

ss lab

STATE-SPACE REPRESENTATION

State-space representation is a time domain model of the form:

$$\frac{d}{dt} \mathbf{z} = \mathbf{A} \mathbf{z} + \mathbf{B} \mathbf{u} \quad (\text{dynamic system}) \quad (1a)$$

$$\mathbf{y} = \mathbf{C} \mathbf{z} + \mathbf{D} \mathbf{u} \quad (\text{output}) \quad (1b) \quad (1)$$

The variables involved in Eq. (1) are:

\mathbf{z} = column of state variables, length N_z

\mathbf{u} = column of input variables, $\rightarrow N_u$

\mathbf{y} = column of output variable $\rightarrow N_y$

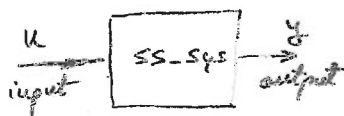
$\mathbf{A}, \mathbf{B}, \mathbf{C}, \mathbf{D}$ = state space matrices

$$N_z \begin{bmatrix} \mathbf{A} \end{bmatrix}^{N_z}$$

$$N_z \begin{bmatrix} \mathbf{B} \end{bmatrix}^{N_u}$$

$$N_y \begin{bmatrix} \mathbf{C} \end{bmatrix}^{N_z}$$

$$N_y \begin{bmatrix} \mathbf{D} \end{bmatrix}^{N_u}$$



The SS representation is a time-domain representation, whereas the TF representation was a Laplace-domain representation.

MATLAB accepts both TF and SS representations.

1a
SS

1st order system State-space representation

Recall

$$T \dot{x}(t) + x(t) = f(t) \quad (1)$$

Rewrite (1) as :

$$\dot{x} = -\frac{1}{T}x + \frac{1}{T}f$$

or

$$\frac{d}{dt}x = -\frac{1}{T}x + \frac{1}{T}f \quad (2)$$

$\uparrow \quad \quad \uparrow \quad \uparrow \quad \uparrow \quad \uparrow$
 $\quad \quad \quad A \quad z \quad B \quad f$

$$\left\{ \begin{array}{l} \frac{d}{dt}z = Az + Bu \\ y = Cz + Du \end{array} \right. \quad \left[\begin{array}{l} z = x \\ u = f \\ y = x \\ A = -1/T \\ B = 1/T \\ C = 1 \\ D = 0 \end{array} \right.$$

²SS 1 dof To derive the SS representation of a 1-dof system, recall its 2nd order ordinary differential equation in standard form, i.e.,

$$\ddot{x} + 2\zeta\omega_n \dot{x} + \omega_n^2 x = \omega_n^2 f(t) \quad (2)$$

Write (2) in terms of x and \dot{x} only, i.e.,

$$\frac{d}{dt} \dot{x} + 2\zeta\omega_n \dot{x} + \omega_n^2 x = \omega_n^2 f(t) \quad (3)$$

Add the identity $\frac{d}{dt} x = \dot{x}$ and write (3) as an extended 1st order system, i.e.,

$$\begin{cases} \frac{d}{dt} x = \dot{x} \\ \frac{d}{dt} \dot{x} = -2\zeta\omega_n \dot{x} - \omega_n^2 x + \omega_n^2 f(t) \end{cases} \quad (4)$$

Express (4) in matrix form, i.e.,

$$\frac{d}{dt} \begin{bmatrix} x \\ \dot{x} \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -\omega_n^2 & -2\zeta\omega_n \end{bmatrix} \begin{bmatrix} x \\ \dot{x} \end{bmatrix} + \begin{bmatrix} 0 \\ \omega_n^2 \end{bmatrix} f(t) \quad (5)$$

(dynamic system)

$$y = [x] \quad (\text{output})$$

SS1dot Define :

$$\left. \begin{aligned} z &= \begin{bmatrix} x \\ \dot{x} \end{bmatrix}, \quad u = \left[\frac{1}{t} \right] \quad y = [x] \\ N_z &= 2 \quad N_u = 1 \quad N_y = 1 \\ A &= \begin{bmatrix} 0 & 1 \\ -\omega_n^2 & -2\zeta\omega_n \end{bmatrix} \quad B = \begin{bmatrix} 0 \\ \omega_n^2 \end{bmatrix} \quad (6) \\ C &= [1 \ 0] \quad D = [0] \end{aligned} \right\}$$

(6) \rightarrow (5) :

$$\left\{ \begin{aligned} \frac{d}{dt} z &= Az + Bu \\ y &= Cz + Du \end{aligned} \right. \quad (7)$$

Egs. (6), (7) form the SS representation of the dynamic system (2). The TF representation of the same system is

