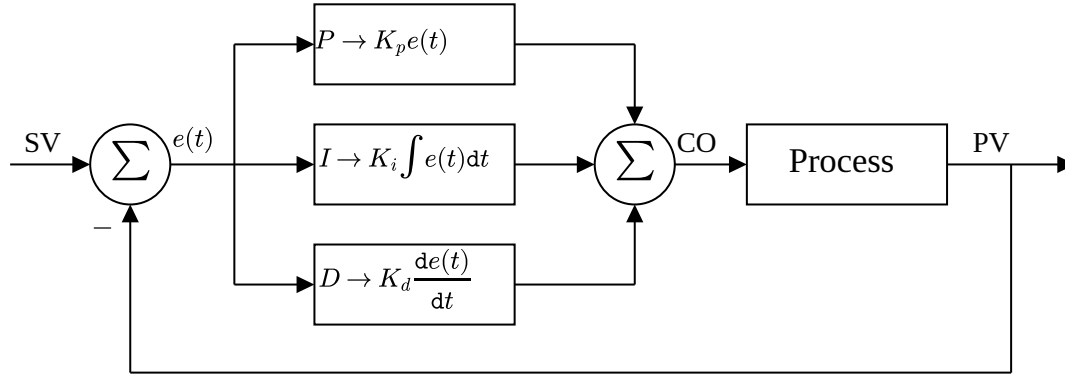


# Notes on PID control with Arduino

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Block diagram of a system/process with a PID controller:



$$\text{CO}(t) = \underbrace{K_p e(t)}_{P(t)} + \underbrace{K_i \int e(t) dt}_{I(t)} + \underbrace{K_d \frac{de(t)}{dt}}_{D(t)} \quad (1)$$

$$\therefore \boxed{\text{CO}(t) = P(t) + I(t) + D(t)} \quad (2)$$

In order to implement the PID control into an Arduino device, we must discretize (1). To do this, there are some tricks that we can use. We will call the tricks as types. These types are non-standardized. The type numbers are given in a convenient manner.

## 1. Discretization

### 1.1. Type-1-PID control

We discretize the PID control as follows:

$$P(k) = K_p e(k) \quad (3)$$

$$I(k) = I(k-1) + K_i e(k) \Delta t \quad (4)$$

$$D(k) = K_d \left( \frac{e(k) - e(k-1)}{\Delta t} \right) \quad (5)$$

### 1.2. Type-2-PID control

The type-2-PID control follows the following form:

$$\text{CO}(t) = K_p e(t) + K_i \int e(t) dt + K_d \frac{d\hat{e}(t)}{dt} \quad (6)$$

where  $\frac{d\hat{e}(t)}{dt}$  is obtained from a filtered  $\frac{de(t)}{dt}$ . The filter that we use is a first-order-low-pass filter. Thus, In  $s$ -domain, we write (6) as follows:

$$\text{CO}(s) = \underbrace{K_p E(s)}_{P(s)} + \underbrace{\frac{K_i E(s)}{s}}_{I(s)} + \underbrace{\frac{K_d s E(s)}{\tau s + 1}}_{D(s)} \quad (7)$$

Here,  $\tau$  is the filter time constant.  $P(k)$  and  $I(k)$  in (7) are similar to type-1-PID control ((3) and (4)). As for  $D(k)$ , we can derive it as follows:

$$\begin{aligned} D(s) &= \frac{K_d s E(s)}{\tau s + 1} \\ D(s)(\tau s + 1) &= K_d s E(s) \\ \tau \dot{D}(t) + D(t) &= K_d \dot{e}(t) \end{aligned}$$

