

• Équilibre local au niveau du nœud

• la somme égale à zéro

• Équilibre global la somme (directionnel) des réactions avec les forces = 0

Séance 03.

Exercice 01.

1) Matrice de rigidité.

Tableau de connectivités:

Barre	Nœuds	L	α	$\cos \alpha$	$\sin \alpha$
1	1-2	L	0	1	0
2	2-3	L	$120 = \frac{2\pi}{3}$	$-\frac{1}{2}$	$\frac{\sqrt{3}}{2}$
3	1-3	L	$60 = \frac{\pi}{3}$	$\frac{1}{2}$	$\frac{\sqrt{3}}{2}$

$$[K_e] = \begin{bmatrix} c^2 & cs & -c^2 & -cs \\ cs & s^2 & -cs & -s^2 \\ -c^2 & -cs & c^2 & cs \\ -cs & -s^2 & cs & s^2 \end{bmatrix}$$

$$\frac{EA}{L}$$

$$[K^0] = \frac{EA}{4L} \begin{bmatrix} u_1 & v_1 & u_2 & v_2 \\ 4 & 0 & -4 & 0 \\ 0 & 0 & 0 & 0 \\ -4 & 0 & 4 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix}$$

$$[K^0] = \frac{EA}{4L} \begin{bmatrix} u_2 & v_2 & u_3 & v_3 \\ 1 & -\sqrt{3} & -1 & \sqrt{3} \\ -\sqrt{3} & 3 & \sqrt{3} & -3 \\ -1 & \sqrt{3} & 1 & -\sqrt{3} \\ \sqrt{3} & -3 & -\sqrt{3} & 3 \end{bmatrix}$$

$$[K^0] = \frac{EA}{4L} \begin{bmatrix} u_1 & v_1 & u_2 & v_2 \\ 1 & \sqrt{3} & -1 & -\sqrt{3} \\ \sqrt{3} & 3 & -\sqrt{3} & -3 \\ -1 & -\sqrt{3} & 1 & \sqrt{3} \\ -\sqrt{3} & -3 & \sqrt{3} & 3 \end{bmatrix}$$

$$[K] = \frac{EA}{4L} \begin{bmatrix} 5 & \sqrt{3} & -4 & 0 & -1 & \sqrt{3} \\ \sqrt{3} & 3 & 0 & 0 & -\sqrt{3} & 3 \\ -4 & 0 & 5 & -\sqrt{3} & 1 & \sqrt{3} \\ 0 & 0 & \sqrt{3} & 3 & \sqrt{3} & -3 \\ -1 & -\sqrt{3} & 1 & \sqrt{3} & 1 & 0 \\ \sqrt{3} & 3 & -\sqrt{3} & -3 & 0 & 6 \end{bmatrix}$$

2) Les déplacements nodaux

$$[K]\{U\} = \{F\}$$

$$\frac{EA}{4L} \begin{bmatrix} u_1 \\ v_1 \\ u_2 \\ v_2 \\ u_3 \\ v_3 \end{bmatrix} = \begin{bmatrix} F_{1x} = R_{1x} \\ F_{1y} = 0 \\ F_{2x} = P \\ F_{2y} = R_{2y} \\ F_{3x} = R_{3x} \\ F_{3y} = R_{3y} \end{bmatrix}$$

CAL.

$$u_1 = 0, v_1 = 0, u_3 = v_3 = 0$$

$$\frac{EA}{4L} \begin{bmatrix} 3 & 0 \\ 0 & 5 \end{bmatrix} \begin{bmatrix} v_2 \\ u_2 \end{bmatrix} = \begin{bmatrix} 0 \\ P \end{bmatrix}$$

$$\Rightarrow v_2 = 0 \text{ et } u_2 = \frac{4}{5} \frac{PL}{EA}$$

3) Les efforts normaux dans la barres:

$$N = \sigma \cdot A = E \epsilon A = E \frac{\Delta L}{L} \cdot A$$

$$N = \frac{EA}{L} [C \ S] \begin{bmatrix} u_j - u_i \\ v_j - v_i \end{bmatrix}$$

$$N_{12} = \frac{EA}{L} [1 \ 0] \begin{bmatrix} u_2 - u_1 \\ v_2 - v_1 \end{bmatrix}$$

$$N_{12} = \frac{4}{5} P$$

(2)

$$N_{2-3}^{(2)} = \frac{EA}{L} \begin{bmatrix} -\frac{1}{2} & \frac{\sqrt{3}}{2} \end{bmatrix} \begin{Bmatrix} U_3 - U_2 \\ V_3 - V_2 \end{Bmatrix}$$

$$N^{(2)} = \frac{2}{5} P$$

$$N_{3-5}^{(3)} = \frac{EA}{L} \begin{bmatrix} \frac{1}{2} & \frac{\sqrt{3}}{2} \end{bmatrix} \begin{Bmatrix} U_5 - U_3 \\ V_5 - V_3 \end{Bmatrix}$$

$$N^{(3)} = 0$$

On ne peut pas tirer cette barre à cause de $3b-h \gg \pi$ (isostatique).

