# **Loop-Shaping Controller Design from Input-Output Data**

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- Control-Oriented ID: Uncertainty description compatible with the controller design method. (Loop-Shaping for available insight & computations.)
- Linear-model estimation: Coprime factor uncertainty (forward and feedback)
- Controller Design: Loop-Shaping (S&T)
- Final Result: Quick design & implementation, Performance, Reliability

## The Application: Control of Paper Machines

#### • Inputs:

- Stock Flow
- Dryer temperatures (set-points to the local PID's)
- Machine speed set-point

#### • Outputs:

- Dry weight
- Moistures
- Machine speed

#### Disturbances:

- Operators change set-points in other loops to maintain overall product quality.
- Feed consistency, especially after paper breaks (re-circulation).
- Other nonlinear effects

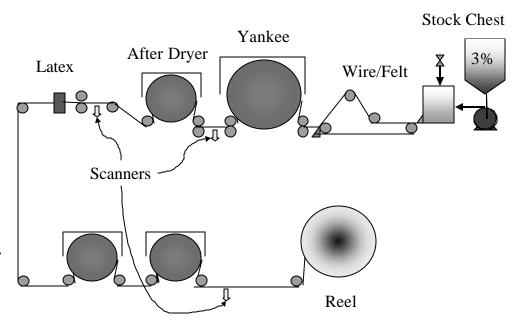


Figure 1. Paper Machine Schematic

## **Generalities: System ID**

- System Identification: Nominal Model and Uncertainty Description
- Control-Oriented ID: Uncertainty description compatible with the controller design method.
- Our choice: Loop-Shaping (available insight, computations) based on sensitivity and complementary sensitivity targets.
- Nominal Model: MISO equation error, yielding a linear estimation model

$$y = N(\theta)[u] + D(\theta)[y] + e = w^T\theta$$

- Estimated parameters include initial conditions; this is important to handle inputoutput sets that begin on a transient.
- Left factorization and a coprime factor description of uncertainty:
  - Handling of low frequency perturbations and changes in unstable modes.
  - Indicates required low-frequency sensitivity roll-off (disturbance attenuation)
  - "Easy" computation of target loop properties

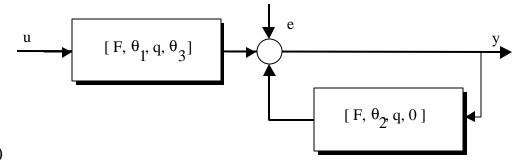


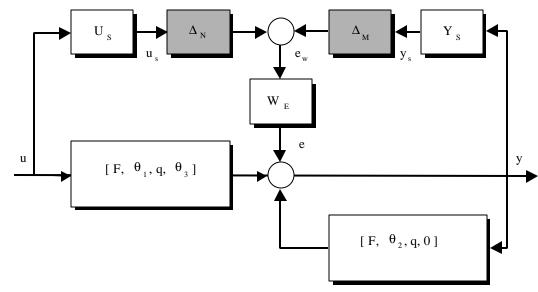
Figure 2. Structure of Parameter Estimator

## **Generalities: Uncertainty Description**

- Error Sources: Plant Input and Plant Output processed by "perturbation" subsystems (uncertainty)
- Uncertainty bound computation and target loop selection: Minimization of a robust stability condition

$$\sigma$$
 [  $U_s$   $C$   $S$   $M^{-1}$   $W_E$  ]  $\sigma$  [ $\Delta_N$ ] +  $\sigma$  [  $Y_s$   $S$   $M^{-1}$   $W_E$  ]  $\sigma$  [ $\Delta_M$ ] < 1

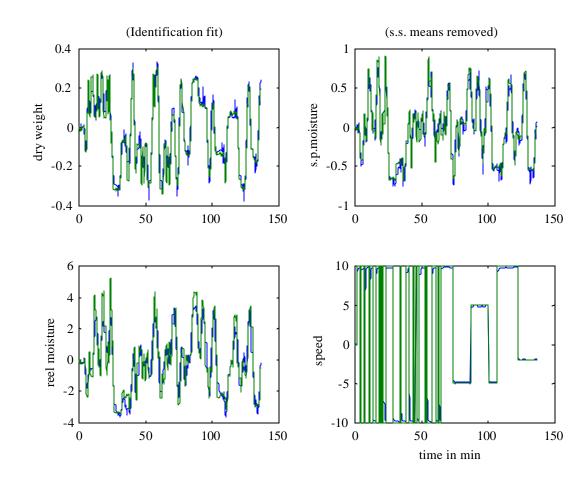
- Controller-independent approximations
- Input-output scaling and whitening to handle disparate channel-bandwidths and measurement units.



