

Polarimetry I

Bob Sault 26 September 2017



Talk Outline

- Polarimetry I
 - What and How?
 - What is polarized light and ways to quantify it
 - Hardware to measure it
 - Calibration
 - Some advanced topics

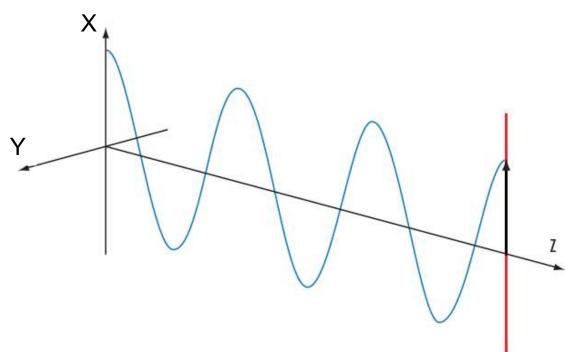
- Polarimetry II George
 - Why?
 - What astrophysics do we learn



Polarized waves

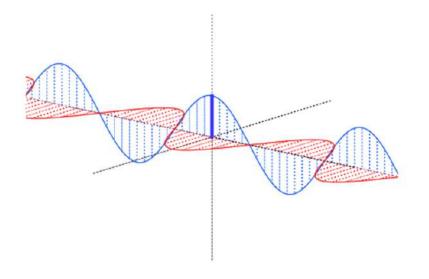
$$\mathbf{E}_{x}(z,t) = \hat{\imath}E_{0x}\cos(kz - \omega t)$$

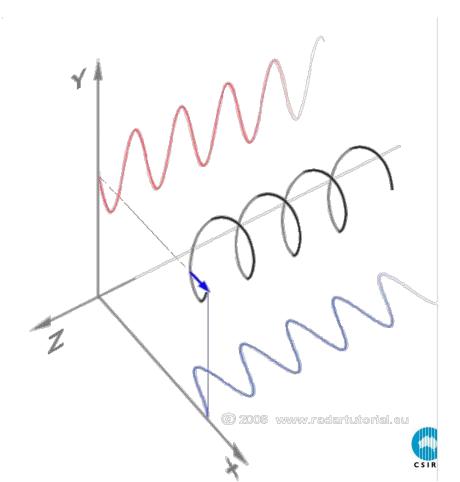
$$\mathbf{E}_{y}(z,t) = \hat{\jmath}E_{0y}\cos(kz - \omega t + \epsilon)$$





Linear and circular





Partially polarized emission

- Three parameters are needed to describe a fully polarized wave (e.g. E_{0x} , E_{0y} , ϵ)
- Natural emission mostly randomly polarized or "unpolarised"
- Four parameters are needed to describe partially polarized emission



Parameterizing partially polarized emission

- Power quantities which are additive
- Compact and "neat"
- Independent of measurement hardware
- Readily measureable
- Stokes parameters





Stokes parameters

- I total power the sum of the power in any two orthogonal components ...
- Q difference in power between the vertical and horizontal components:

$$E_0^2 - E_{90}^2$$

• U – difference between ±45° components.

$$E_{45}^2 - E_{-45}^2$$

 V – difference between circularly polarized components.

$$E_{RCP}^2 - E_{LCP}^2$$



Stokes parameter properties

- Q,U,V are the differences of comparable powers. Just as likely to be negative as positive!
- Polarized fraction

$$p = \frac{\sqrt{Q^2 + U^2 + V^2}}{I}$$

Angle of linear polarization

$$\theta = \frac{1}{2} \operatorname{atan2}(U, Q)$$



Hardware to measure it

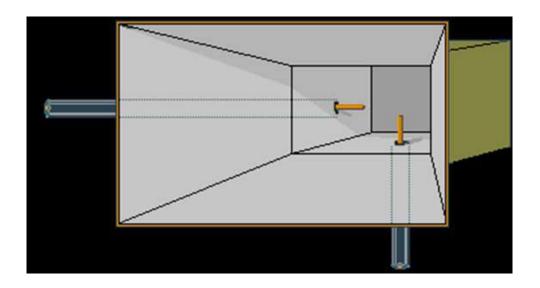
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Feeds

