

- Équilibre locale au niveau de nœud
- ① la somme égale à zéro
- Équilibre globale la somme des forces des réactions avec les forces = 0.

Schéma 03.

Exercice 03.

1) Matrice de rigidité.

Tableau de connectivités.

Barre	Nœud 1	L	α	$\cos \alpha$	$\sin \alpha$
1	1-2	L	0	1	0
2	2-3	L	$180 - \frac{2\pi}{3}$	$-\frac{\sqrt{3}}{2}$	$\frac{\sqrt{3}}{2}$
3	1-3	L	$60 = \frac{\pi}{3}$	$\frac{1}{2}$	$\frac{\sqrt{3}}{2}$

$$[K_E] = \frac{EA}{L} \begin{bmatrix} C^2 & CS & -C^2 & -CS \\ CS & S^2 & -CS & -S^2 \\ -C^2 & -CS & C^2 & CS \\ -CS & -S^2 & CS & S^2 \end{bmatrix}$$

$$[K^0] = \frac{EA}{4L} \begin{bmatrix} 4 & 0 & -4 & 0 \\ 0 & 0 & 0 & 0 \\ -4 & 0 & 4 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} U_1 \\ V_1 \\ U_2 \\ V_2 \end{bmatrix}$$

$$[K^0] = \frac{EA}{4L} \begin{bmatrix} 1 & -\sqrt{3} & -1 & \sqrt{3} \\ -\sqrt{3} & 3 & \sqrt{3} & -3 \\ -1 & \sqrt{3} & 1 & -\sqrt{3} \\ \sqrt{3} & -3 & -\sqrt{3} & 3 \end{bmatrix} \begin{bmatrix} U_1 \\ V_1 \\ U_2 \\ V_2 \end{bmatrix}$$

$$[K^0] = \frac{EA}{4L} \begin{bmatrix} 1 & \sqrt{3} & -1 & -\sqrt{3} \\ \sqrt{3} & 3 & -\sqrt{3} & -3 \\ -1 & -\sqrt{3} & 1 & \sqrt{3} \\ -\sqrt{3} & -3 & \sqrt{3} & 3 \end{bmatrix} \begin{bmatrix} U_1 \\ V_1 \\ U_2 \\ V_2 \end{bmatrix}$$

$$[K] = \frac{EA}{4L} \begin{bmatrix} 5 & \sqrt{3} & 1 & 0 & -1 & \sqrt{3} \\ \sqrt{3} & 3 & 0 & 0 & -\sqrt{3} & 3 \\ 1 & 0 & 5 & -\sqrt{3} & 1 & \sqrt{3} \\ 0 & 0 & -\sqrt{3} & 3 & \sqrt{3} & -3 \\ -1 & -\sqrt{3} & 1 & \sqrt{3} & 1 & 0 \\ -\sqrt{3} & 3 & -3 & -3 & 0 & 6 \end{bmatrix} \begin{bmatrix} U_1 \\ V_1 \\ U_2 \\ V_2 \\ U_3 \\ V_3 \end{bmatrix}$$

2) Les déplacements nodaux

$$[K] \{U\} = \{F\}$$

$$\left[\begin{array}{c|ccccc} EA & U_1 & U_2 & U_3 & V_1 & V_2 \\ \hline U_1 & 0 & F_{1x} = R_{1x} \\ U_2 & 0 & F_{2y} = 0 \\ U_3 & 0 & F_{3x} = P \\ V_1 & 0 & F_{2x} = R_{2y} \\ V_2 & 0 & F_{3x} = R_{3x} \\ V_3 & 0 & F_{3y} = R_{3y} \end{array} \right]$$

