

Discussion Week 11

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```
# Load needed libraries
library(tidyverse)
library(readr)
library(knitr)
library(sqldf)
```

Do other factors affect Home Run Distance besides exit velocity?

```
filename <- tempfile()
download.file("https://raw.githubusercontent.com/audiorunner13/Masters-Coursework/main/DATA605%20Fall%202021%20Data%20Set%201.csv", filename)
```

```
hr_stad_CFYS_2017 <- read.csv.sql(filename, "select TRUE_DISTANCE, EXIT_VELOCITY, ELEVATION_ANGLE, HORIZONTAL_ANGLE, APEX from hr_stad_CFYS_2017")
```

In my last discussion I am created a simple model to show if there is a direct correlation with the exit velocity of a ball hit out of the park and the distance that it travels. My conclusion was that there is. In this discussion I will add the other measures to determine if those also affect the distance of a homerun. I will limit the data to home runs hit out of Coors Field in Denver and Yankee Stadium for better clarity. The stadium will be my dichotomus variable.

```
coors_bp <- ifelse(hr_stad_CFYS_2017$BALLPARK == 'Coors Field', 1, 0)

(hr_stad_CFYS_2017_out <- data.frame(TRUE_DISTANCE = hr_stad_CFYS_2017$TRUE_DISTANCE, EXIT_VELOCITY = hr_stad_CFYS_2017$EXIT_VELOCITY, ELEVATION_ANGLE = hr_stad_CFYS_2017$ELEVATION_ANGLE, HORIZONTAL_ANGLE = hr_stad_CFYS_2017$HORIZONTAL_ANGLE, APEX = hr_stad_CFYS_2017$APEX, coors_bp = coors_bp))
```

##	TRUE_DISTANCE	EXIT_VELOCITY	ELEVATION_ANGLE	HORIZONTAL_ANGLE	APEX
## 1	387	106.6	25.9	121.8	69
## 2	397	98.8	29.5	78.4	91
## 3	420	106.1	27.5	71.3	86
## 4	487	118.9	25.0	103.2	104
## 5	408	104.6	23.8	80.0	69
## 6	424	102.3	33.2	94.9	124
## 7	428	104.1	30.5	78.2	107
## 8	429	108.7	32.5	61.4	112
## 9	362	97.2	38.6	62.6	121
## 10	365	96.5	24.7	80.0	66
## 11	392	104.7	27.7	60.5	76
## 12	392	104.3	26.1	66.9	71

## 13	417	110.6	19.9	82.9	60
## 14	423	103.0	26.6	92.5	90
## 15	427	112.6	26.3	118.2	82
## 16	349	96.3	27.3	65.4	68
## 17	358	97.5	29.8	116.7	81
## 18	372	97.5	34.6	70.8	113
## 19	390	99.5	32.5	102.2	112
## 20	412	102.7	34.8	107.3	124
## 21	428	106.8	25.5	99.5	87
## 22	389	101.1	26.3	73.1	73
## 23	431	110.7	24.8	106.2	83
## 24	453	109.5	24.4	94.8	85
## 25	366	110.0	21.2	124.1	49
## 26	376	100.2	28.1	68.5	80
## 27	384	98.7	31.1	74.1	99
## 28	385	98.5	31.4	79.0	107
## 29	401	105.4	33.8	99.9	144
## 30	404	102.1	31.1	104.0	109
## 31	426	106.9	26.0	104.5	83
## 32	346	93.8	31.5	62.4	80
## 33	377	98.6	32.0	66.3	95
## 34	432	110.7	19.7	93.3	65
## 35	390	108.0	23.9	63.8	63
## 36	390	103.6	34.2	77.1	138
## 37	366	94.1	33.8	79.1	105
## 38	437	108.4	27.0	101.8	100
## 39	442	109.4	31.7	112.1	117
## 40	363	97.1	30.4	70.0	92
## 41	379	97.9	33.0	63.2	95
## 42	390	102.9	24.3	76.1	69
## 43	404	106.6	27.8	66.4	89
## 44	423	105.1	24.3	93.3	85
## 45	431	109.6	26.1	110.9	81
## 46	432	114.7	37.7	65.8	171
## 47	351	100.8	24.5	62.2	59
## 48	375	100.1	33.9	64.2	108
## 49	410	103.1	28.6	79.0	101
## 50	419	109.6	25.9	116.3	75
## 51	432	103.3	31.1	97.1	113
## 52	367	97.5	32.5	64.4	94
## 53	374	102.8	37.6	117.1	134
## 54	381	106.6	22.2	70.7	56
## 55	417	105.7	24.6	79.9	78
## 56	420	102.9	26.8	87.0	92
## 57	431	104.1	28.6	92.0	106
## 58	440	117.2	23.6	115.7	72
## 59	407	101.7	29.4	73.6	91
## 60	425	106.8	32.8	115.3	113
## 61	456	112.8	30.2	65.3	109
## 62	422	107.6	30.9	120.4	97
## 63	409	104.5	30.1	61.5	89
## 64	415	106.1	28.5	62.7	83
## 65	434	104.6	27.4	80.8	90
## 66	365	97.3	29.3	122.9	70

## 67	370	98.4	28.9	118.6	70
## 68	374	106.6	22.3	113.4	54
## 69	396	98.6	35.9	70.0	116
## 70	413	102.6	28.0	94.0	104
## 71	425	103.5	32.6	106.6	113
## 72	468	119.9	22.5	106.5	77
## 73	379	101.6	34.2	111.5	120
## 74	427	109.4	30.6	108.2	120
## 75	436	105.4	24.8	88.9	80
## 76	380	101.8	26.9	117.0	68
## 77	381	98.7	36.6	