

Integrating High-Fidelity Aerodynamics into Optimization and Control via Deep Learning and Koopman Theory

by

Andrew Tagg

A prospectus submitted to the faculty of
Department of Mechanical Engineering
Brigham Young University

November 3, 2025



MECHANICAL ENGINEERING

Prospectus Approval

Prospectus submitted by:

Andrew Tagg

Date

This prospectus has been approved by each member of the Graduate Committee:

Committee Member - Chair

Date

Committee Member

Date

Committee Member

Date

1 Problem Statement

High-fidelity aerodynamic modeling is an essential tool for analyzing modern aircraft, yet its use in applications such as design optimization and real-time control is severely limited by high computational costs. Instead, current optimization and control loops mainly rely on simplified, steady-state aerodynamic models, which are desirable for rapid evaluation but neglect essential characteristics of unsteady flight. If we can overcome the computational hurdle and incorporate high-fidelity, unsteady aerodynamics into our design and control algorithms, we can significantly improve the performance, safety, and reliability of next-generation aircraft systems.

In this work, we propose a framework to fully incorporate high-fidelity aerodynamics into optimization and control loops through an unsteady vortex particle method (VPM). We will accelerate VPM simulation with a novel deep learning technique designed to reduce the number of time steps required to solve the governing differential equations. This will significantly reduce computational cost, thereby enhancing the practicality of the VPM in large-scale iterative optimization. For real-time control, we will leverage Koopman operator theory to learn linear representations of VPM dynamics and develop methods to improve the generalizability of the Koopman learning process. By learning linear representations of the underlying flow dynamics, we will support rapid and accurate control synthesis using tried-and-true linear techniques.

Through the development of these key innovations, we will enable large-scale integration of VPM aerodynamics into the design and control process. High-fidelity aerodynamics will inform decisions from early conceptual design all the way through to the flight control stage. These decisions will not only consider how the aircraft behaves, but also how the surrounding air moves and evolves during complex maneuvers. With these enhanced modeling capabilities available during moments of crucial decision-making, we will open the door for aircraft that are not only more efficient and capable, but fundamentally more intelligent in how they interact with their environment.

2 Background

The next generation of aircraft systems is being conceived to operate in increasingly challenging conditions and execute mission profiles that span multiple diverse flight regimes. Some aircraft are capable of morphing their wings to access the post-stall region for precision landings [1]. Other biologically inspired vehicles replicate nature and achieve remarkable agility [2, 3]. Electric vertical takeoff and landing (eVTOL) aircraft employ lifting propulsors and fixed-wing components to take off in hover and then transition to cruise.

All of these aircraft pose significant operational challenges because they must undergo complex dynamic maneuvers in which unsteady aerodynamics play a leading role. For example, the eVTOL transition from hover to cruise is largely characterized by wake mixing and unsteady interactions between propellers and lifting surfaces that are difficult to predict. In the presence of strong unsteady loading, the aircraft must execute a series of complex control inputs that balance forward motion with vertical propulsion while simultaneously managing rotation. In addition, successful transitions often require adherence to constraints on power

[4], acceleration [5], acoustic output [6], and obstacle avoidance [7]. Considering all of these factors at once quickly becomes an overwhelming task for a pilot.

The key to navigating this complex space of decisions is trajectory optimization, which is the process of optimizing the path and control inputs of the maneuver to minimize some desired objective subject to required constraints. Recent work in eVTOL trajectory optimization has exposed key insights that highlight the importance of considering complex aerodynamics when optimizing these transition maneuvers. [8] optimized the takeoff trajectory of a tilt-wing aircraft and found that optimal trajectories involve operating at or near the stall region. This was complemented by other work which investigated the possibility of using active flow control to delay stall during a tilt-wing transition [9]. Another study directly implemented a constraint to avoid the vortex ring state during takeoff and landing and showed how this affected the optimal path [10].

Considering these unsteady aerodynamic phenomena during trajectory optimization is crucial for safe and optimal performance and therefore affects overall aircraft design decisions. Recent work has shown that trajectory optimization plays a key role in battery sizing [11] and can inform airfoil design [9]. This is why several studies have directly incorporated the trajectory into the overall aircraft design process [12, 13, 14].

One of the most important results of trajectory optimization is its natural application to automation and control. Classical control methods often rely on linear models that are only valid locally and cannot be simultaneously applied to the entire flight envelope of a modern transitioning vehicle. Instead, many efforts have employed trajectory optimization as a planning process to develop controllers that evolve over time through gain scheduling [15] or onboard control policy updates [16].

Notably, there are approaches that allow for the use of a single control policy for the entire transition. These either employ advanced robust control strategies such as H^∞ methods [17] or rely on Koopman operator theory to learn globally linear dynamic representations [18, 19, 20]. Koopman operator theory presents an especially promising option because it provides a way to learn dynamics that are linear everywhere in the state space, thus opening the door for linear controllers that are accurate and can be applied in any flight regime without sacrificing performance. The main limitation preventing the widespread use of current Koopman methods is that they require exhaustive data to be completely general, which is difficult to obtain for high-dimensional or high-fidelity problems.

The large foundation of work in trajectory optimization and control during complex transition maneuvers represents a robust and versatile framework for operating across multiple flight regimes. This existing work has exposed critical design tradeoffs for these types of aircraft and highlighted the importance of considering time-varying dynamics during the transition phase.

However, the main limitation of the current base of research is that nearly all of these studies rely heavily on overly simplified aerodynamic models, which either assume steady-state flow or other idealizations that are not accurate during an unsteady maneuver. This is a real problem. There is strong evidence to suggest that model fidelity has a severe effect on the outcome of trajectory optimization [21]. Some studies have directly compared steady-state models with unsteady models during an eVTOL transition and found significant discrepancies [22]. Others have quantified the effect of unsteady aerodynamics during rotational motion and found that it greatly impacts the dynamic stability of the aircraft

[23]. Clearly, unsteady aerodynamics play an important role during the transition of these aircraft and cannot be justifiably ignored during analysis and optimization.

Some effort has been made toward improving model fidelity in optimization and control applications. One common approach is to generate high-fidelity data from computational fluid dynamics (CFD) simulations and then tune the parameters of the low-fidelity model [24, 3, 25]. This approach is a clear improvement, but unless the parameters are updated constantly, it is still subject to the limitations of a steady-state model. Other studies have focused on applying fast unsteady aerodynamic models like the harmonic balance method [26] and Theodorsen’s theory [27]. While useful, these methods apply only to very simple oscillatory motions and cannot represent a more complex maneuver.

