

Combined analysis

Purpose : use all the tools to evaluate the system stability

Time domain: Root locus of G
• Step response of G_L

Frequency domain:

- Nyquist plot of G
- Bode plots of G : margins $\left\{ \begin{array}{l} \text{gain } K_g \\ \text{phase } \phi \end{array} \right.$

Given: $G(s)$



Find: combined analysis: Quad plot

Nyquist plot	Margins on Bode plot
Root locus for Gain=1	Step response

Examples :

open MATLAB
codes

aircraft roll mode

- Nyquist plot : STABLE
- root locus 
- step response 

Bode plot : INSUFFICIENT phase margin

B11.9 - STABLE : N-plot

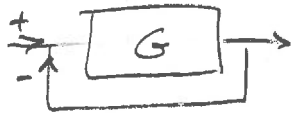
$\frac{1}{2}$ locus

step response

- INSUFFICIENT phase margin

B11.8 UNSTABLE

Combined analysis
of aircraft roll model.



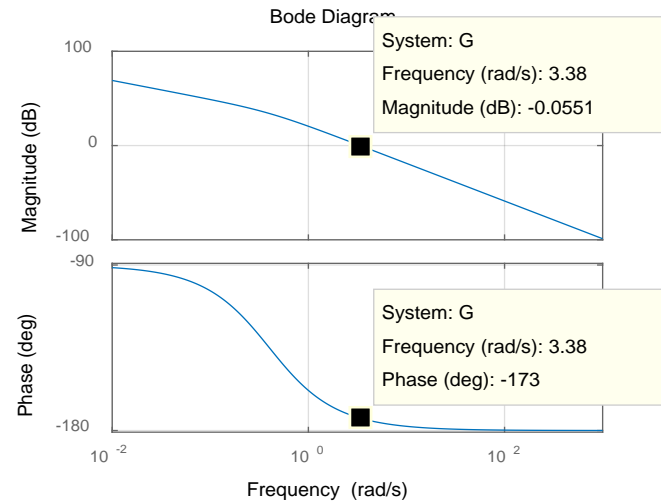
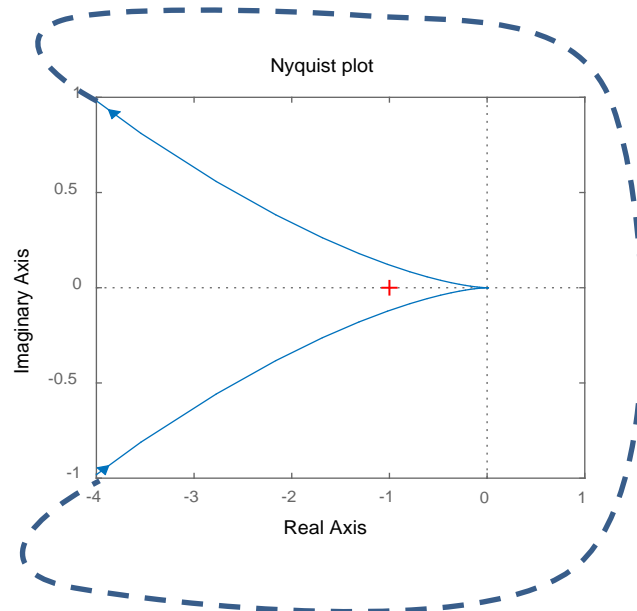
$$G(s) = \frac{K}{Js^2 + cs} = \frac{114}{10s^2 + 4s}$$

