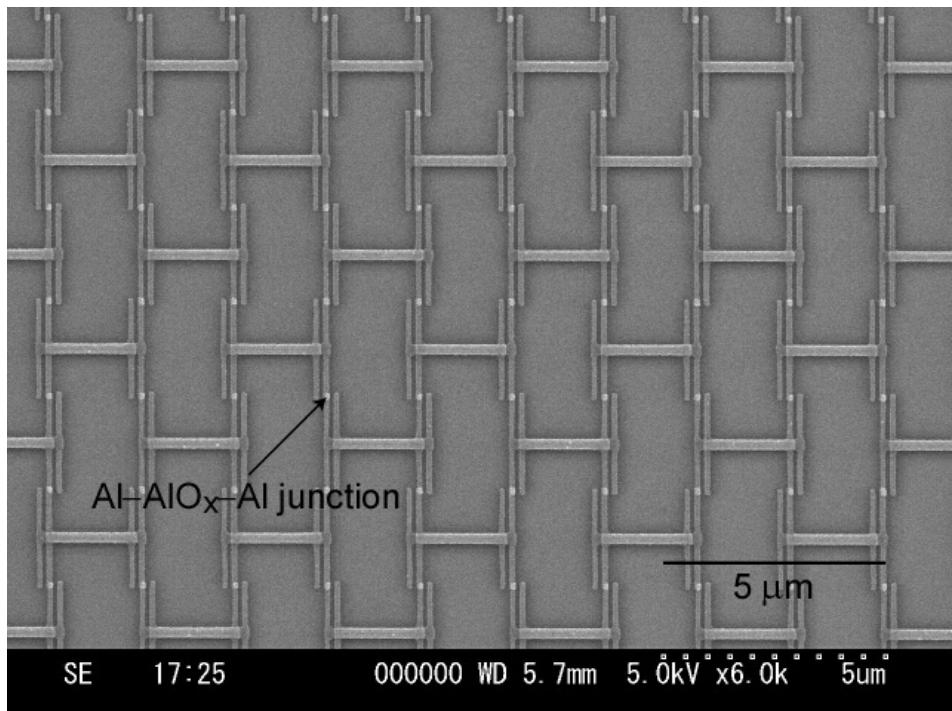


Synchrony and stability in electric power systems (and Josephson Junction arrays)

Philippe Jacquod
ECS14 - mpipks Dresden - 22.09.2014

Josephson junction arrays vs. electric power systems ?

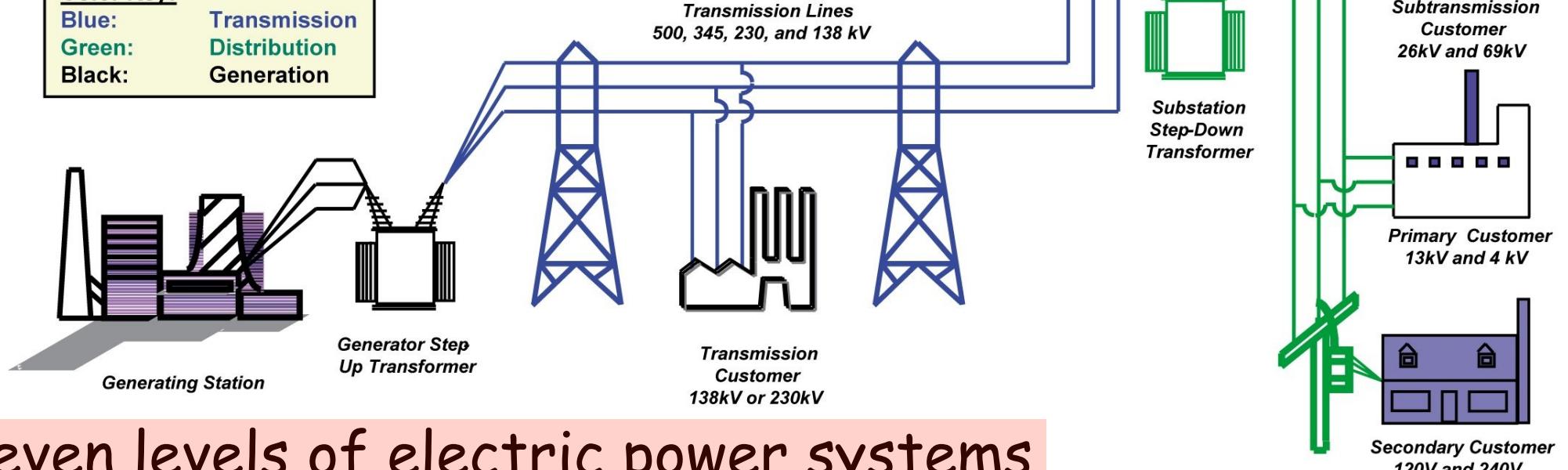


Takahide, Yagi, Kanda, Ootuka, and Kobayashi
Phys. Rev. Lett. 85, 1974 (2000)

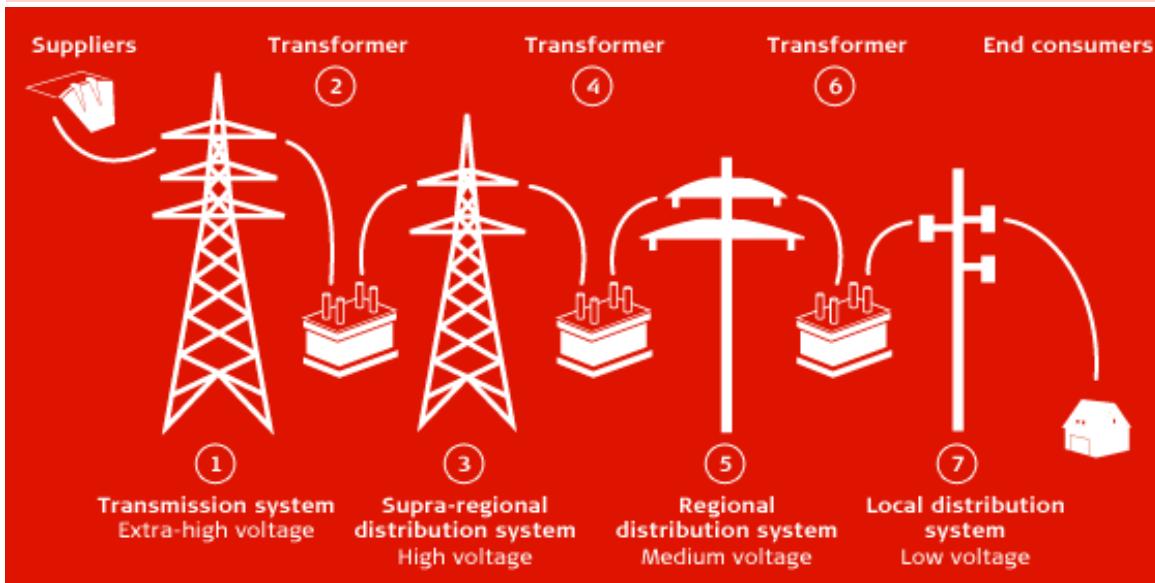
What are electric power systems ?

Basic Structure of the Electric System

| Color Key: | |
|------------|--------------|
| Blue: | Transmission |
| Green: | Distribution |
| Black: | Generation |



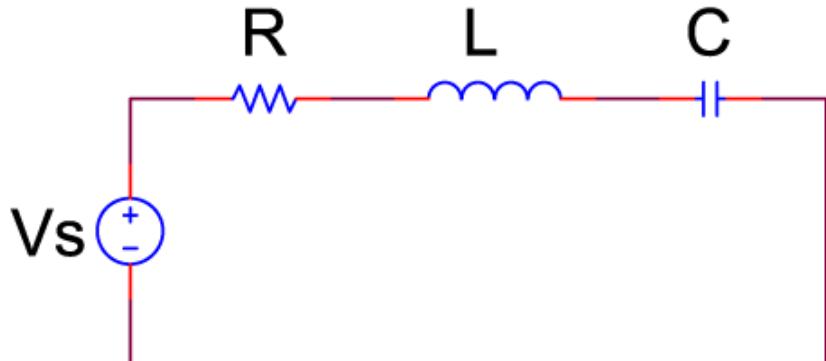
Seven levels of electric power systems



Power is ~conserved
i.e. write Eq. for power

What are electric power systems ?