$$G(s) = \frac{\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2}$$

The TF and SS representations are interchangeable in MATLAB

4
SS/dof

Comparison of TF and SS representations

initial data: fn, Hz; z% =

2 2

TF poles =

-0.2513 +12.5639i

-0.2513 -12.5639i

f_TF, Hz; z_TF% =

1.9996 2.0000

1.9996 2.0000

SS poles =

-0.2513 +12.5639i

-0.2513 -12.5639i

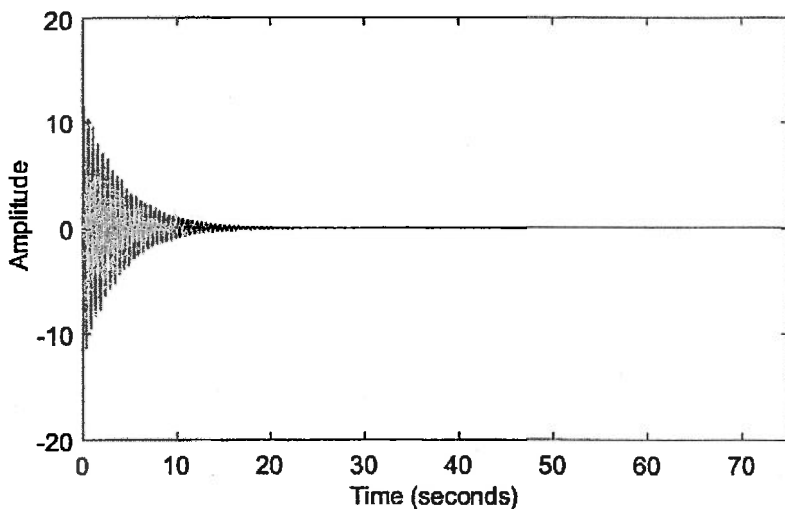
f_SS, Hz; z_SS% =

1.9996 2.0000

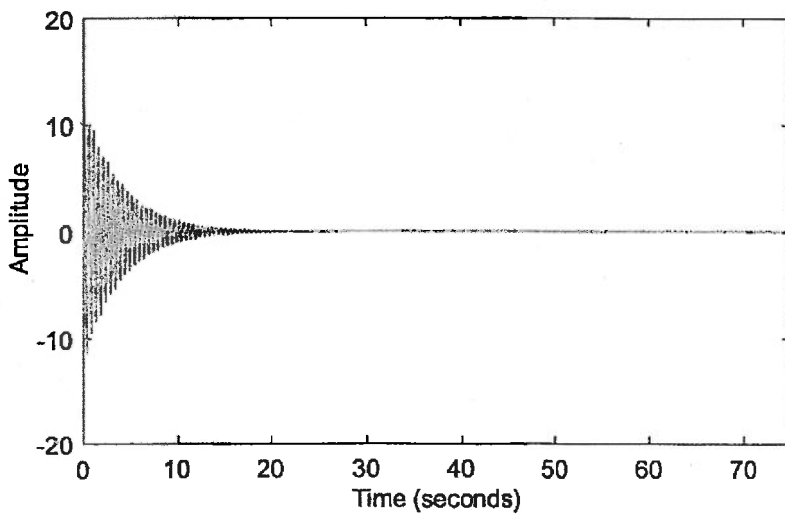
1.9996 2.0000

5
SS 1 dot

impulse response of TF system: z TF= 2%



impulse response of SS system: z SS= 2%



```

1 %% DESCRIPTION
2 %{
3 SISO system time response
4 Comparison of TF and SS representations
5 %}
6 %% initialization
7 opengl hardwarebasic      % switch to basic hardware graphics functions
8 clc                      % clear command window
9 clear                    % clear workspace
10 % close all              % close all plots
11 format compact
12 tol=1e-10; % tolerance for discarding machine zero
13 %% DEFINE PARAMETERS
14 % ----- data for class -----
15 fn=2; wn=2*pi*fn; % plunge frequency, Hz
16 z=2e-2;          % plunge damping ratio
17 %% DEFINE TIME RANGE
18 T=1/fn; % time scale
19 % dt=1e-3;
20 % tmax=50*T;
21 tmax=150*T;
22 Nt=1000; dt=tmax/Nt;
23 t=0:dt:tmax; % time range
24 %% CALCULATE SISO TRANSFER MATRIX
25 G=tf([wn^2],[1 2*z*wn wn^2]);
26 %% CALCULATE POLES OF G
27 [~,poles_TF,~]=zpkdata(G); s_TF=poles_TF{1,1}; % poles
28 % display(s_TF,'poles of G')
29 f_TF=abs(imag(s_TF))/(2*pi); % frequencies
30 zz=-real(s_TF)./abs(s_TF); z_TF=zz.*(abs(zz)>tol); % damping
31 %% CALCULATE IMPULSE RESPONSE OF TF SYSTEM
32 figure(1);
33 subplot(2,1,1); impulse(G,t);
34 title(['impulse response of TF system: z TF= ' num2str(z_TF(1)*100) '%'])
35 %% DISPLAY TF RESULTS
36 display('Comparison of TF and SS representations')
37 display([fn z*100], 'initial data: fn, Hz;  z%');
38 display(s_TF, 'TF poles');
39 display([f_TF z_TF*100], 'f_TF, Hz;  z_TF%');
40 %% CALCULATE SISO STATE SPACE MODEL
41 %----- state space matrices -----
42 A=[ 0          1 ;
43     -wn^2      -2*z*wn];
44 B=[ 0 ;
45     wn^2];
46 C=[1 0];
47 D=[0];
48 ss_sys=ss(A,B,C,D);
49 %% EXTRACT POLES, FREQUENCY, DAMPING
50 [~,zz,poles_SS]=damp(ss_sys);

