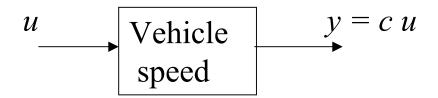
Two basic concepts of feedback systems: Performance, Robustness

An extremely simplified model

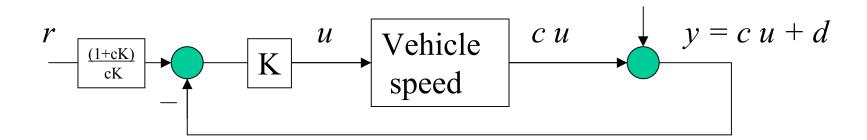


(All models are wrong, some are useful DR)

- Objective y = r (e.g., c=100, r=50)
- Easy choice: u = r/c

Performance...

- Add a disturbance: y = cu + d (say d = -20)
- Then y = c(r/c) + d = 50-20 = 30:(
- Measure *y* and close the loop:



- $u = K(r_f y)$, $r_f = (1+cK)/cK$ (adjusted ref.)
- Then $y = cK(r_f y) + d = \dots = r + d/(1 + cK)$

Performance...

• Conclusion: As the controller gain (K) increases, the effect of the disturbance is reduced.

- Rule#1: High gain => Performance
- Similar conclusion for variations in c (a bit more messy)
- So, take K = 1000000...
- Too good, too easy? ...

Robustness...

• Suppose there is an unmodeled small delay between application of input and output:

$$y(t) = cu(t-\tau)$$

Without the disturbance,

$$y(t) = cK[r_f(t-\tau) - y(t-\tau)]$$

• Look at the sample times τ , 2τ , 3τ , ...

$$y[n\tau] = -cK y[(n-1)\tau] + cKr_f$$

• If cK > 1, $|y(n\tau)|$ grows exponentially! :(

Robustness...

• For a continuous time version of this argument, use a Pade approximation of the delay:

$$e^{-s\tau} \approx \frac{1 - s\frac{\tau_{2}}{2}}{1 + s\frac{\tau_{2}}{2}}$$

$$y = c\frac{1 - s\frac{\tau_{2}}{2}}{1 + s\frac{\tau_{2}}{2}}K(y - r_{f}) \Rightarrow y = \frac{cK(1 - s\frac{\tau_{2}}{2})}{(1 - cK)\frac{\tau_{2}}{2}s + (1 + cK)}r_{f}$$

$$poles: \frac{1 + cK}{1 - cK}\frac{2}{\tau}$$

• Hence, the closed loop is unstable for cK > 1.

Robustness...

- Conclusion: High controller gains can cause instability due to unmodeled dynamics.
- Alternative interpretation: Our controller did not respect the limitations of the model (Models have limitations, stupidity does not!^{AAR, MA})
- Rule#2: Respect the uncertain^{GS}
- NOTE: For unstable systems, low controller gains can lead to instability as well, but this is predicted by the model.

- A nominal model by itself is not very useful. We also need an uncertainty estimate.
- Multiplicative uncertainty (relative error)

$$G(s) = [I + \Delta_m(s)]G_0(s)$$

$$|\Delta_m(j\omega)| = \frac{|G(j\omega) - G_0(j\omega)|}{|G_0(j\omega)|} \approx \frac{|y_0(j\omega) - y(j\omega)|}{|y_0(j\omega)|}$$

- Estimate the bound analytically or from data.
- Small Gain Theorem: the controller should satisfy

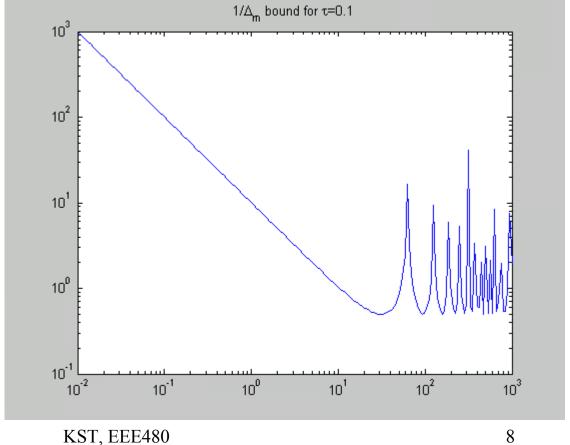
$$|T(j\omega)| < 1/|\Delta_m(j\omega)|$$

where $T = G_0C/(1+G_0C)$ (complementary sensitivity)

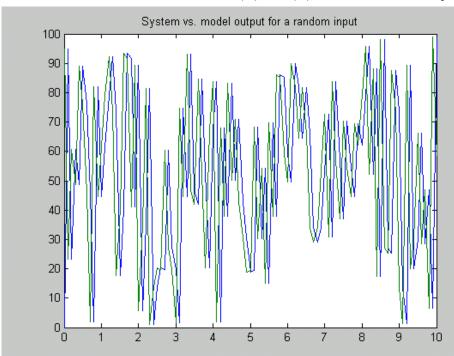
• In our case, $G_0=c$, C=K, so T=cK/(1+cK)T is a constant, so we must have T< 1/2 for all ω .