64.8	117
## 78	404	104.1	27.4	72.3	85
## 79	415	106.3	22.4	83.8	69
## 80	367	95.1	30.4	76.7	89
## 81	394	102.8	34.7	77.5	135
## 82	355	96.9	35.6	118.3	108
## 83	356	96.6	33.4	59.4	93
## 84	402	100.3	30.0	80.8	102
## 85	406	104.8	37.4	106.6	148
## 86	412	103.3	28.7	110.0	86
## 87	433	103.8	26.6	87.4	88
## 88	434	105.3	32.3	108.4	113
## 89	388	98.4	32.0	68.4	95
## 90	416	103.0	31.8	106.6	110
## 91	439	105.9	28.2	101.6	96
## 92	346	96.1	28.9	116.1	76
## 93	367	103.3	22.8	70.3	57
## 94	386	99.1	26.3	79.9	77
## 95	389	106.7	24.3	66.0	66
## 96	397	105.2	28.5	63.2	86
## 97	429	106.4	27.4	107.0	86
## 98	343	93.6	37.4	66.6	113
## 99	368	101.6	38.1	116.6	134
## 100	379	99.4	33.5	110.2	110
## 101	420	106.6	21.8	87.7	71
## 102	389	98.7	37.0	114.8	118
## 103	422	112.2	26.3	127.7	74
## 104	443	111.9	21.9	98.5	68
## 105	404	99.6	29.2	75.7	85
## 106	453	109.8	23.9	95.6	82
## 107	365	99.4	26.9	118.1	65
## 108	378	96.0	30.9	110.3	84
## 109	406	98.9	34.3	79.0	116
## 110	415	102.0	30.8	74.4	100
## 111	430	105.9	23.5	88.1	75
## 112	439	104.7	26.9	88.0	92
## 113	365	95.4	36.3	117.6	106
## 114	411	101.2	27.6	80.5	85
## 115	433	106.3	23.4	89.4	74
## 116	438	108.4	27.5	72.1	90
## 117	452	108.6	24.6	85.8	84
## 118	374	111.9	20.5	123.7	47
## 119	389	102.4	38.3	111.8	140
## 120	433	105.1	25.1	88.7	83

## 121	375	97.8	33.2	106.3	109
## 122	376	103.4	41.0	116.0	154
## 123	378	109.9	19.9	72.0	49
## 124	381	97.3	29.2	79.1	90
## 125	403	98.0	34.9	73.6	109
## 126	425	107.9	25.7	104.4	85
## 127	427	101.7	29.5	90.7	101
## 128	433	102.8	30.4	83.2	105
## 129	387	97.6	29.8	81.5	96
## 130	390	99.3	32.7	76.6	111
## 131	390	103.7	31.6	60.1	98
## 132	407	103.1	29.1	75.4	100
## 133	417	107.1	27.2	71.1	90
## 134	418	106.0	24.0	99.0	76
## 135	352	100.9	25.7	53.9	58
## 136	355	97.0	30.3	62.9	83
## 137	375	110.6	18.7	75.8	45
## 138	407	103.8	30.9	73.7	112
## 139	411	103.8	28.9	101.3	106
## 140	336	97.4	40.3	63.6	135
## 141	388	107.4	24.0	65.1	65
## 142	426	104.8	28.7	98.7	105
## 143	391	100.4	28.6	109.5	82
## 144	406	110.2	24.5	120.2	65
## 145	423	104.6	24.3	94.0	77
## 146	432	108.9	22.6	97.8	71
## 147	380	97.2	35.3	108.9	113
## 148	404	107.7	24.9	114.6	67
## 149	411	111.8	24.3	120.8	66
## 150	397	99.9	29.3	107.0	86
## 151	431	104.3	27.7	82.2	95
## 152	437	109.3	21.2	88.7	69
## 153	341	93.7	34.3	64.7	100
## 154	346	105.4	21.9	52.8	48
## 155	388	101.9	37.4	59.1	123
## 156	391	100.6	31.9	109.1	103
## 157	421	103.1	26.8	81.4	85
## 158	408	103.8	27.4	104.2	89
## 159	351	101.3	24.8	123.3	56
## 160	332	97.8	40.4	116.9	137
## 161	371	100.9	34.5	111.6	121
## 162	378	105.0	23.0	110.2	59
## 163	409	107.7	32.8	61.0	114
## 164	414	102.3	28.1	96.2	98
## 165	387	108.6	22.5	113.4	58
## 166	393	105.2	29.2	60.2	87
## 167	397	99.7	27.5	82.9	91
## 168	458	113.4	25.3	101.4	101
## 169	364	96.6	26.4	75.6	72
## 170	380	98.6	32.7	107.1	106
## 171	384	100.3	29.8	69.6	91
## 172	385	110.2	21.2	67.6	53
## 173	327	91.6	32.2	59.4	79
## 174	335	95.4	36.9	63.1	116

## 175	390	102.4	34.2	111.5	119
## 176	384	99.5	24.8	82.3	76
## 177	400	102.2	28.7	112.5	83
## 178	410	101.9	32.5	69.5	105
## 179	412	110.3	24.8	118.8	68
## 180	419	106.2	33.9	120.9	112
## 181	445	110.0	22.4	94.6	73
## 182	465	108.6	29.6	96.4	115
## 183	402	113.4	21.1	66.0	54
## 184	418	107.2	28.9	118.3	87
## 185	424	107.3	27.3	110.9	84
## 186	391	102.0	30.4	123.9	83
## 187	415	102.2	32.0	107.1	107
## 188	421	103.3	25.9	82.3	79
## 189	435	106.0	24.1	87.9	77
## 190	441	109.1	30.6	112.6	108
## 191	442	104.3	28.4	86.2	98
## 192	421	102.7	27.7	80.9	89
## 193	434	101.9	29.7	87.5	98
## 194	444	111.3	22.8	99.8	73
## 195	399	101.5	26.5	75.4	76
## 196	404	104.4	24.5	104.1	69
## 197	453	111.6	29.0	66.4	99
## 198	454	108.8	24.7	85.9	85
## 199	382	97.1	28.5	79.1	84
## 200	413	102.1	26.5	84.8	85
## 