$$\begin{aligned}
\dot{D}(t) &= \frac{K_d \dot{e}(t) - D(t)}{\tau} \\
\frac{D(k) - D(k-1)}{\Delta t} &= \frac{K_d \dot{e}(t) - D(k)}{\tau} \\
D(k) &= \frac{\Delta t K_d \dot{e}(t) - \Delta t D(k)}{\tau} + D(k-1) \\
D(k) + \frac{\Delta t}{\tau} D(k) &= \frac{\Delta t K_d \dot{e}(t)}{\tau} + D(k-1) \\
D(k) \left( \frac{\tau + \Delta t}{\tau} \right) &= \frac{\Delta t K_d \dot{e}(t) + \tau D(k-1)}{\tau} \\
D(k) &= \frac{\Delta t K_d \dot{e}(t) + \tau D(k-1)}{\tau + \Delta t}
\end{aligned}$$

In conclusion, we now have:

$$D(k) = \frac{\Delta t K_d \dot{e}(t) + \tau D(k-1)}{\tau + \Delta t} \quad (8)$$

### 1.3. Type-3-PID control

To avoid derivative kicks contributed by the filtering the error, we will filter the process value instead of filtering the error.

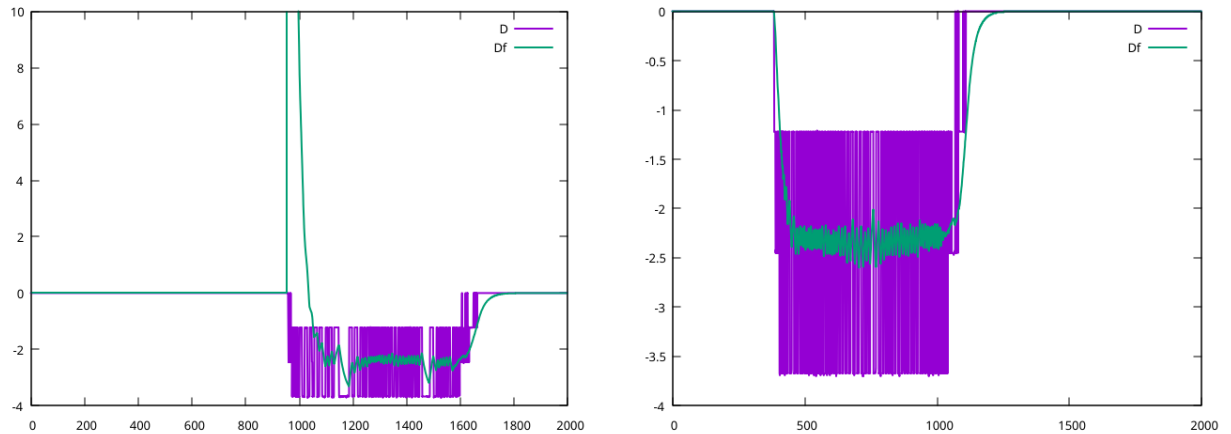
$$CO(s) = \underbrace{K_p E(s)}_{P(s)} + \underbrace{\frac{K_i E(s)}{s}}_{I(s)} + \underbrace{\frac{K_d (-\dot{P}V(s))}{\tau s + 1}}_{D(s)} \quad (9)$$

The negative sign in  $\dot{P}V$  is because at the steady state condition,  $\dot{P}V = 0$ . In this case, we simply rewrite (8) as follows:

$$D(k) = \frac{-\Delta t K_d \dot{P}V(t) + \tau D(k-1)}{\tau + \Delta t} \quad (10)$$

## 2. Remarks

Type-1 is generally unusable since the derivative operation amplifies noise. Therefore, we will only implement type-2-PID control and type-3-PID control. In type-2-PID control we expect derivative kicks for step inputs. As in type-3-PID control, there will be no derivative kicks since PV is always continuous regardless the inputs.



Blue line is the unfiltered derivative term (D). Green line is the filtered derivative term (Df). The cutoff frequency of the filter is 10 Hz ( $\tau = 0.1$ ). The left figure is for type-2-PID control while the right figure is for type-3-PID control. In the left figure we can see the derivative kick.