Exercice 02,

1) La matrice de rigidité globale,

Barre	Nœud	L	α	$\cos \alpha$	$\sin \alpha$
1	1-2	$2L$	60°	$\frac{1}{2}$	$\frac{\sqrt{3}}{2}$
2	1-3	$\frac{2}{3}L$	30°	$\frac{\sqrt{3}}{2}$	$\frac{1}{2}$
3	1-4	L	0	1	0
4	1-5	$\frac{2}{\sqrt{3}}L$	-30°	$\frac{\sqrt{3}}{2}$	$-\frac{1}{2}$

$$[K^{(1)}] = \frac{\sqrt{3}EA}{8L} \begin{bmatrix} 3 & \sqrt{3} \\ \sqrt{3} & 1 \end{bmatrix} \begin{Bmatrix} U_1 \\ V_1 \end{Bmatrix}$$

$$[K^{(2)}] = \frac{\sqrt{3}EA}{8L} \begin{bmatrix} 3 & \sqrt{3} \\ \sqrt{3} & 1 \end{bmatrix} \begin{Bmatrix} U_3 \\ V_3 \end{Bmatrix}$$

$$[K^{(3)}] = \frac{\sqrt{3}EA}{8L} \begin{bmatrix} 3 & \sqrt{3} \\ \sqrt{3} & 1 \end{bmatrix} \begin{Bmatrix} U_5 \\ V_5 \end{Bmatrix}$$

$$[K^{(4)}] = \frac{\sqrt{3}EA}{9L} \begin{bmatrix} 3 & -\sqrt{3} \\ -\sqrt{3} & 1 \end{bmatrix} \begin{Bmatrix} U_5 \\ V_5 \end{Bmatrix}$$

$$[K] = \frac{EA}{8L} \begin{bmatrix} 9+6\sqrt{3} & \sqrt{3} & 0 & 0 & 0 \\ \sqrt{3} & 3+2\sqrt{3} & 0 & 0 & 0 \\ -1 & \sqrt{3} & 1 & 0 & 0 \\ -\sqrt{3} & -3 & 0 & 1 & 0 \\ -3\sqrt{3} & -3 & 0 & 0 & 1 \\ 0 & 0 & 0 & 0 & 0 \\ -3\sqrt{3} & 3 & 0 & 0 & 0 \\ 3 & 0 & 0 & 0 & 0 \end{bmatrix}$$

photo nacer

2) Réaction et déplacement au nœud 1,

$$U_2 = V_2 = U_3 = V_3 = U_4 = V_4 = U_5 = V_5 = 0$$

$$U_5 = -V_5 \text{ à partir de } \tan 45^\circ = \frac{V_5}{U_5} = 1$$

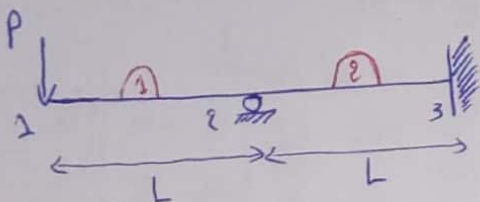
$$[K] \begin{Bmatrix} U_1 \\ V_1 \\ U_2 \\ V_2 \\ U_3 \\ V_3 \\ U_4 \\ V_4 \\ U_5 \\ V_5 \end{Bmatrix} = \begin{Bmatrix} F_{1x} \\ F_{1y} \\ F_{2x} \\ F_{2y} \\ F_{3x} \\ F_{3y} \\ F_{4x} \\ F_{4y} \\ F_{5x} \\ F_{5y} \end{Bmatrix}$$

$$\frac{EA}{8L} \begin{bmatrix} 9+6\sqrt{3} & \sqrt{3} \\ \sqrt{3} & 3+2\sqrt{3} \end{bmatrix} \begin{Bmatrix} U_1 \\ -U_1 \end{Bmatrix} = \begin{Bmatrix} R_1 \cos 45^\circ \\ R_1 \sin 45^\circ - F \end{Bmatrix}$$

$$\begin{cases} U_3 = -v_3 = \frac{4(2-\sqrt{3})FL}{3EA} \\ R_{su} = \sqrt{2}(3+\sqrt{3}) \end{cases}$$