**Figure 2.** Structure of Identification Uncertainty

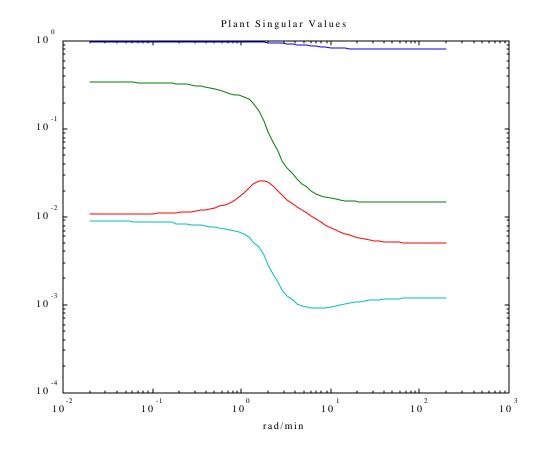
#### **Identification 1**

- Honeywell's high-fidelity simulator (TDC3000)
- Perform Identification
  - $y = N(\theta)[u] + D(\theta)[y] + e$
- Simulate Id'd system clockwise from top left:
  - dry weight
  - size-press moisture
  - reel moisture
  - machine speed
- Nominal plant: M<sup>-1</sup>N, (M=I-D)

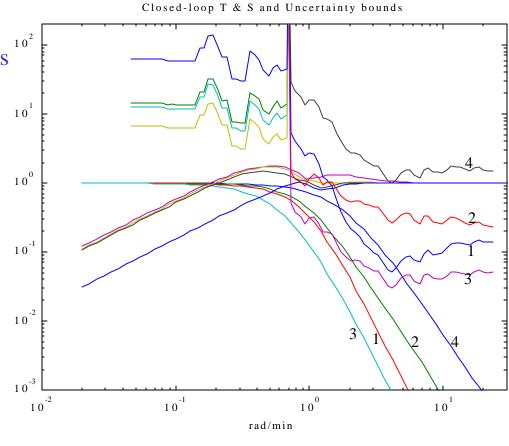


### **Identification 2**

- Identified plant singular values
  - Eigenvalue spread: 0.57 5
  - RHP transmission zeros:
    0.95, 2.1, 2.4, 1.7+/-2j, 4.3
- Main interactions
  - Stock flow moisture
  - Machine speed moisture and dry weight



- Target selection (T & S)
  - approx. per-channel contributions
- Uncertainty constraints (more critical in moisture channels)
- RHP zeros constraints (more critical in dry-weight)
- Final check through robust stability condition
- Achievable specs determined within a few iterations.



- Weighted sensitivity minimization (standard software)
- A computational alternative: Glover-McFarlane

$$\min_{K} \left\| \frac{KSM^{-1}}{SM^{-1}} \right\|_{H_{\infty}}$$

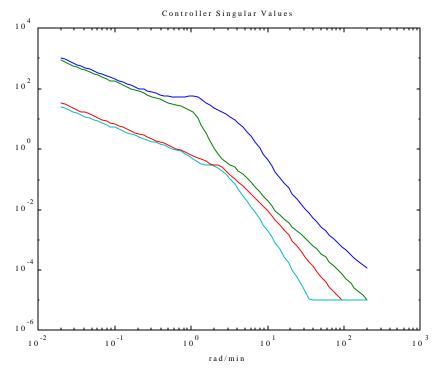
M, N = ncf(G)