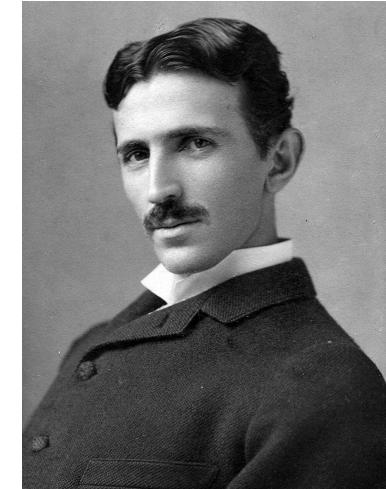
- AC electric current/voltages
(minimize losses ~ high voltages,
but then need transformers)
- current and voltage not in phase



$$u(t) = u_0 \exp[i\omega t]$$

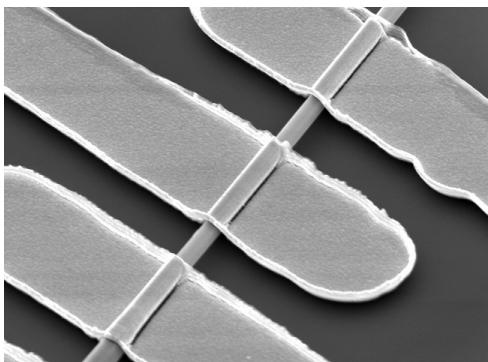
$$i(t) = i_0 \exp[i(\omega t + \phi)]$$

$$\tan(\phi) = (\omega L - 1/\omega C)/R$$

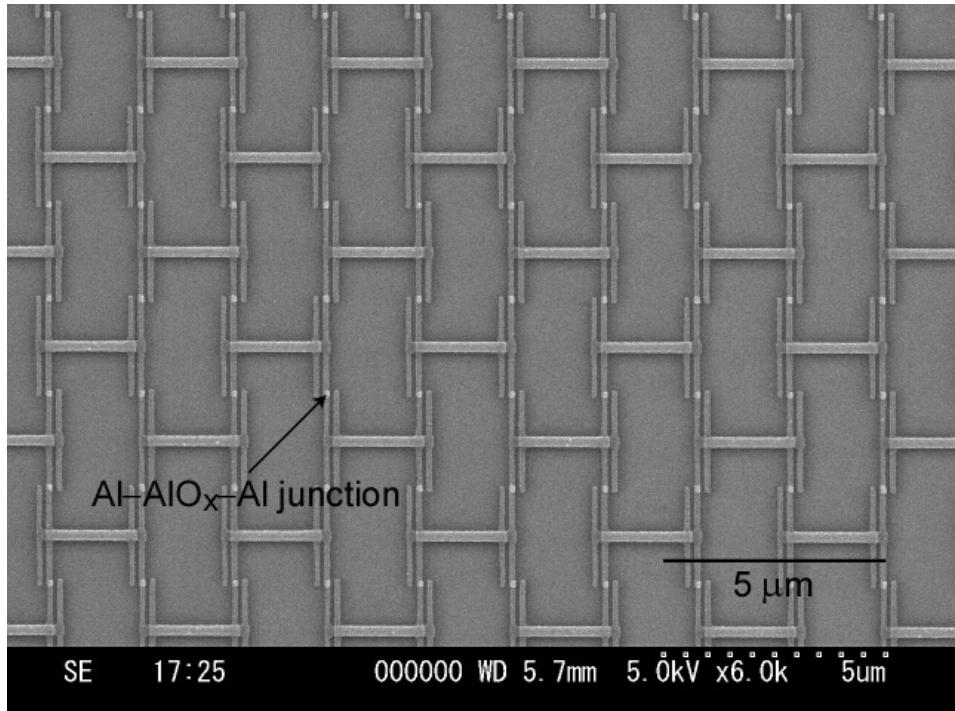


N Tesla 1856-1943

- complex impedance $u(\omega) = Z(\omega) i(\omega)$ $Z(\omega) = R + i\omega L - i/\omega C$
- inductance more important than resistance for large conductors



Josephson junction arrays vs. electric power systems !



Josephson current

$$I_{ij} = I_c \sin(\theta_j - \theta_i)$$

Transmitted power

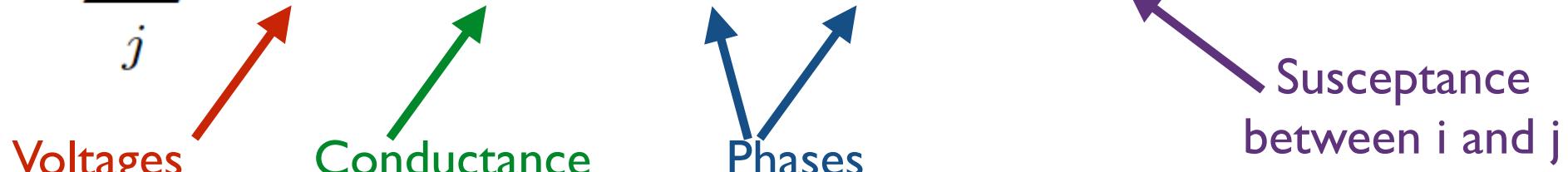
$$P_{ij} \simeq |V_i V_j| K_{ij} \sin(\theta_j - \theta_i)$$

Power flow equations

- Three-phase system (AC)
- Symmetric (all phases with same amplitude+phase)
- Power grid/network with buses (nodes) and lines
- Buses characterized by voltage, current and relative phase
- Active and reactive power injected/extracted

$$P_i = \sum_j |V_i V_j| [G_{ij} \cos(\theta_j - \theta_i) + K_{ij} \sin(\theta_j - \theta_i)]$$

$$Q_i = \sum_j |V_i V_j| [G_{ij} \sin(\theta_j - \theta_i) - K_{ij} \cos(\theta_j - \theta_i)]$$



Voltages at buses i and j Conductance between i and j Phases at buses i and j Susceptance between i and j

Power flow equations (power is conserved upon voltage transformation)

$$P_i = \sum_j |V_i V_j| [G_{ij} \cos(\theta_j - \theta_i) + K_{ij} \sin(\theta_j - \theta_i)]$$

$$Q_i = \sum_j |V_i V_j| [G_{ij} \sin(\theta_j - \theta_i) - K_{ij} \cos(\theta_j - \theta_i)]$$

- These equations ***must*** be obeyed at any time for steady-state operation of the electric power network
- Voltages (+-), G's and K's are fixed

Power flow equations - linear regime

- inductance more important for large conductors

$$P_i \simeq \sum_j |V_i V_j| K_{ij} \sin(\theta_j - \theta_i)$$

- linear regime

$$P_i \simeq \sum_j |V_i V_j| K_{ij} (\theta_j - \theta_i)$$

- i.e. analogous to Landauer-Büttiker

$$I_i = \frac{2e^2}{h} \sum_j G_{ij} (V_j - V_i)$$

Note (important) :