The vortex particle method (VPM) offers a compelling middle ground between traditional CFD and lower-order aerodynamic models. Unlike grid-based solvers, VPM is meshless, alleviating issues related to mesh generation, deformation, and dissipation. Instead, the VPM represents vorticity as a collection of Lagrangian particles, enabling efficient simulation of vortex shedding, wake roll-up, and other inherently unsteady flow phenomena. Prior work has demonstrated that VPM can deliver orders-of-magnitude computational speed-ups compared to traditional CFD solvers while retaining high-fidelity unsteady flow physics [28]. Furthermore, our research group has developed a reformulated VPM that exhibits substantially improved numerical stability relative to conventional implementations [29]. Because of its remarkable computational efficiency, the VPM is well-suited for analyzing unsteady aerodynamics during complex maneuvers involving multiple rotor–surface interactions. However, computation is still a major bottleneck, and large-scale application in trajectory optimization and control remains limited.

The best effort so far to fully incorporate VPM into optimization and control loops has come from a pair of studies that employed a lightweight two-dimensional vortex particle method for trajectory optimization [30] and then real-time control [16] for fixed-wing perching maneuvers. Even though these VPM models were limited to two dimensions and fewer than 100 particles, the studies showed improved performance and more accurate precision landings when the unsteady model was used. This is direct evidence that employing high-fidelity models in control loops can lead to better results, but the scope of these improvements is still very much limited by computational cost, as demonstrated by the need for such a lightweight version of the VPM.

One promising alternative is the use of deep learning to capture unsteady fluid dynamics. There have been many studies which apply vanilla neural networks [31, 32], convolutional neural networks [33, 34], and physics-informed neural networks [35, 36] to learn fluid flows or aerodynamic coefficients. Other papers have attempted to learn high-resolution flow fields from low-resolution solutions [37, 38] or focus on learning the underlying dynamics of the system using neural ODEs [39, 40]. These approaches offer a compelling solution to the problem of high-fidelity optimization and control because they allow for rapid evaluation of the deep surrogate network at significantly reduced cost. Despite the significant advancements in deep learning, existing data-driven approaches often struggle to generalize completely unless exhaustive training data are provided, which is extremely difficult in the high-dimensional and computationally expensive world of CFD.

Deep learning offers the potential for rapid evaluation and can capture unsteady aerodynamic effects, but traditional data-driven approaches often fail to generalize without pro-

hibitively large datasets. Low-fidelity models are computationally efficient and generalize well, yet they neglect critical unsteady phenomena. High-fidelity simulations, on the other hand, are accurate and broadly applicable but are too computationally expensive for practical use in iterative optimization and real-time control. What is needed is a methodology that combines speed, accuracy, and generality, enabling unsteady aerodynamics to directly inform design and control decisions.

The proposed work addresses this challenge through a novel integration of high-fidelity simulation and deep learning. Rather than using data to fully replace the VPM, we focus on accelerating the simulation of known VPM dynamics by reducing the number of required time steps. This approach will make VPM-based trajectory optimization significantly more feasible by reducing a primary bottleneck in VPM simulation. Building on this foundation, we will develop a method for learning Koopman linear representations of VPM dynamics without relying on an exhaustive training dataset. This will improve the generalizability of Koopman learning and enable Koopman linearization of high-dimensional and computationally expensive models. The resulting framework will enable real-time control informed by high-fidelity aerodynamics, bridging the gap between computationally expensive simulations and practical control applications.

3 Research Objectives

The central goal of this work is to facilitate the incorporation of high-fidelity, unsteady aerodynamics into optimization and control processes. To accomplish this goal, we will focus on four primary research objectives.

1. **Demonstrate VPM-based trajectory optimization for an eVTOL transition maneuver.** We will apply the VPM to simulate unsteady aerodynamic effects during an eVTOL hover-to-cruise maneuver and use this model to optimize the transition trajectory. This objective will address practical challenges associated with VPM-based optimization, such as noise and convergence, and provide a baseline in terms of computation time for comparison against future VPM acceleration efforts. Included in this study will be a comparison of high-fidelity and low-fidelity models and an analysis of their impact on the trajectory optimization.
2. **Develop a methodology to accelerate VPM simulations by reducing the number of required time steps.** By addressing a major computational bottleneck in the VPM, this objective aims to make high-fidelity simulations fast enough to be used in iterative optimization. We will validate the method by quantifying the speedup and the accuracy of the accelerated VPM simulations compared to baseline simulations.
3. **Develop a methodology to learn Koopman linear representations of VPM dynamics and improve generalizability.** This objective will seek to uncover linear representations of VPM dynamics, enabling real-time control synthesis informed by the VPM. We will apply a combination of physics-informed deep learning and PDE solution methods to demonstrate improved generality over existing approaches.

4. **Apply these new techniques to the eVTOL transition maneuver problem.**

This objective will be an application of the novel techniques developed and will serve to demonstrate their effectiveness in the context of an eVTOL transition maneuver. We will conduct trajectory optimization using the accelerated VPM simulations and control synthesis using the learned Koopman operator. Through this application study, we will show reduced computational cost and improved aircraft performance when compared to existing methods.

Together, these objectives establish a cohesive research plan which will unite high-fidelity aerodynamic modeling with optimization and control. By first demonstrating the practical feasibility and importance of unsteady aerodynamics in trajectory optimization, and then systematically addressing computational challenges that limit its broader use, this research will lay the groundwork for rapid optimization and real-time control using models that are based on sound physical foundations.

4 Proposed Research

As outlined above, the proposed work consists of four primary thrusts. First, we will apply the VPM to an eVTOL transition trajectory optimization problem to establish feasibility and demonstrate the need for high-fidelity aerodynamic modeling. Second, we will develop and validate a deep learning approach to accelerate VPM simulations via neural time-step reduction. Third, we will extend this framework to learn Koopman models of VPM dynamics, enabling efficient linear prediction of complex flow behavior. Finally, these tools will be integrated to perform trajectory optimization and closed-loop control for the eVTOL transition. The following sections describe the technical approach and methodologies developed to accomplish these objectives.

4.1 Trajectory Optimization

For trajectory optimization, we represent the aircraft as a set of dynamic states \mathbf{x} , and control inputs \mathbf{u} and we express the discrete time evolution of the aircraft states as

$$\mathbf{x}_{k+1} = F(\mathbf{x}_k, \mathbf{u}_k) \quad (1)$$

where k denotes the current time step, and F is the function that advances the state to time step $k + 1$.

We then formulate the following optimization problem

$$\begin{aligned} & \underset{\mathbf{x}_k, \mathbf{u}_k}{\text{minimize}} && \sum_{k=0}^N \mathbf{u}_k^T R \mathbf{u}_k \\ & \text{subject to} && \mathbf{x}_{k+1} = F(\mathbf{x}_k, \mathbf{u}_k) \\ & && \mathbf{x}_0 = \mathbf{x}_{\text{init}} \\ & && \mathbf{x}_N = \mathbf{x}_{\text{des}} \end{aligned} \quad (2)$$

The objective is a quadratic penalty on control effort that is determined by the weight matrix R . The system must adhere to the discrete dynamic equations $\mathbf{x}_{k+1} = F(\mathbf{x}_k, \mathbf{u}_k)$, and it must start at a predetermined state \mathbf{x}_{init} and end at a desired state \mathbf{x}_{des} . Therefore solving this optimization problem will mean that the system successfully maneuvered to the desired location while expending the least ammount of control effort possible.

