OSNOVE BIOMEDICINSKOG INŽENJERSTVA

DIFERENCIJALNI POJAČAVAČ

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- Polazna osnova za projektovanje elektrofizioloskog pojačavača;
- Pojačava razliku signala na svojim ulaznim priključcima;
- · Veliko diferencijalno pojačanje;
- Visok CMRR;
- Mala ulazna impedansa;

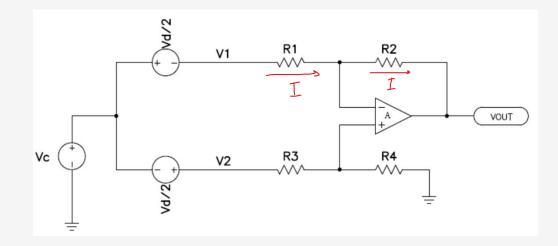
$$V_{1} = V_{C} - \frac{V_{D}}{2}$$

$$V_{2} = V_{C} + \frac{V_{D}}{2}$$

$$V^{+} = \frac{R_{4}}{R_{3} + R_{4}} \cdot V_{2}$$

Zbog postajanja negativne povratne sprege i velikog pojačanja u otvorenoj povratnoj sprezi, naponi na invertujućem i neinvertujućem <mark>ulazu</mark> su jednaki, tj.

$$V^{-} = V^{+} = \frac{R_4}{R_3 + R_4} \cdot V_2$$



$$\begin{split} V_{OUT} = & \left(\frac{R_1 + R_2}{R_1} \cdot \frac{R_4}{R_3 + R_4} - \frac{R_2}{R_1} \right) \cdot V_C + \frac{1}{2} \cdot \left(\frac{R_1 + R_2}{R_1} \cdot \frac{R_4}{R_3 + R_4} + \frac{R_2}{R_1} \right) \cdot V_D \\ V_{OUT} = & A_C \cdot V_C + A_D \cdot V_D \\ A_C = & \frac{R_1 + R_2}{R_1} \cdot \frac{R_4}{R_3 + R_4} - \frac{R_2}{R_1} \\ A_D = & \frac{1}{2} \cdot \left(\frac{R_1 + R_2}{R_1} \cdot \frac{R_4}{R_3 + R_4} + \frac{R_2}{R_1} \right) \end{split}$$

Diferencijalni pojačavač

Ad – Pojačanje diferencijalnog signala Ac – Slabljenje signala zajedničkog moda

$$CMRR_{dB} = 20\log\left(\frac{A_{D}}{A_{C}}\right) = 20\log\left(\frac{R_{4} \cdot (R_{1} + R_{2}) + R_{2} \cdot (R_{3} + R_{4})}{2 \cdot (R_{4} \cdot (R_{1} + R_{2}) - R_{2} \cdot (R_{3} + R_{4}))}\right)$$

Da bi CMRR bio što je moguće veći, neophodno je balansirati pojačavač.

$$\begin{split} A_C &= 0 \\ \frac{R_1 + R_2}{R_1} \cdot \frac{R_4}{R_3 + R_4} - \frac{R_2}{R_1} &= 0 \Rightarrow \frac{R_4}{R_3} = \frac{R_2}{R_1} \\ A_D &= \frac{\overline{R}_2}{R_1} \end{split}$$

Diferencijalni pojačavač

Ukoliko na ulaz pojačavača postavimo elektrode istih otpornosti, pojačanje pojačavača postaje:

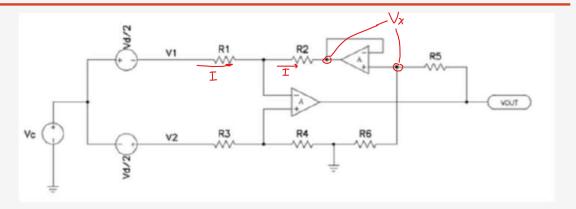
$$A_D = \frac{R_2}{R_1 + R_E}$$

Ukoliko na ulaz pojačavača postavimo elektrode različitih otpornosti, pojačanje pojačavača postaje:

$$\begin{split} V_{OUT} &= A_C \cdot V_C + A_D \cdot V_D \\ A_C &= \left(\frac{R_2}{R_1 + R_2 + R_{E1}} \cdot \frac{R_1 + R_2 + R_{E1}}{R_1 + R_{E2}} - \frac{R_2}{R_1 + R_{E1}} \right) \\ A_D &= \frac{1}{2} \cdot \left(\frac{R_2}{R_1 + R_2 + R_{E1}} \cdot \frac{R_1 + R_2 + R_{E1}}{R_1 + R_{E2}} + \frac{R_2}{R_1 + R_{E1}} \right) \end{split}$$