201	423	105.4	31.7	114.9	103
## 202	452	109.6	25.2	82.3	90
## 203	469	113.2	23.3	83.7	82
## 204	345	93.2	33.6	58.8	85
## 205	397	100.5	34.2	115.5	107
## 206	414	108.8	24.3	109.2	70
## 207	443	102.8	31.3	87.6	108
## 208	357	103.0	40.1	68.9	156
## 209	384	99.9	29.9	70.8	92
## 210	395	110.2	21.5	69.3	55
## 211	426	104.2	26.9	93.2	98
## 212	428	103.3	27.8	97.7	92
## 213	433	108.3	29.5	114.2	96
## 214	445	105.2	28.1	87.7	100
## 215	445	107.1	29.5	91.5	121
## 216	400	98.9	31.0	74.5	94
## 217	361	99.6	24.3	72.2	62
## 218	390	99.2	31.1	82.8	112
## 219	397	100.4	27.3	75.2	77
## 220	400	102.1	28.0	80.9	102
## 221	401	101.1	33.1	82.1	126
## 222	418	100.9	27.9	86.9	84
## 223	455	116.1	22.1	78.3	80
## 224	457	107.2	27.0	93.4	96
## 225	405	103.3	36.9	69.7	135
## 226	428	111.8	21.0	80.4	62
## 227	438	110.3	29.2	118.9	92
## 228	453	118.0	18.2	94.8	61

## 229	382	100.6	30.0	58.8	80
## 230	397	99.8	31.8	70.7	99
## 231	437	104.0	33.6	85.4	129
## 232	453	110.3	27.9	73.2	97
## 233	355	98.2	27.7	119.1	69
## 234	366	98.2	37.2	66.6	122
## 235	408	102.0	30.7	102.8	106
## 236	418	102.4	29.8	83.4	107
## 237	420	103.0	26.1	89.5	88
## 238	401	103.8	29.3	116.2	86
## 239	406	107.2	24.2	107.9	69
## 240	440	105.3	31.2	97.9	117
## 241	343	96.5	27.4	60.8	66
## 242	387	96.8	37.7	70.1	119
## 243	398	101.5	34.3	106.5	122
## 244	405	106.9	23.4	106.2	65
## 245	422	102.8	29.5	89.6	110
## 246	430	104.0	27.2	83.3	92
## 247	345	94.8	34.9	61.6	100
## 248	375	97.1	34.8	66.0	106
## 249	382	98.4	27.3	78.1	80
## 250	387	100.5	30.1	71.9	96
## 251	402	105.4	32.7	113.8	116
## 252	419	100.9	30.2	83.0	101
## 253	385	107.5	21.8	108.0	57
## 254	388	99.9	34.7	79.4	128
## 255	391	100.9	28.8	66.5	80
## 256	400	110.7	21.6	71.5	59
## 257	420	105.5	22.9	92.7	74
## 258	430	102.8	35.0	88.8	135
## 259	450	114.8	28.0	56.2	89
## 260	361	95.7	36.8	120.6	107
## 261	376	95.2	33.6	111.3	96
## 262	388	101.8	37.1	110.1	135
## 263	434	107.8	28.8	109.4	98
## 264	440	106.8	33.0	102.3	130
## 265	373	95.4	34.2	63.6	95
## 266	373	95.3	36.6	67.3	110
## 267	384	99.1	32.8	57.7	91
## 268	430	102.2	29.3	84.3	98
## 269	440	111.6	21.0	84.3	64
## 270	385	101.8	26.5	113.0	70
## 271	414	106.0	23.3	80.0	68
## 272	438	105.3	31.1	101.7	113
## 273	392	101.4	32.0	108.6	108
## 274	401	112.4	19.4	77.3	52
## 275	450	114.5	22.2	101.1	73
## 276	496	119.6	26.4	102.8	117
## 277	379	99.9	27.0	70.7	73
## 278	391	101.2	29.3	109.8	89
## 279	397	116.0	21.6	131.4	53
## 280	400	100.0	29.3	101.7	93
## 281	402	102.4	27.9	71.1	79
## 282	405	116.5	18.4	103.3	49

## 283	440	110.1	25.2	102.7	87
## 284	367	97.9	34.4	64.9	106
## 285	390	98.5	33.4	78.2	113
## 286	409	107.0	25.8	70.4	78
## 287	456	113.2	23.4	99.8	77
## 288	408	101.9	27.4	83.2	94
## 289	415	105.9	24.9	78.5	79
## 290	415	110.3	22.6	105.3	67
## 291	399	101.6	32.6	108.9	109
## 292	399	99.9	27.2	83.4	86
## 293	440	105.0	27.3	85.3	94
## 294	384	106.4	23.1	110.5	63
## 295	387	99.5	36.9	55.5	109
## 296	391	103.5	29.2	110.8	96
## 297	402	104.0	26.3	70.4	74
## 298	408	102.4	29.2	108.5	89
## 299	408	107.4	27.5	68.9	92
## 300	426	111.3	20.4	82.2	61
## 301	438	112.0	25.8	73.9	94
## 302	460	109.4	26.0	96.4	94
## 303	430	103.5	29.1	80.4	98
## 304	436	106.2	25.9	80.8	84
## 305	400	102.1	27.9	70.8	80
## 306	401	109.1	21.4	75.6	57
## 307	377	104.8	22.7	71.3	60
## 308	382	106.1	21.9	106.7	57
## 309	388	99.2	33.5	70.0	108
## 310	393	101.8	39.2	103.9	150
## 311	429	100.0	34.7	89.0	120
## 312	439	110.9	20.4	88.3	66
## 313	447	103.7	31.3	83.9	108
## 314	406	103.6	36.3	106.8	138
## 315	408	106.8	28.3	114.3	90
## 316	413	104.2	33.1	101.1	130
## 317	387	105.0	39.2	64.5	149
## 318	407	102.7	30.9	78.0	112
## 319	420	108.4	28.5	117.3	90
## 320	392	101.5	28.0	73.1	86
## 321	340	95.3	28.8	57.5	68
## 322	371	102.0	24.7	68.6	64
## 323	374	104.7	37.4	65.8	143
## 324	385	101.3	25.4	75.4	73
## 325	398	102.7	28.3	107.5	90
## 326	420	106.3	30.8	106.1	115
## 327	376	101.0	35.1	111.0	124
## 328	387	100.9	33.6	103.4	124
## 329	398	105.9	23.5	75.2	68
## 330	403	104.8	30.7	67.7	104
## 331	344	92.5	31.1	65.0	77
## 332	380	98.6	27.3	75.3	77
## 333	389	113.0	21.5	59.8	54
## 334	389	96.2	36.2	78.1	115
## 335	389	114.4	20.7	124.3	49
## 336	395	99.1	34.5	106.0	116

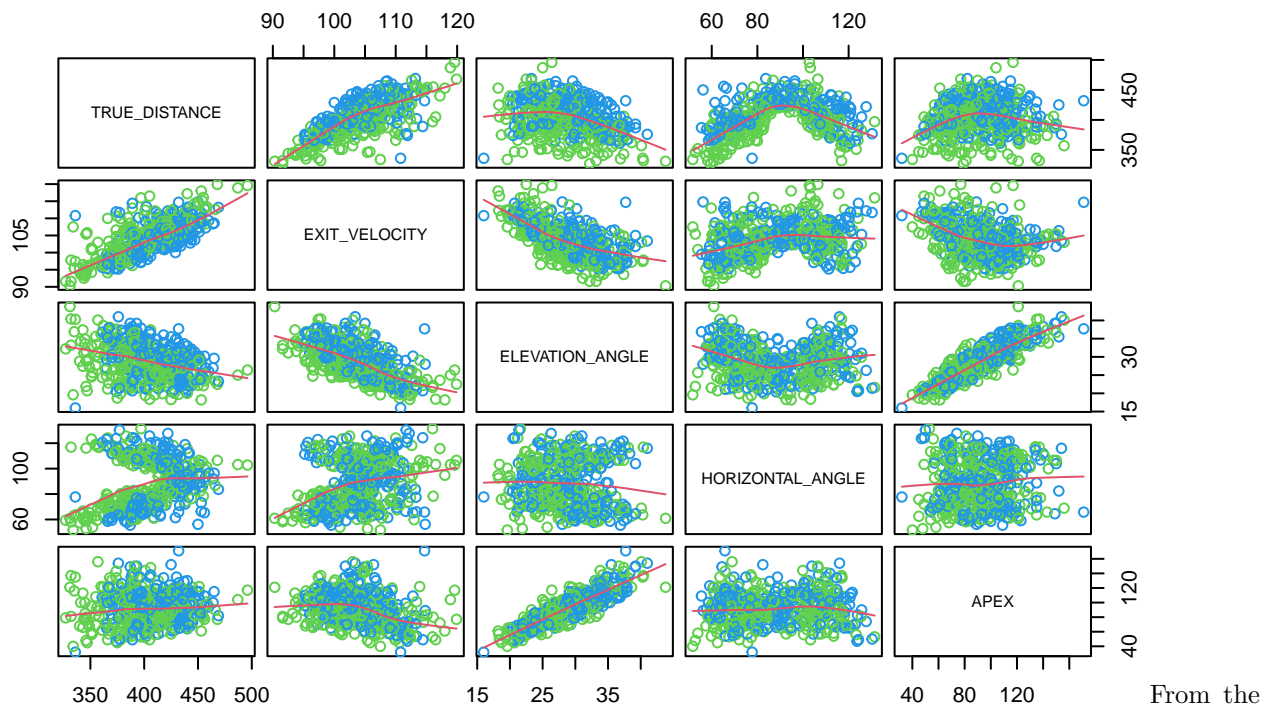