This problem is highly nonlinear due to the system dynamics F , which include unsteady wake mixing from the VPM. To make the problem tractable, we construct a local linear approximation of the dynamics using a first-order Taylor series expansion:

$$\mathbf{x}_{k+1} = F(\mathbf{x}_k, \mathbf{u}_k) \approx F(\mathbf{x}^*, \mathbf{u}^*) + A(\mathbf{x}_k - \mathbf{x}^*) + B(\mathbf{u}_k - \mathbf{u}^*) \quad (3)$$

where A and B are the Jacobians of F with respect to the states and inputs, evaluated about a nominal point $(\mathbf{x}^*, \mathbf{u}^*)$. For convenience, we rearrange and write

$$\mathbf{x}_{k+1} = A\mathbf{x}_k + B\mathbf{u}_k + C \quad (4)$$

where $C = F(\mathbf{x}^*, \mathbf{u}^*) - A\mathbf{x}^* - B\mathbf{u}^*$

This now represents a linear approximation of the nonlinear dynamics, but it is only valid close to \mathbf{x}^* and \mathbf{u}^* . For an eVTOL transition, this is problematic because the final desired state is cruise, which is very different from hover. To remedy this, we update the linear model at every time step, and allow A , B and C to vary with time. The equation now becomes

$$\mathbf{x}_{k+1} = A_k\mathbf{x}_k + B_k\mathbf{u}_k + C_k \quad (5)$$

And the optimization problem becomes

$$\begin{aligned} & \underset{\mathbf{x}_k, \mathbf{u}_k}{\text{minimize}} && \sum_{k=0}^N \mathbf{u}_k^T R \mathbf{u}_k \\ & \text{subject to} && \mathbf{x}_{k+1} = A_k\mathbf{x}_k + B_k\mathbf{u}_k + C_k \\ & && \mathbf{x}_0 = \mathbf{x}_{\text{init}} \\ & && \mathbf{x}_N = \mathbf{x}_{\text{des}} \end{aligned} \quad (6)$$

Because this formulation features a quadratic objective and linear constraints, it is classified as a quadratic program (QP) and can be solved analytically. However, the linear dynamics described by A_k , B_k , and C_k are an approximation that is only valid close to the original trajectory that was used to construct the taylor series. If we use this model to solve the QP problem we will get an updated trajectory that is potentially different from the original one, and the model will no longer be valid. Therefore, iteration is required to converge to the true optimal solution. The procedure to iteratively solve the full nonlinear optimization problem is as follows:

1. Provide an initial guess trajectory.
2. Linearize the dynamics at each point along the trajectory to obtain A_k , B_k , and C_k .
3. Solve the QP problem defined in 6 to obtain a new trajectory.

4. Repeat steps 2–3 until convergence is achieved.

This procedure allows us to solve arbitrary nonlinear trajectory optimization problems, but solving it in the VPM presents additional challenges that need to be overcome. The main challenge associated with VPM-based trajectory optimization is derivative computation. The jacobian matrices A_k and B_k are computed as

$$A_k = \frac{\partial F}{\partial \mathbf{x}} \Big|_{\mathbf{x}_k^*, \mathbf{u}_k^*} \quad B_k = \frac{\partial F}{\partial \mathbf{u}} \Big|_{\mathbf{x}_k^*, \mathbf{u}_k^*} \quad (7)$$

These derivatives are obtained via automatic differentiation (AD) by propagating derivatives through the VPM simulation, which is computationally expensive. The fine temporal resolution required in VPM often leads to simulations with thousands of time steps, further increasing the cost of derivative calculations along the trajectory.

To reduce this computational burden, A_k and B_k are not computed at every time step. Instead, they are evaluated at a limited number of key points along the trajectory, exploiting the observation that the Jacobians typically change gradually as the aircraft transitions from hover to cruise.

Once A_k and B_k have been calculated at these select points, the missing values at intermediate time steps are estimated by fitting a curve using least-squares regression. This approach substantially reduces the number of derivative computations required, thereby lowering overall computational cost.

Another challenge presented by the VPM is the fact that the linear model matrices A_k , B_k , and C_k are generally very noisy. This noise is inherent in an unsteady aerodynamic model because vortical structures in the flow are shed from rotors that are spinning at a very high RPM. The high blade passage frequency causes rapidly oscillating unsteady forces, which is completely consistent from a physics stand point, but nonetheless causes numerical issues for the optimization and makes it difficult to achieve convergence.

In order to improve the numerical performance of the optimization, we seek to filter out the high frequency content of the VPM. This is partly achieved through the regression of the derivative values described previously - fitting a relatively low order curve to the values A_k , B_k , and C_k ensures a smooth progression in time. However, there is still a significant amount of noise in these matrices across optimization iterations, which causes irregular optimizer steps, and hinders convergence.

To address this, we apply an exponential moving average of the matrices to smooth out the noise from iteration to iteration

$$\bar{A}_k = \alpha A_k + (1 - \alpha) \bar{A}_k \quad (8)$$

where \bar{A}_k is the tracked average of the derivatives across iterations, A_k is the newly computed derivative, and α is a tuning parameter which regulates the level of filtering.

Using this filtering technique, as well as the derivative curve fit and iterative linearization, we were able to apply the VPM to trajectory optimization of a tilt-rotor eVTOL inspired by the Joby S4 aircraft. The aircraft trajectory and control inputs were optimized to perform a hover to cruise transition maneuver in the presence of fully unsteady aerodynamic interactions as calculated by the VPM. The results of the trajectory optimization are presented

in Fig. 1 which shows that the aircraft was able to reach a target velocity of 55 meters per second by gradually tilting its rotors forward while maintaining constant altitude by pitching the aircraft up to increase lift.