$$p_1 = 0$$

$$p_2 = -0.4$$

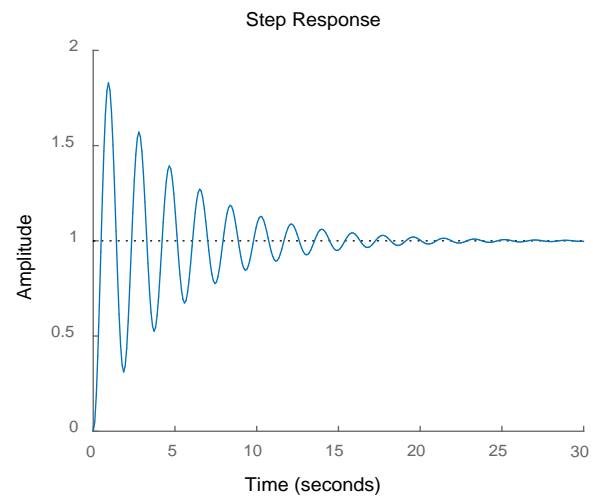
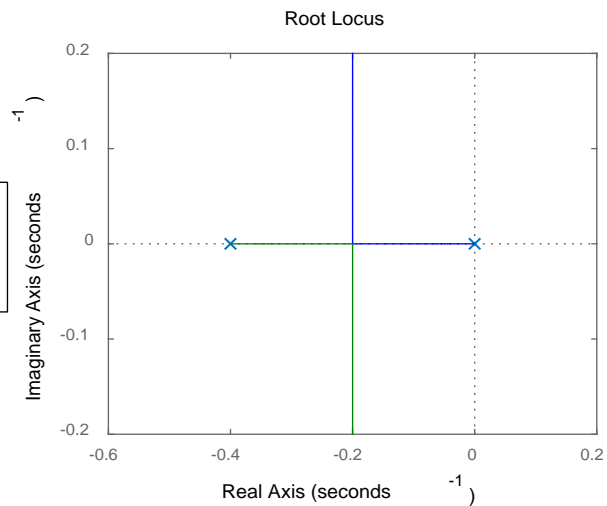
See plot

$P=0$
 $N=0$
 $Z=0$
 STABLE



$GM=\infty$
 $PM=7^\circ$
 INSUFFICIENT PM

roots always
 in LHS



Very lightly damped
 step response
 with many oscillations

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2017 04 17

Aircraft roll model combined analysis (cont.)

Nyquist.

✓ stable

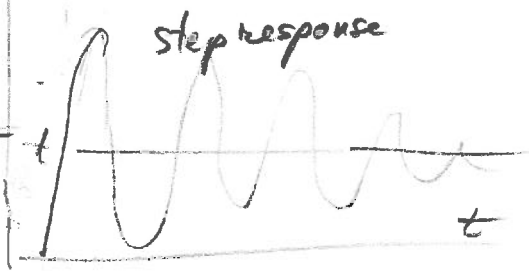
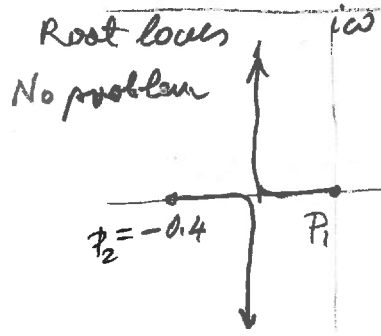
$Z=0$

Bode

Margins

$(K_g)_{dB} = \infty$ ✓

$\gamma^0 = 7^0$ Not sufficient



Conclusion

- Nyquist and root locus indicate stable system.
- Margin analysis warns about low phase margin: need compensator
- step response — oscillatory

Problem B11.9



$$G(s) = \frac{20 (s^2 + s + 0.5)}{s(s-1)(s+10)}$$

$$\left. \begin{array}{l} p_1 = 0 \\ p_2 = +1 \\ p_3 = -10 \end{array} \right\} P = 1$$