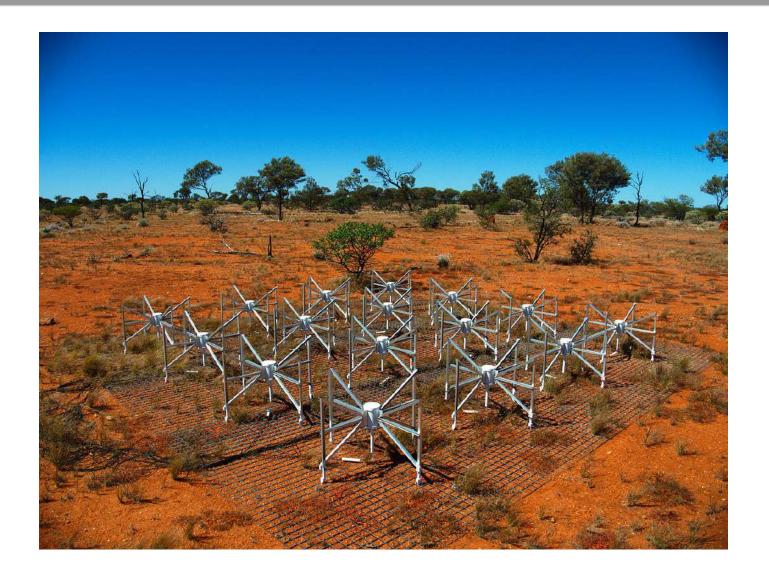
- Linearly-polarized feeds. Dipoles.
 - "Vertical" and "horizontal" "X" and "Y" (note X is vertical, Y is horizontal)





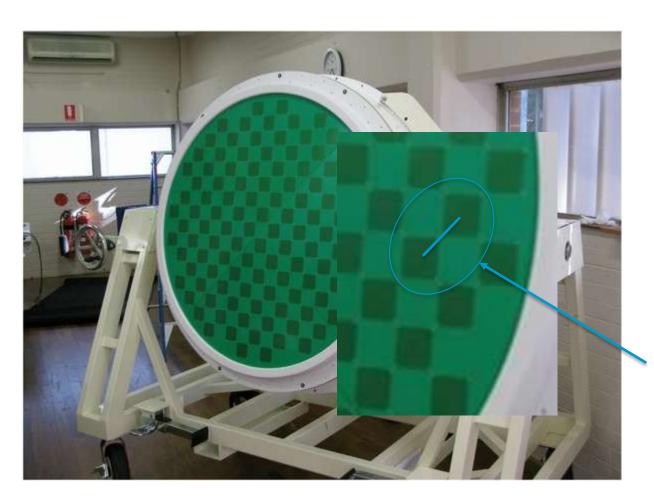


MWA dipoles





ASKAP checkerboard



"Dipole"



Circularly-polarized feeds

- Helical feeds.
 - "Right handed" and "left handed"



- Quadrature hybrids.
 - Circularly-polarized feeds synthesized by linears with 90 degree phase shifter (quadrature hybrid)



Measuring Stokes parameters in the radio

Stokes parameters

$$I = E_0^2 + E_{90}^2$$

$$Q = E_0^2 - E_{90}^2$$

$$U = E_{45}^2 - E_{-45}^2$$

$$V = E_{RCP}^2 - E_{LCP}^2$$

Stokes parameters

$$\begin{array}{rcl} I &=& XX+YY\\ Q &=& XX-YY\\ U &=& XY+YX\\ V &=& i(YX-XY)\\ \end{array}$$
 where $X\!\!=\!E_0$, $Y\!\!=\!E_{90}$



Factors of 2!

Is Stokes I

$$XX + YY$$

or

$$(XX + YY)/2$$



Making Stokes images

- Each antenna measures two orthogonal polarizations - X and Y.
- For every baseline, form all four possible correlations XX, YY, XY, YX.
- Calibration etc
- Appropriately combine the four correlations to get four Stokes "visibilities".
- Perform standard imaging with these Stokes visibilities to make Stokes images.