$$\sum_i P_i = \sum_{ij} G_{ij} \cos(\theta_j - \theta_i)$$

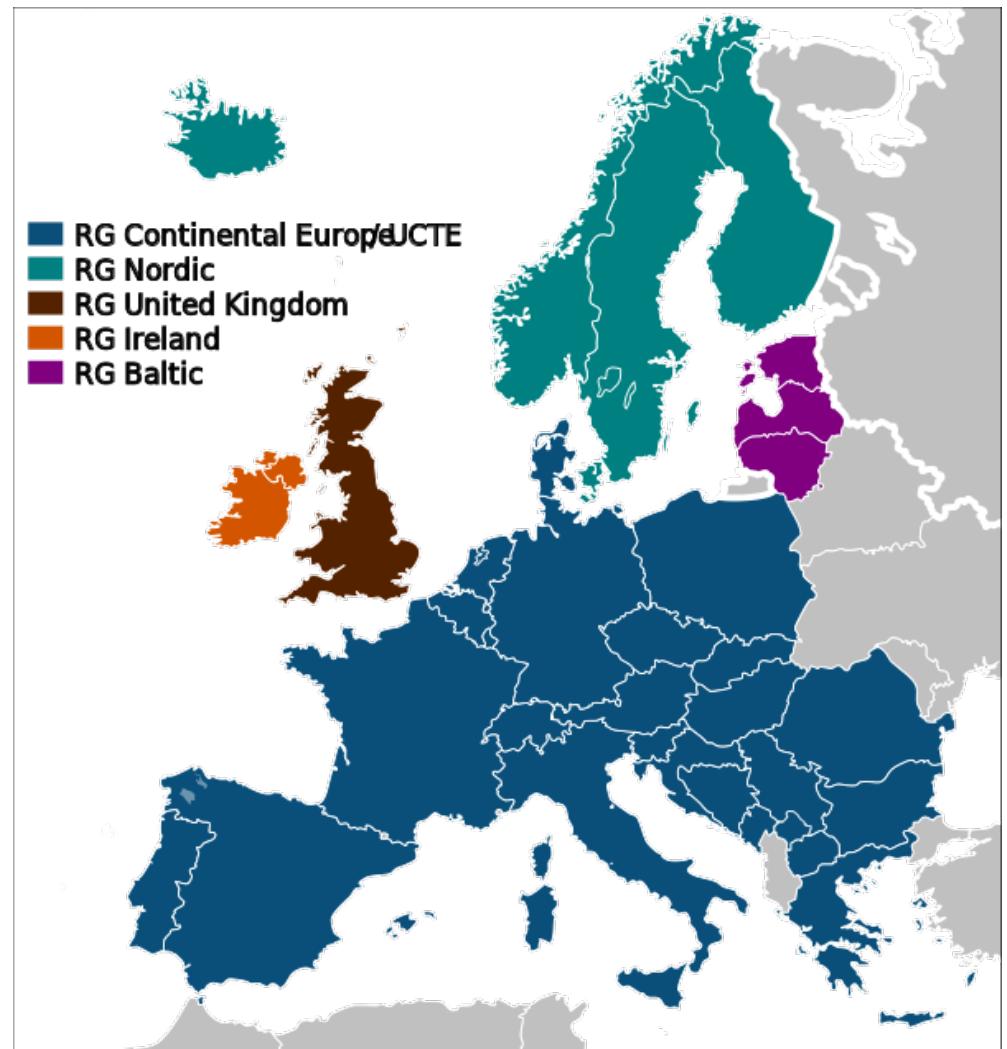
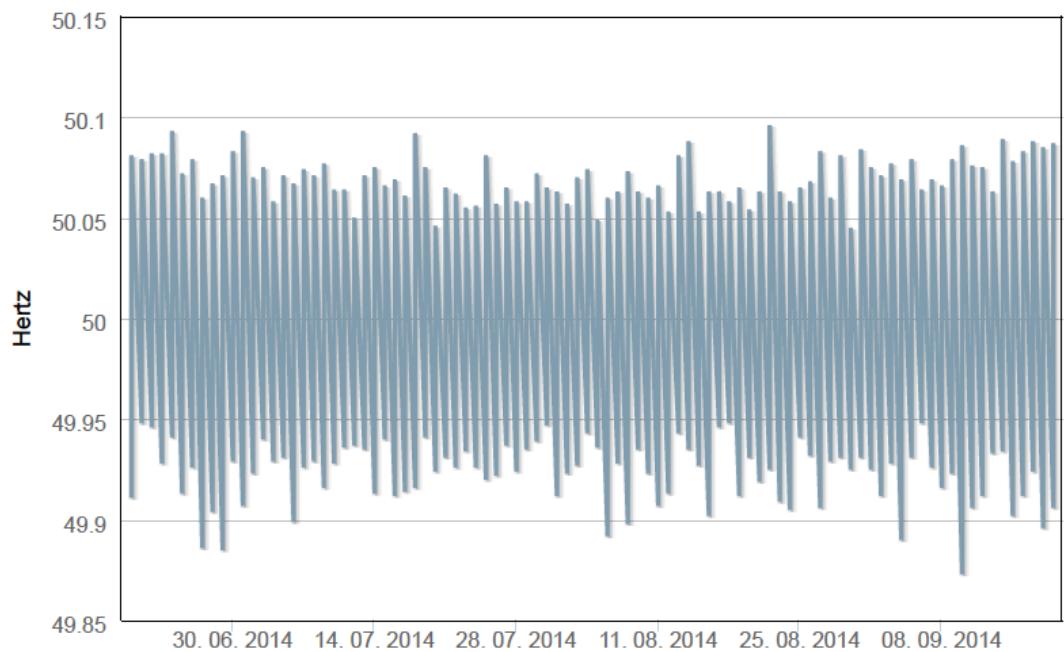