## 337	420	108.2	25.3	106.0	83
## 338	421	109.1	24.5	74.0	77
## 339	425	106.4	35.5	82.4	152
## 340	426	104.2	24.7	91.8	80
## 341	428	109.7	20.0	90.4	65
## 342	451	107.4	29.7	103.3	105
## 343	457	108.4	25.3	90.6	97
## 344	464	108.4	27.0	92.0	100
## 345	366	99.6	32.2	60.0	94
## 346	397	97.3	37.9	66.0	115
## 347	397	104.0	24.5	75.5	72
## 348	435	108.2	21.9	90.0	70
## 349	370	99.0	29.8	59.4	78
## 350	379	97.9	37.3	71.9	126
## 351	408	103.8	24.9	78.3	73
## 352	393	99.7	37.3	121.6	114
## 353	433	104.3	32.7	71.0	110
## 354	444	103.7	32.1	98.6	114
## 355	397	97.1	35.1	104.7	112
## 356	413	111.2	21.3	104.4	57
## 357	377	111.7	21.4	130.3	50
## 358	418	101.3	33.9	100.6	120
## 359	451	106.0	30.2	94.6	115
## 360	397	103.6	24.7	104.9	71
## 361	426	103.0	30.1	93.0	116
## 362	440	112.7	20.0	94.5	65
## 363	332	91.6	33.2	58.2	81
## 364	360	97.1	36.2	71.6	122
## 365	383	102.5	29.9	125.6	81
## 366	384	97.7	32.3	82.5	112
## 367	384	104.0	25.4	68.0	71
## 368	391	104.9	35.0	110.1	141
## 369	406	106.8	30.0	111.5	110
## 370	379	99.8	26.4	72.3	72
## 371	408	103.0	27.3	76.8	86
## 372	425	107.1	23.7	97.4	84
## 373	430	106.1	26.7	99.5	93
## 374	370	100.1	37.4	68.4	131
## 375	381	98.0	31.9	105.9	102
## 376	410	102.2	25.3	85.9	81
## 377	415	107.6	22.6	101.5	69
## 378	435	105.4	30.7	83.9	120
## 379	348	95.5	29.3	60.7	71
## 380	410	112.2	19.6	100.3	56
## 381	412	105.1	29.1	108.7	97
## 382	414	103.3	24.9	85.4	82
## 383	417	109.1	23.2	75.4	70
## 384	425	112.3	18.3	92.6	57
## 385	454	115.1	23.8	105.4	83
## 386	466	112.6	23.3	86.9	90
## 387	396	103.0	34.8	74.9	135
## 388	413	104.5	30.2	70.7	102
## 389	420	107.1	29.8	115.9	95
## 390	441	113.3	22.1	77.5	71

## 391	394	104.4	25.0	70.3	67
## 392	398	102.6	32.5	64.3	104
## 393	440	104.8	30.1	95.6	113
## 394	367	98.8	37.9	60.7	121
## 395	370	98.1	30.8	61.6	83
## 396	411	105.7	33.3	65.8	119
## 397	435	106.8	23.4	89.3	78
## 398	441	106.9	24.7	91.5	85
## 399	370	96.4	34.1	111.9	102
## 400	415	107.2	29.6	63.6	96
## 401	426	102.7	28.5	89.1	101
## 402	389	105.9	23.3	69.7	59
## 403	398	100.0	33.9	72.6	113
## 404	411	102.2	30.6	108.3	97
## 405	418	106.6	36.0	114.7	134
## 406	426	102.6	27.2	90.7	91
## 407	336	110.8	16.0	77.7	32
## 408	388	100.2	34.5	63.3	107
## 409	449	106.8	29.1	87.9	115
## 410	334	107.5	19.6	51.7	40
## 411	405	108.3	21.7	101.7	63
## 412	423	106.0	24.2	83.3	81
## 413	451	113.9	29.1	106.5	122
## 414	423	104.2	30.0	99.6	109
## 415	426	104.7	26.5	80.7	89
## 416	399	104.7	29.8	115.9	93
## 417	405	101.7	29.6	102.4	100
## 418	447	114.4	23.1	104.9	82
## 419	331	90.3	43.8	60.9	121
## 420	357	96.7	31.3	117.1	89
## 421	444	109.4	27.5	76.4	99
## 422	363	96.0	32.9	73.8	106
## 423	376	101.3	24.5	71.8	61
## 424	371	99.7	26.4	70.6	72
## 425	389	105.0	21.6	79.4	60
## 426	421	106.9	25.2	77.9	84
## 427	351	94.2	33.0	68.4	95
## 428	373	101.2	26.6	113.0	73
## 429	397	104.3	26.7	110.2	81
## 430	390	104.9	23.6	71.7	61
## 431	391	102.8	34.0	107.3	127
## 432	435	105.9	26.8	87.4	101
## 433	397	98.8	30.3	76.4	93
## 434	400	103.0	30.6	64.4	93
## 435	421	104.9	29.0	104.9	101
## 436	452	109.0	23.8	89.0	86
## 437	347	105.8	20.7	62.5	45
## 438	366	96.7	35.3	58.6	100
## 439	376	98.5	29.8	63.6	79
## 440	378	98.1	26.2	80.2	80
## 441	378	96.6	32.0	79.8	105
## 442	391	105.4	36.7	106.5	150
## 443	393	97.8	32.9	77.0	106
## 444	416	101.3	32.1	101.0	110