CAL,

$$U_1 = 0, V_2 = 0, U_3 = V_3 = 0$$

$$\frac{EA}{4L} \begin{bmatrix} 3 & 0 \\ 0 & 5 \end{bmatrix} \begin{bmatrix} V_1 \\ U_2 \end{bmatrix} = \begin{bmatrix} 0 \\ P \end{bmatrix}$$

$$\Rightarrow V_1 = 0 \text{ et } U_2 = \frac{P}{5} \frac{PL}{EA}$$

3) Les effets normaux dans la barres:

$$N = E \cdot A = E \cdot EA = E \cdot \frac{A}{L} \cdot A$$

$$N = \frac{EA}{L} [C \ S] \begin{bmatrix} U_j - U_i \\ V_j - V_i \end{bmatrix}$$

$$N_{1-2} = \frac{EA}{L} [1 \ 0] \begin{bmatrix} U_2 - U_1 \\ V_2 - V_1 \end{bmatrix}$$

$$N = \frac{4}{5} P$$

(2)

$$N_{2-3}^{\textcircled{2}} = \frac{EA}{L} \left[-\frac{1}{2} \frac{\sqrt{3}}{2} \right] \begin{cases} U_3 - U_2 \\ V_3 - V_2 \end{cases}$$

$$[N^{\textcircled{1}} = \frac{2}{5} P]$$

$$N_{3-5}^{\textcircled{3}} = \frac{EA}{L} \left[\frac{1}{2} \frac{\sqrt{3}}{2} \right] \begin{cases} U_3 - U_5 \\ V_3 - V_5 \end{cases}$$

$$[N^{\textcircled{2}} = 0]$$

On ne peut pas tirer cette barre à cause de
 $3b - h \geqslant$ (isostatique).

$$[K] \frac{EA}{8L}$$

$$[K^{\textcircled{1}}] = \frac{\sqrt{3}EA}{9L} \begin{bmatrix} u_1 & v_1 & u_3 & v_3 & u_5 & v_5 \\ 3 & -\sqrt{3} & \cdot & \cdot & \cdot & \cdot \\ \sqrt{3} & 3 & -1 & \cdot & \cdot & \cdot \\ \cdot & \cdot & \cdot & \cdot & \cdot & \cdot \\ \cdot & \cdot & \cdot & \cdot & \cdot & \cdot \\ \cdot & \cdot & \cdot & \cdot & \cdot & \cdot \\ u_1 & v_1 & u_3 & v_3 & u_5 & v_5 \end{bmatrix}$$

$$\begin{bmatrix} 1 & \sqrt{3} & 3 & -1 & -\sqrt{3} & -3 \\ \sqrt{3} & 3 & 1 & -1 & -3 & -3 \\ -1 & -3 & -1 & 1 & 1 & 1 \\ -\sqrt{3} & -3 & -3 & -1 & 1 & 1 \\ 3 & 1 & 1 & 1 & 1 & 1 \\ -3 & -1 & -1 & -1 & -1 & -1 \\ 0 & 0 & 0 & 0 & 0 & 0 \\ -3\sqrt{3} & -3 & -3 & -3 & -3 & -3 \\ 3 & -3 & -3 & -3 & -3 & -3 \end{bmatrix}$$

photo nacelle

Exercice 02.

I) La matrice de rigidité globale,

Barre	Nœud	L	θ	$\cos \theta$	$\sin \theta$
1	1-2	$2L$	60°	$\frac{1}{2}$	$\frac{\sqrt{3}}{2}$
2	1-3	$\frac{2}{3}L$	30°	$\frac{\sqrt{3}}{2}$	$\frac{1}{2}$
3	1-4	L	0	1	0
4	1-5	$\frac{2}{3}L$	-30°	$\frac{\sqrt{3}}{2}$	$-\frac{1}{2}$

$$[K^{\textcircled{1}}] = \frac{\sqrt{3}EA}{8L} \begin{bmatrix} u_1 & v_1 & u_2 & v_2 \\ u_1 & v_1 & u_2 & v_2 \\ - & - & + & + \\ - & - & + & + \end{bmatrix} \begin{bmatrix} \frac{1}{2} & 1 \\ 1 & \frac{1}{2} \end{bmatrix}$$

$$[K^{\textcircled{2}}] = \frac{\sqrt{3}EA}{8L} \begin{bmatrix} 3 & \sqrt{3} \\ \sqrt{3} & 3 \end{bmatrix} \begin{bmatrix} u_1 & v_1 \\ u_1 & v_1 \\ u_3 & v_3 \\ u_3 & v_3 \end{bmatrix}$$

$$[K^{\textcircled{3}}] = \frac{\sqrt{3}EA}{8L} \begin{bmatrix} 3 & 1 & -1 & -1 \\ -1 & 3 & 1 & 1 \\ -1 & 1 & 3 & -1 \\ 1 & -1 & -1 & 3 \end{bmatrix}$$

ii) Réaction et déplacement au nœud 1.