Note: current conservation

$$\sum_j K_{ij} = 0$$

$$\sum_j G_{ij} = 0$$

Steady-state operation : synchrony over 1000's of kms

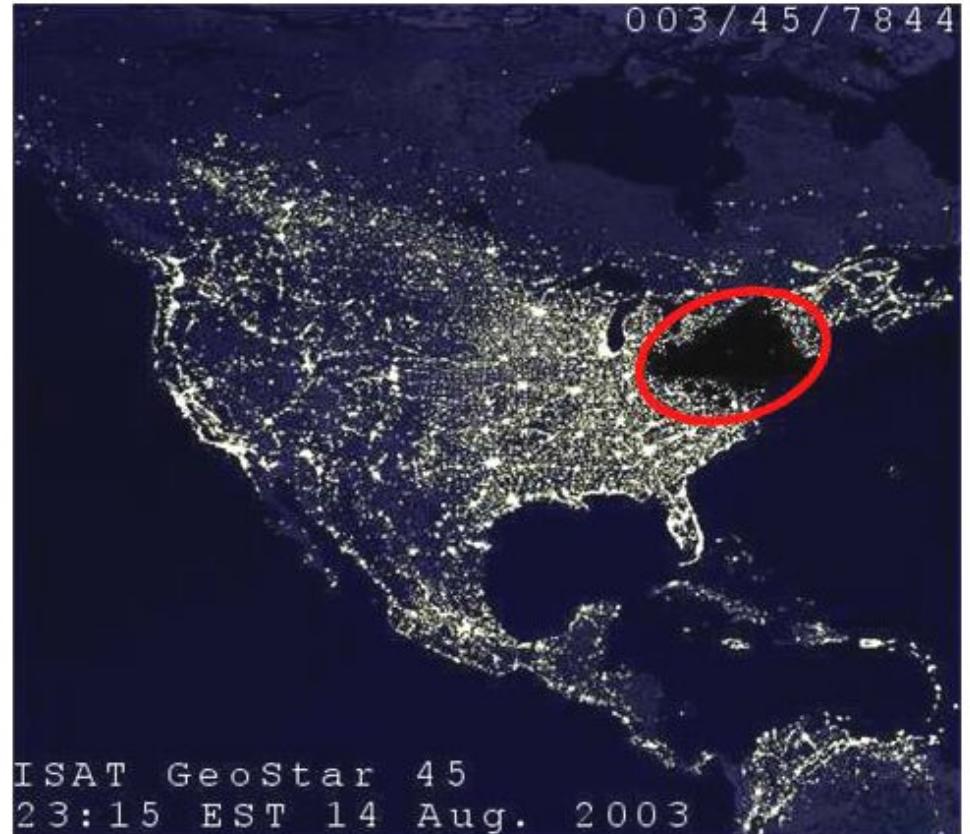


Loss of synchrony : blackouts

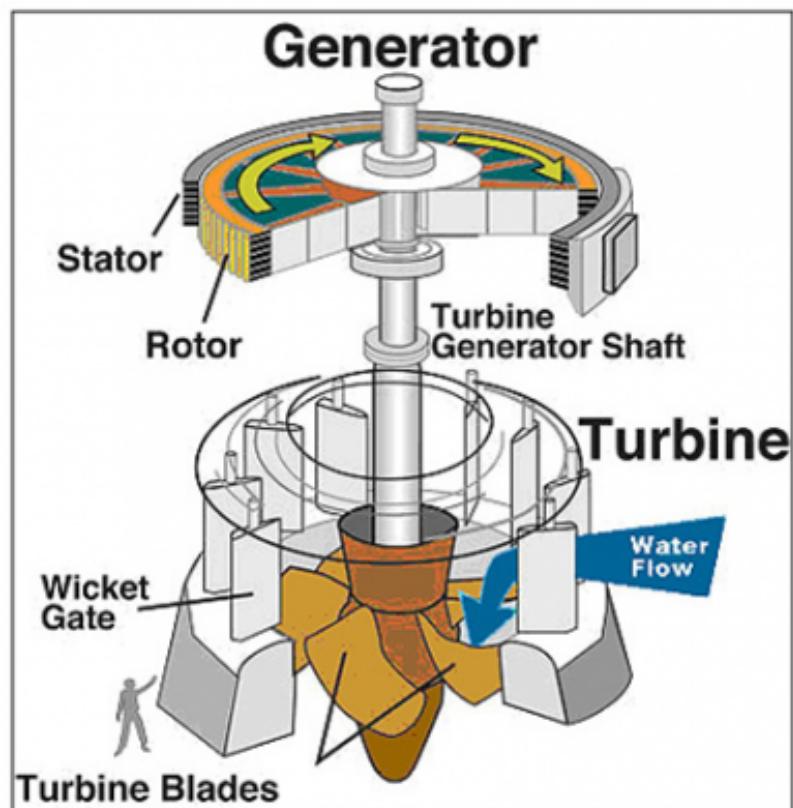
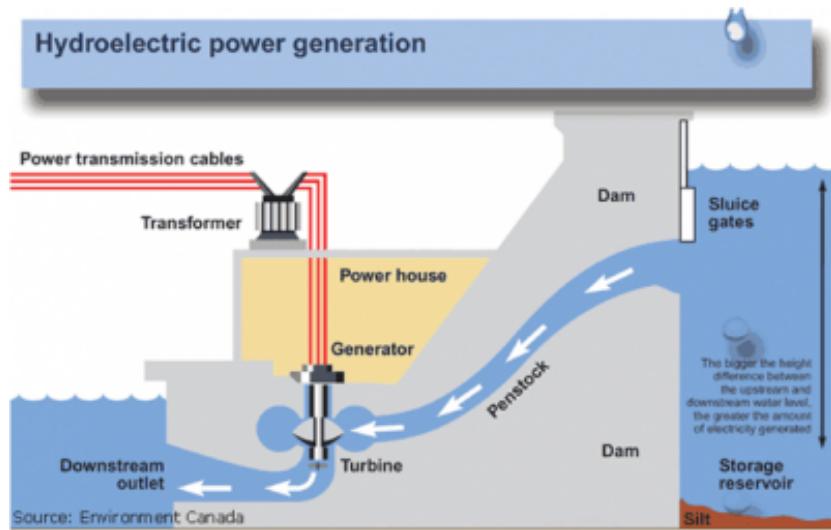
Italy blackout, sep 28 2003



Northeast blackout, aug 14 2003



Time-evolution of frequency : swing equations



- Electricity production with rotating machines
- Potential, chemical, nuclear or thermal energy converted into mechanical energy (rotation)
- Mechanical power converted into electric power
- Time-dependence : think power instead of energy
- Balance between power in, power out and energy change in rotator : **SWING EQUATIONS**

Time-evolution of frequency : swing equations

- Power balance

$$\frac{dW_i}{dt} + P_i^{(d)} = P_i^{(m)} - P_i^{(g)}$$

Change in KE of rotator

Damping power (losses from friction)

Power input

Electric power output

The diagram shows the power balance equation for a rotator. It consists of four terms: a red arrow pointing up to the first term $\frac{dW_i}{dt}$ labeled 'Change in KE of rotator'; a green arrow pointing up to the second term $P_i^{(d)}$ labeled 'Damping power (losses from friction)'; a blue arrow pointing up to the third term $P_i^{(m)}$ labeled 'Power input'; and a purple arrow pointing down to the fourth term $-P_i^{(g)}$ labeled 'Electric power output'.

- Swing equation for angles

$$\alpha \frac{d^2\theta_i}{dt^2} + \frac{d\theta_i}{dt} = P_i - \sum_j K_{ij} \sin(\theta_j - \theta_i)$$

From inertia of rotator

Damping / friction

The diagram shows the swing equation for angles. It consists of several terms: a red arrow pointing up to the first term $\alpha \frac{d^2\theta_i}{dt^2}$ labeled 'From inertia of rotator'; a green arrow pointing up to the second term $\frac{d\theta_i}{dt}$ labeled 'Damping / friction'; a blue arrow pointing up to the third term P_i labeled 'Power input'; and a purple arrow pointing down to the fourth term $-\sum_j K_{ij} \sin(\theta_j - \theta_i)$ labeled 'Interaction with other rotators'.

Coupled oscillators and synchronization

Neglect $\alpha \frac{d^2\theta_i}{dt^2}$

$$\frac{d\theta_i}{dt} = P_i - \sum_j K_{ij} \sin(\theta_j - \theta_i)$$

frequency of oscillator #i free frequency of oscillator #i coupling between i and j (periodic in angle)

Ubiquitous model :

- biology (heart; brain; crickets; fireflies)
- physics (lasers; Josephson junctions)
- engineering (power systems)



C Huygens 1629-1695

Coupled oscillators and synchronization

$$\frac{d\theta_i}{dt} = P_i - \sum_j K_{ij} \sin(\theta_j - \theta_i)$$

frequency of oscillator #i free frequency of oscillator #i coupling between i and j (periodic in angle)

Different types of spontaneous synchrony

- phase/angle synchrony
- frequency synchrony



Gauge invariance : physicists do not care about phase/angle synchrony... or do they ? C Huygens 1629-1695

Coupled oscillators and synchronization

$$\frac{d\theta_i}{dt} = P_i - \sum_j K_{ij} \sin(\theta_j - \theta_i)$$

- Winfree (1967) : do mean field theory
- Kuramoto (1984)

(i) $K_{ij}=K/N$

i.e. all oscillators (nodes; buses) coupled to each other with same coupling

(ii) Introduce order parameter

$$r(t) = \left| \frac{1}{N} \sum_j \exp[i\theta_j(t)] \right| = |r(t)| \exp[i\Psi(t)]$$

Coupled oscillators and synchronization

$$\frac{d\theta_i}{dt} = P_i - \sum_j K_{ij} \sin(\theta_j - \theta_i)$$

- Kuramoto model $K_{ij}=K/N$

mean field justified, i.e.

$$\frac{d\theta_i}{dt} = P_i - Kr \sin(\Psi - \theta_i)$$

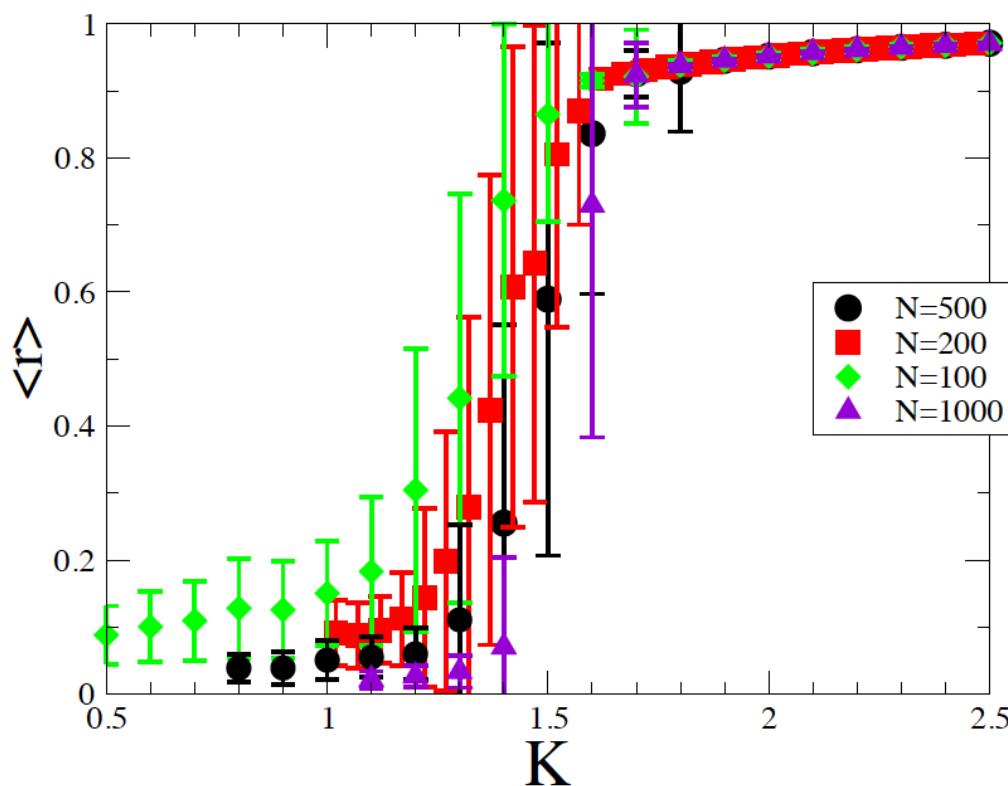
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Coupled oscillators and synchronization