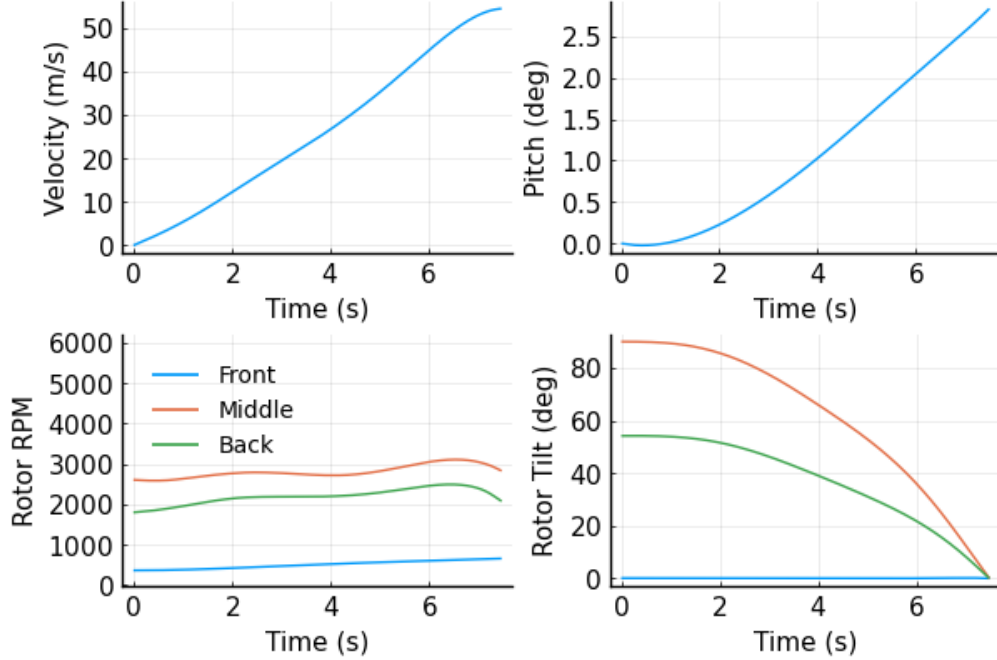


Figure 1: Optimal trajectory and control inputs for a tilt-rotor eVTOL aircraft during a hover to cruise transition modeled in the VPM. Aircraft velocity and pitch steadily increase with time, and rotors gradually tilt forward (0 deg is forward, 90 deg is vertical).

As part of this study, we compare the force predictions from the VPM with those of a lower fidelity vortex lattice method (VLM) which analyzes the forces on a wing assuming steady state flow. We show that the VLM does predict the correct trends, but does not capture the influence of a morphing wake during transition. This discrepancy is shown in Fig. 2 where the two methods disagree by over 1000 N during early transition.

4.2 Neural Time Step Reduction

The techniques outlined above present a feasible approach to trajectory optimization in the VPM by overcoming key challenges such as noise and the high cost of derivatives. However, the optimization took roughly 428 hours to complete, which is a major limitation on the practicality of this approach. A large part of this cost is due to the extremely small time steps necessary to resolve particle dynamics. This means that simulations often need 5000 - 10000 time steps just to simulate 10 seconds of real-time flight. To address this issue, we will present a novel methodology that aims to accelerate the VPM by reducing the time steps necessary to solve the governing differential equations. While a major motivation of this method is directed toward accelerating the VPM, it is completely general and can be applied to any explicit ordinary differential equation (ODE).

Consider a general system of ODEs

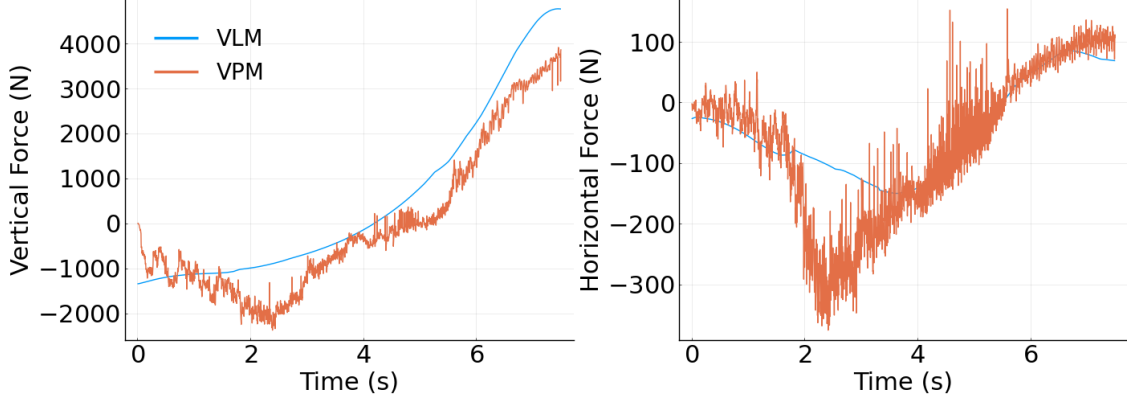


Figure 2: Vertical and horizontal forces on the wing during the transition maneuver as computed by the VPM (orange) and VLM (blue). VLM predicts correct trends, but the two models disagree significantly during early transition (2 second mark)

$$\frac{d\mathbf{x}}{dt} = f(\mathbf{x}) \quad (9)$$

If the dynamics of the system are fast, then small time steps will be necessary to resolve the correct trajectory, and if they are slow, then larger time steps may be sufficient, and we can simulate accurately with fewer of them.

The best metric for determining whether the dynamics are fast or slow is the spectral radius of the system’s Jacobian, defined as

$$\rho\left(\frac{df}{d\mathbf{x}}\right) = \|\boldsymbol{\lambda}\|_{\infty} \quad (10)$$

where $\|\boldsymbol{\lambda}\|_{\infty}$ is the magnitude of the largest eigenvalue of $\frac{df}{d\mathbf{x}}$

We desire a dynamic system which has a small spectral radius, and therefore slow dynamics, so that we can simulate the system accurately with larger time steps. To achieve this, we will leverage two neural networks ϕ , and ψ that together form an autoencoder pair.

$$\mathbf{z} = \phi(\mathbf{x}) \quad \mathbf{x} = \psi(\mathbf{z}) \quad (11)$$

where $\mathbf{z} \in \mathbb{R}^m$ is a learned latent space, and is of higher dimension than $\mathbf{x} \in \mathbb{R}^n$: $m > n$. Then, by the chain rule,

$$\frac{d\mathbf{z}}{dt} = \frac{d\phi}{d\mathbf{x}} \frac{d\mathbf{x}}{dt} \quad (12)$$

Both $\frac{d\phi}{d\mathbf{x}}$ and $\frac{d\mathbf{x}}{dt}$ are functions of \mathbf{x} , but we can substitute $\mathbf{x} = \psi(\mathbf{z})$ to obtain

$$\frac{d\mathbf{z}}{dt} = \frac{d\phi}{d\mathbf{x}}(\psi(\mathbf{z})) \frac{d\mathbf{x}}{dt}(\psi(\mathbf{z})) \quad (13)$$

We have now expressed the dynamic system entirely in \mathbf{z} space. Because it was derived from the known dynamics of the system and the chain rule, Eq. 13 will generalize to the entire state space, assuming the autoencoder can learn a valid mapping from \mathbf{x} to \mathbf{z} .