$$U_2 = V_2 = U_3 = V_3 = U_4 = V_4 = U_5 = V_5 = 0$$

$$[U_1 = -V_1] \text{ à partir de } \tan 45^\circ = \frac{V_1}{U_1} = 1$$

$$[K] = \begin{bmatrix} u_1 \\ v_1 \\ u_2 \\ v_2 \\ u_3 \\ v_3 \\ u_4 \\ v_4 \\ u_5 \\ v_5 \end{bmatrix} = \begin{bmatrix} F_{1x} \\ F_{1y} \\ F_{2x} \\ F_{2y} \\ F_{3x} \\ F_{3y} \\ F_{4x} \\ F_{4y} \\ F_{5x} \\ F_{5y} \end{bmatrix}$$

$F_{1x} = R_{1x} = R_1 \cos 45^\circ$
 $F_{1y} = R_{1y} = R_1 \sin 45^\circ$
 $R_{1x} = R_1 \cos 45^\circ - F$
 $R_{1y} = R_1 \sin 45^\circ$

$$\frac{EA}{8L} \begin{bmatrix} 3+6\sqrt{3} & \sqrt{3} \\ \sqrt{3} & 3+2\sqrt{3} \end{bmatrix} \begin{bmatrix} U_1 \\ -U_1 \end{bmatrix} = \begin{bmatrix} R_1 \cos 45^\circ \\ R_1 \sin 45^\circ - F \end{bmatrix}$$

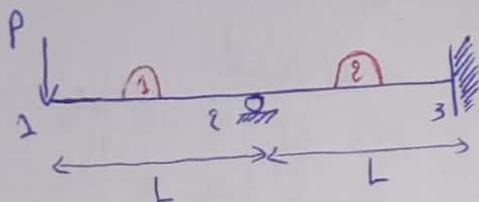
$$\left\{ \begin{array}{l} U_3 = -V_1 = \frac{u(2-\sqrt{3})FL}{3EA} \\ R_{3n} = \sqrt{2}(3+\sqrt{3}) \end{array} \right.$$

$$\rightarrow \frac{EI}{L^3} \times \frac{EI}{L}$$

MEF

Série 09

Exercice 01



1) La matrice de rigidité globale :

$$[K^G] = \frac{EI}{L^3} \begin{bmatrix} V_1 & \Phi_1 & V_2 & \Phi_2 \\ V_2 & 6L & -12 & 6L \\ \Phi_1 & -12 & 4L^2 & -6L & 2L^2 \\ V_3 & 6L & -6L & 2L^2 & 8L^2 \\ \Phi_2 & 6L & 2L^2 & 8L^2 & 12 \end{bmatrix} \begin{bmatrix} V_1 \\ \Phi_1 \\ V_2 \\ \Phi_2 \end{bmatrix} = \begin{bmatrix} -P \\ 0 \\ 0 \\ 0 \end{bmatrix}$$

synt

$$[K^D] = \frac{EI}{L^3} \begin{bmatrix} V_1 & \Phi_1 & V_2 & \Phi_2 \\ V_2 & - & - & - \\ \Phi_1 & - & - & - \\ V_3 & - & - & - \\ \Phi_2 & - & - & - \end{bmatrix} \begin{bmatrix} V_1 \\ \Phi_1 \\ V_2 \\ \Phi_2 \\ V_3 \\ \Phi_3 \end{bmatrix}$$

$$[K] = \frac{EI}{L^3} \begin{bmatrix} V_1 & \Phi_1 & V_2 & \Phi_2 & V_3 & \Phi_3 \\ V_2 & 6L & -12 & 6L & 0 & 0 \\ \Phi_1 & -12 & 4L^2 & -6L & 2L^2 & 0 \\ V_3 & 6L & -6L & 2L^2 & 0 & -12 \\ \Phi_2 & 6L & 2L^2 & 0 & 8L^2 & -6L & 2L^2 \\ 0 & 0 & -12 & -6L & 12 & -6L & 0 \\ 0 & 0 & 6L & 2L^2 & -6L & 4L^2 & 0 \end{bmatrix} \begin{bmatrix} V_1 \\ \Phi_1 \\ V_2 \\ \Phi_2 \\ V_3 \\ \Phi_3 \end{bmatrix}$$