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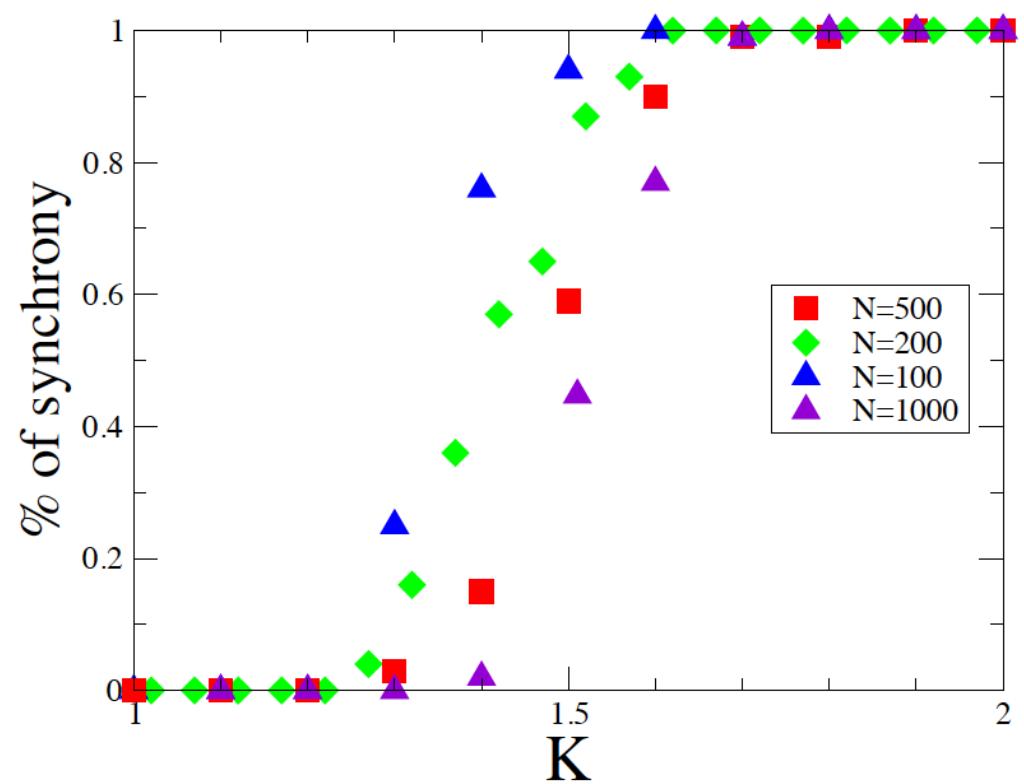
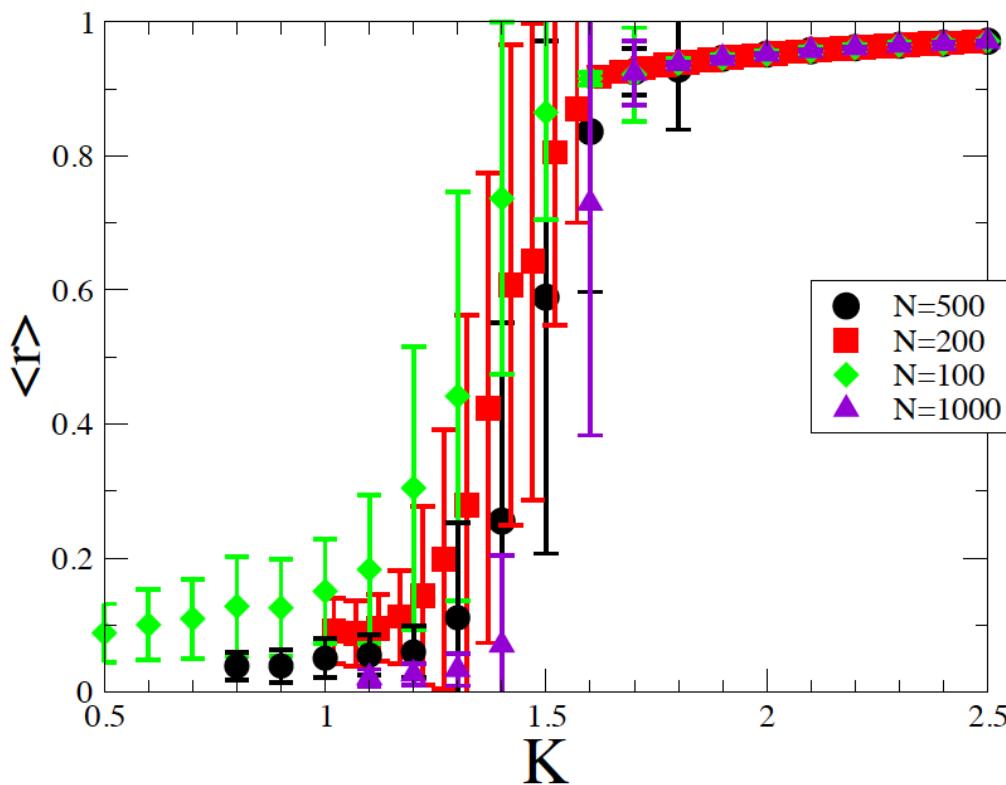
Theoretical threshold
for spontaneous synchrony:
 $K_c = 4/\pi$ (Kuramoto)

Coupled oscillators and synchronization

$$\alpha \frac{d^2\theta_i}{dt^2} + \frac{d\theta_i}{dt} = P_i - \sum_j K_{ij} \sin(\theta_j - \theta_i)$$

- Kuramoto model $K_{ij}=K/N$

order parameter vs. frequency locking !

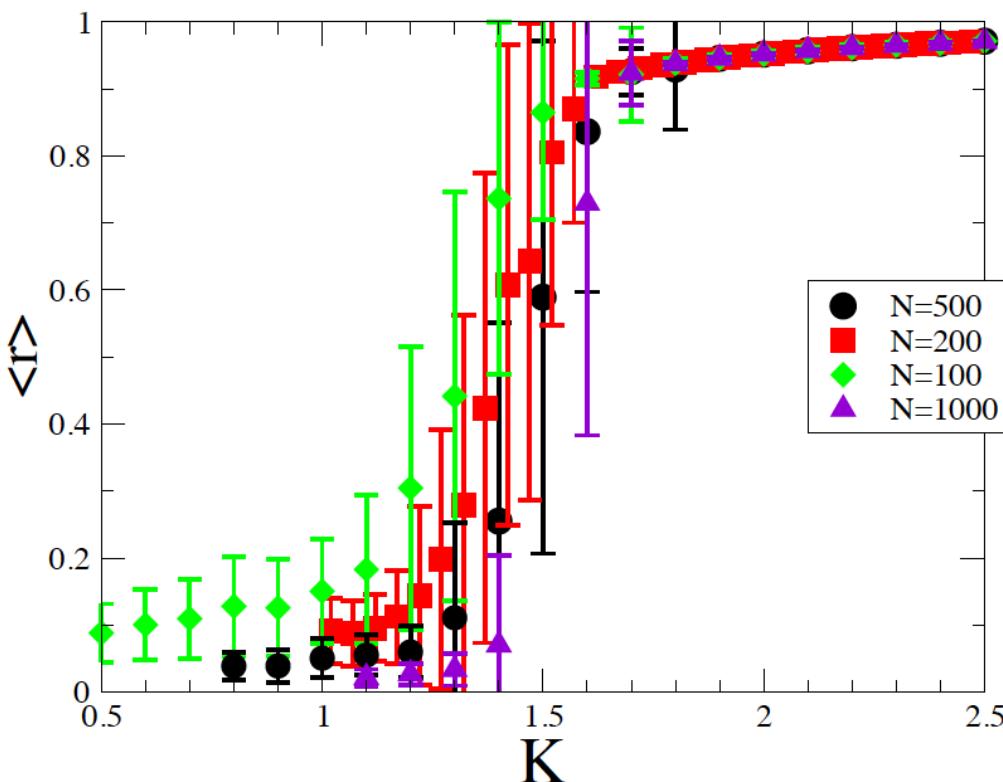


Coupled oscillators and synchronization

$$\alpha \frac{d^2\theta_i}{dt^2} + \frac{d\theta_i}{dt} = P_i - \sum_j K_{ij} \sin(\theta_j - \theta_i)$$

- Kuramoto model $K_{ij}=K/N$

$$r(t) = \left| \frac{1}{N} \sum_j \exp[i\theta_j(t)] \right| = |r(t)| \exp[i\Psi(t)]$$



- phase synchrony for $r > 0.8$
- phase synchrony and frequency synchrony

? WHY ?

