

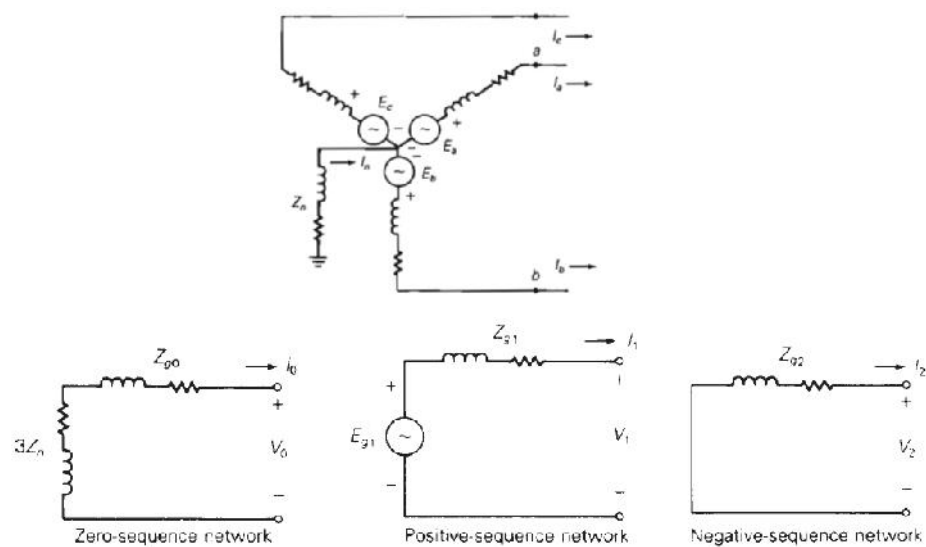
EE493 Protection of Power Systems I

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Chapter 8 of “Power System Analysis and Design”, Fifth Edition, 2012, J. D. Glover, M. S. Saema, T. J. Overbye

SEQUENCE NETWORKS OF ROTATING MACHINES



Sequence networks of a Y-connected synchronous generator

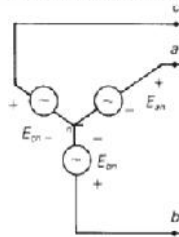
It is assumed generator is balanced and E_{g1} (positive sequence voltage). $=E_{an}$ (phase to neutral voltage). Therefore, if line-line voltage is give, you should calculate line-neutral voltage

$$E_{an} = \frac{E_{ab} \angle -30}{\sqrt{3}}$$

Reminder:

Always in balanced three-phase systems line to line voltages are $\sqrt{3}$ Times bigger than line to ground voltages and they lead the line to ground voltages by 30 degrees

It can be seen by looking at the following example



$$E_{an} = 10 \angle 0^\circ$$

$$E_{bn} = 10 \angle -120^\circ = 10 \angle +240^\circ$$

$$E_{cn} = 10 \angle +120^\circ = 10 \angle -240^\circ \text{ volts}$$

Now if we calculate line to line voltage for phases a and b:

$$E_{ab} = E_{an} - E_{bn}$$

$$E_{ab} = 10 \angle 0^\circ - 10 \angle -120^\circ = 10 - 10 \left[\frac{-1 - j\sqrt{3}}{2} \right]$$

$$E_{ab} = \sqrt{3}(10) \left(\frac{\sqrt{3} + j1}{2} \right) = \sqrt{3}(10 \angle 30^\circ) \text{ volts}$$

It shows that E_{ab} is $\sqrt{3}$ times bigger than E_{an} and leads E_{an} by 30 degrees

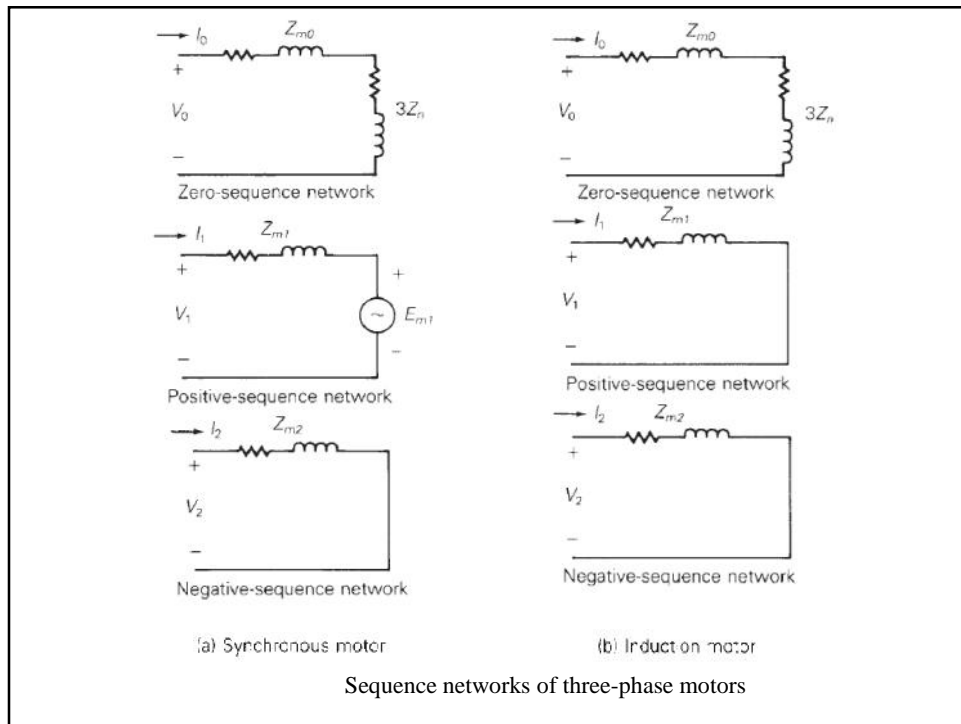
The voltage drop in the generator neutral impedance is $Z_n I_n$, which can be written as $(3Z_n)I_0$, since the neutral current is three times the zero-sequence current.