```
## 445      433      106.1      23.9      89.1  75
## 446      436      104.2      28.8      86.2 105
## 447      393      102.1      25.9     107.5  70
## 448      430      101.8      31.7      91.7 113
## 449      432      103.9      33.9     100.5 127
## 450      433      109.1      21.9      94.7  65
## 451      405      105.3      31.0     125.7  90
```

```
pairs(hr_stad_CFYS_2017_out, gap=0.5, panel = panel.smooth, main = "Home Run data", col = 3 + (coors_bp
```

Home Run data



From the pairs view we can see that the elevation angle of the ball's trajectory has a negative impact on distance. I'll now create a multiple regression model to determine how the other factors come into play.

```
(hr_stad_CFYS_2017_lm <- lm(TRUE_DISTANCE ~ EXIT_VELOCITY + ELEVATION_ANGLE + HORIZONTAL_ANGLE + APEX ,
```

```
##
## Call:
## lm(formula = TRUE_DISTANCE ~ EXIT_VELOCITY + ELEVATION_ANGLE +
##     HORIZONTAL_ANGLE + APEX, data = hr_stad_CFYS_2017_out)
##
## Coefficients:
##      (Intercept)      EXIT_VELOCITY      ELEVATION_ANGLE      HORIZONTAL_ANGLE
##          237.87211           2.07560          -6.48694           0.05274
##              APEX
##              1.43415
```

```
summary(hr_stad_CFYS_2017_lm)
```

```
##
```

```
## Call:
## lm(formula = TRUE_DISTANCE ~ EXIT_VELOCITY + ELEVATION_ANGLE +
##     HORIZONTAL_ANGLE + APEX, data = hr_stad_CFYS_2017_out)
##
## Residuals:
##      Min       1Q   Median       3Q      Max
## -78.049  -9.454   1.385  12.643  37.616
##
## Coefficients:
##              Estimate Std. Error t value Pr(>|t|)
## (Intercept)    237.87211    34.88470   6.819  3.0e-11 ***
## EXIT_VELOCITY     2.07560     0.27259   7.614  1.6e-13 ***
## ELEVATION_ANGLE  -6.48694     0.55444 -11.700 < 2e-16 ***
## HORIZONTAL_ANGLE  0.05274     0.04449   1.185   0.236
## APEX              1.43415     0.09581  14.969 < 2e-16 ***
## ---
## Signif. codes:  0 '***' 0.001 '**' 0.01 '*' 0.05 '.' 0.1 ' ' 1
##
## Residual standard error: 17.05 on 446 degrees of freedom
## Multiple R-squared:  0.6752, Adjusted R-squared:  0.6722
## F-statistic: 231.7 on 4 and 446 DF,  p-value: < 2.2e-16
```

Since horizontal angle p-value > .05, let's remove that factor and recalculate.

```
(hr_stad_CFYS_2017_lm <- lm(TRUE_DISTANCE ~ EXIT_VELOCITY + ELEVATION_ANGLE + APEX , data = hr_stad_CFYS_2017_out))
```