2) Les déplacements nodaux :

$$[K] \begin{bmatrix} V_1 \\ \Phi_1 \\ V_2 \\ \Phi_2 \\ V_3 \\ \Phi_3 \end{bmatrix} = \begin{bmatrix} F_{y1} \\ M_1 \\ F_{y2} \\ M_2 \\ F_{y3} \\ M_3 \end{bmatrix}$$

c. a. l.

$$V_2 = 0 ; V_3 = \Phi_3 = 0$$

Syst réduit,

$$\frac{EI}{L^3} \begin{bmatrix} 12 & 6L & 6L \\ 6L & 4L^2 & 2L^2 \\ 6L & 2L^2 & 8L^2 \end{bmatrix} \begin{bmatrix} V_1 \\ \Phi_1 \\ \Phi_2 \end{bmatrix} = \begin{bmatrix} -P \\ 0 \\ 0 \end{bmatrix}$$

$$\Rightarrow V_1 = -\frac{7}{32} \frac{PL^3}{EI} ; \quad \Phi_1 = \frac{3}{4} \frac{PL^2}{EI}$$

$$\Phi_2 = \frac{1}{4} \frac{PL^2}{EI}$$

- Pour vérifier l'équilibre, on fait la somme des réactions = 0, et la somme des moments = 0

3) Des forces nodales globales :

$$F_{y1} = -P ; \quad M_1 = 0 ; \quad F_{y2} = \frac{5}{2}P$$

$$M_2 = 0 ; \quad F_{y3} = 0 ; \quad M_3 = \frac{PL}{2}$$

4) Des forces nodales locales :

$$\text{Elément 1. } \begin{bmatrix} F_{y1}^0 \\ M_1^0 \\ F_{y2}^0 \\ M_2^0 \end{bmatrix} = [K^G] \begin{bmatrix} V_1 \\ \Phi_1 \\ V_2 \\ \Phi_2 \end{bmatrix}$$

$$F_{y1}^0 = P ; \quad M_1^0 = 0$$

$$F_{y2}^0 = +P ; \quad M_2^0 = -PL$$

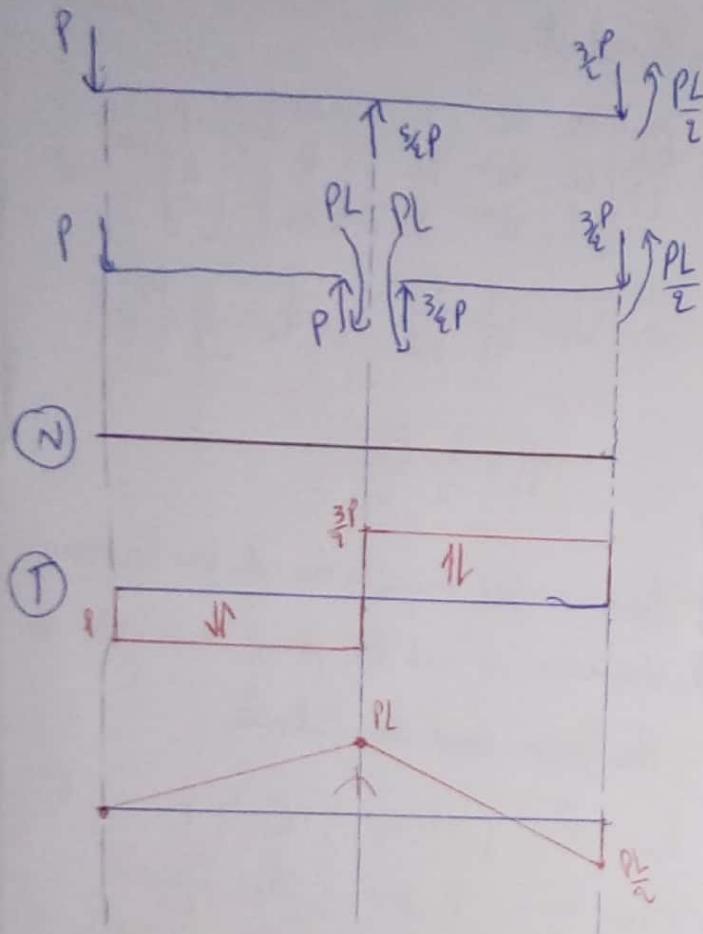


$$\text{Elément 2. } \begin{bmatrix} F_{y2}^0 \\ M_2^0 \\ F_{y3}^0 \\ M_3^0 \end{bmatrix} = [K^G] \begin{bmatrix} V_2 \\ \Phi_2 \\ V_3 \\ \Phi_3 \end{bmatrix}$$