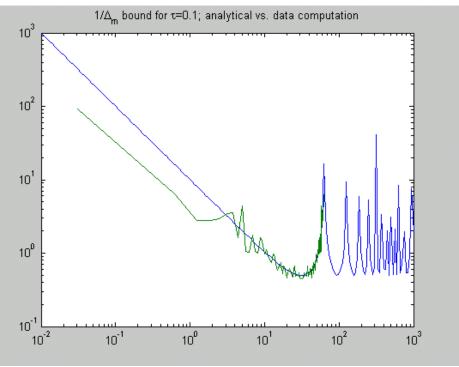
$$=> cK<1$$

For the plot, >> w=logspace(-2,3,200); $>> d = \exp(j*w*.1);$ >> loglog(w, 1./abs(1-d))



- Estimating the uncertainty from data:
 - Collect data with a random input
 - >> dd=abs(fft(y-y0)./fft(y0));
 - >> ww=([1:pts]'-1)*2*pi/pts/dt;ww(1)=ww(2)/20;
 - %fft frequencies for pts number of points, sampled every dt.
 - %w(1)=w(2)/20, an arbitrary choice.





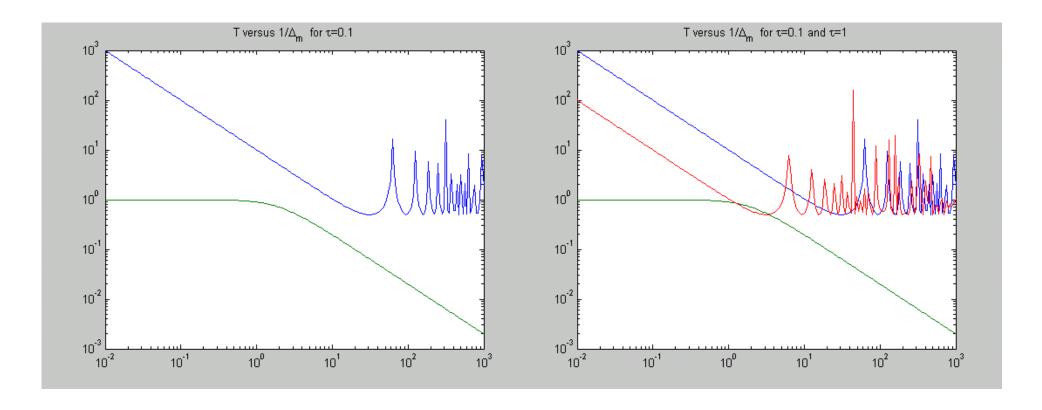
- Dynamic controllers: Getting better performance at some frequencies.
- The uncertainty constraint is not active at low frequencies => we should be able to increase the gain there.
- PI control: $u = (K_p s + K_i)/s[e]$, (e = error = r y)
 - For simplicity, consider the I-part only; for our easy system we do not need the P- nor the D-part. We loose some performance at high frequencies but our typical d is a low frequency signal.
 - Controller gain = $|C(j\omega)| = K_i/\omega$; large at low frequencies. Also interpreted as an internal model of constant disturbances.

• Find the complementary sensitivity (nominal)

$$T(s) = \frac{\frac{cK_i}{s}}{1 + \frac{cK_i}{s}} = \frac{cK_i}{s + cK_i}$$

- Should have $|T(j\omega)| < 1/|\Delta_m(j\omega)|$
- Roughly, closed-loop bandwidth = $cK_i < \omega_{max}$ (uncertainty crossover frequency), which is ~ 10.
- Leave some margin too, so $K_i = 2/c$
- Analysis: (takes a while)
 Stable closed loop, y converges to r for any constant d, small errors for slowly varying d! :)

- The better performance has a price: This controller cannot tolerate arbitrary delays...
 - Left figure: closed-loop T vs. uncertainty bound;
 - Right figure: what happens if the delay increases...



Conclusions

- Concepts demonstrated by this example:
 - Performance-robustness tradeoff
 - Improvement with dynamic controllers
 - Our expectations from the model
 - All models are wrong, some are useful^{DR}
 - Model uncertainty restricts our expectations from the controller
 - Controllers have limitations, stupidity does not!^{AAR, MA}

Conclusions

- Concepts carefully hidden in this example:
 - High order systems can impose further constraints on what is achievable
 - Additional constraints can come from non-invertible elements (RHP poles-zeros)
 - More of the same from nonlinear elements
 - Nominal controller design can get quite complicated for high order systems
 - and so does the analysis (though the principles stay largely the same)