```
##
## Call:
## lm(formula = TRUE_DISTANCE ~ EXIT_VELOCITY + ELEVATION_ANGLE +
##     APEX, data = hr_stad_CFYS_2017_out)
##
## Coefficients:
##      (Intercept)      EXIT_VELOCITY  ELEVATION_ANGLE           APEX
##          234.365           2.146          -6.460           1.436
```

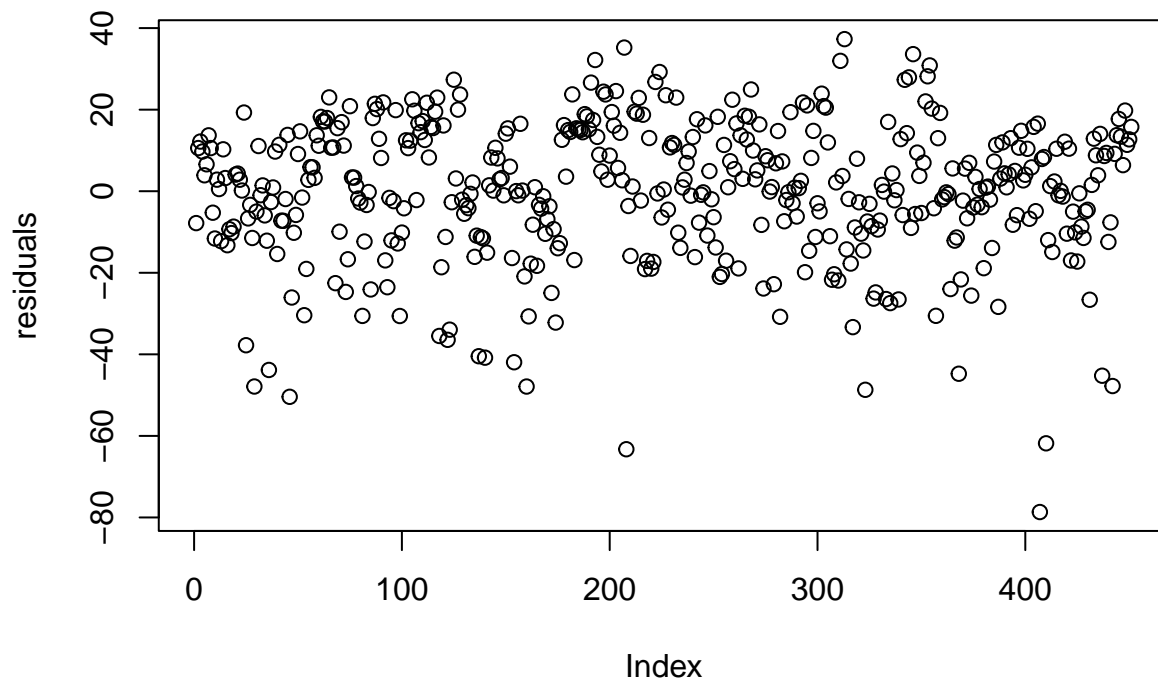
```
summary(hr_stad_CFYS_2017_lm)
```

```
##
## Call:
## lm(formula = TRUE_DISTANCE ~ EXIT_VELOCITY + ELEVATION_ANGLE +
##     APEX, data = hr_stad_CFYS_2017_out)
##
## Residuals:
##      Min       1Q   Median       3Q      Max
## -78.669  -9.361   1.133  12.644  37.291
##
## Coefficients:
##              Estimate Std. Error t value Pr(>|t|)
## (Intercept)    234.36522    34.77479   6.740  4.92e-11 ***
## EXIT_VELOCITY     2.14553     0.26625   8.058  7.12e-15 ***
## ELEVATION_ANGLE  -6.46031     0.55423 -11.656 < 2e-16 ***
## APEX              1.43574     0.09584  14.980 < 2e-16 ***
```

```
## ---
## Signif. codes:  0 '***' 0.001 '**' 0.01 '*' 0.05 '.' 0.1 ' ' 1
##
## Residual standard error: 17.06 on 447 degrees of freedom
## Multiple R-squared:  0.6741, Adjusted R-squared:  0.6719
## F-statistic: 308.2 on 3 and 447 DF,  p-value: < 2.2e-16
```

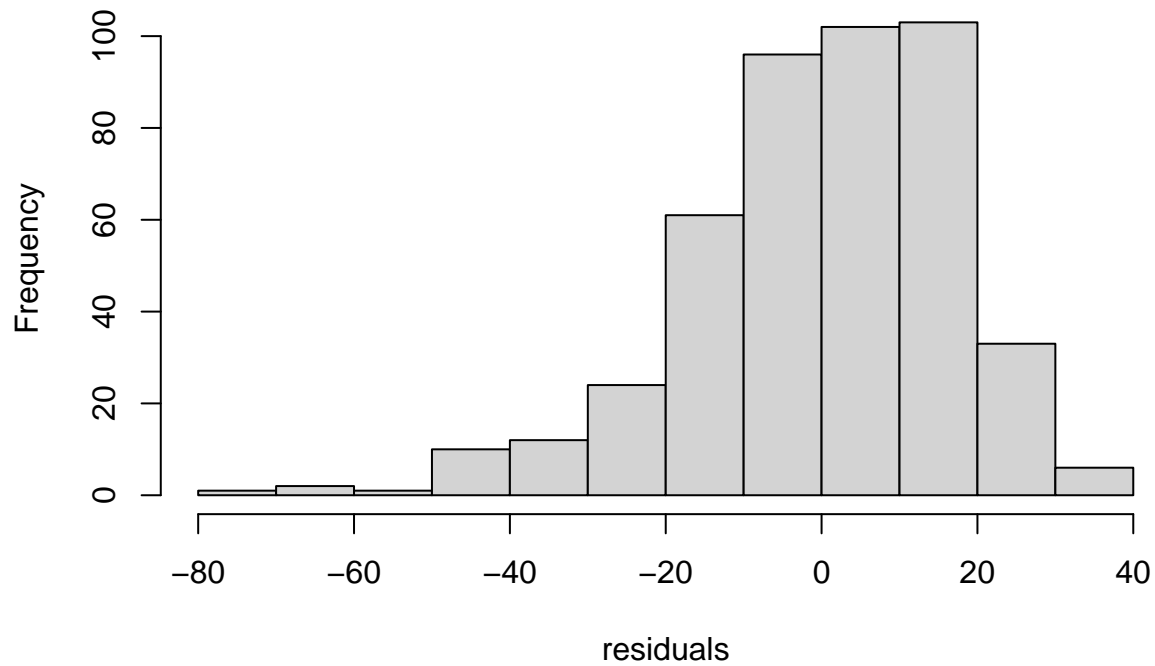
Now that all p-values are below .05, I am still not comfortable to call this a good model but let's analyze the residuals.