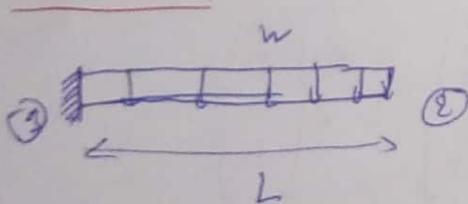
$$F_{y2}^0 = \frac{3}{2}P ; \quad M_2^0 = -PL$$

$$F_{y3}^0 = -\frac{3}{2}P ; \quad M_3^0 = \frac{PL}{2}$$

5) Les diagrammes N, T, M:



Exercice 02:



1) v_2 et ϕ_2 ?

$$[K] = \frac{EI}{L^3} \begin{bmatrix} 32 & 6L & -32 & 6L \\ 6L & 4L^2 & -6L & 2L^2 \\ -32 & -6L & 32 & -6L \\ 6L & 2L^2 & -6L & 4L^2 \end{bmatrix}$$

Symt

$$[K][U] = \{F\}$$

$$[K] \begin{pmatrix} v_2 \\ \phi_2 \\ v_2 \\ \phi_2 \end{pmatrix} = \begin{pmatrix} F_{y1} \\ M_1 \\ F_{y2} \\ M_2 \end{pmatrix}$$

$$\frac{G \cdot A \cdot L}{v_2 = \phi_2 = 0}$$

Quel forces nodal?

Tableau \rightarrow

$$\begin{cases} F_{y1} = -\frac{WL}{2} + R_1 \\ M_1 = -\frac{WL^2}{24} + M_{ext} \end{cases}$$

$$\begin{cases} F_{y2} = -\frac{WL}{2} \\ M_2 = \frac{WL^2}{24} \end{cases} \Rightarrow \begin{array}{c} \text{Syst Reduct:} \\ \frac{EI}{L^3} \begin{bmatrix} 32 & -6L & v_2 \\ -6L & 4L^2 & \phi_2 \end{bmatrix} \begin{bmatrix} -\frac{WL}{2} \\ \frac{WL^2}{24} \end{bmatrix} \end{array}$$

$$v_2 = -\frac{1}{8} \frac{WL^4}{EI}; \phi_2 = -\frac{1}{6} \frac{WL^3}{EI}$$

2) Réactions (forces natales).

$$\{F\} = [K]\{U\}$$

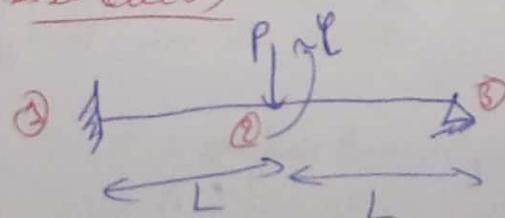
$$\{F\} = \left\{ \begin{array}{l} F_{y1} = \frac{1}{2} WL \\ M_1 = \frac{5}{32} WL^2 \end{array} \right\} \Rightarrow R_1 = WL$$

$$\{F\} = \left\{ \begin{array}{l} F_{y2} = -\frac{WL}{2} \\ M_2 = \frac{WL^2}{24} \end{array} \right\} \Rightarrow M_{ext} = \frac{WL^2}{2}$$

$$\{F\} = \left\{ \begin{array}{l} F_{y1} = -\frac{WL}{2} \\ M_1 = \frac{WL^2}{24} \end{array} \right\}$$

$$\{F\} = \left\{ \begin{array}{l} F_{y2} = -\frac{WL}{2} \\ M_2 = \frac{WL^2}{24} \end{array} \right\}$$

Exercice 03



Les mêmes questions :

\Rightarrow même matrice de rigidité de l'exo 01

2) CAL , $v_1 = \phi_1 = 0, v_2 = 0$