

Homework: GM Car Following

14.2, 14.8

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14.2

General Motors has developed several car following models. Of these, GM5 is given as in Equation 1.

$$\ddot{x}_i(t + \tau_i) = \alpha \frac{[\dot{x}_i(t + \tau_i)]^m}{[x_{i-1}(t) - x_i(t)]^l} \times [\dot{x}_{i-1}(t) - \dot{x}_i(t)] \quad (1)$$

If $m = 0$ and $l = 1$, we can show that GM5 integrates to the Greenberg model (given by $v = v_m \ln(k_j/k)$):

$$\begin{aligned} \ddot{x}_i(t + \tau_i) &= \alpha \frac{[\dot{x}_i(t + \tau_i)]^0}{[x_{i-1}(t) - x_i(t)]^1} \times [\dot{x}_{i-1}(t) - \dot{x}_i(t)] \\ &= \alpha \frac{1}{x_{i-1}(t) - x_i(t)} \times [\dot{x}_{i-1}(t) - \dot{x}_i(t)] \\ &= \alpha \frac{\dot{x}_{i-1}(t) - \dot{x}_i(t)}{x_{i-1}(t) - x_i(t)} \\ &= \alpha \frac{\Delta \dot{x}}{\Delta x} \\ \int \ddot{x} dt &= \alpha \int \frac{\dot{x}}{x} dt = \alpha \int \frac{dx/dt}{x} dt = \alpha \int \frac{dx}{x}. \end{aligned}$$

Then, if v is flow speed and $k = 1/x$ is vehicle density:

$$\begin{aligned} \int \ddot{x} dt &= \alpha \int \frac{dx}{x} \\ v &= \alpha \ln \left(\frac{1}{k} \right) + C. \end{aligned}$$

If $v = 0$, then $k = k_j$, the jam density:

$$\begin{aligned} 0 &= \alpha \ln \left(\frac{1}{k_j} \right) + C \\ C &= -\alpha \ln \left(\frac{1}{k_j} \right) \\ C &= \alpha \ln(k_j). \end{aligned}$$

This then gives us

$$\begin{aligned} v &= \alpha \ln \left(\frac{1}{k} \right) + \alpha \ln(k_j) \\ &= \alpha \ln \left(\frac{k_j}{k} \right). \end{aligned} \tag{2}$$

In order to find α , we must first derive the flow-density equation from Equation 2:

$$q = kv = k\alpha \ln \left(\frac{k_j}{k} \right).$$

q_m , the maximum flow rate, is found by maximizing this equation with respect to k (with k_m equal to the density at q_m):

$$\begin{aligned} \frac{dq}{dk} &= 0 = \frac{d}{dk} \left[k\alpha \ln \left(\frac{k_j}{k} \right) \right] \\ 0 &= \alpha \frac{d}{dk} [k \times (\ln k_j - \ln k)] \\ 0 &= \alpha \left[\ln \left(\frac{k_j}{k_m} \right) + k_m \frac{-1}{k_m} \right] = \alpha \left[\ln \left(\frac{k_j}{k_m} \right) - 1 \right]. \end{aligned}$$

Assuming $\alpha \neq 0$:

$$\begin{aligned} 0 &= \ln \left(\frac{k_j}{k_m} \right) - 1 \\ 1 &= \ln \left(\frac{k_j}{k_m} \right) \\ k_m &= \frac{k_j}{e}. \end{aligned}$$

Defining v_m as the speed at q_m , the above and Equation 2 gives us:

$$\begin{aligned} v_m &= \alpha \ln \left(\frac{k_j}{k_m} \right) \\ v_m &= \alpha \ln \left(\frac{k_j}{k_j/e} \right) \\ v_m &= \alpha. \end{aligned}$$

Then:

$$v = v_m \ln \left(\frac{k_j}{k} \right),$$

which is the Greenberg model.

14.8

a

Using GM1 ($\ddot{x}(t + \tau_i) = \alpha[\dot{x}_{i-1}(t) - \dot{x}_i(t)]$), with $\alpha = 0.51 \text{ s}^{-1}$, $\dot{x}_{i-1}(t) = 72 \text{ kph} = 20 \text{ m/s}$, $\dot{x}_i(t) = 108 \text{ kph} = 30 \text{ m/s}$, and $\tau_i = 1.5 \text{ s}$, the acceleration that driver i will adopt after a perception-reaction time is:

$$\begin{aligned} \ddot{x}(t + 1.5) &= \frac{0.51}{\text{s}} [30 - 20] \text{ m/s} \\ &= -5.1 \text{ m/s}^2. \end{aligned}$$

b (and c)

Using GM2 ($\ddot{x}(t + \tau_i) = \begin{pmatrix} \alpha_1 \\ \alpha_2 \end{pmatrix} [\dot{x}_{i-1}(t) - \dot{x}_i(t)]$), with $\alpha = 0.74$ gives:

$$\begin{aligned} \ddot{x}(t + 1.5) &= \frac{0.74}{\text{s}} [30 - 20] \text{ m/s} \\ &= -7.4 \text{ m/s}^2. \end{aligned}$$

d

Using GM3, with vehicle length $l_{i-1} = l_i = 6 \text{ m}$, vehicle spacing (front bumper to front bumper) $s_i = 40 \text{ m}$, and therefore $x_{i-1}(t) - x_i(t) = 40 - 6 = 34 \text{ m}$, and $\alpha = 10 \text{ m/s}$:

$$\begin{aligned} \ddot{x}(t + 1.5) &= 10 \frac{-10 \text{ m/s}}{34 \text{ m}} \\ &= -2.94 \text{ m/s}^2 \end{aligned}$$

e

GM4, with $\alpha = 0.5$:

$$\begin{aligned} \ddot{x}_i(t + 1.5) &= 0.5 \times \frac{30 \times (20 - 30)}{34} \\ &= -4.41 \text{ m/s}^2 \end{aligned}$$

f

GM5, with $\alpha = 0.5$, $l = 2$, and $m = 2$:

$$\begin{aligned}\ddot{x}_i(t + 1.5) &= 0.5 \times \frac{30^2 \times (20 - 30)}{34^2} \\ &= -3.89 \text{ m/s}^2\end{aligned}$$