Serie 04

Exercice 01



1) La matrice de rigidité globale :

$$[K^0] = \frac{EI}{L^3} \begin{bmatrix} 12 & 6L & -12 & 6L \\ 6L & 4L^2 & -6L & 2L^2 \\ -12 & -6L & 12 & -6L \\ 6L & 2L^2 & -6L & 4L^2 \end{bmatrix} \begin{matrix} V_1 \\ \phi_1 \\ V_2 \\ \phi_2 \end{matrix}$$

syst

$$[K^0] = \frac{EI}{L^3} \begin{bmatrix} V_2 & \phi_2 & V_3 & \phi_3 \\ V_2 & \phi_2 & V_3 & \phi_3 \\ V_2 & \phi_2 & V_3 & \phi_3 \\ V_2 & \phi_2 & V_3 & \phi_3 \end{bmatrix} \begin{matrix} V_2 \\ \phi_2 \\ V_3 \\ \phi_3 \end{matrix}$$

$$[K] = \frac{EI}{L^3} \begin{bmatrix} 12 & 6L & -12 & 6L & 0 & 0 \\ 6L & 4L^2 & -6L & 2L^2 & 0 & 0 \\ -12 & -6L & 12 & 0 & -12 & 6L \\ 6L & 2L^2 & 0 & 8L^2 & -6L & 2L^2 \\ 0 & 0 & -12 & -6L & 12 & -6L \\ 0 & 0 & 6L & 2L^2 & -6L & 4L^2 \end{bmatrix} \begin{matrix} V_1 \\ \phi_1 \\ V_2 \\ \phi_2 \\ V_3 \\ \phi_3 \end{matrix}$$

2) Les déplacements nodaux :

$$[K] \begin{Bmatrix} V_1 \\ \phi_1 \\ V_2 \\ \phi_2 \\ V_3 \\ \phi_3 \end{Bmatrix} = \begin{Bmatrix} F_{y1} \\ M_1 \\ F_{y2} \\ M_2 \\ F_{y3} \\ M_3 \end{Bmatrix}$$

C.A.L

$$V_2 = 0 ; V_3 = \phi_3 = 0$$

Syst réduit,

$$\frac{EI}{L^3} \begin{bmatrix} 12 & 6L & 6L \\ 6L & 4L^2 & 2L^2 \\ 6L & 2L^2 & 8L^2 \end{bmatrix} \begin{Bmatrix} V_1 \\ \phi_1 \\ \phi_2 \end{Bmatrix} = \begin{Bmatrix} -P \\ 0 \\ 0 \end{Bmatrix}$$

$$\Rightarrow V_1 = -\frac{7}{12} \frac{PL^3}{EI} ; \phi_1 = \frac{3}{4} \frac{PL^2}{EI}$$

$$\phi_2 = \frac{1}{4} \frac{PL^2}{EI}$$

• Pour vérifier l'équilibre, on fait la somme des réactions = 0, et la somme des moments = 0

3) Les forces nodales globales :

$$F_{y1} = -P ; M_1 = 0 ; F_{y2} = \frac{5}{2} P$$

$$M_2 = 0 ; F_{y3} = 0 ; M_3 = \frac{PL}{2}$$

4) Les forces nodales locales :

Element 1, $\begin{Bmatrix} F_{y1}^0 \\ m_1^0 \\ F_{y2}^0 \\ m_2^0 \end{Bmatrix} = [K^0] \begin{Bmatrix} V_1 \\ \phi_1 \\ V_2 \\ \phi_2 \end{Bmatrix}$

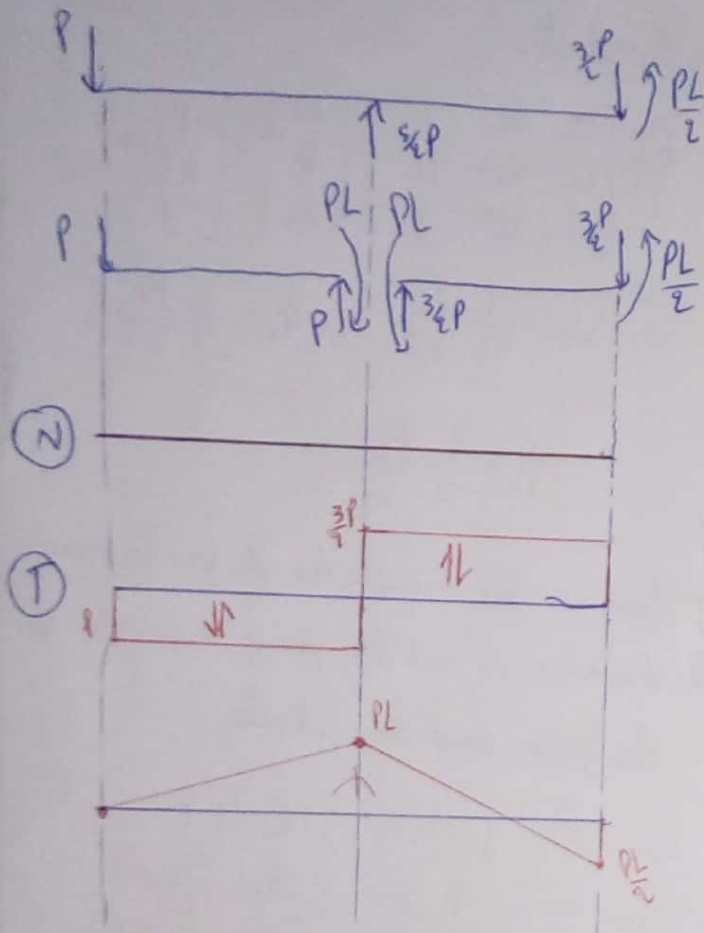
$$\begin{cases} F_{y1}^0 = -P \\ F_{y2}^0 = +P \end{cases} ; \begin{cases} m_1^0 = 0 \\ m_2^0 = -PL \end{cases}$$