```

```
51 % display(ss,'poles of ss_sys')
52 s_SS=poles_SS; % poles
53 f_SS=abs(imag(poles_SS))/(2*pi); % frequencies
54 z_SS=zz.*(abs(zz)>tol); % damping
55 %% DISPLAY SS RESULTS
56 % display(' ');
57 display(s_SS, 'SS poles');
58 display([f_SS z_SS*100], 'f_SS, Hz; z_SS%');
59 %% CALCULATE IMPULSE RESPONSE OF SS SYSTEM
60 subplot(2,1,2); impulse(ss_sys,t);
61 title(['impulse response of SS system: z SS= ' num2str(z_SS(1)*100) '%'])
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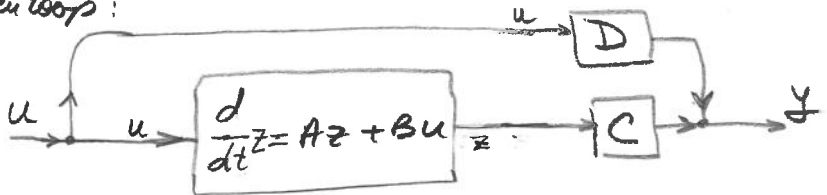

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FB of SS system

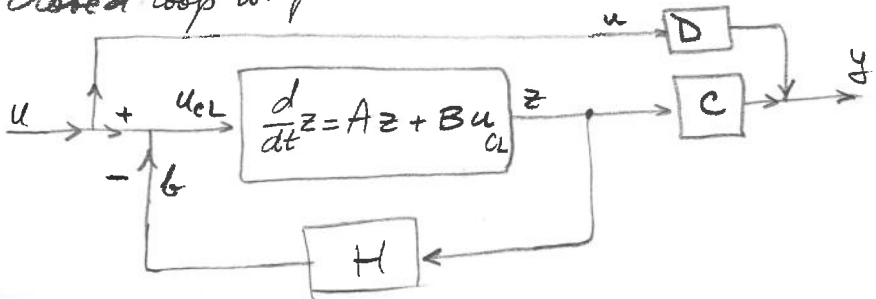
$$\frac{d}{dt} z = Az + Bu \quad (1a)$$

$$y = Cz + Du \quad (1b)$$

open loop:



closed loop w. feedback H:



$$u_{CL} = u - b = u - Hz$$

$$\frac{d}{dt} z = Az + Bu_{CL} = Az + Bu - BH z$$

$$\frac{d}{dt} z = (A - BH)z + Bu$$

$$A_{CL} = A - BH$$

same A_{CL} as for simplified model

$$\left\{ \begin{array}{l} \frac{d}{dt} z = A_{CL} z + Bu \\ y = Cz + Du \end{array} \right. \quad \begin{array}{l} \text{SS sys} \\ \text{w. feedback H} \end{array}$$

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H for velocity feedback

Recall $z = \begin{bmatrix} x \\ \dot{x} \end{bmatrix}$ (6)

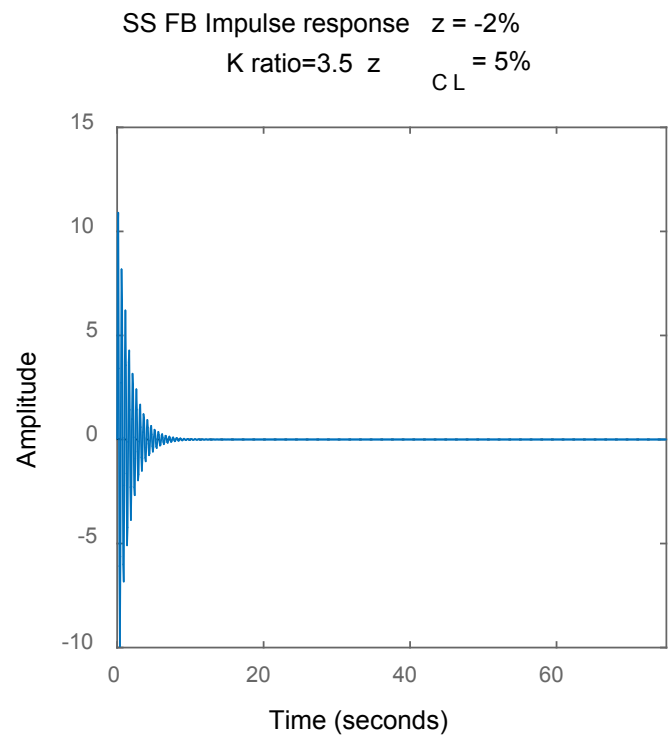
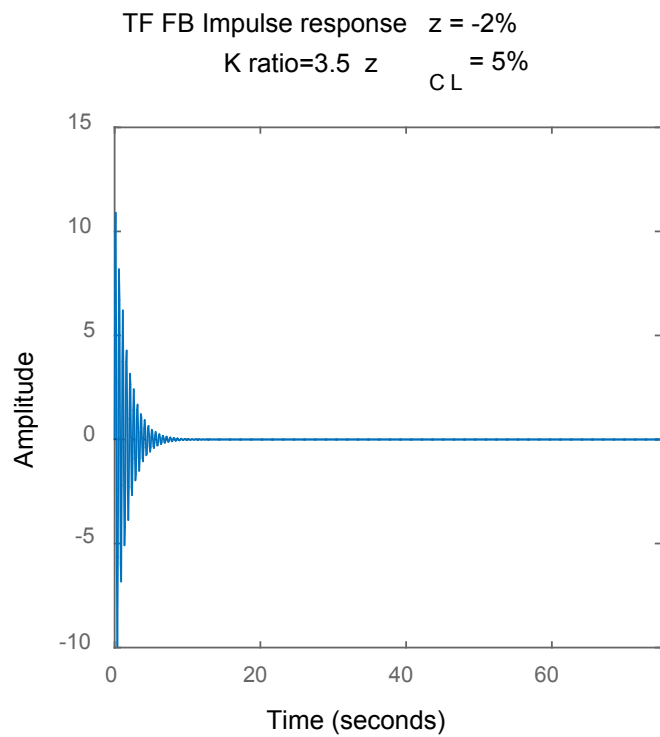
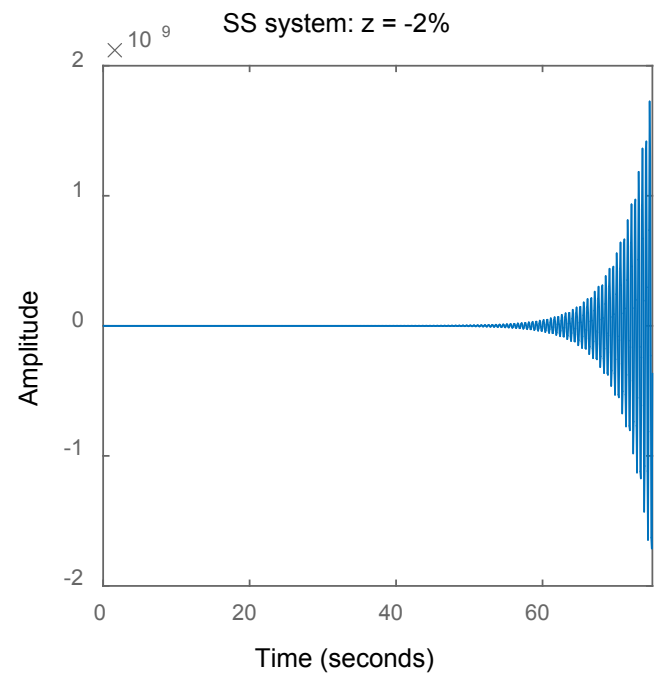
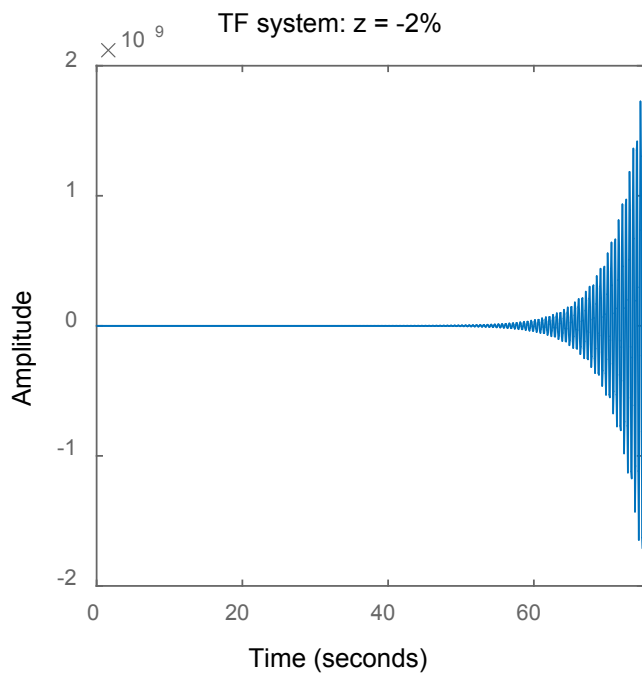
For velocity feedback use

$$H = \begin{bmatrix} 0 & K \end{bmatrix} \quad (7)$$

The $b(t) = Hz(t) = \begin{bmatrix} 0 & K \end{bmatrix} \begin{bmatrix} x(t) \\ \dot{x}(t) \end{bmatrix} = K\dot{x}(t)$ (8)

feedback signal $b(t)$

is proportional to velocity $\dot{x}(t)$.