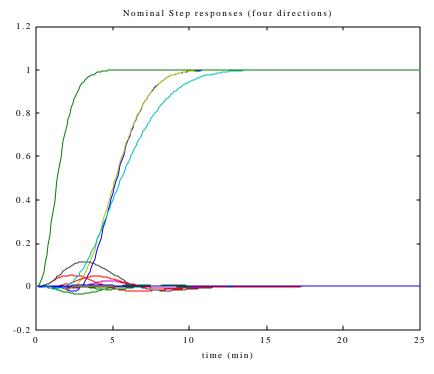
- Plant-Controller augmentation
  - S&T approximate loop-shaping
  - Avoids g-iteration but increases dimensionality
  - Fairly efficient with scalar targets
- Other alternatives, 2-DOF compensators (Open)
- Controller Implementation
  - Observers to substitute missing measurements
  - Anti-windup modifications

$$\min_{K} \left\| W_{T}^{-1} \Theta_{n}^{-1} \Theta_{m} M_{o} T M_{o}^{-1} \right\|_{H}$$

- Controller singular values
  - Reduction to remove unnecessary modes (low/high frequencies)

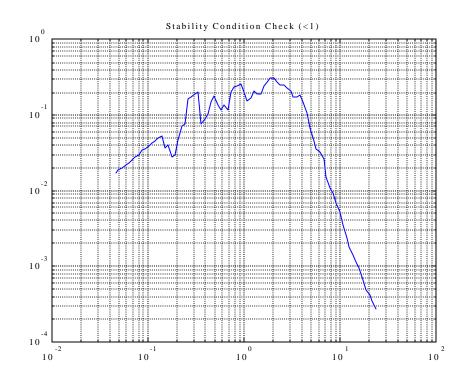
- Nominal Step responses in four directions.
  - Some coupling between channels remains due to RHP zeros

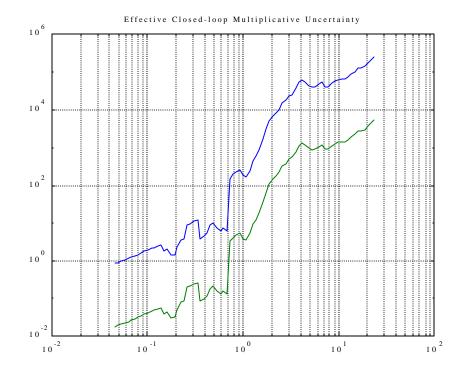




- Robust stability condition
- Tests with different controllers
- Closed-loop confidence: effective mult. uncertainty for scaled and un-scaled output

$$\begin{split} & \delta_{CL,e} < \{\sigma \left[ \ S \ M^{\text{-}1} \ W_{_E} \ \right] \ \sigma \left[ \ U_{_S} \ C \ S \ \right] \ \sigma \left[ \ T^{\text{-}1} \ \right] \ \sigma \left[ \Delta_{_N} \right] + \sigma \left[ \ Y_{_S} \ S \ M^{\text{-}1} \ W_{_E} \ \right] \ \sigma \left[ \Delta_{_M} \right] \ \} \ \alpha \ \kappa(Y_{_S}) \\ & \alpha = (1 - \sigma \left[ \ U_{_S} \ C \ S \ M^{\text{-}1} \ W_{_E} \ \right] \ \sigma \left[ \Delta_{_N} \right] - \sigma \left[ \ Y_{_S} \ S \ M^{\text{-}1} \ W_{_E} \ \right] \ \sigma \left[ \Delta_{_M} \right] \ )^{\text{-}1;} \ \kappa(Y_{_S}) = \sigma(Y_{_S}) \ \sigma(Y_{_S}^{\text{-}1}) \end{split}$$

