1.10 A typical heat transfer model is
$$mcpT = -hA(T-T_0) + \tilde{e}$$

where was man of the heated object, Cp is the specific heat, h is the heat transfer coefficient. A is the area made has To is the ambient temperature and e is the net supplied former. These models are usually expressed in terms of the temperature difference T-To = T, so

mcpT = - hAT+ e

=> T=- hA T+ Image.

It is unclear whether the given model assumes $T_0=0$ or 25 and whether T(0)=0 or 25. We will work with $C=T-T_0$ and (meaning that unforced solutions converge to $T=T_0$) and C(0)=0 in the first case, C(0)=25 in the second.

From the given transfer functions & has two components, one is supplied power (heating) and the other is the door state (cooling). Each of these terms is converted to net power by a proportionality constant. After division with map the final model is (C(4) = T(4))

 $C = -0.5 c + 2e + 2.5 d \implies C(s) = \frac{2}{S + 0.5} e^{-\frac{1}{100}} = \frac{2.5}{S + 0.5} d(s)$ The fine constant is $T = \frac{1}{0.5} = 2 \text{ min}$.

$$C(S) = \frac{2}{5+0.5} \left[\frac{5}{5} \right] = \frac{20}{5} - \frac{20}{5+0.5} \Rightarrow C(4) = 20 \text{ u}(4) - 20 \text{ e} \text{ u}(4)$$

$$C = -0.5c + 2e - 2.5d \iff S(S) - C(0) = -0.5 C(S) + 2e(S)$$

$$\Rightarrow C(s) = \frac{2}{5+0.5} e(s) - \frac{2.5}{5+0.5} d(s) + \frac{C(0)}{5+0.5}$$

For
$$C(0) = 25$$
, $C(4) = 20 u(4) - 20e^{-0.5t}u(4) + 25e^{-0.5t}$
= $\left(20 + 5e^{-0.5t}\right)u(4)$.

d With d= u(+-2) and C*(+) denoting the solin of (b)

$$C(s) = C_*(s) + \frac{-2.5}{s+0.5} \left[\frac{e^{-2s}}{s} \right]$$

$$\Rightarrow C(t) = C_{*}(t) - \int_{0}^{-1} \left\{ \frac{2.5}{5(s+0.5)} \right\} = C_{*}(t) - \left\{ \frac{8}{10} (t-2) - \frac{1}{10} e^{-0.5(t-2)} \right\}$$

$$= 20 \left(1 - e^{-0.5t}\right) u(t) - 10 \left(1 - e^{-0.5(t-2)}\right) u(t-2)$$

$$c_{\infty} = 10.15$$

$$2.7 \quad E(z) = \frac{z}{(z+1)^2}$$

:.
$$\lim_{k \to 1} (2-1) E(2) = 0$$
 but $e_k = -k(-1)^k$ which does not have a limit.

$$E(2) = \frac{2}{(2-1)^2} \qquad \lim_{z \to 1} (2-1)E(z) = \lim_{z \to 1} \frac{z}{z-1} = \infty$$

$$e(u) = k(1)^k : \text{diverges on well.}$$

$$E(z) = \frac{z}{(z-0.9)^2} \Rightarrow \frac{1}{0.9} k(0.9)^k \rightarrow 0 = \lim_{z \to 1} (z-1) E(z)$$

$$E(z) = \frac{z}{(z-1.1)^2} \Rightarrow \frac{1}{1.1} k (1.1)^k \text{ diverges but } \lim_{z \to 1} (z-1) E(z) = 0$$

$$\frac{2.11}{2} = \frac{2^{2}}{4} = \frac{2^{2}}{4} = \frac{3}{4} = \frac{1}{2} = \frac{1}{2} = \frac{1}{2}$$

$$\frac{2}{3}$$
 $y(k) = 2.667 u(k-1) - 8 (0.5)^{k-1} u(k-1) + 5.333 (0.25) u(k-1)$

Evaluating this expression,

$$y(0) = 0$$

 $y(1) = 2.667 - 8 + 5.333 = 0$
 $y(2) = 2.667 - 8 + 5.333 / 4 = 0$
 $y(3) = 2.667 - 8 / 4 + 5.333 / 16 = 1$
 $y(4) = 2.667 - 8 / 8 + 5.333 / 64 = 1.75$

$$y(3) = e(1) + 3/4 y(2) - 1/8 y(1) = 1$$

 $y(4) = e(2) + 3/4 y(3) - 1/8 y(2) = 7/4 = 1.75$

etc.