The next step is to train ϕ and ψ to enforce slow dynamics in the latent representation. We define a loss function to be the spectral radius of the new dynamic system's Jacobian.

$$L_d = \rho \left(\frac{d\dot{\mathbf{z}}}{d\mathbf{z}} \right) \quad (14)$$

If we want the dynamics to be slow over a large domain in \mathbf{z} space, then we need to penalize the spectral radius of the Jacobian at many points \mathbf{z}_k in that domain

$$L_d = \frac{1}{N} \sum_{k=0}^N \rho \left(\frac{d\dot{\mathbf{z}}}{d\mathbf{z}} \Big|_{\mathbf{z}_k} \right) \quad (15)$$

The other loss function that we need to define is the standard autoencoder reconstruction loss to ensure that we learn a valid latent representation

$$L_r = \frac{1}{N} \sum_{k=0}^N \|\mathbf{x}_k - \psi(\phi(\mathbf{x}_k))\|_2^2 \quad (16)$$

The autoencoder pair is then trained to minimize the weighted combination of the two loss functions

$$\underset{\phi, \psi}{\text{minimize}} \quad \frac{1}{N} \sum_{k=0}^N w_1 \rho \left(\frac{d\dot{\mathbf{z}}}{d\mathbf{z}} \Big|_{\mathbf{z}_k} \right) + w_2 \|\mathbf{x}_k - \psi(\phi(\mathbf{x}_k))\|_2^2 \quad (17)$$

This method has been shown to be successful in reducing the number of time steps necessary to simulate the following ODE

$$\frac{dx}{dt} = -15x \quad (18)$$

which has eigenvalue $\lambda = -15$. Because the dynamics are relatively fast, a time step of 0.01 was necessary to accurately simulate the trajectory using euler integration. An autoencoder was trained using the above loss function, and then simulated accurately with a time step of 0.1 - an order of magnitude larger than what was required for the original system. As shown in Fig. 3 we simulated this new system and then reconstructed the original states using the decoder network. The new system was shown to simulate much more accurately than the original system when using a large time step of 0.1

4.3 Koopman Learning

The neural time step reduction method described above has the potential to significantly speed up VPM simulations, and enable their use in iterative optimization loops. However, on its own, neural time step reduction is unlikely to achieve the speedups necessary for real time control, which requires many full simulations every second. In order to facilitate real time VPM-based control, we seek linear models that can be used to solve the optimal control problem analytically.

In order to achieve this, we leverage Koopman operator theory, which states that for any dynamic system

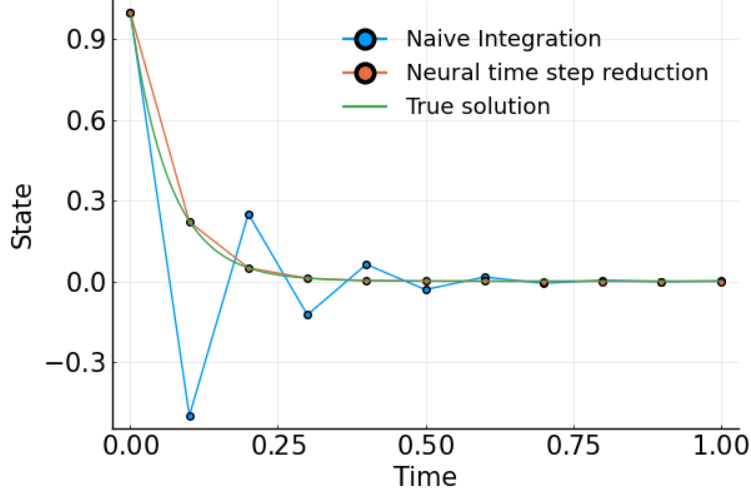


Figure 3: Simulation of the dynamic system $\frac{dx}{dt} = -15x$ using large time steps. The original system (blue) is compared to the learned system (orange) and the analytic solution (green). Using neural time step reduction drastically increases the accuracy of the simulation when using a large time step of 0.1.

$$\frac{d\mathbf{x}}{dt} = f(\mathbf{x}) \quad (19)$$

there exists a mapping $\mathbf{z} = \phi(\mathbf{x})$ such that

$$\frac{d\mathbf{z}}{dt} = K\mathbf{z} \quad (20)$$

where K is the Koopman operator and represents the globally linear dynamics of \mathbf{z} space. Koopman operator theory states that such a map exists, but that it is potentially infinite dimensional.

To overcome this challenge, most current approaches apply machine learning to learn a finite dimensional approximation to the Koopman operator. For the mapping $\mathbf{z} = \phi(\mathbf{x})$ one can use existing basis functions like Hermite polynomials, but it's generally better to train a neural network to learn the best mapping possible.

Because current methods typically rely on trajectory data simulated or experimentally obtained beforehand, there is always a risk of overfitting to the specific trajectories in the data set. Therefore, we pursue a methodology that will improve the generalizability of the Koopman learning process, and mitigate the risk of overfitting when data is limited.

One way to approach learning the linear Koopman dynamic system is by considering the set of partial differential equations that arise from applying the chain rule to the learned latent space.

$$\frac{d\mathbf{z}}{dt} = \frac{\partial \mathbf{z}}{\partial \mathbf{x}} \frac{d\mathbf{x}}{dt} = \frac{\partial \mathbf{z}}{\partial \mathbf{x}} f(\mathbf{x}) \quad (21)$$

Setting this equal to Eq. 20 gives

$$\frac{\partial \mathbf{z}}{\partial \mathbf{x}} f(\mathbf{x}) = K \mathbf{z} \quad (22)$$

which is a linear partial differential equation that can be routinely solved using the method of characteristics. The method of characteristics solves for \mathbf{z} along characteristic curves by reducing the problem to a set of ordinary differential equations parameterized by a variable t

$$\frac{d\mathbf{x}}{dt} = f(\mathbf{x}), \quad \frac{d\mathbf{z}}{dt} = K \mathbf{z} \quad (23)$$

This is the expected result and tells us that as \mathbf{x} evolves according to $f(\mathbf{x})$, \mathbf{z} evolves according to $K\mathbf{z}$. By itself, this is not useful yet because in order to solve for \mathbf{z} we need to simulate the original dynamic system.

We can go further by solving the \mathbf{z} ODE analytically as a function of t

$$\mathbf{z} = e^{Kt} \mathbf{z}_0 \quad (24)$$

where \mathbf{z}_0 is the initial condition. Ideally we would like to solve for \mathbf{z} as a function of \mathbf{x} rather than t , but due to the nonlinearity of the system, we cannot solve for $t(\mathbf{x})$ analytically. Instead, we propose approximating $t(\mathbf{x})$ using a neural network. This acts as a "time-to-reach" function, predicting how long it takes to reach a certain point in \mathbf{x} space from a given initial point.

$t(\mathbf{x})$ alone only applies along a specific trajectory. In order to describe the full solution, we also need to identify which trajectory a point belongs to. To address this, we introduce another scalar valued network $l(\mathbf{x})$ to act as a "label" for each trajectory. Given a point in \mathbf{x} space, $l(\mathbf{x})$ identifies which trajectory we are on, and $t(\mathbf{x})$ tells how far along that trajectory we are.