```
residuals <- resid(hr_stad_CFYS_2017_lm)
plot(residuals)
```



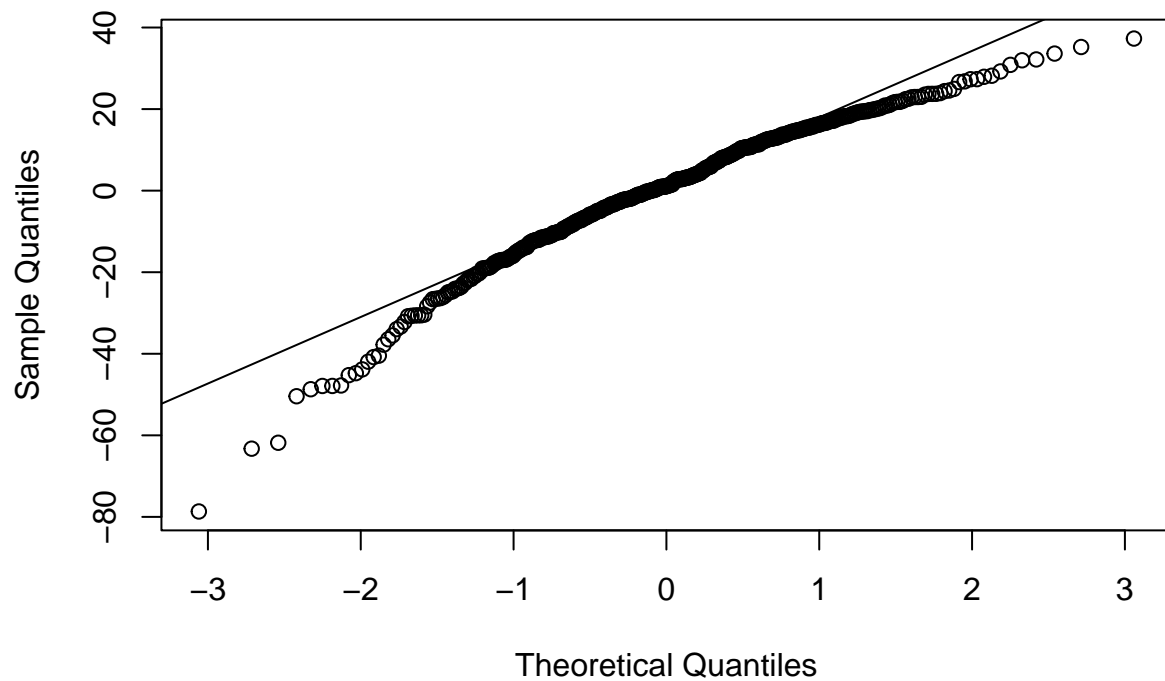
```
hist(residuals)
```

Histogram of residuals



```
qqnorm(resid(hr_stad_CFYS_2017_lm))  
qqline(resid(hr_stad_CFYS_2017_lm))
```

Normal Q-Q Plot



After removing the horizontal angle factor and plotting the residuals, it appears to have a normal distribution but the histogram shows a skew to the right. I will select the elevation angle as my quadratic variable because

of it's negative affect on the distribution and recalculate.

```
elevation_sq <- hr_stad_CFYS_2017_out$ELEVATION_ANGLE ^ 2
```

```
(hr_stad_CFYS_2017_lm_2 <- lm(TRUE_DISTANCE ~ EXIT_VELOCITY + ELEVATION_ANGLE + APEX + elevation_sq, da
```

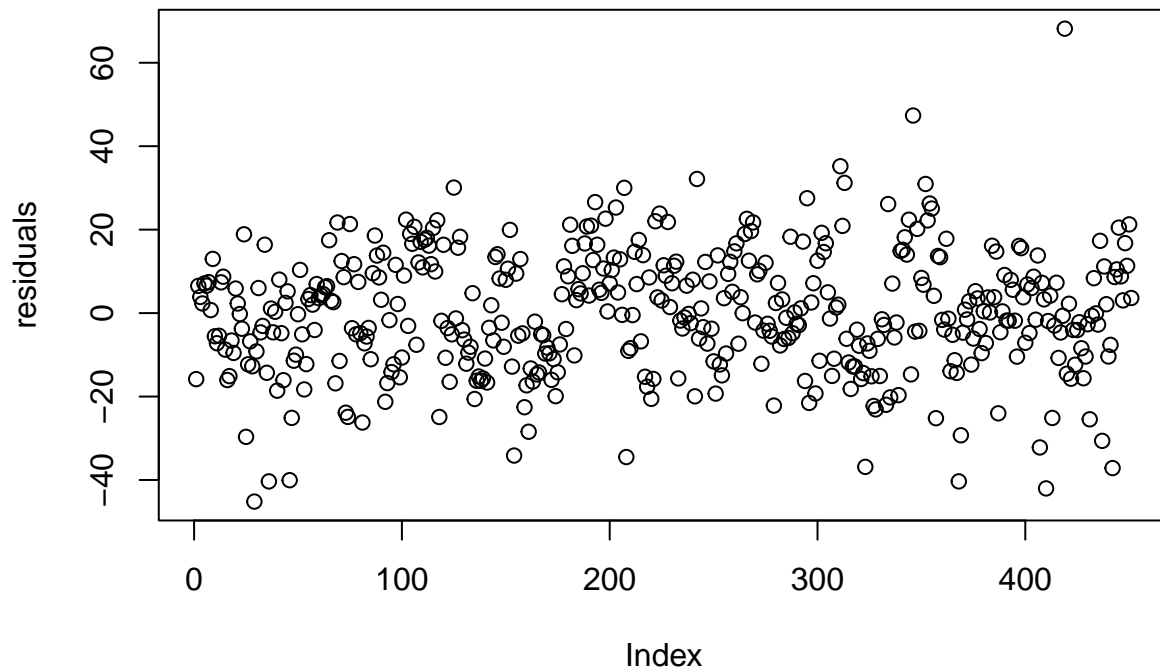
```
##
## Call:
## lm(formula = TRUE_DISTANCE ~ EXIT_VELOCITY + ELEVATION_ANGLE +
##     APEX + elevation_sq, data = hr_stad_CFYS_2017_out)
##
## Coefficients:
##      (Intercept)      EXIT_VELOCITY  ELEVATION_ANGLE          APEX
##      -153.6721          3.1230          13.7079          1.1787
##      elevation_sq
##      -0.3172
```