Rotation of the sky





Alt-az mount





Equatorial mounts

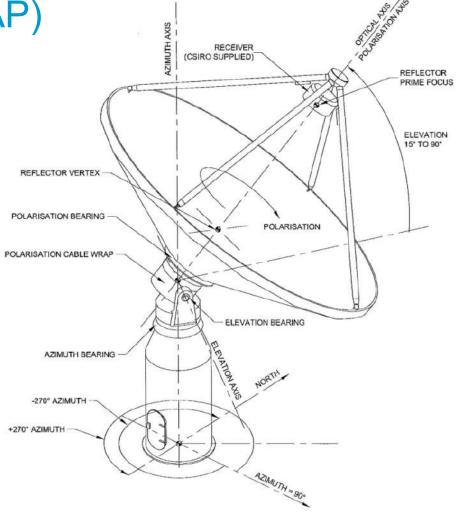




Counteract the rotation

"Parallactifiers"

"Sky mount" (ASKAP)





And others ...





Calibration

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Calibration

- Calibration accounts for a number of effects
 - Rotation of the sky
 - Polarization leakage
 - XY phase
 - Ionospheric Faraday rotation
 - Off-axis polarization response (Polarimetry II)



Just say no!



Polarization leakage

• For real-world feeds, the feed will respond both to the desired polarization, and to a small degree the orthogonal polarization:

$$E_X' = E_X + d_x E_Y$$
$$E_Y' = E_Y + d_y E_X$$

The leakage ("d term") is typically ~10⁻². It is caused by alignment error, feed ellipticity, etc. Generic linear model (will suit any system with a linear response).



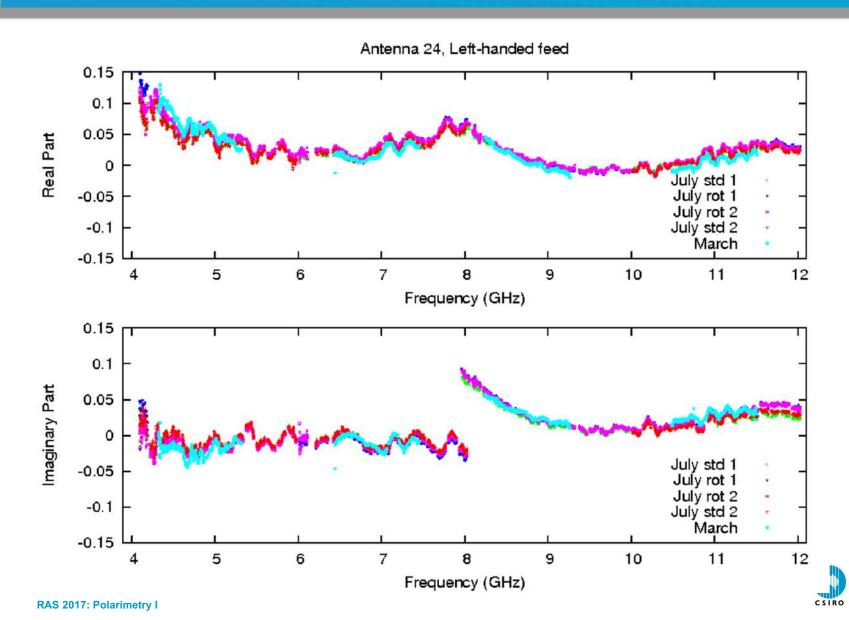
Polarization leakage (continued)

• Leakages a function of antenna, position in beam, frequency (?) and possibly time (??).

• ASKAP field centre leakage very low and independent of frequency. ASKAP leakage as a function of position in beam more an issue (Widefield polarimetry in next lecture).



VLA leakages



Polarization leakage (continued)

- Determine leakage terms.
 - "To good order", simple regular observations of "typical" calibrator is all that is needed to allow a solution for leakages to be made.
 - Q and U Stokes parameters of calibrator either
 - Must be known and accounted for, or
 - Decoupled from polarization leakage using rotation of the sky (resulting from antenna mount or ionosphere).
 - V should be know (usually safe to assume 0)



XY phase

- Instrumental phase difference between X and Y polarization channels can be poorly know.
- Correcting for XY phase is often the most important step for polarimetry.
- Calibration approaches
 - Injected calibration signal (continuous for the ATCA, under development for ASKAP, not available for VLA).
 - Observation of source with strong polarization (required for the VLA).
 - More exotic schemes.