With these two functions defined, we have

$$\mathbf{z} = e^{Kt(\mathbf{x})} \mathbf{z}_0(l(\mathbf{x})) \quad (25)$$

where \mathbf{z}_0 is a function that accepts the trajectory label and returns the initial conditions in \mathbf{z} space. This can be any function, but it should be injective to ensure unique initial conditions for each label value.

We now have a model that is parameterized by the networks $t(\mathbf{x})$, $l(\mathbf{x})$, the function \mathbf{z}_0 , and the matrix K . This model is more interpretable, and generalizable than the traditional mapping defined by a single network $\mathbf{z}(\mathbf{x})$, because it encodes the known PDE solution method of characteristics.

For training, we aim to find $t(\mathbf{x})$ and $l(\mathbf{x})$ satisfying

$$\frac{dt}{dt} = \frac{\partial t}{\partial \mathbf{x}} \frac{d\mathbf{x}}{dt} = 1 \quad (26)$$

$$\frac{dl}{dt} = \frac{\partial l}{\partial \mathbf{x}} \frac{d\mathbf{x}}{dt} = 0 \quad (27)$$

In other words, t increases unitarily along the trajectories, and l is constant along the trajectories.

This method was used to learn a solution to the Koopman problem for a simulated glider undergoing a transient maneuver before stabilizing. The results were compared to the standard method of simply defining a vanilla neural network for $\mathbf{z}(\mathbf{x})$. In both methods, the latent states were simulated from initial conditions using the learned Koopman operator K , and compared to their "true" values which were encoded directly from the original trajectory.

The results of this comparison are shown in Fig. 4. Note that the figure shows the learned latent space dynamics for each network - because the networks learn very different latent representations, they produce very different graphs. The difference between the two methods is seen in how accurately the Koopman operator K can predict those latent dynamics, which is represented by the dashed lines in each graph. The method of characteristics approach is much more accurate than the standard method for the same number of data points.

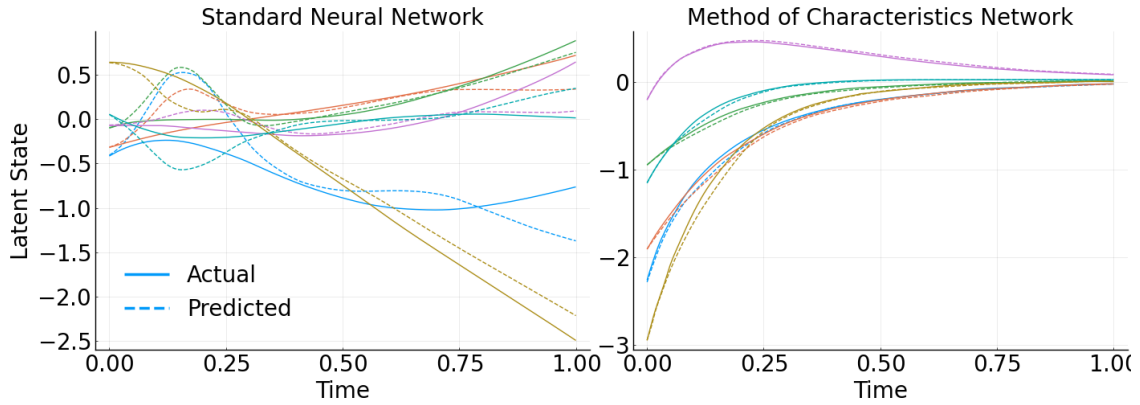


Figure 4: Simulation of Koopman linearized dynamics of a glider which were learned by a standard neural network (left), and by the method of characteristics approach (right). The simulated values (dashed) are compared to the true values (solid) for both cases. For the same number of sample points, the method of characteristics approach is much more accurate than the standard approach, suggesting improved generality.

4.4 Project Outline

In order to successfully accomplish all of the specified research objectives, we will adhere to the project timeline shown in Fig. 5

During the first year, this project has focused on applying the VPM to an eVTOL hover to cruise transition optimization. An optimization methodology has been developed to overcome noisy VPM derivatives and improve convergence. The VPM was used to model a tilt-rotor aircraft, and this framework was applied to optimize the transition maneuver.

The second year of this project will be devoted to the development of the neural time step reduction method. This method will then be used to solve example ODEs that traditionally require fine time discretization - these benchmarks will highlight the benefit of the novel technique. After the methodology is finalized and validated, it will be applied to the VPM, and tuned to achieve the maximum possible speedups.