```
summary(hr_stad_CFYS_2017_lm_2)
```

```
##
## Call:
## lm(formula = TRUE_DISTANCE ~ EXIT_VELOCITY + ELEVATION_ANGLE +
##     APEX + elevation_sq, data = hr_stad_CFYS_2017_out)
##
## Residuals:
##      Min       1Q   Median       3Q      Max
## -45.175  -9.616  -0.269   9.544  68.166
##
## Coefficients:
##              Estimate Std. Error t value Pr(>|t|)
## (Intercept)   -153.67212    42.77902   -3.592 0.000364 ***
## EXIT_VELOCITY    3.12304     0.24127  12.944 < 2e-16 ***
## ELEVATION_ANGLE  13.70788     1.66196   8.248 1.82e-15 ***
## APEX            1.17875     0.08475  13.908 < 2e-16 ***
## elevation_sq   -0.31720     0.02504 -12.665 < 2e-16 ***
## ---
## Signif. codes:  0 '***' 0.001 '**' 0.01 '*' 0.05 '.' 0.1 ' ' 1
##
## Residual standard error: 14.64 on 446 degrees of freedom
## Multiple R-squared:  0.7603, Adjusted R-squared:  0.7582
## F-statistic: 353.7 on 4 and 446 DF,  p-value: < 2.2e-16
```

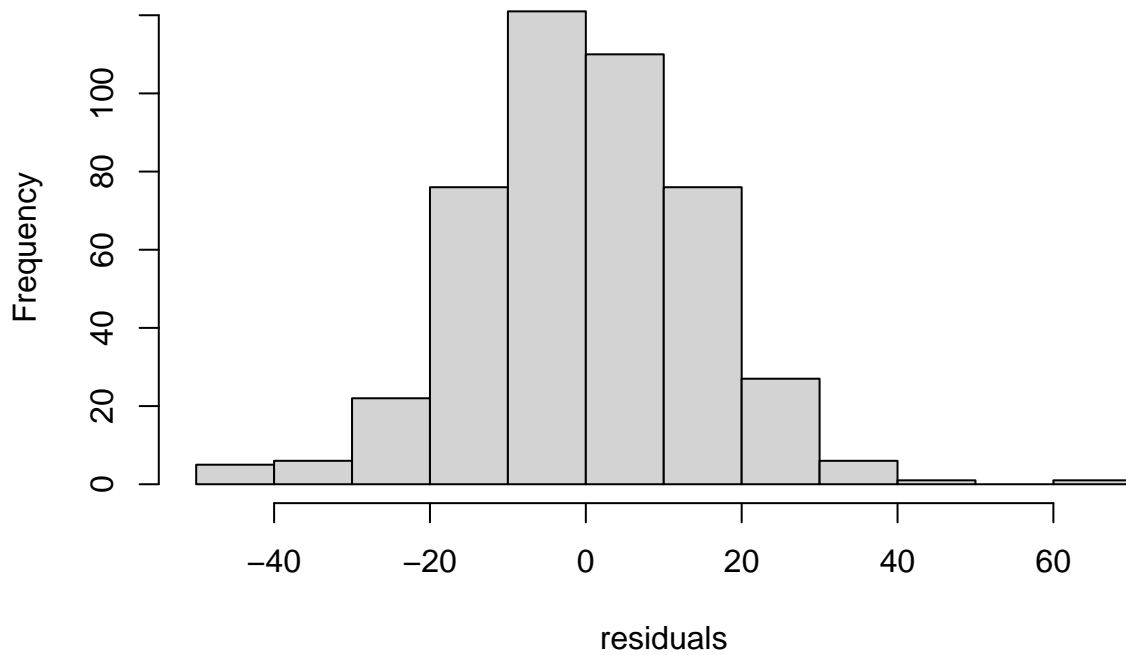
After doing so, you'll notice the median is now very close to 0 and the min/max range seems to have improved. Plotting the residuals does seem to show more of a normal distribution in all plots below.

```
residuals <- resid(hr_stad_CFYS_2017_lm_2)
plot(residuals)
```



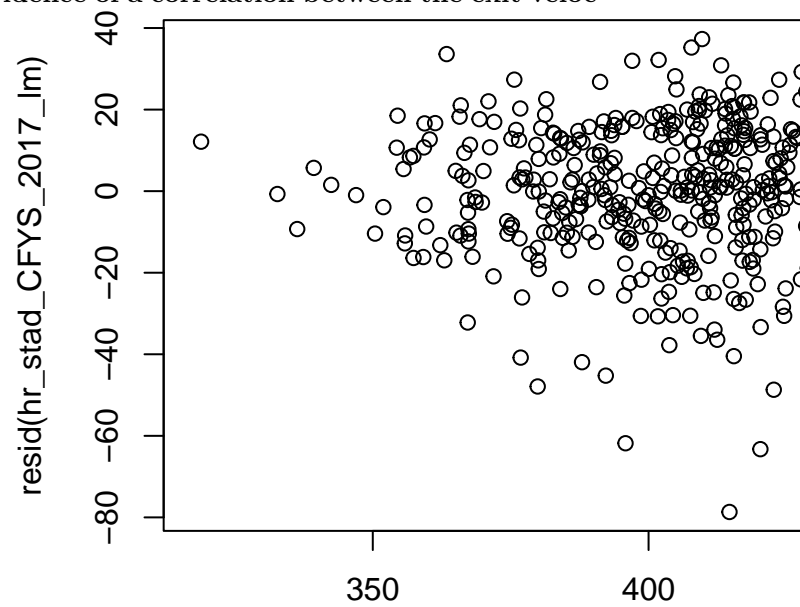
```
hist(residuals)
```

Histogram of residuals



```
plot(fitted(hr_stad_CFYS_2017_lm), resid(hr_stad_CFYS_2017_lm))
```

The large t-value ratio of 30.62 there is strong evidence of a correlation between the exit veloc-



ity of the hit ball and the distance that it travels.

```
par(mfrow=c(2,2))
plot(hr_stad_CFYS_2017_lm)
```