Ionospheric Faraday rotation

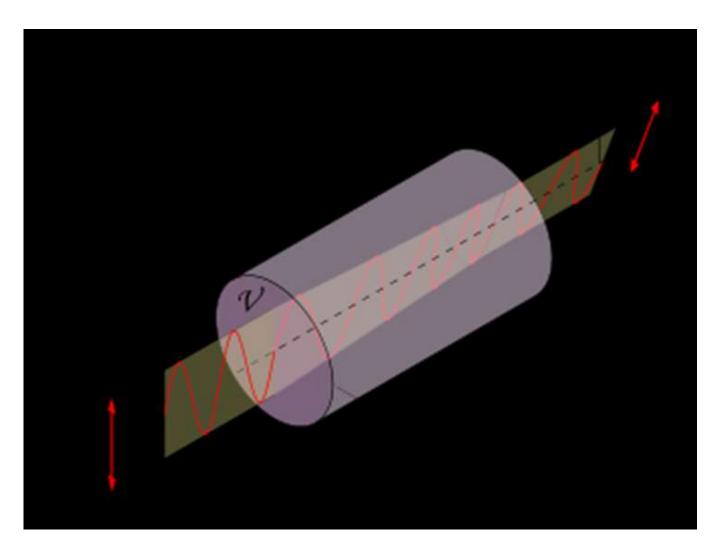
- The ionosphere is a significantly variable plasma layer 100-300 km in the upper atmosphere threaded by Earth's magnetic field.
- Propagation through this medium causes
 Faraday rotation – the rotation of the direction
 of linear polarization. For rotation measure
 RM, the angle of rotation is

$$\varphi = RM \lambda^2$$

Ionospheric RM typically 1-10 rad/m²

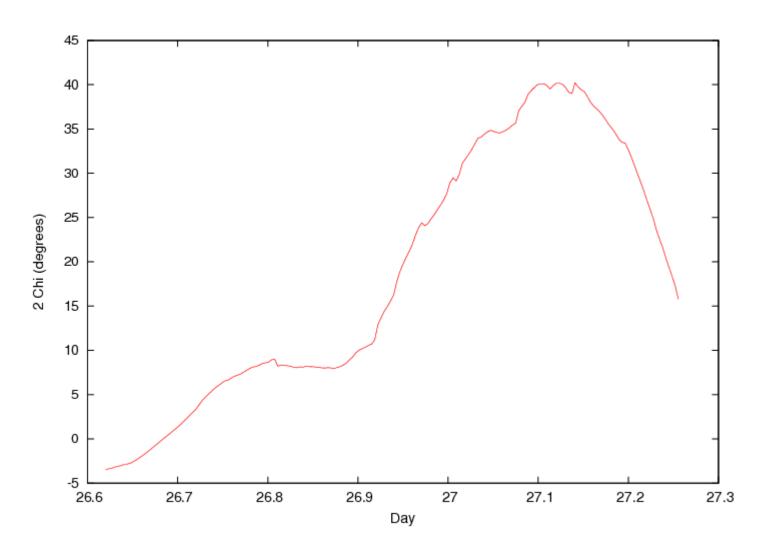


Faraday rotation





ASKAP example at 700 MHz





Ionospheric Faraday rotation (continued)

 Ionospheric Faraday rotation generally only an issue below 2 GHz. Probably needs to be accounted for below 1 GHz.

Calibration:

- GPS stations provide global continuous monitoring of the ionosphere. These data plus models give Faraday rotation accuracy of a ~0.2 rad/m².
- Frequent monitoring of "position angle" calibrator also possible.



Jones matrices

 The response of an optical component to polarized light can described by a simple linear operation on the voltages:

$$E_X' = a_{11} E_X + a_{12} E_Y$$
 Leakage
$$E_Y' = a_{21} E_X + a_{22} E_Y \begin{bmatrix} E_X' = E_X + d_x E_Y \\ E_Y' = E_Y + d_y E_X \end{bmatrix}$$



Jones matrices

 The response of an optical component to polarized light can described by a simple linear operation on the voltages:

$$E_X' = a_{11}E_X + a_{12}E_Y$$

$$E_Y' = a_{21}E_X + a_{22}E_Y$$

or more simply, in matrix form – the "Jones" matrix

$$e' = Je$$

for a complex system, the overall Jones matrix will be the product of several matrices:

$$e' = J_1 J_2 J_3 ... J_n e$$



Jones matrices continued ...