Nyquist

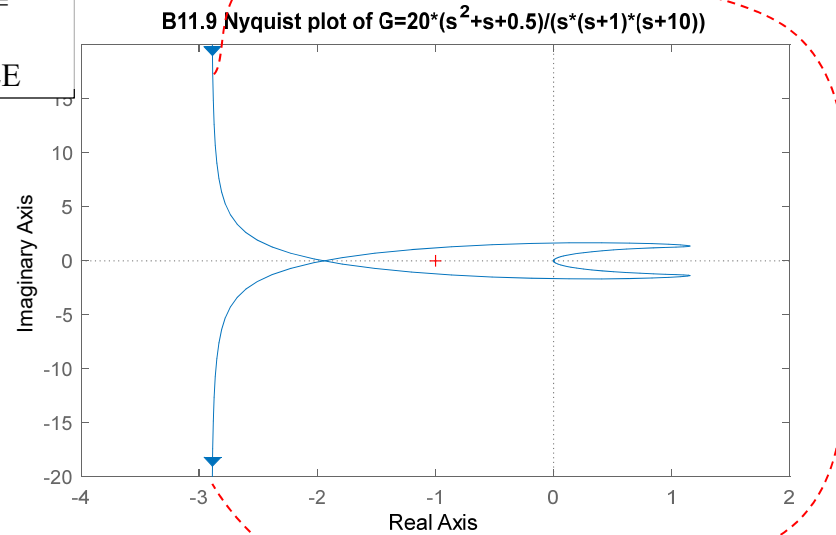
Bode

root locus

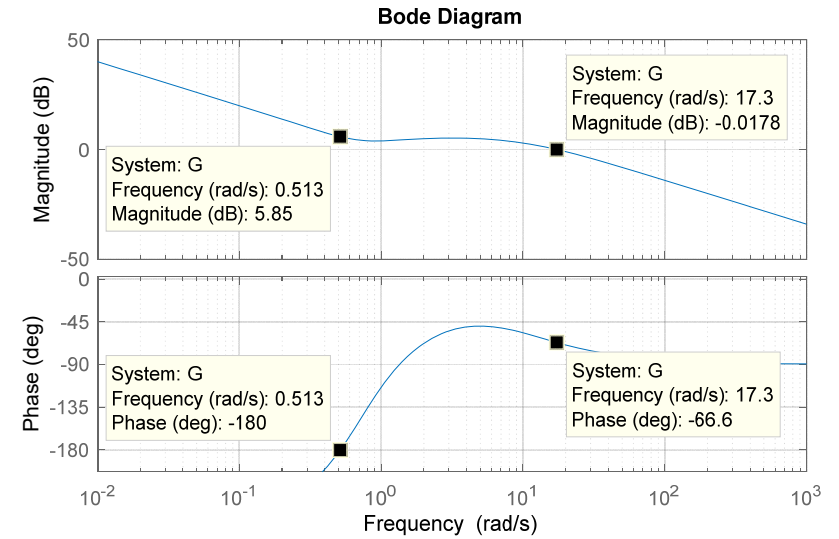
step response

see plot

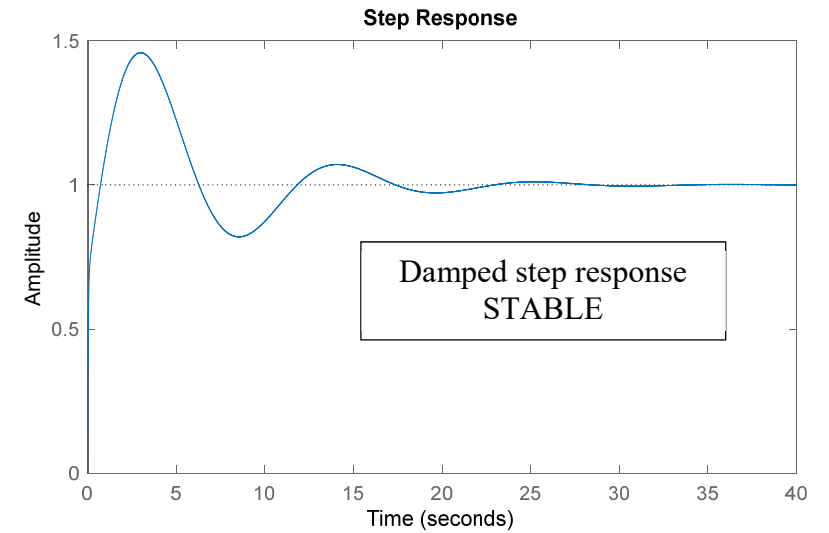
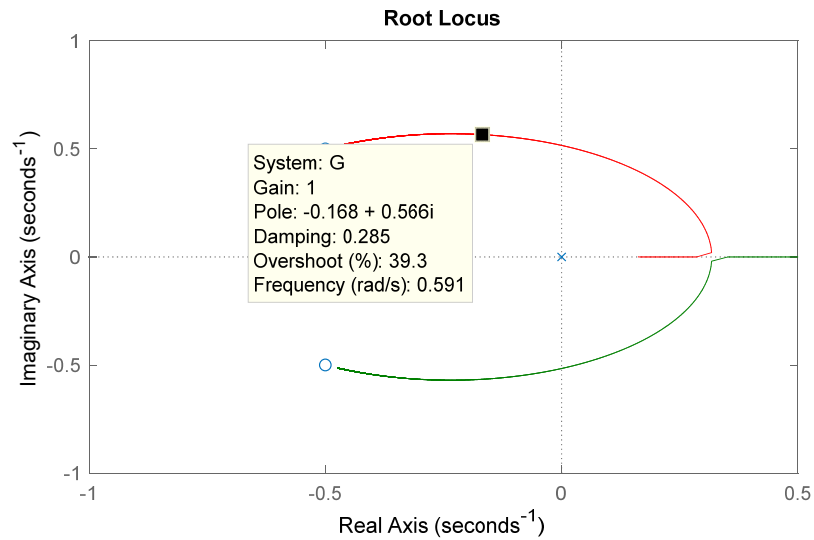
$N = -2$
 $P = +1$
 $Z = -1$
STABLE