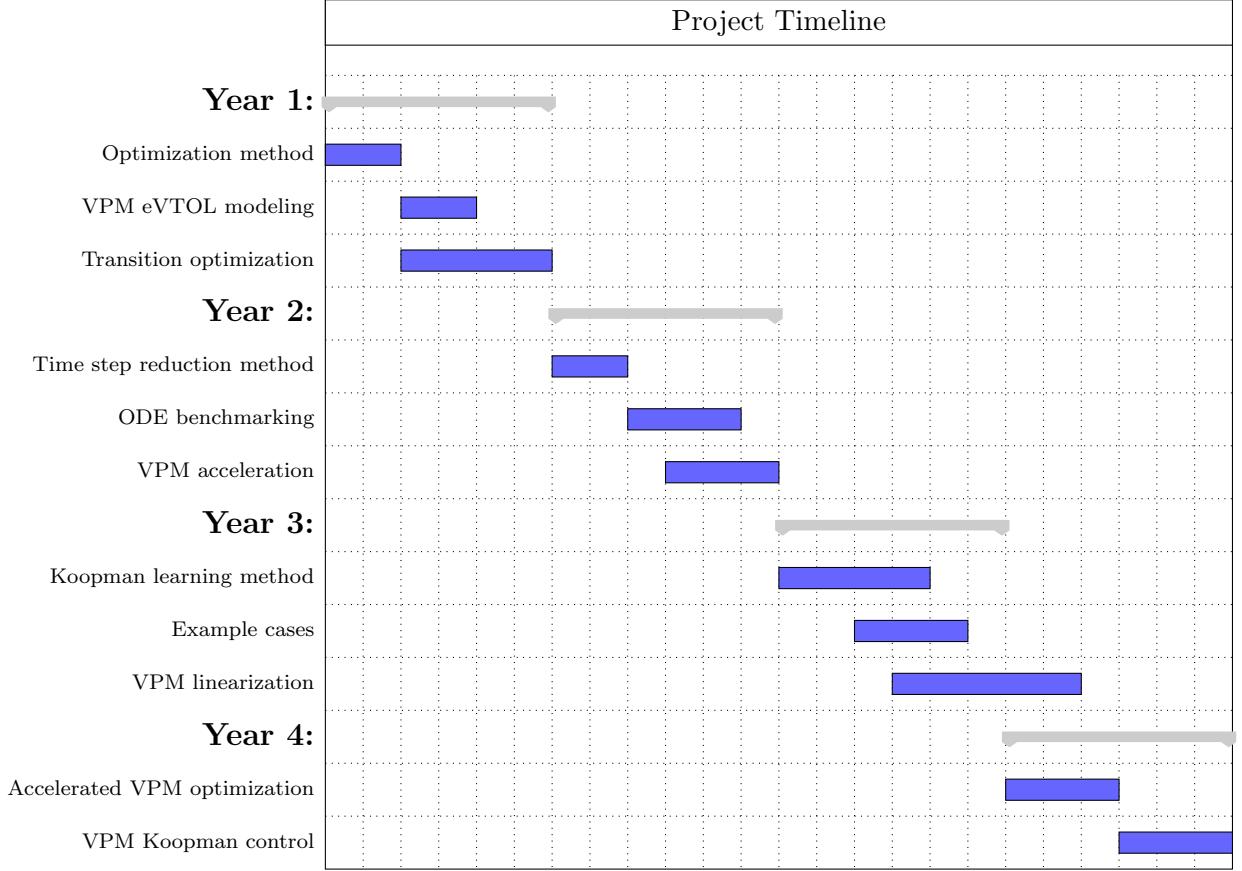


Figure 5: Visualization of the project timeline outlining each year’s subtasks and anticipated durations.

The third year of the project will be dedicated to the development of an improved Koopman learning method, which will be more general, and require less data for training than current methods. This method will again be validated against the standard method through a series of simple example cases, and then applied to learn globally linear VPM dynamics.

The fourth and final year of the project will be characterized mainly by application of these techniques to large scale VPM problems, including a VPM-based trajectory optimization, and active feedback control application.

The successful completion of this project will not only depend on adherence to the project timeline, but it will also require access to high-performance computational resources. We will take advantage of the FLOW Lab workstation for preliminary testing, and utilize BYU’s supercomputing facilities in order to efficiently perform optimization, and training of our deep learning models.

5 Anticipated Contributions

The proposed work, as outlined in the previous section, aims to bridge the gap between high-fidelity simulation, and iterative optimization and control applications through several

key contributions:

1. A practical demonstration of VPM-based trajectory optimization, including a comparative analysis that underscores the importance of unsteady modeling during eVTOL transition phases.
2. The development of a neural time-step reduction methodology applicable to any general set of ODEs, which will substantially accelerate high-fidelity simulations while preserving accuracy.
3. An enhancement of the generalizability of the Koopman learning process, enabling more robust linearization of nonlinear dynamics and supporting real-time control of complex, high-fidelity systems.

Together, these efforts will create a cohesive framework that unites high-fidelity aerodynamic modeling, machine learning, and control theory. By overcoming the computational and modeling barriers that have traditionally separated simulation from real-time decision making, this research will make it possible for optimization and control algorithms to directly leverage unsteady aerodynamic effects. In doing so, it lays the foundation for a new generation of aircraft design and control strategies—ones that are not only faster and more efficient, but also fundamentally more adaptive and aware of the physics that govern aircraft motion.

References

- [1] S. Bakhshi, S. Kaneko, J. Martins, and A. Sharma, “Coupled trajectory and aerostuctural optimization of a uav with modular morphing wings,” 07 2025.
- [2] S.-G. Lee, H.-H. Yang, R. Addo-Akoto, and J.-H. Han, “Transition flight trajectory optimization for a flapping-wing micro air vehicle with unsteady vortex-lattice method,” *Aerospace*, vol. 9, p. 660, 10 2022.
- [3] R. Tian, L. Li, W. Wang, X. Chang, S. Ravi, and G. Xie, “Cfd based parameter tuning for motion control of robotic fish,” *Bioinspiration and Biomimetics*, vol. 15, 02 2020.
- [4] N. Moradi, C. Wang, and F. Mafakheri, “Urban air mobility for last-mile transportation: A review,” *Vehicles*, vol. 6, no. 3, pp. 1383–1414, 2024. [Online]. Available: <https://www.mdpi.com/2624-8921/6/3/66>
- [5] S. Xiang, A. Xie, M. Ye, X. Yan, X. Han, H. Niu, Q. Li, and H. Huang, “Autonomous evtol: A summary of researches and challenges,” *Green Energy and Intelligent Transportation*, vol. 3, no. 1, p. 100140, 2024. [Online]. Available: <https://www.sciencedirect.com/science/article/pii/S2773153723000762>
- [6] W. Raza and R. S. Stansbury, “Noise prediction and mitigation for uas and evtol aircraft: A survey,” *Drones*, vol. 9, no. 8, 2025. [Online]. Available: <https://www.mdpi.com/2504-446X/9/8/577>
- [7] P. Shukla, S. Shukla, and A. Kumar Singh, “Trajectory-prediction techniques for unmanned aerial vehicles (uavs): A comprehensive survey,” *IEEE Communications Surveys and Tutorials*, vol. 27, no. 3, pp. 1867–1910, 2025.
- [8] S. S. Chauhan and J. R. R. A. Martins, “Tilt-wing evtol takeoff trajectory optimization,” *Journal of Aircraft*, vol. 57, no. 1, pp. 93–112, 2020. [Online]. Available: <https://doi.org/10.2514/1.C035476>
- [9] L. Panish and M. Basic, “Tiltwing evtol transition trajectory optimization,” *Journal of Aircraft*, vol. 62, no. 1, pp. 81–93, 2025. [Online]. Available: <https://doi.org/10.2514/1.C037862>
- [10] J. Park, I. Kim, J. Suk, and S. Kim, “Trajectory optimization for takeoff and landing phase of uam considering energy and safety,” *Aerospace Science and Technology*, vol. 140, p. 108489, 06 2023.
- [11] M. Liu, Z. Su, J. Zhu, F. Guo, and Y. You, “Flight analysis and optimization design of vectored thrust evtol based on cooperative flight/propulsion control,” *Aerospace Science and Technology*, vol. 149, p. 109143, 2024. [Online]. Available: <https://www.sciencedirect.com/science/article/pii/S1270963824002761>
- [12] D. Sarojini, M. Ruh, A. J. Joshy, J. Yan, A. Ivanov, L. Scotzniovsky, A. Fletcher, N. Orndorff, M. Sperry, V. Gandarillas, I. Asher, J. Chambers, H. Gill, S. Lee, Z. Cheng,