```

1 %% DESCRIPTION
2 %{
3 SISO system time response with feedback
4 Comparison of TF and SS representations
5 use feedback function in TF
6 use direct definition of A_CL in SS
7 %}
8 %% initialization
9 opengl hardwarebasic % switch to basic hardware graphics functions
10 clc % clear command window
11 clear % clear workspace
12 % close all % close all plots
13 format compact;
14 tol=1e-10; % tolerance for discarding machine zero
15 %% DEFINE PARAMETERS
16 % ----- data for example -----
17 % ----- data for HW -----
18 m=2; % mass, kg
19 fn=2; wn=2*pi*fn; % plunge frequency, Hz
20 z=-2e-2; % plunge damping ratio
21 z_ratio=2.5; % desired z_ratio defined as zCL/|z|
22 display('HW06a')
23 display([fn z*100], 'initial data: fn, Hz; z%');
24 %% CALCULATE critical FB gain
25 K_cr=2*abs(z)/wn; % critical FB gain
26 %% DEFINE TIME RANGE
27 T=1/fn; % time scale
28 % dt=1e-3;
29 % tmax=50*T;
30 tmax=150*T;
31 Nt=1000; dt=tmax/Nt;
32 t=0:dt:tmax; % time range
33 %% CALCULATE SISO TRANSFER MATRIX
34 G=tf(wn^2,[1 2*z*wn wn^2]); % transfer function G
35 %% EXTRACT TF POLES, FREQUENCY, DAMPING of G
36 [~,poles_TF,~]=zpkdata(G); s_TF=poles_TF{1,1}; % poles
37 % display(s_TF,'poles of G')
38 f_TF=abs(imag(s_TF)/(2*pi)); % frequencies
39 zz=-real(s_TF)./abs(s_TF); z_TF=zz.*(abs(zz)>tol); % damping
40 %% CALCULATE IMPULSE RESPONSE OF TF SYSTEM
41 figure(1);
42 subplot(2,2,1); impulse(G,t);
43 title(['TF system: z = ' num2str(z_TF(1)*100) '%'])
44 %% CALCULATE SISO STATE SPACE MODEL
45 %----- state space matrices -----
46 AA=[ 0 1 ;
47 -wn^2 -2*z*wn];
48 BB=[ 0 ;
49 wn^2];
50 CC=[1 0];

```