Coupled oscillators, synchronization and stability

$$\alpha \frac{d^2\theta_i}{dt^2} + \frac{d\theta_i}{dt} = P_i - \sum_j K_{ij} \sin(\theta_j - \theta_i)$$

- suppose a synchronized solution exists
- what is its stability under angle perturbation ?
A.: linearize the dynamics about that solution

$$\frac{d\delta\theta_i}{dt} = - \sum_j K_{ij} \cos[\theta_j^{(0)} - \theta_i^{(0)}] (\delta\theta_j - \delta\theta_i)$$

Coupled oscillators, synchronization and stability

$$\frac{d\theta_i}{dt} = P_i - \sum_j K_{ij} \sin(\theta_j - \theta_i)$$

- suppose a synchronized solution exists
- what is its stability ?

A.: linearize the dynamics about that solution

$$\frac{d\delta\vec{\theta}}{dt} = -\underline{\kappa}(\vec{\theta}^{(0)}) \delta\vec{\theta}$$

stability/instability vs. eigenvalues of $\underline{\kappa}(\vec{\theta}^{(0)})$

Properties of the stability matrix

$$\frac{d\delta\vec{\theta}}{dt} = -\underline{\kappa}(\vec{\theta}^{(0)}) \delta\vec{\theta}$$

Depends on network and synchronous solution

$$\kappa_{ij} = \delta_{ij} \sum_k K_{ik} \cos(\theta_k^{(0)} - \theta_i^{(0)}) - K_{ij}(1 - \delta_{ij}) \cos(\theta_j^{(0)} - \theta_i^{(0)})$$

- one e-value = 0 (~current conservation/gauge invariance)
- all e-values positive if, for all i,j $\cos(\theta_j - \theta_i) \geq 0$
- if, for all i,j $\cos(\theta_j - \theta_i) = 1$

| | |
|---|---|
| <ul style="list-style-type: none">• if, for all i,j $\cos(\theta_j - \theta_i) = 1$ and connectivity $C > N$ | <p>e-values =0 1-fold</p> <hr/> <p>=KN (N-1)-fold</p> <hr/> <p>e-values =0 1-fold</p> <p>=KC (N-1)-fold</p> |
|---|---|

Properties of the stability matrix

$$\frac{d\vec{\theta}}{dt} = -\underline{\kappa}(\vec{\theta}^{(0)}) \delta\vec{\theta}$$

Depends on network and synchronous solution

- Qualitatively :
 1. no negative e-value = stability for $\cos(\theta_j - \theta_i) \geq 0$
 2. smaller positive e-values = less (but still) stable for lesser connectivity
 3. smaller line capacity/coupling requires larger angle differences to carry fixed power current ~ less stable
 4. when angles differ by more than 90° , instability sets in and synchronous solutions cease to exist

CONNECTION BETWEEN ANGLE AND FREQUENCY SYNCHRONY

General strategy :

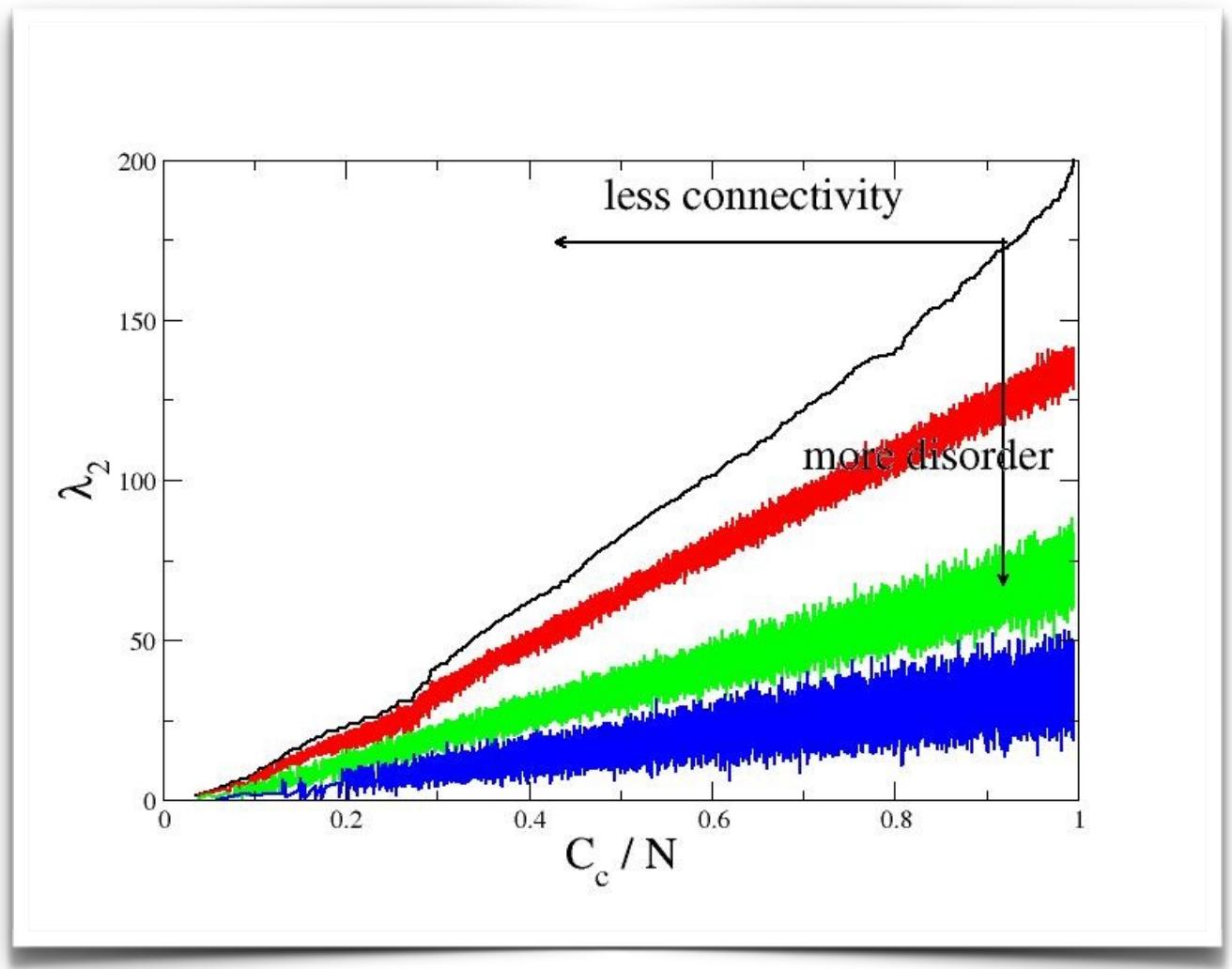
- (i) investigate the properties of the stability matrix vs. the distribution of angles
- (ii) understand the distribution of angles in synchrony vs. properties of the network/grid