Good phase margin $PM = \sim 114$ deg
 Bad gain margin $GM = \sim 5.85$ dB

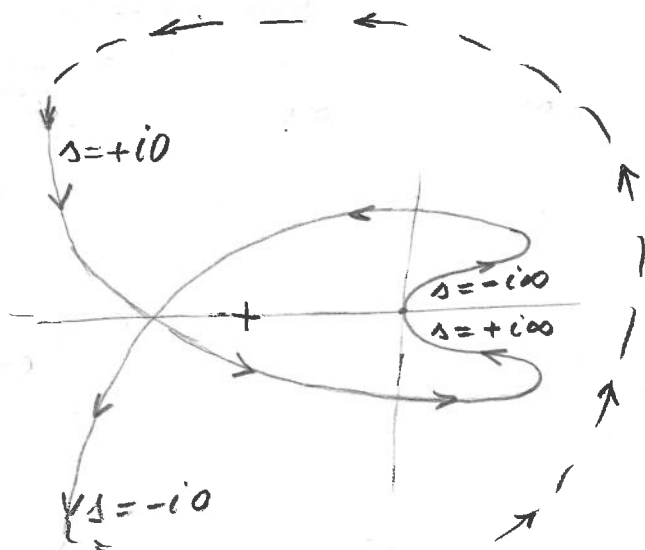


$K = 1$ point
 is in LHS
STABLE



Problem B11.9 (cont.)

Nyquist plot



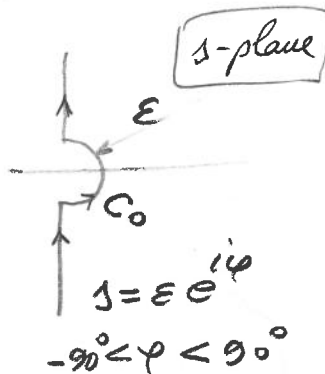
G-plane

$$G^0 = \frac{z_0}{-1} = -2 \frac{1}{\epsilon} e^{-i\varphi}$$

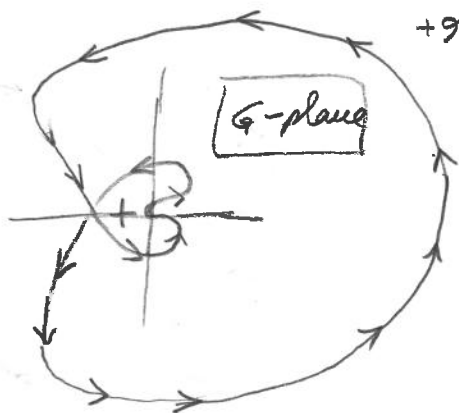
$$G^0 = \frac{2}{\epsilon} e^{i(180^\circ - \varphi)}$$

$$-90^\circ < \varphi < 90^\circ$$

$$-90^\circ < \angle G^0 < -270^\circ + 90^\circ$$



s-plane



$$N = -2$$

$$P = 1$$

$$Z = -1$$

stable

(B11.9 cont.)

Bode plot

Good phase margin: $\gamma \approx 114^\circ @ 16.6 \frac{\text{rad}}{\text{sec}}$

Bad gain margin: $K_g = -5.3 \text{ dB} @ 0.55 \frac{\text{rad}}{\text{sec}}$
at low freq.