```

51 DD=[0];
52 ss_sys=ss(AA,BB,CC,DD);
53 %% EXTRACT SS POLES, FREQUENCY, DAMPING
54 [~,zz,poles_SS]=damp(ss_sys);
55 % display(ss,'poles of ss_sys')
56 s_SS=poles_SS; % poles
57 f_SS=abs(imag(poles_SS))/(2*pi); % frequencies
58 z_SS=zz.*(abs(zz)>tol); % damping
59 %% CALCULATE IMPULSE RESPONSE OF SS SYSTEM
60 subplot(2,2,2); impulse(ss_sys,t);
61 title(['SS system: z = ' num2str(z_SS(1)*100) '%'])
62 %% ADD VELOCITY FEEDBACK TO IMPROVE DAMPING
63 K_ratio=1+z_ratio;
64 K=K_ratio*K_cr; % FB gain
65 display([z_ratio K_ratio K], 'z_ratio K_ratio K')
66 H=K*tf([1 0],1);
67 %% TF SYSTEM WITH FB
68 G_CL=feedback(G,H);
69 [~,p_CL_TF,~]=zpkdata(G_CL); s_CL_TF=p_CL_TF{1,1};
70 f_CL_TF=abs(imag(s_CL_TF))/(2*pi); % frequencies
71 zz=-real(s_CL_TF)./abs(s_CL_TF); z_CL_TF=zz.*(abs(zz)>tol); % damping
72 %% CALCULATE TF IMPULSE RESPONSE WITH FB
73 subplot(2,2,3); impulse(G_CL,t);
74 T1=['TF FB Impulse response'];
75 T2=[' z = ' num2str(z*100) '%'];
76 T3=['K ratio=' num2str(K_ratio)];
77 T4=[' z_C_L= ' num2str(z_CL_TF(1)*100) '%'];
78 line1=[T1 T2];
79 line2=[T3 T4];
80 title({line1; line2})
81 %% SS SYSTEM WITH FB
82 % ---- SS velocity feedback MATRIX-----
83 H=[0 K]; % FB matrix
84 % ===== state space matrices with FB =====
85 AA_CL=AA-BB*H; % state matrix AA with FB
86 % AA_CL=feedback(ss_sys,H); % this does not work; H should be also ss
87 CC_CL=CC-DD*H; % state matrix CC with FB
88 ss_sys_CL=ss(AA_CL, BB, CC_CL, DD);
89 %% EXTRACT POLES, FREQUENCY, DAMPING
90 [~,zz_CL_SS,poles_CL_SS]=damp(ss_sys_CL);
91 %ss_CL=eig(AA0);
92 % display(ss_CL,'poles of G_CL')
93 s_CL_SS=poles_CL_SS; % poles
94 f_CL_SS=abs(imag(poles_CL_SS))/(2*pi); % frequencies
95 z_CL_SS=zz_CL_SS.*(abs(zz_CL_SS)>tol); % damping
96 %% CALCULATE IMPULSE RESPONSE OF SS SYSTEM WITH FB
97 subplot(2,2,4); impulse(ss_sys_CL,t);
98 title(['impulse response of SS FB system: zCL SS= ' num2str(z_CL_SS(1)*100) '%'])
99 T1_SS=['SS FB Impulse response'];
100 T2_SS=[' z = ' num2str(z*100) '%'];