Note: order parameter at synchrony
vs. variance of angle distributions

$$r_\infty \simeq [1 - \text{var}(\theta)/2]$$

Properties of the stability matrix : stability regime

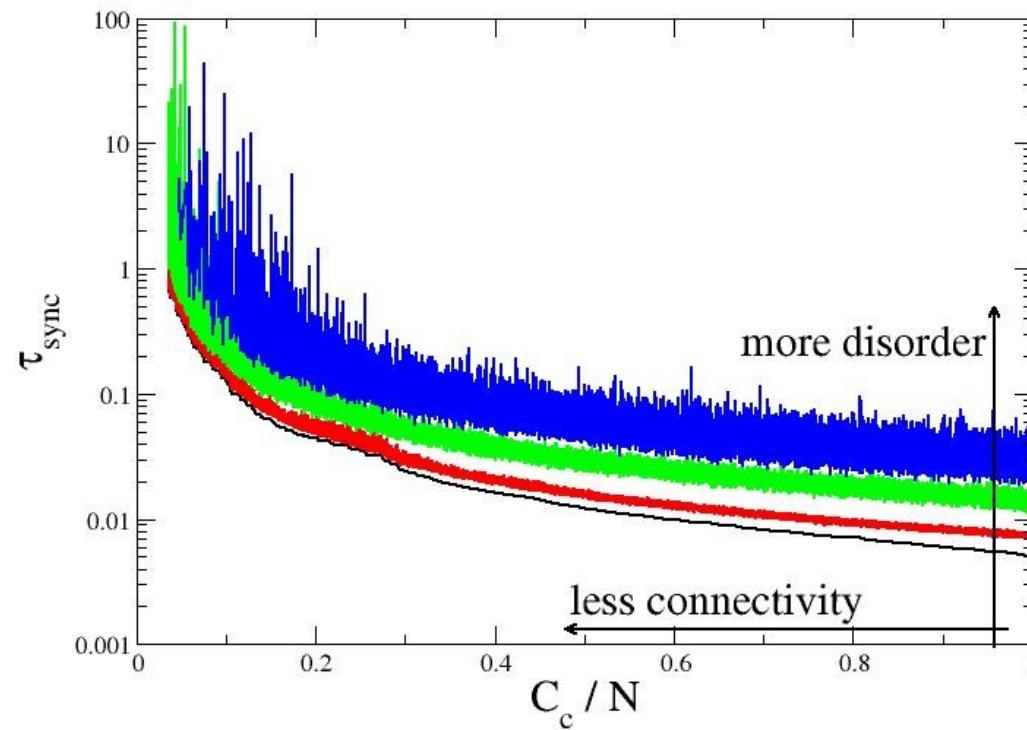
- Degree of stability determined by second smallest (positive) e-value



$$\kappa_{ij} = \delta_{ij} \sum_k K_{ik} \cos(\theta_k^{(0)} - \theta_i^{(0)}) - K_{ij}(1 - \delta_{ij}) \cos(\theta_j^{(0)} - \theta_i^{(0)})$$

Properties of the stability matrix : stability regime

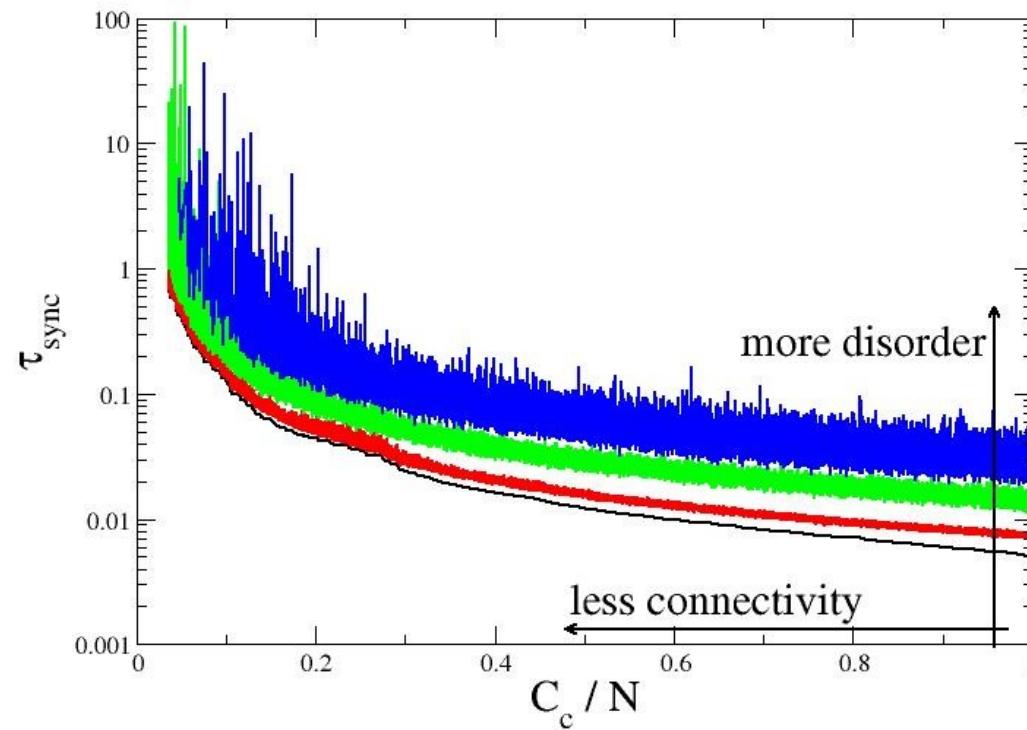
- Re-synchronization time (after perturbation) $\tau_{\text{sync}} = \lambda_2^{-1}$



- Re-synchronization time increases with
 - increasing disorder (variance of angles)
 - decreasing network connectivity

Properties of the stability matrix : stability regime

- Re-synchronization time (after perturbation) $\tau_{\text{sync}} = \lambda_2^{-1}$



- Re-synchronization time fluctuations increase with
 - increasing disorder (variance of angles)
 - decreasing network connectivity

- The goal is to investigate stability / resynchronisation via a random matrix theory of the stability matrix
- Why *random* ?
(Angles are determined by network, frequencies, couplings...)
- Does this make any sense at all vs. true synchrony problem ?

- The goal is to investigate stability / resynchronisation via a random matrix theory of the stability matrix
- Why *random* ?
(Angles are determined by network, frequencies, couplings...)
- Does this make any sense at all vs. true synchrony problem ?

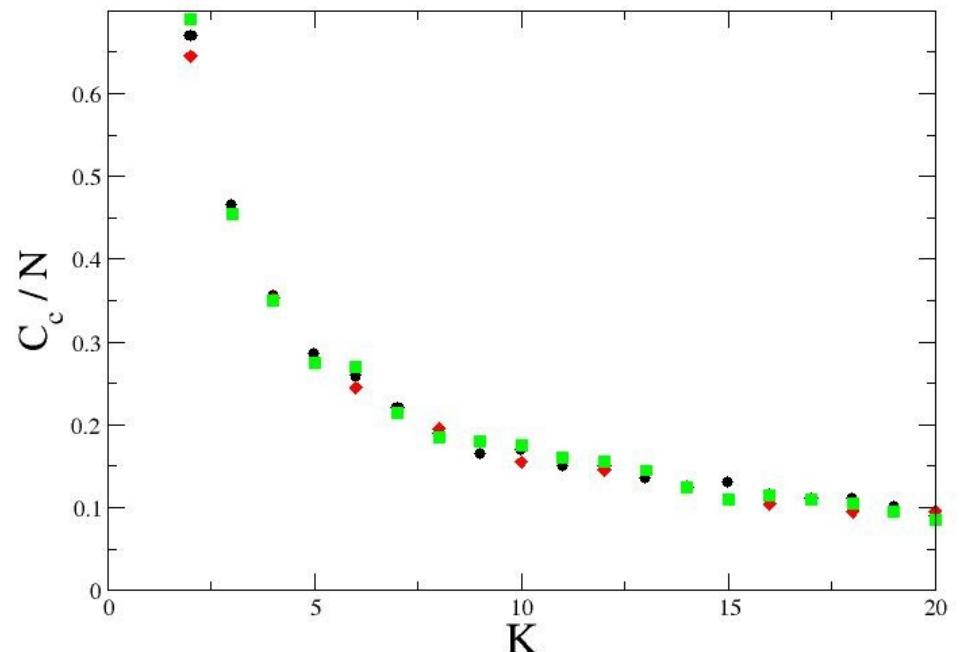
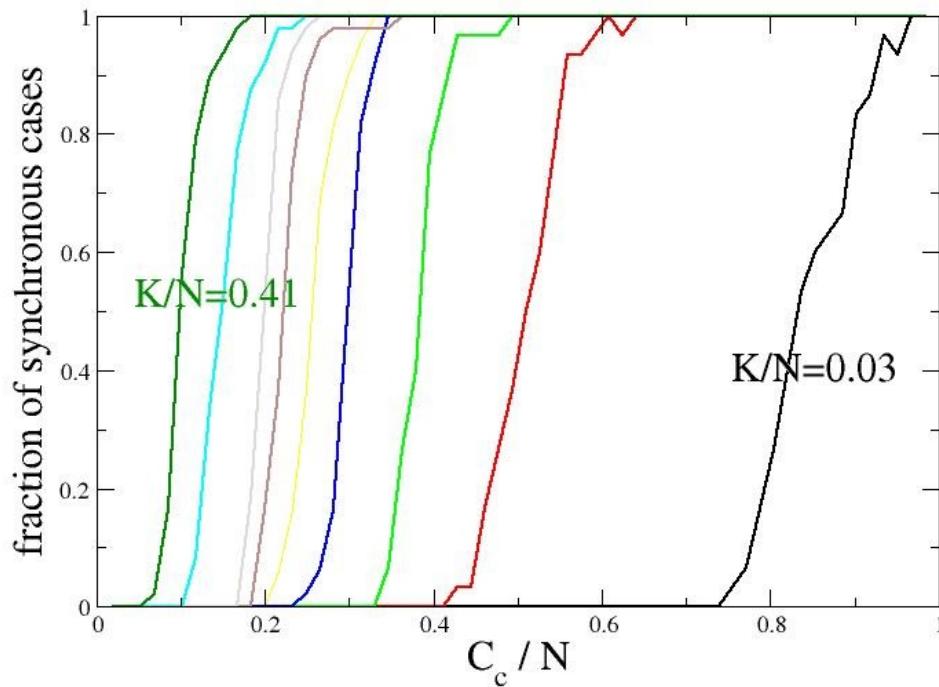
Back to original problem : damped, coupled oscillators

$$\alpha \frac{d^2\theta_i}{dt^2} + \frac{d\theta_i}{dt} = P_i - \sum_j K_{ij} \sin(\theta_j - \theta_i)$$