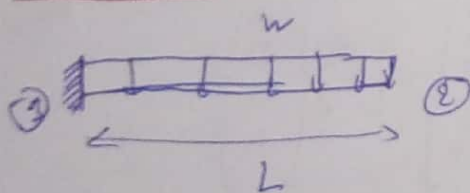
Element 2, $\begin{Bmatrix} F_{y2}^0 \\ m_2^0 \\ F_{y3}^0 \\ m_3^0 \end{Bmatrix} = [K^0] \begin{Bmatrix} V_2 \\ \phi_2 \\ V_3 \\ \phi_3 \end{Bmatrix}$

$$\begin{cases} F_{y2}^0 = \frac{3}{2} P \\ F_{y3}^0 = -\frac{3}{2} P \end{cases} ; \begin{cases} m_2^0 = -PL \\ m_3^0 = \frac{PL}{2} \end{cases}$$

5) Les diagrammes N, T, M:



Exercice 02.



1) V_2 et ϕ_2 ?

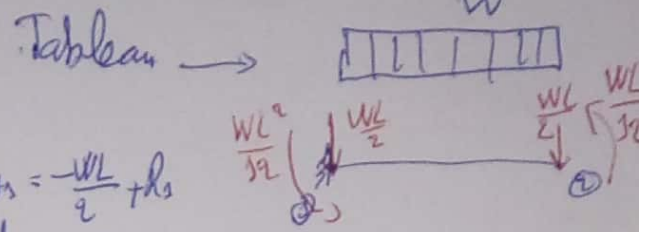
$$[K] = \frac{EI}{L^3} \begin{bmatrix} 12 & 6L & -12 & 6L \\ 6L & 4L^2 & -6L & 2L^2 \\ \text{Symet} & 12 & -6L & 4L^2 \end{bmatrix}$$

$$[K][U] = \{F\}$$

$$[K] \begin{Bmatrix} V_1 \\ \phi_1 \\ V_2 \\ \phi_2 \end{Bmatrix} = \begin{Bmatrix} F_{y1} \\ M_1 \\ F_{y2} \\ M_2 \end{Bmatrix}$$

$$G.A.L \quad V_1 = \phi_1 = 0$$

Vet forces nod ?



$$\begin{cases} F_{y2} = -\frac{wL}{2} \\ M_2 = \frac{wL^2}{12} \end{cases} \Rightarrow \frac{EI}{L^3} \begin{bmatrix} 12 & -6L \\ -6L & 4L^2 \end{bmatrix} \begin{Bmatrix} V_2 \\ \phi_2 \end{Bmatrix} = \begin{Bmatrix} -\frac{wL}{2} \\ \frac{wL^2}{12} \end{Bmatrix}$$

$$V_2 = -\frac{1}{8} \frac{wL^4}{EI}; \phi_2 = -\frac{1}{6} \frac{wL^3}{EI}$$

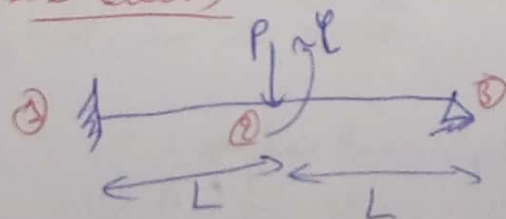
2) Réactions (forces nodales).

$$\{F\} = [K]\{U\}$$

$$\begin{cases} F_{y1} = \frac{1}{2} wL \Rightarrow R_1 = wL \\ M_1 = \frac{5}{12} wL^2 \Rightarrow M_{e1} = \frac{wL^2}{2} \end{cases}$$

$$\begin{cases} F_{y2} = -\frac{wL}{2} \\ M_2 = \frac{wL^2}{12} \end{cases}$$

Exercice 03



les mêmes questions :

\Rightarrow faire matrice de rigidité de l'exercice 01

2) CAL, $V_1 = \phi_1 = 0$, $V_3 = 0$