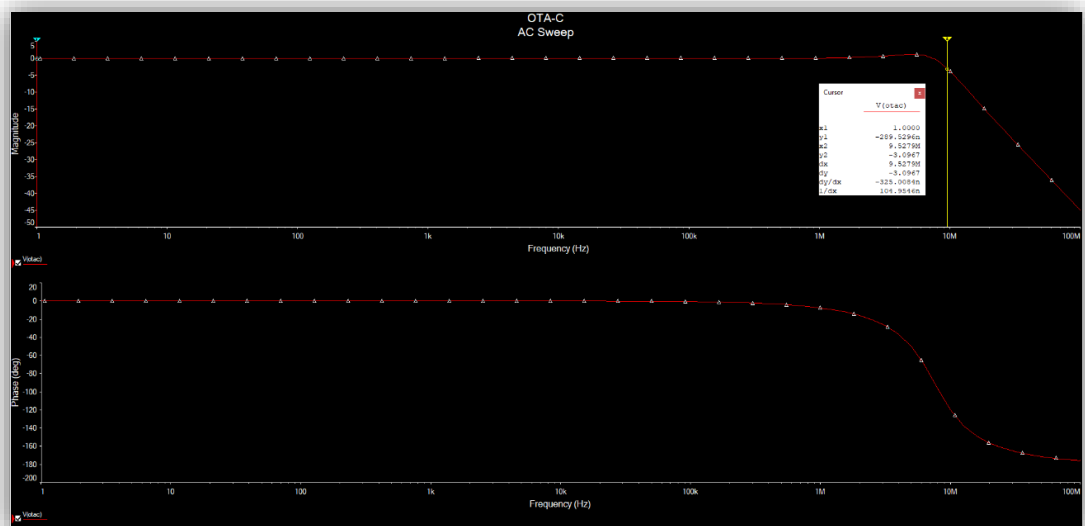
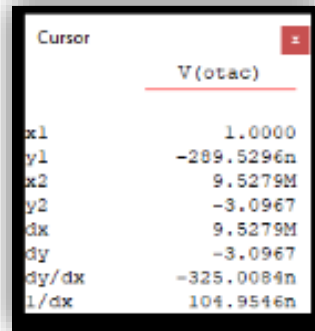


Figure 2 simulated amplitude and phase frequency responses of the filter at  $V_b = -1.6$



For  $V_b = -1.6$

(d) Comment on the simulated results given above by comparing the simulated cut-off frequency with its ideal value. Discuss deviation if any and what OTA nonidealities may have caused the deviation and why.

(40%)

When changing  $V_b$  to other values to observe how the filter cutoff frequency  $f_o$  is tuneable by the bias voltage, the results we got are below.

$V_b$	$f_o$
-1.3	12.7896M
-1.4	11.710M
-1.5	10.7277M
<b>-1.6</b>	<b>9.5279M</b>
-1.7	8.4768M
-1.8	7.3187M
-1.9	6.3188M
-2.0	5.2543M

As  $V_b$  decreases, cut off frequency decreases.

When  $V_b$  is equal to  $-1.6V$ ;

$f_o = 9.5279\text{MHz}$  as a result of the simulation although  $f_o$  is specified  $10\text{MHz}$ . This result shows that there is a deviation due to OTA nonideality.

An ideal OTA which is a voltage controlled current source has infinite input/output impedances and constant transconductance. Moreover, the OTA has tunable transconductance. It can work high frequencies. It is one of the most important features for fully integrated high-frequency filter design. In addition, practical OTA has finite input and output impedances. The transconductance of OTA is frequency-dependent at very high frequencies. Nonideal characteristics will decrease frequency performances of OTA-C filters.

The input conductance of the CMOS operational transconductance amplifier is very small so it may be neglected. OTA input and output capacitances rises the total capacitances or cause parasitic poles. Both can decrease the operation frequency. Parasitic capacitances can be absorbed into the grounded circuit capacitances. This approach specifies the real component values by removing the parasitic caused increases from the nominal values.

The finite OTA output resistance  $R_o$  or finite OTA DC voltage gain decrease Q and filter gain. This impact can require to be removed by using negative resistance in high-Q applications. The OTA frequency dependent transconductance causes instability at higher frequencies, limiting the operation frequency. Transconductance frequency dependence or excess phase has a Q increase effect. The impact can be compensated when connecting a resistor in series with the capacitor. This resistor is normally achieved utilizing a MOSFET in the triode or ohmic region in IC design. The equivalent resistance value may be set by voltage  $V_B$ .

#### REFERENCES

- Sun, Y., Ebooks Corporation, Books24x7, I. & Institution of Electrical Engineers 2002, *Design of High Frequency Integrated Analogue Filters*, The Institution of Engineering and Technology, Stevenage.
- Lecture Notes