C With nonzero I.C. we use the 2-transform Ppty.

Then,
$$z^2 Y(z) - \frac{3}{4} Z Y(z) + \frac{1}{8} Y(z) = z^2 y(0) + z y(1) - \frac{3}{4} z y(0)$$

$$\Rightarrow Y(z) = \frac{z(z - \frac{11}{4})}{(z - 0.5)(z - 0.25)} = z \left[\frac{10}{z - 0.25} - \frac{9}{z - 0.5} \right]$$

$$\Rightarrow y(k) = 10(0.25)^{k}u(k) - 9(0.5)^{k}u(k)$$
Evaluating, $y(0) = 1$

$$y(1) = -2$$

$$y(2) = -1.625$$

$$y(3) = -0.9688$$

The same result is obtained from the recursion, starting with y(0)=1, y(1)=-2. An alternative to these computations is to use the state-space version of the ODE:

$$x_{k} = \begin{pmatrix} y_{k} \\ y_{k+1} \end{pmatrix} \Rightarrow x_{k+1} = \begin{pmatrix} 0 & 1 \\ -1/8 & 3/4 \end{pmatrix} \times x_{k} + \begin{pmatrix} 0 \\ 1 \end{pmatrix} e_{k}$$

$$y_{k} = \begin{pmatrix} 1 & 0 \end{pmatrix} \times x_{k}$$

$$- C \Rightarrow$$

With $x_0 = \begin{pmatrix} 1 \\ 2 \end{pmatrix}$, we can compute

$$y(0) = C \times 0$$

 $y(1) = C \times 0$
 $y(2) = C \times 0$
 $y(2) = C \times 0$
 $y(3) = C \times 0$
 $y(3) = C \times 0$

dc.

b)
$$\Rightarrow Y(2) = \frac{T}{2-1} X(2)$$

e)
$$y(k) = \sum_{i=-\infty}^{k-1} x_i$$

Pight side
c)
$$4 \text{ kH} = 4 \text{ k} + \times \text{ kH} + \times \text{ k$$

$$\varphi(u) = \sum_{i=-\infty}^{\infty} x_i$$

Taking 2- transform

$$\Rightarrow (2-1) Y(2) = \frac{T}{2} (2+1) X(2)$$

$$S = \frac{Y(2)}{X(2)} = \frac{T}{2} = \frac{2+1}{2-1}$$
 (Tustin equivalent of)

$$\frac{2.26}{V(2)} = \begin{pmatrix} 0 & 1 \\ 0 & 3 \end{pmatrix} \quad B = \begin{pmatrix} 1 \\ 1 \end{pmatrix}, \quad C = \begin{pmatrix} -2 & 1 \\ -2 & 1 \end{pmatrix}, \quad D = 0$$

$$\frac{V(2)}{V(2)} = \begin{pmatrix} C & (2I - A)B + D = (-2, 1) \begin{bmatrix} 2 & -1 \\ 0 & 2 - 3 \end{bmatrix} \begin{bmatrix}$$

b)
$$T = \begin{bmatrix} 1 & -1 \end{bmatrix}$$
 (sum + difference of states) $\tilde{x} = Tx$

$$T'' = \frac{1}{2} \begin{bmatrix} 1 & 1 \end{bmatrix}$$

$$\chi_{k+1} = T \chi_{k+1} = T \Lambda T \chi_{k} + T R u_{k}$$
 $\chi_{k+1} = C T \chi_{k} + D u_{k}$

$$A = \begin{bmatrix} 1 & -1 \\ -2 & 2 \end{bmatrix}, B = \begin{bmatrix} 0 \\ 2 \end{bmatrix}, C = \frac{1}{2} \begin{bmatrix} -3 & -1 \end{bmatrix}, D = 0$$

c)
$$\frac{Y(2)}{U(2)} = \frac{-2+4}{2(2-3)}$$
 (invariant under similarity transformations)

d) Eigenvalues of A,
$$\widetilde{A}$$
 are 0,3

Det. $A = 0 = \det \widetilde{A}$

trace $A = 3 = \operatorname{trace} \widetilde{A}$.