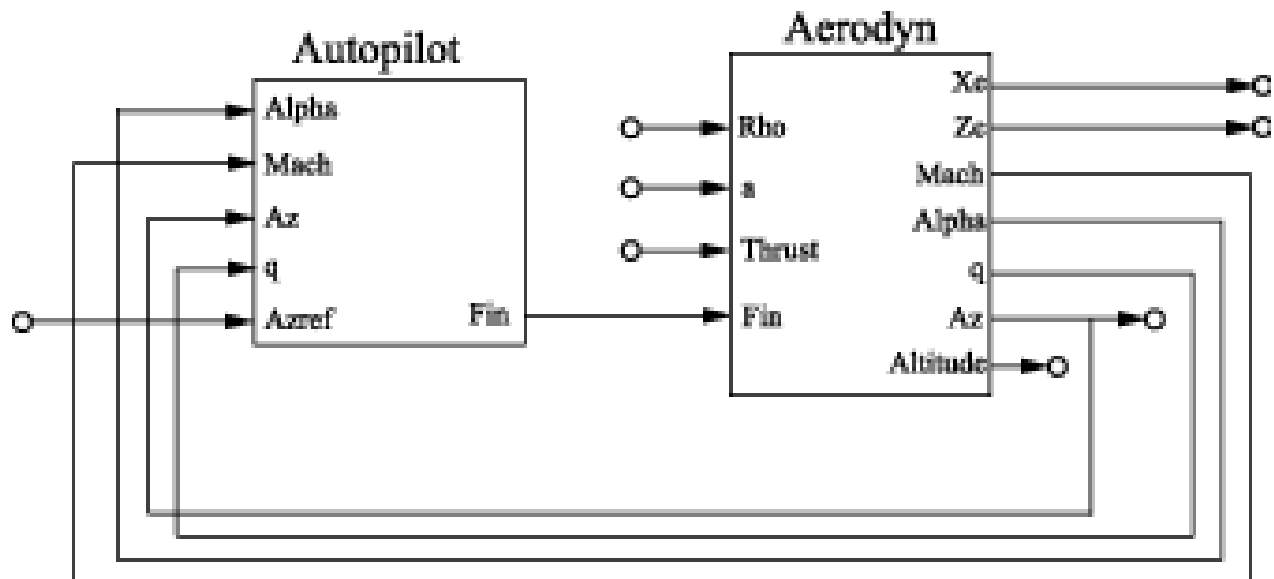
```

```
101 T3_SS=['K ratio=' num2str(K_ratio)];
102 T4_SS=[' z_CL_L= ' num2str(z_CL_TF(1)*100) '%'];
103 line1_SS=[T1_SS T2_SS];
104 line2_SS=[T3_SS T4_SS];
105 title({line1_SS; line2_SS})
106 %% DISPLAY TF RESULTS
107 display(s_TF, 'TF poles');
108 display([f_TF z_TF*100], 'f_TF, Hz; z_TF%');
109 %% DISPLAY TF FB RESULTS
110 display(s_CL_TF, 'TF FB poles');
111 display([f_CL_TF z_CL_TF*100], 'f_CL, Hz; zh_CL %');
112 %% DISPLAY SS RESULTS
113 % display(' ');
114 display(s_SS, 'SS poles');
115 display([f_SS z_SS*100], 'f_SS, Hz; z_SS%');
116 %% DISPLAY SS FB RESULTS
117 % display(' ');
118 display(s_CL_SS, 'SS FB poles');
119 display([f_CL_SS z_CL_SS*100], 'f_CL_SS, Hz; z_CL_SS%');
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```

MIMO Feedback Loop

This example shows how to obtain the closed-loop response of a MIMO feedback loop in three different ways.

In this example, you obtain the response from Azref to Az of the MIMO feedback loop of the following block diagram.



You can compute the closed-loop response using one of the following three approaches:

- Name-based interconnection with `connect`
- Name-based interconnection with `feedback`
- Index-based interconnection with `feedback`

You can use whichever of these approaches is most convenient for your application.

Load the plant `Aerodyn` and the controller `Autopilot` into the MATLAB® workspace. These models are stored in the datafile `MIMOfeedback.mat`.

```
load(fullfile(matlabroot,'examples','control','MIMOfeedback.mat'))
```

`Aerodyn` is a 4-input, 7-output state-space (ss) model. `Autopilot` is a 5-input, 1-output ss model. The inputs and outputs of both models names appear as shown in the block diagram.

Compute the closed-loop response from `Azref` to `Az` using `connect`.

```
T1 = connect(Autopilot,Aerodyn,'Azref','Az');
```

Warning: The following block inputs are not used: Rho,a,Thrust.

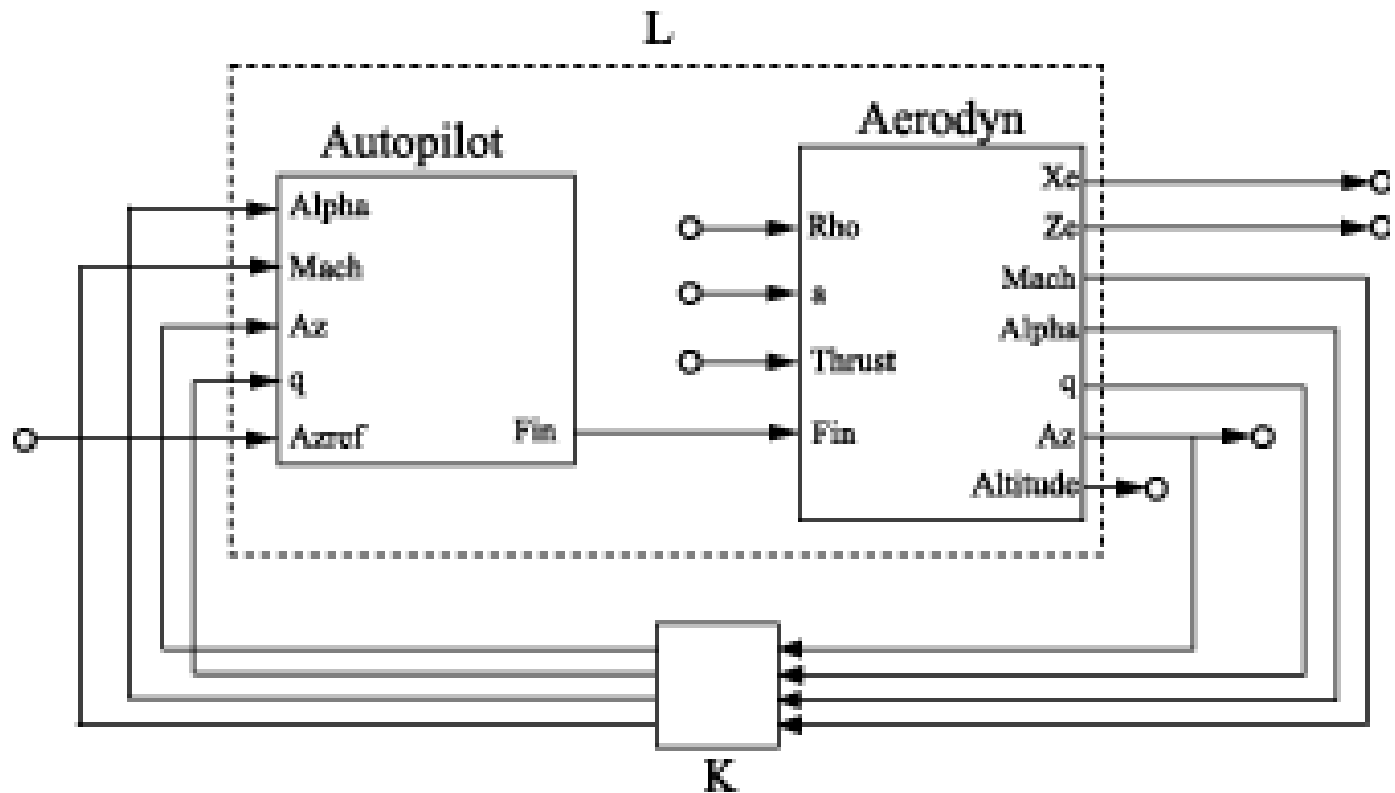
Warning: The following block outputs are not used: Xe,Ze,Altitude.