 Jones matrices are "antenna based" and complex valued

 Antenna gain: (includes XY phase)

$$G = \left(\begin{array}{cc} g_x & 0\\ 0 & g_y \end{array}\right)$$

•Polarization leakage: $D = \left(\begin{array}{cc} 1 & d_x \\ d_y & 1 \end{array} \right)$

$$R = \begin{pmatrix} \cos \theta & \sin \theta \\ -\sin \theta & \cos \theta \end{pmatrix}$$

Polarimetric interferometry

The overall Jones matrix for an antenna will be

$$J = GDR_{\rm s}R_{\rm i}$$

then for baseline *k-I*, the response will be

$$V'_{kl} = J_k \otimes J_l^* V_{kl}$$

- J_k is the antenna Jones matrix.
- V_{kl} is a vector of 4 polarization correlations (e.g. XX, XY, YX and YY correlations).
- \otimes represents Kronecker matrix product



Depolarization

Depolarization = loss of polarimetric signal.

 Caused by the system polarimetric response not being constant (i.e. varying spatially, with time, across bandwidth etc etc) smearing out the polarimetric signal.

• <u>Calibrated</u> interferometer arrays generally have very low depolarization (in polarimetric jargon, a system with no depolarization is called "pure").



Mueller matrices

A Muller matrix is a 4x4 matrix, *M*, that relates output Stokes parameters of a system to the inputs:

$$\begin{pmatrix} I' \\ Q' \\ U' \\ V' \end{pmatrix} = \begin{pmatrix} a_{11} & a_{12} & a_{13} & a_{14} \\ a_{21} & a_{22} & a_{23} & a_{24} \\ a_{31} & a_{32} & a_{33} & a_{34} \\ a_{41} & a_{42} & a_{43} & a_{44} \end{pmatrix} \begin{pmatrix} I \\ Q \\ U \\ V \end{pmatrix}$$

For a system with no depolarization, the Mueller matrix has an associated Jones matrix

$$M = S^{-1}(J \otimes J^*)S$$



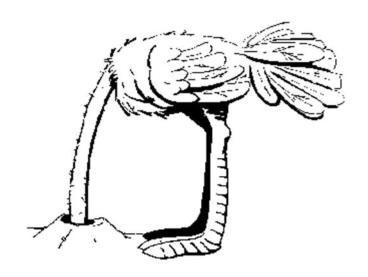
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Ostrich calibration approach





Advanced calibration

 Polarimetric calibration converts an interferometer into a system with no depolarization. There are 7 parameters that are potentially ill-determined.

$$I \iff I$$
 (flux calibration)
 $I \iff Q$
 $I \iff U$
 $I \iff V$
 $Q \iff U$
 $Q \iff V$
 $U \iff V$



Advanced calibration ...

- "Standard" calibration removes leakage of Stokes I into Q,U,V. It does not calibrate out leakage of Q,U,V into each other. These leakages are second-order and often not important.
- Formally three independent "observations" of known calibrators are needed to fully solve for all corrupting/leakage terms.
 Astrophysical requirements and "rotation" can reduce this number.



Off-axis polarimetry (more next lecture)

- Polarimetric response (and Jones matrices) generally a function of position within the primary beam. A good body of theory exists for dealing with position-variant polarimetric response.
- Fractional off-axis polarization (e.g. a the half power points or beyond) can be large if uncorrected. Treat with caution!



Linearly- vs circularly-polarized feeds

 Although this lecture has been framed for linearly-polarized feeds, similar situation applies for circularly-polarized feed systems (different details but same concepts).

• Some debate on whether linearly- (e.g. ATCA, ASKAP, WSRT, KAT) or circularly-polarized feeds (e.g. VLA) are "best".



3D movie cinemas





Linears vs circulars

- Fundamentally both are equivalent in some sense. Both work in practice.
- The sky and engineering reality breaks the symmetry. "General" polarization calibration easier with circulars.
- Engineering tends to make linearly-polarized feeds more attractive. Precision polarization calibration easier with linears.



Sit on the fence





Thank you