Transfer function invariance.

$$\frac{2.36}{100}$$
 a) num = [3 4], den = [1 5 6]
[a,b,c,d] = +f2ss (mum, den)

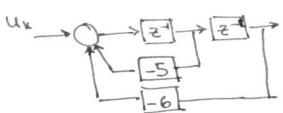
$$\Rightarrow$$
 $Q = \begin{bmatrix} -5 & -6 \\ 1 & 0 \end{bmatrix}$, $b = \begin{pmatrix} 1 \\ 0 \end{pmatrix}$, $c = \begin{pmatrix} 8 & 4 \end{pmatrix}$, $d = 0$

Alt. Gs = ss(G), α = Gs. α , b = Gs. b ... this produces α small difference in the realization α = $\begin{bmatrix} -5 & -6 \\ 2 & 0 \end{bmatrix}$ etc.

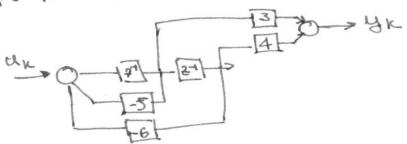
b) For the simulation diagram we start with the delays:

But x2 = x1, so

Bring in the imput: Xkt1 = -5 Xk - 6 Xk + Uk



And form the output yn = 3 x h + 4 x k



c) This simulation diagram is the same as Fig. 2.9 (controllable canonical form)

$$\frac{3.17}{G(s)} = \frac{1 - e^{-Ts}}{s}, \quad \angle G = \frac{\pi \omega}{\omega s} + \Theta = -\frac{\omega T}{2} + \Theta$$

Θ= ≤ 0 if sin Two > 0, π otherwise

We expect (Nyquist) w >> ω, ω ε [0, 10 Hz] so Θ=0

(20H is roughly half-sample delay)

The movinum lag appears at w = 10 Hz = 62.8 rad/sand it is $\angle G = -5 \text{ T} \times 6.28 = -31.4 \text{ T} \text{ rad} = 1800 \text{ T}^\circ$.

Nyquist rale = 0.05 s : 10° Lag is sampling about 10x (10 Hz)

3.24 a) 0-10V, 4 bit A/D

V_max = Vfs
$$(2^{-1}+2^{-2}+2^{-3}+2^{-4}) = 9.375 \text{ V}$$

(resolution 0.0625 × 10 5 losing 1 bit from max)

b) $2^{-4} \times 10 = 0.625 \text{ V}$ min. Possible Voltage

c) $V = 10 \left(\alpha 2^{-1} + \beta 2^{-2} + 3 2^{-3} \right) = \alpha, \beta, \gamma \in [0,1]$
 $= 0,1.95, 2.5, 3.75, 5, 6.25, 7.5, 8.75$

d) $(2^{-n}) = 0 < 0.005 \Rightarrow -n \log 2 < \log 5 \epsilon - 4$
 $\Rightarrow n > + \frac{\log 2 \epsilon 3}{\log 2} = 10.966$
 $\Rightarrow m = 11 \left(2^{11} \approx 16 - 3 \cdot \frac{1}{2} \right)$

- 3.25 a) Since No is a truncation (rather than rounding) max error is 1 bit occurring when the voltage is slightly above the next quantization level. So, wax error = (2^{-8}) 10 = 0.039 V.
 - b) 04_{HK} corresponds to a voltage (2^{-6}) to V = 0.156 V.

 According to Fig. 3.22 the ADC is mounding up so

 the voltageo producing 04_{HK} are (0.156-0.039, 0.156]VFor a rounding down operation the interval would be [0.156, 0.156+0.039]V.