The `connect` function combines the models by joining the inputs and outputs that have matching names. The last two arguments to `connect` specify the input and output signals of the resulting model. Therefore, `T1` is

a state-space model with input Azref and output Az. The connect function ignores the other inputs and outputs in Autopilot and Aerodyn.

Compute the closed-loop response from Azref to Az using name-based interconnection with the feedback command. Use the model input and output names to specify the interconnections between Aerodyn and Autopilot.

When you use the feedback function, think of the closed-loop system as a feedback interconnection between an open-loop plant-controller combination L and a diagonal unity-gain feedback element K. The following block diagram shows this interconnection.



```
L = series(Autopilot,Aerodyn,'Fin');

FeedbackChannels = {'Alpha','Mach','Az','q'};
K = ss(eye(4),'InputName',FeedbackChannels,...
      'OutputName',FeedbackChannels);

T2 = feedback(L,K,'name',+1);
```

The closed-loop model T2 represents the positive feedback interconnection of L and K. The 'name' option causes feedback to connect L and K by matching their input and output names.

T2 is a 5-input, 7-output state-space model. The closed-loop response from Azref to Az is T2('Az','Azref').

Compute the closed-loop response from Azref to Az using feedback, using indices to specify the interconnections between Aerodyn and Autopilot.

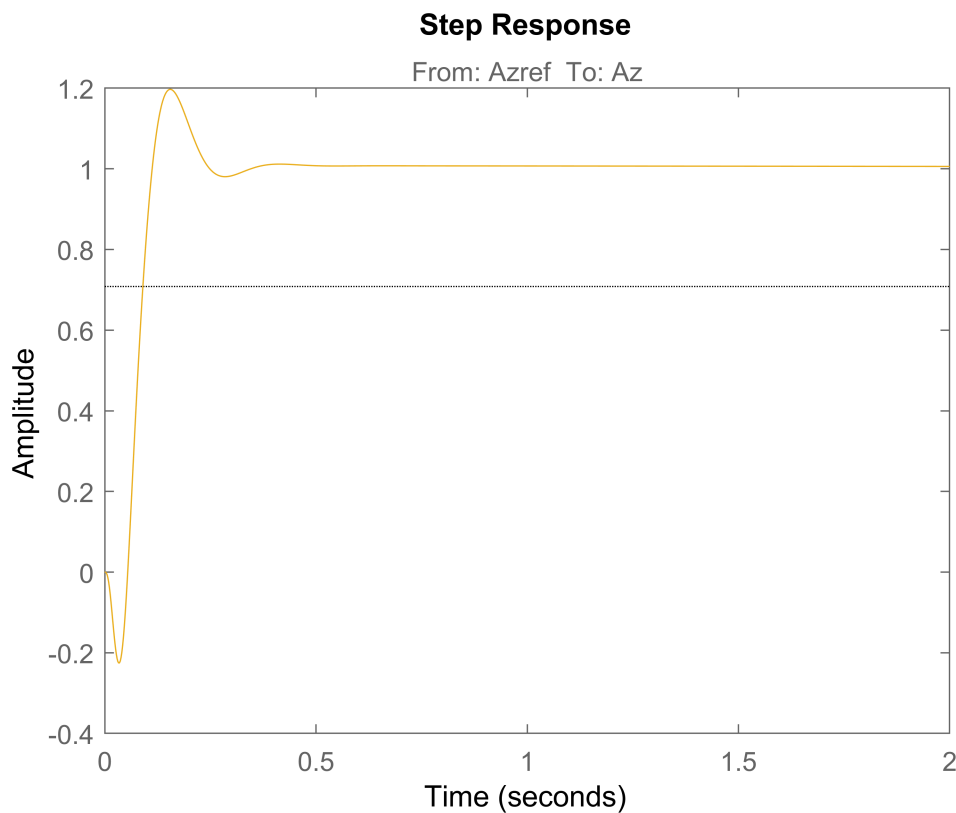
```
L = series(Autopilot,Aerodyn,1,4);  
K = ss(eye(4));  
T3 = feedback(L,K,[1 2 3 4],[4 3 6 5],+1);
```

The vectors [1 2 3 4] and [4 3 6 5] specify which inputs and outputs, respectively, complete the feedback interconnection. For example, feedback uses output 4 and input 1 of L to create the first feedback interconnection. The function uses output 3 and input 2 to create the second interconnection, and so on.

T3 is a 5-input, 7-output state-space model. The closed-loop response from Azref to Az is T3(6,5).

Compare the step response from Azref to Az to confirm that the three approaches yield the same results.

```
step(T1,T2('Az','Azref'),T3(6,5),2)
```



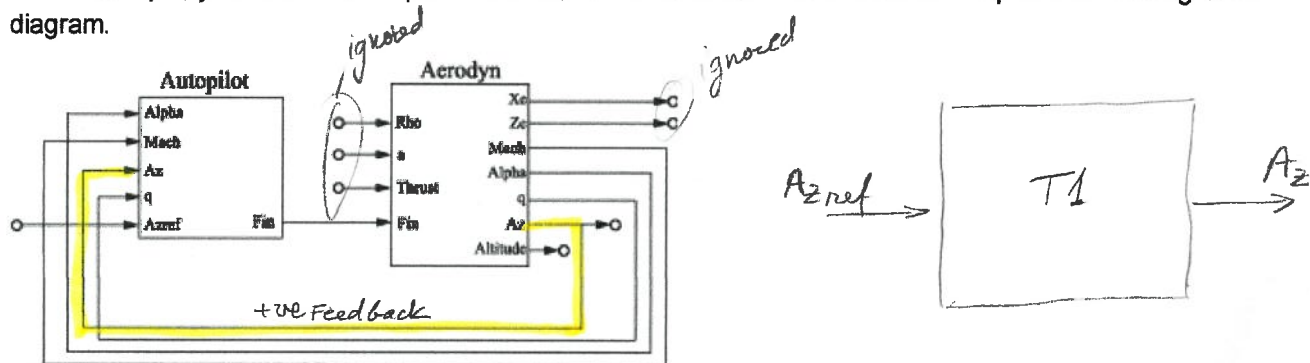
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MIMO Feedback Loop

This example shows how to obtain the closed-loop response of a MIMO feedback loop in three different ways.