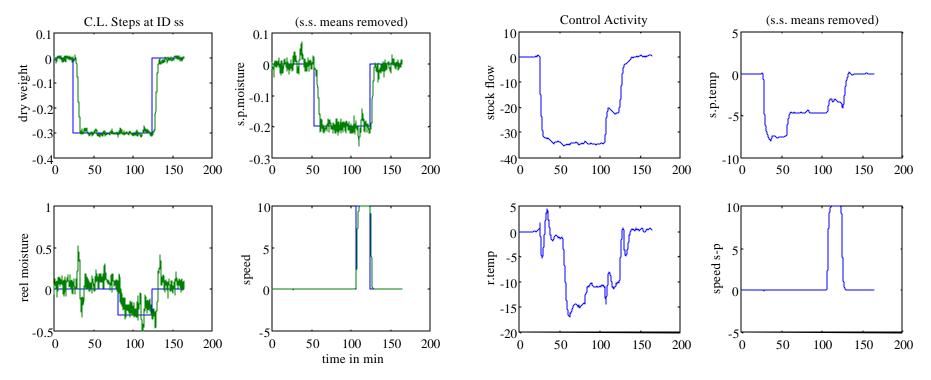




#### **Controller Evaluation 1**

- Step responses at nominal steady-state (identified)
- Reasonably smooth control activity
- Overall behavior assessment: excellent

- Small error definitions:
  - dry weight  $\sim 0.1$  (lb)
  - moisture ~0.1 0.2 (%)
  - higher for reel moisture



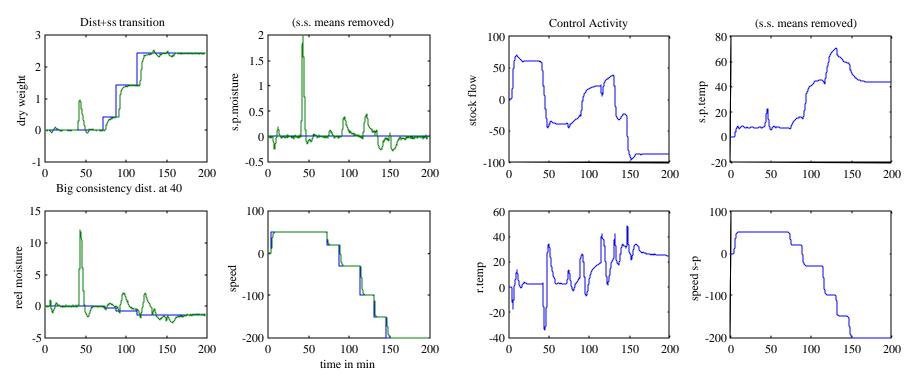
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#### **Controller Evaluation 2**

- Consistency Disturbance

   (unreasonably large) at t=40.

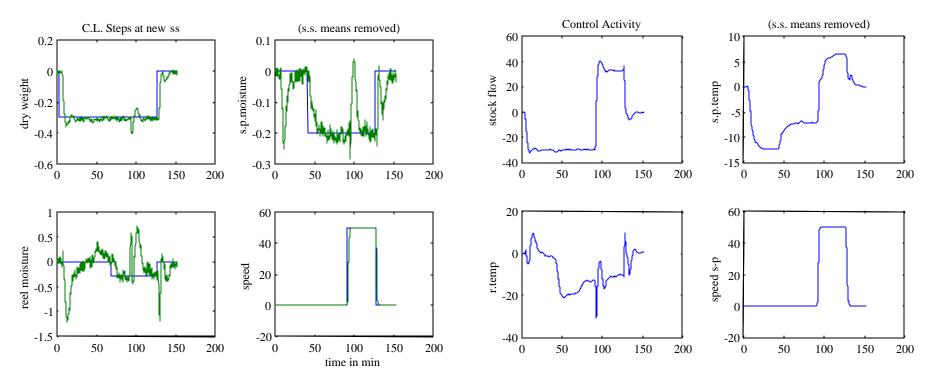
  Quick recovery without excessive errors.
- Steady-state transition to a new operating point under closed-loop control. (Normally done in open loop)
- Overall behavior assessment: excellent



## **Controller Evaluation 3**

• Step responses at new operating condition

- More coupling appears but still within acceptable limits
- Overall behavior assessment: very good



#### **Conclusions**

- Approach: "Coprime factor" uncertainty estimation
  - Flexible and reasonable framework (theoretically, computationally)
  - Compatible with established loop-shaping controller design
- Controller Performance
  - Excellent disturbance attenuation properties (sensitivity minimization)
  - Reliability (minimal iterations, work well the first time)
- Controller design
  - Quick design turn-around time
  - Very quick refinements!
  - Fast execution cycle
- Simulation results
  - Full first-principles, Nonlinear, High fidelity, but still a simulator
  - Preliminary results with real plant data support the same conclusions