- G. Rodriguez, S. Zhao, C. Mi, T. Nascenzi, and J. Hwang, "Large-scale multidisciplinary design optimization of an evtol aircraft using comprehensive analysis," 01 2023.
- [13] S. Kaneko and J. R. Martins, "Simultaneous optimization of design and takeoff trajectory for an evtol aircraft," *Aerospace Science and Technology*, vol. 155, p. 109617, 2024. [Online]. Available: <https://www.sciencedirect.com/science/article/pii/S1270963824007466>
 - [14] S. Kaneko and J. Martins, "Simultaneous design and trajectory optimization strategies for computationally expensive models," *AIAA Journal*, vol. 63, 01 2025.
 - [15] D. Thompson, "Robust control of an evtol through transition with a gain scheduling lqr controller," Master's Thesis, University of Maryland, College Park, Maryland, 2020.
 - [16] A. Gupta, K. Wolfe, G. Perrotta, and J. Moore, "Real-time planning and control with a vortex particle model for fixed-wing uavs in unsteady flows," 2025. [Online]. Available: <https://arxiv.org/abs/2509.16079>
 - [17] H. Yang and R. Morales, "Robust full-envelope flight control design for an evtol vehicle," *AIAA Scitech 2021 Forum*, 2021. [Online]. Available: <https://arc.aiaa.org/doi/abs/10.2514/6.2021-0254>
 - [18] M. Korda and I. Mezić, "Linear predictors for nonlinear dynamical systems: Koopman operator meets model predictive control," *Automatica*, vol. 93, pp. 149–160, 2018.
 - [19] I. Abraham, G. D. L. Torre, and T. D. Murphey, "Model-based control using koopman operators," *Robotics: Science and Systems*, 2017.
 - [20] V. Zinage and E. Bakolas, "Koopman operator based modeling for quadrotor control on $se(3)$," 2021, arXiv preprint.
 - [21] R. Anderson, J. Willis, J. Johnson, A. Ning, and R. W. Beard, *A Comparison of Aerodynamics Models for Optimizing the Takeoff and Transition of a Bi-wing Tailsitter*, 2021.
 - [22] A. C. Tagg, R. Anderson, C. Joseph, and A. Ning, "Trajectory optimization of evtol and conventional aircraft: A comparative analysis of vortex particle method and vortex lattice + blade element momentum theory," *AIAA AVIATION FORUM AND ASCEND 2024*. [Online]. Available: <https://arc.aiaa.org/doi/abs/10.2514/6.2024-3587>
 - [23] W.-Q. Q. T.-J. Z. Y.-Q. C. Q. Wang, K.-F. He and K.-Y. Wu, "Unsteady aerodynamics modeling for flight dynamics application," *Acta Mechanica Sinica*.
 - [24] J. Dean, S. Morton, D. Mcdaniel, J. Clifton, and D. Bodkin, "Aircraft stability and control characteristics determined by system identification of cfd simulations," 08 2008.
 - [25] S. Görtz, D. Mcdaniel, and S. Morton, "Towards an efficient aircraft stability and control analysis capability using high-fidelity cfd," *Collection of Technical Papers - 45th AIAA Aerospace Sciences Meeting*, vol. 18, 01 2007.

- [26] J. P. Thomas, E. H. Dowell, and K. C. Hall, “Modeling viscous transonic limit cycle oscillation behavior using a harmonic balance approach,” *Journal of Aircraft*, vol. 41, no. 6, pp. 1266–1274, 2004. [Online]. Available: <https://doi.org/10.2514/1.9839>
- [27] N. Bhoir and S. N. Singh, “Output feedback nonlinear control of an aeroelastic system with unsteady aerodynamics,” *Aerospace Science and Technology*, vol. 8, no. 3, pp. 195–205, 2004. [Online]. Available: <https://www.sciencedirect.com/science/article/pii/S1270963803001378>
- [28] E. J. Alvarez, “Reformulated vortex particle method and meshless large eddy simulation of multirotor aircraft,” Ph.D. dissertation, Brigham Young University, 2022, order No. 29340504. Available from ProQuest Dissertations & Theses Global (2723858290). [Online]. Available: <https://www.proquest.com/dissertations-theses/reformulated-vortex-particle-method-meshless/docview/2723858290/se-2>
- [29] E. J. Alvarez and A. Ning, “Stable vortex particle method formulation for meshless large-eddy simulation,” *AIAA Journal*, vol. 62, no. 2, pp. 637–656, 2024. [Online]. Available: <https://doi.org/10.2514/1.J063045>
- [30] G. Perrotta, L. Scheuer, Y. Kopel, M. Basescu, A. Polevoy, K. Wolfe, and J. Moore, “Planning and control for a dynamic morphing-wing uav using a vortex particle model,” 2023. [Online]. Available: <https://arxiv.org/abs/2307.02371>
- [31] M. Collotta, G. Pau, and R. Caponetto, “A real-time system based on a neural network model to control hexacopter trajectories,” pp. 222–227, 2014.
- [32] C. Sabater, P. Stuermer, and P. Bekemeyer, “Fast predictions of aircraft aerodynamics using deep learning techniques,” 08 2021.
- [33] Abucide, K. Portal-Porras, U. Fernandez-Gamiz, E. Zulueta, and A. Teso-Fz-Betoño, “A data augmentation-based technique for deep learning applied to cfd simulations,” *Mathematics*, vol. 9, p. 1843, 08 2021.
- [34] W. Hwang, D. Lee, J. Shin, K. Cho, and S. Choi, “Aerodynamic flow analysis using conditional convolutional autoencoder in various flow conditions and application to cfd-based design optimization,” *Advances in Aerodynamics*, vol. 7, 09 2025.
- [35] M. Raissi, P. Perdikaris, and G. Karniadakis, “Physics-informed neural networks: A deep learning framework for solving forward and inverse problems involving nonlinear partial differential equations,” *Journal of Computational Physics*, vol. 378, pp. 686–707, 2019. [Online]. Available: <https://www.sciencedirect.com/science/article/pii/S0021999118307125>
- [36] J. Lin, S. Chen, H. Yang, Q.-f. Jiang, and J. Liu, “A physics-informed neural network-based aerodynamic parameter identification method for aircraft,” *Physics of Fluids*, vol. 37, 02 2025.
- [37] V. Sharma, A. Rauch, and V. Raman, “Accelerating cfd simulations with super-resolution feedback-informed adaptive mesh refinement,” 01 2025.

- [38] H. Gao, L. Sun, and J.-X. Wang, “Super-resolution and denoising of fluid flow using physics-informed convolutional neural networks without high-resolution labels,” *Physics of Fluids*, vol. 33, no. 7, p. 073603, Jul. 2021. [Online]. Available: <http://dx.doi.org/10.1063/5.0054312>
- [39] G. Jarry, R. Dalmau, X. Olive, and P. Very, “A neural ode approach to aircraft flight dynamics modelling,” 2025. [Online]. Available: <https://arxiv.org/abs/2509.23307>
- [40] J. Ma, Y. Li, J. Tu, Y. Zhang, J. Ai, and Y. Dong, “Development and implementation of physics-informed neural ode for dynamics modeling of a fixed-wing aircraft under icing/fault,” *Guidance, Navigation and Control*, vol. 04, no. 01, p. 2350024, 2024. [Online]. Available: <https://doi.org/10.1142/S2737480723500243>