[Open This Example](#)

In this example, you obtain the response from Azref to Az of the MIMO feedback loop of the following block diagram.



Compute the closed-loop response from Azref to Az using connect.

T1

```
T1 = connect(Autopilot,Aerodyn,'Azref','Az');
```

Warning: The following block inputs are not used: Rho,a,Thrust.

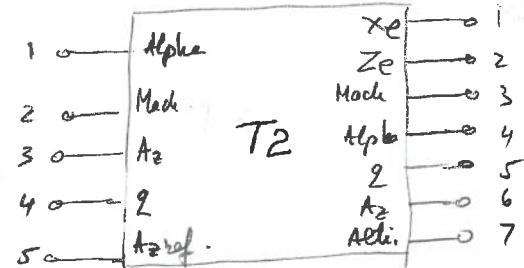
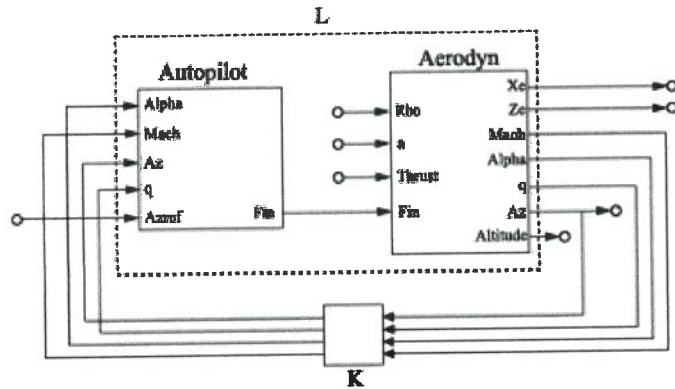
Warning: The following block outputs are not used: Xe,Ze,Altitude.

The **connect** function combines the models by joining the inputs and outputs that have **matching names**. The last two arguments to connect specify the input and output signals of the resulting model. Therefore, T1 is a

T2

Compute the closed-loop response from Azref to Az using name-based interconnection with the feedback command. Use the model input and output names to specify the interconnections between Aerodyn and Autopilot.

When you use the feedback function, think of the closed-loop system as a feedback interconnection between an open-loop plant-controller combination L and a diagonal unity-gain feedback element K. The following block diagram shows this interconnection.



`L = series(Autopilot,Aerodyn,'Fin');` *series construct using variable Fin*

`FeedbackChannels = {'Alpha','Mach','Az','q'};`
`K = ss(eye(4),'InputName',FeedbackChannels,...`
`'OutputName',FeedbackChannels);`

`T2 = feedback(L,K,'name',(1));` *match names +ve feedback*

T3

Compute the closed-loop response from Azref to Az using feedback, using indices to specify the interconnections between Aerodyn and Autopilot.

```

L = series(Autopilot, Aerodyn, 1, 4);
K = ss(eye(4));
T3 = feedback(L, K, [1 2 3 4], [4 3 6 5], +1);

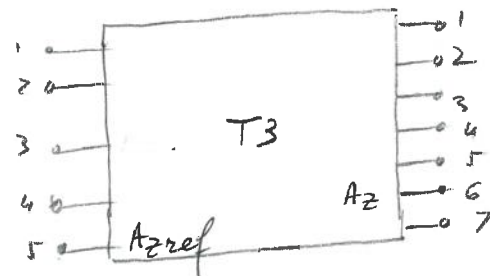
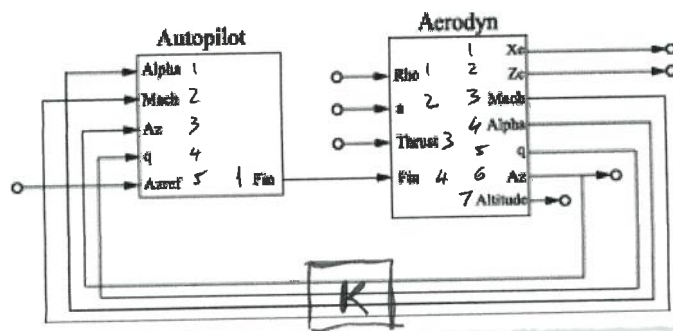
```

Handwritten notes:
 Fix out, Fix in
 Alpha Made, Alpha Made
 +ve feedback
 feedback (G, H, input, output, ±1)

The vectors $[1 \ 2 \ 3 \ 4]$ and $[4 \ 3 \ 6 \ 5]$ specify which inputs and outputs, respectively, complete the feedback interconnection. For example, feedback uses output 4 and input 1 of L to create the first feedback interconnection. The function uses output 3 and input 2 to create the second interconnection, and so on.

T3 is a 5-input, 7-output state-space model. The closed-loop response from Azref to Az is $T3(6, 5)$.

5 → siso → 6



Compare the step response from Azref to Az to confirm that the three approaches yield the same results.

```
step(T1,T2('Az','Azref'),T3(6,5),2)
```