Good gain margin at higher $\omega > 16 \frac{\text{rad}}{\text{sec}}$, \angle

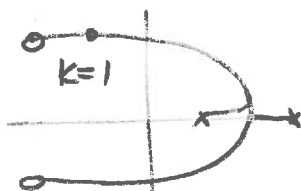
(ϕ does not cross -180°)

There could be problems at low ω
($\omega \sim 0.5 \text{ rad/sec}$) due to imperfections

Root locus

$K=1$ in LHS

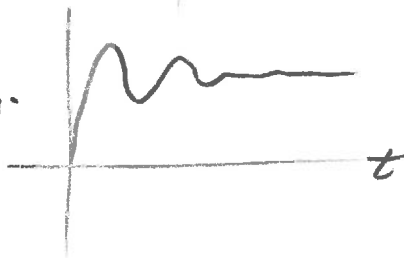
Stable



Step response

damped oscillation.

STABLE



Problem B11.8



$$G(s) = \frac{320(s+2)}{s(s+1)(s^2+8s+44)}$$

4 Poles: 0

-1

$-4 \pm i5.3$

all in LHS

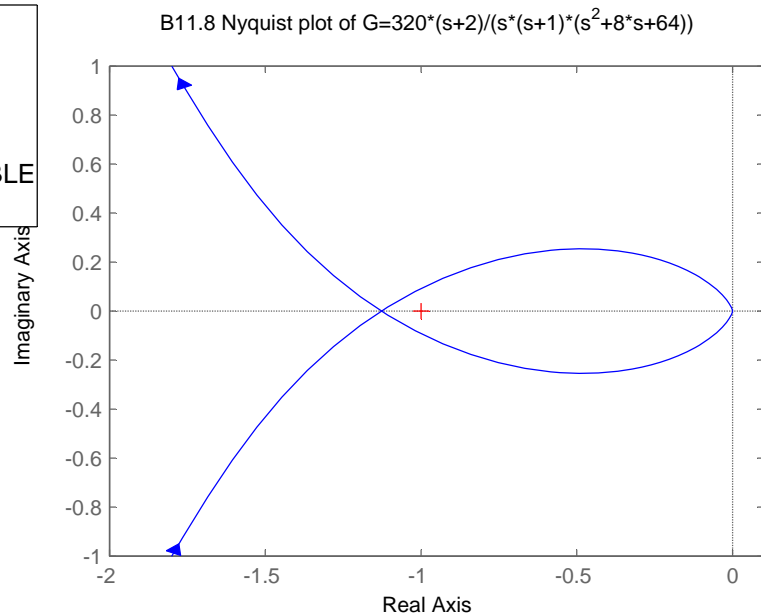
N	B
R	S

see plot

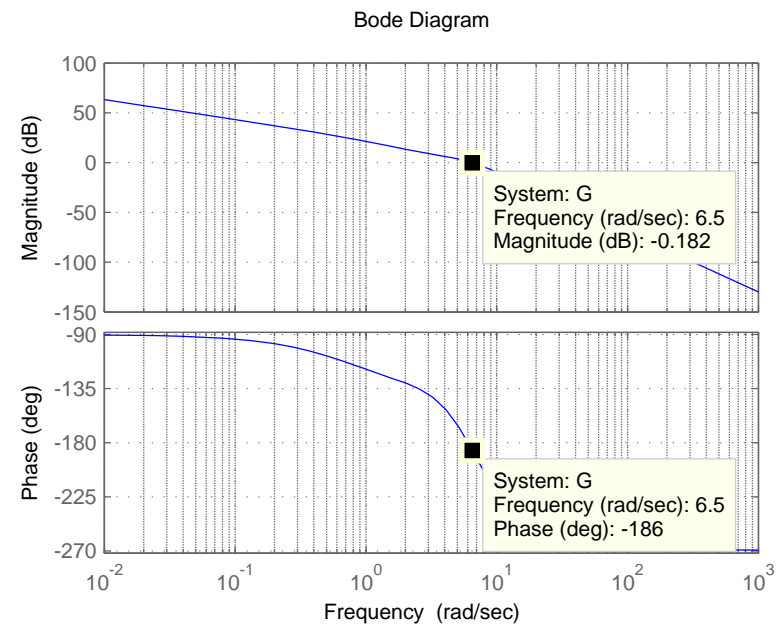
N=2
P=0

Z=2

UNSTABLE

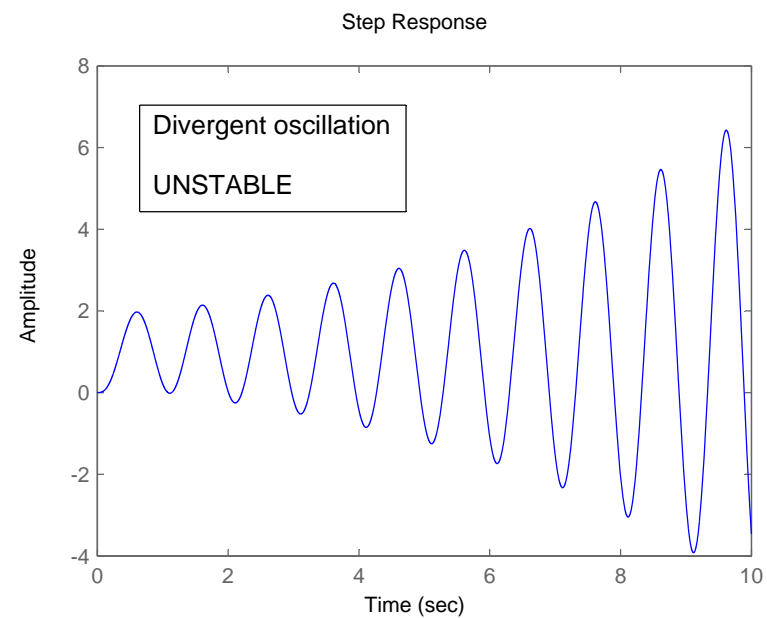
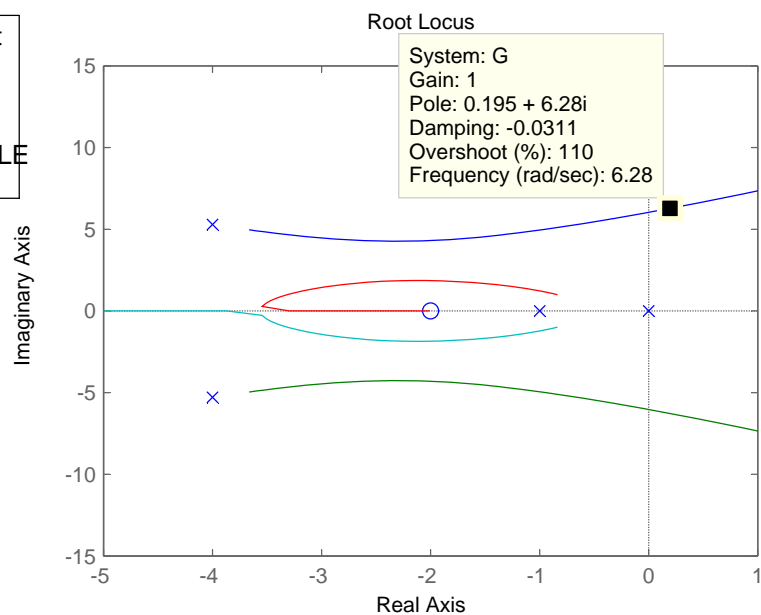


Negative phase and gain margins: UNSTABLE



K=1 point
is in the
RHS

UNSTABLE



Problem B11.8 (cont.)