$$I_n = I_a + I_b + I_c$$

$$I_0 = \frac{1}{3}(I_a + I_b + I_c)$$

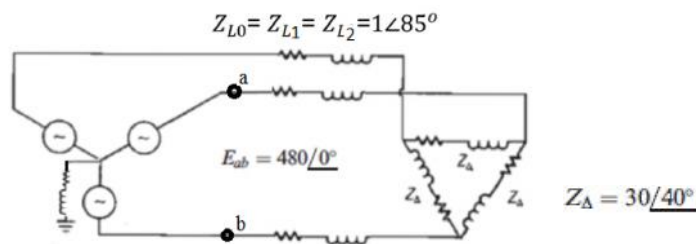
$$I_n = 3I_0$$

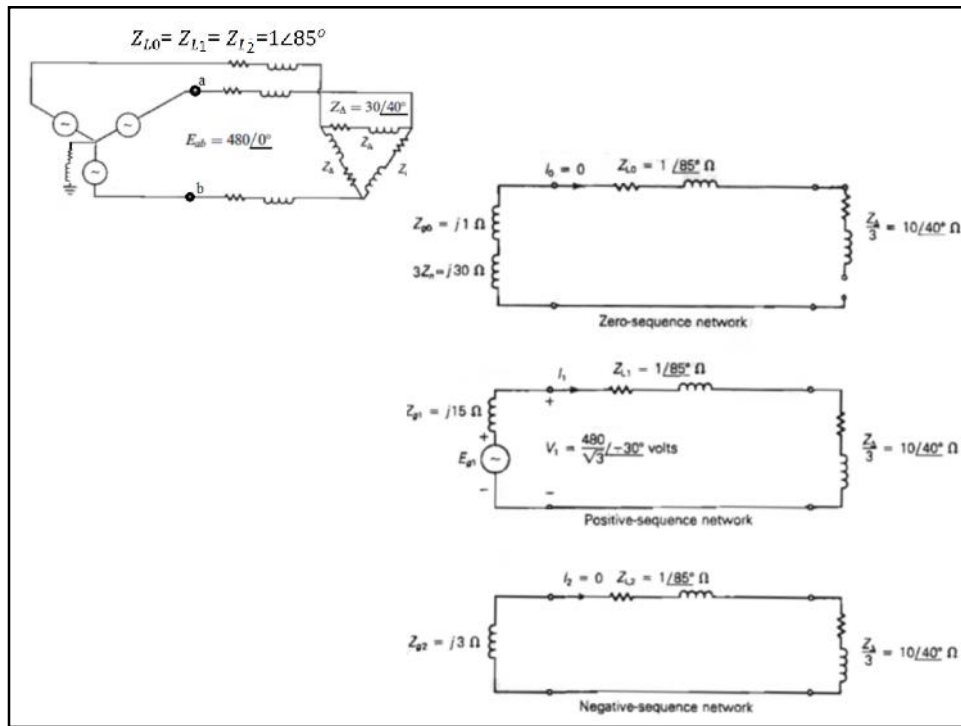
Since this voltage drop is due only to zero-sequence current, an impedance $(3Z_n)$ is placed in the zero-sequence network in series with the generator zero-sequence impedance Z_{g0} .



EXAMPLE

calculate the sequence components of the line current. Assume that the generator neutral is grounded through an impedance $Z_n = j10 \Omega$, and that the generator sequence impedances are $Z_{g0} = j1 \Omega$, $Z_{g1} = j15 \Omega$, and $Z_{g2} = j3 \Omega$.





It is clear that $I_0 = I_2 = 0$ since there are no sources in the zero- and negative-sequence networks. Also, the positive-sequence generator terminal voltage V_1 equals the generator line-to-neutral terminal voltage. Therefore, from the positive-sequence network

$$I_1 = \frac{V_1}{(Z_{L1} + \frac{1}{3}Z_{\Delta})} = 25.83 \angle -73.78^\circ \text{ A} = I_\phi$$

$$\begin{bmatrix} I_a \\ I_b \\ I_c \end{bmatrix} = \begin{bmatrix} 1 & 1 & 1 \\ 1 & a^2 & a \\ 1 & a & a^2 \end{bmatrix} \begin{bmatrix} I_0 \\ I_1 \\ I_2 \end{bmatrix}$$

I_1 equals the line current I_a , since $I_0 = I_2 = 0$.