Some results

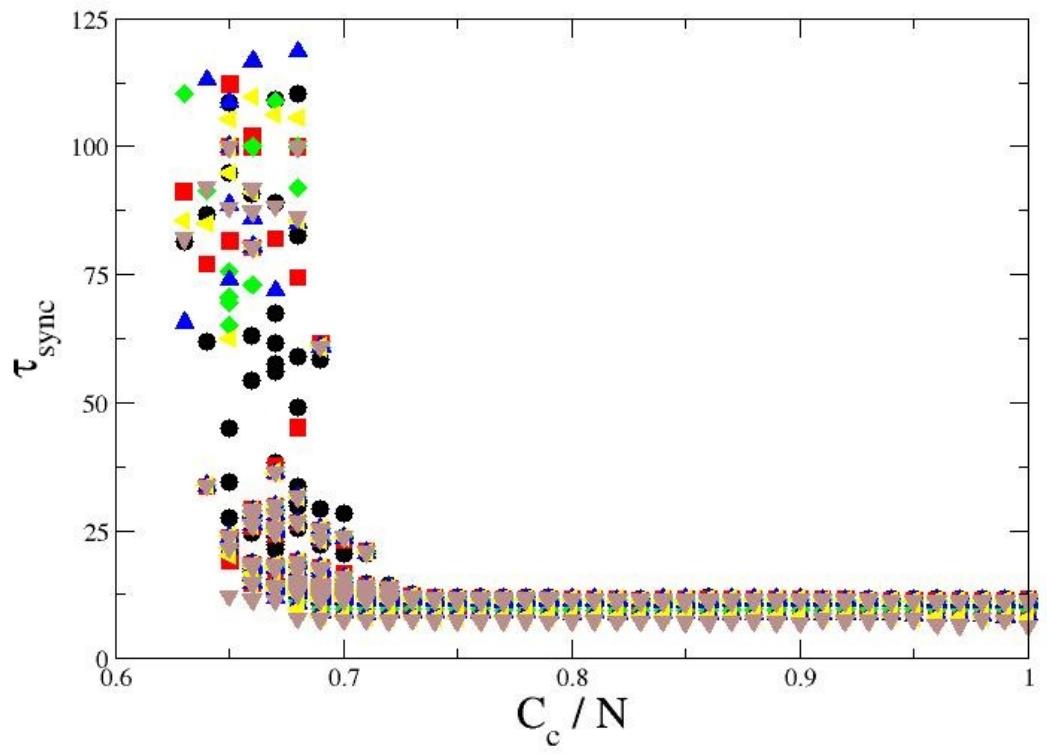
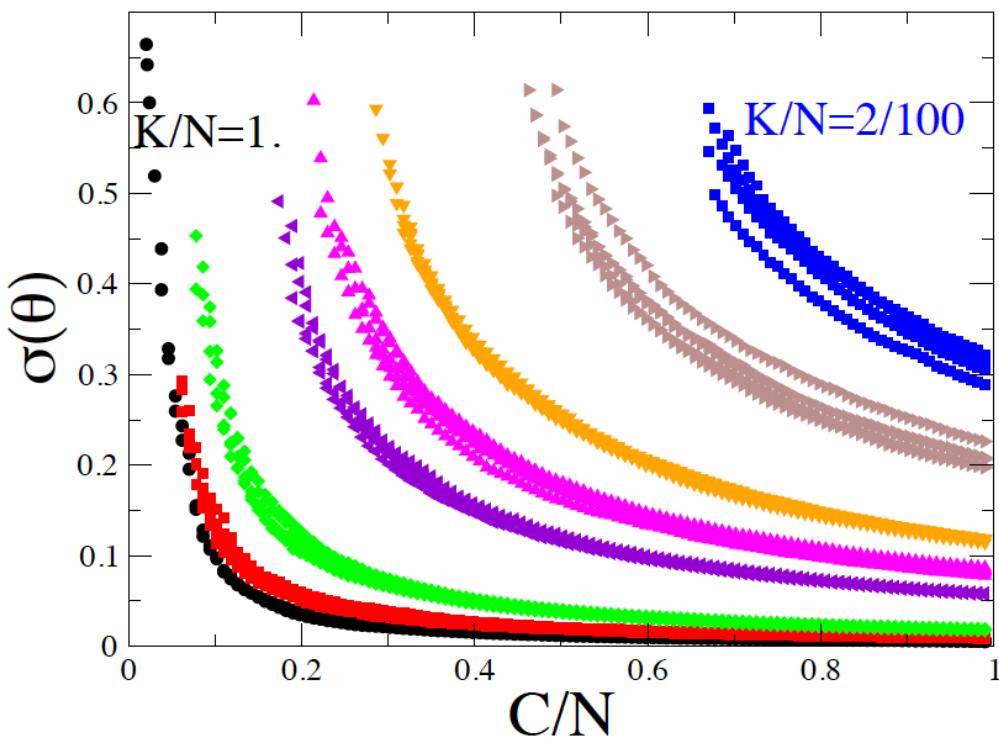
Harder to get spontaneous synchrony with

- smaller coupling (line capacity)
- less couplings (smaller connectivity)



Some results

All this seems to be related to broadening of angle distribution at synchrony and the associated increase in stability time !!



New route for understanding synchrony in coupled oscillators systems via distribution of angles at synchron

Towards a random matrix theory of electric power syste

Dedicated to

Quantum transport Quantum echoes

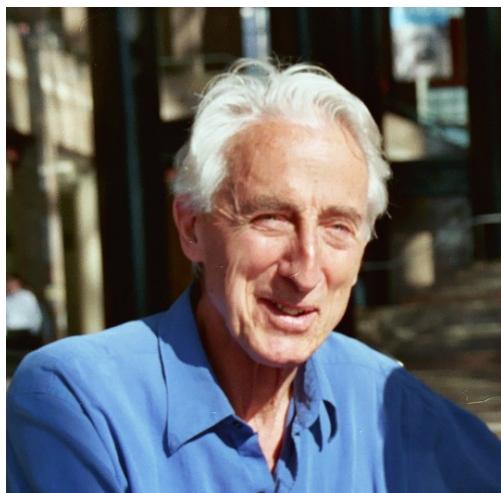


M Büttiker



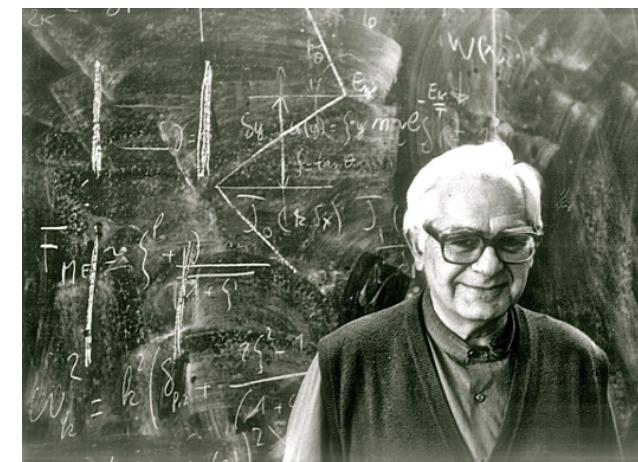
P Levstein

Semiclassical methods



M Gutzwiller

Random matrix theory



O Bohigas