Nyquist plot

$P = 0$ no poles in RHS

$N = 2$

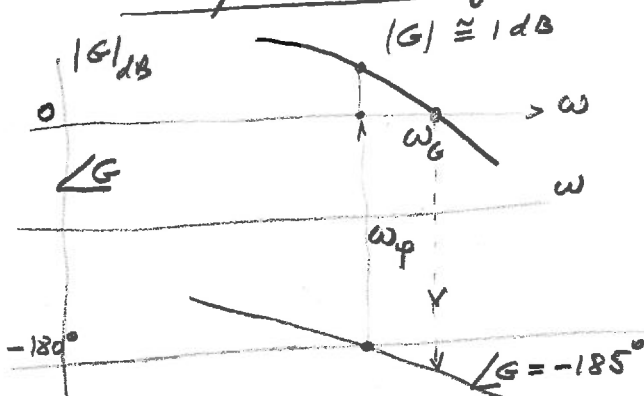
$Z = P + N = 2$ zeros
in RHS of $1 + G(s)$
UNSTABLE

because

$$G_{CL} = \frac{G(s)}{1 + G(s)}$$

Bode plot: margins

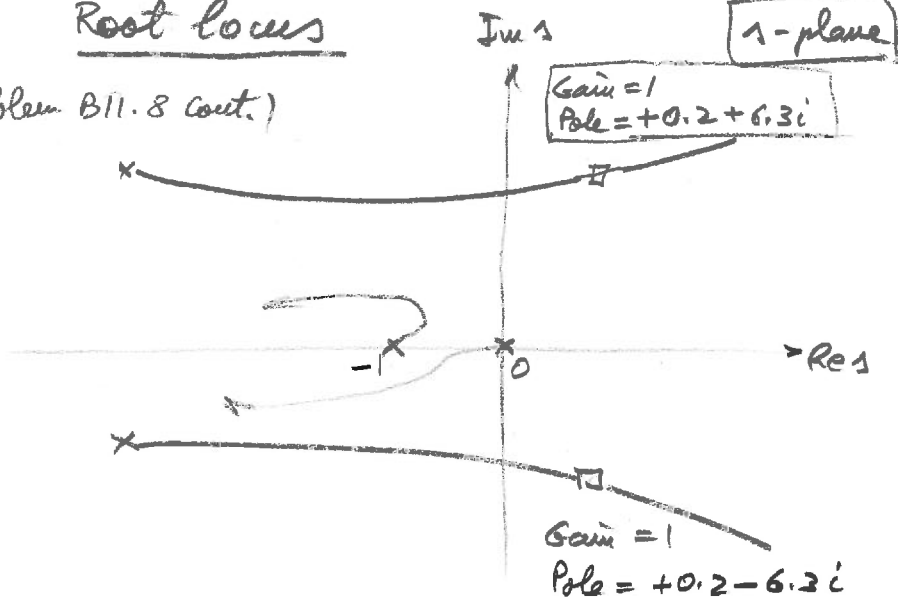
$K_g = -1 \text{ dB} < 0 \text{ dB}$



UNSTABLE

Root locus

(Problem B11.8 cont.)

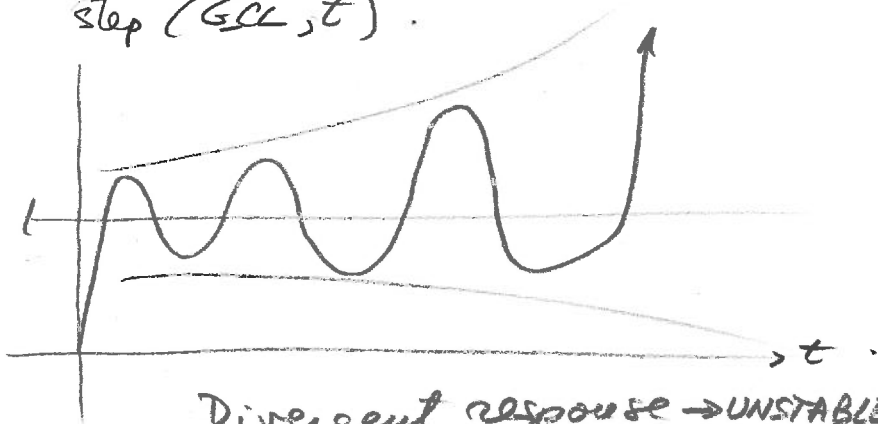


Roots in RHS \rightarrow UNSTABLE.

Step response

$$G_{CL} = \text{feedback}(G, 1).$$

$$\text{step}(G_{CL}, t).$$



Divergent response \rightarrow UNSTABLE

All four criteria predicted an

UNSTABLE closed loop response

ACTION: DO NOT close the loop!