Modifikovani diferencijalni pojačavač

- Standardni diferencijalni pojačavač ima problem jednostavne promene diferencijalnog pojačanja;
- Problem promene pojačanja se može rešiti dodavanjem bafera i razdelnika napona u negativnu povratnu spregu;



$$V_{OUT} = \frac{R_5 + R_6}{R_6} \cdot \left(\frac{R_1 + R_2}{R_1} \cdot \frac{R_4}{R_3 + R_4} - \frac{R_2}{R_1} \right) \cdot V_C + \frac{1}{2} \cdot \frac{R_5 + R_6}{R_6} \cdot \left(\frac{R_1 + R_2}{R_1} \cdot \frac{R_4}{R_3 + R_4} + \frac{R_2}{R_1} \right) \cdot V_D$$

$$V_{OUT} = A_C \cdot V_C + A_D \cdot V_D$$

$$A_C = \frac{R_5 + R_6}{R_6} \cdot \left(\frac{R_1 + R_2}{R_1} \cdot \frac{R_4}{R_3 + R_4} - \frac{R_2}{R_1} \right)$$

$$A_D = \frac{1}{2} \cdot \frac{R_5 + R_6}{R_6} \cdot \left(\frac{R_1 + R_2}{R_1} \cdot \frac{R_4}{R_3 + R_4} + \frac{R_2}{R_1} \right)$$

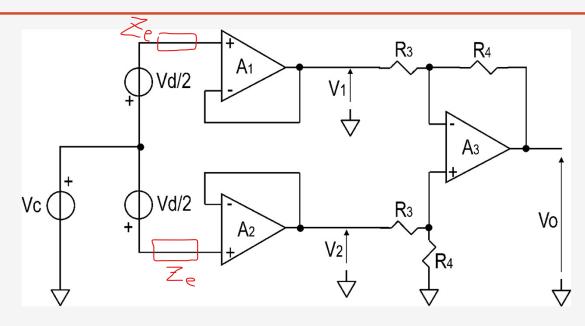
Na osnovu izraza za Ac, može se videti da modifikacija ne utiče na potiskivanje signala zajedničkog moda i da se balansiranje vrši isto kao kod standardnog diferencijalnog pojačavača.

$$A_D = \frac{R_2}{R_1} \cdot \frac{R_5 + R_6}{R_6}$$

Modifikovani diferencijalni pojačavač

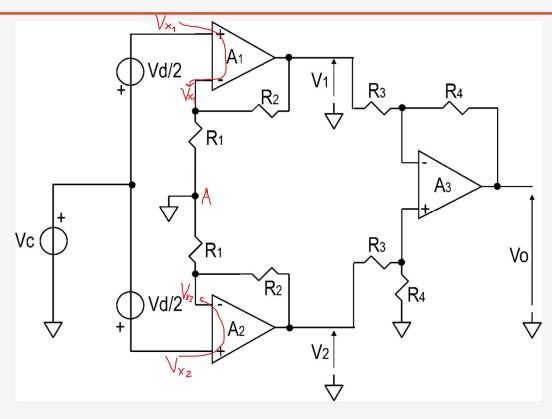
- Modifikacijom standardnog diferencijalnog pojačavača, rešen je problem jednostavne promene pojačanja;
- Pojačanje se može menjati u dva stepena. Preporuka je da se prvo postavi minimalna vrednost pojačanja pomoću otponika R1 i R2, a u dodatnoj mreži da se postavi ostatak pojačanja;
- Jednostavna promena pojačanja se može implementirati ubacivanjem potenciometra umesto otpornika R5;
- Problem male ulazne impedanse ostaje nerešen;

Baferovani diferencijalni pojačavač



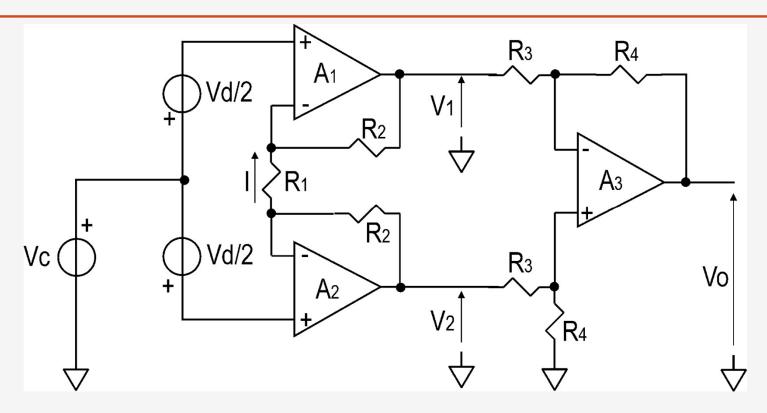
$$V_1 = V_c - \frac{V_d}{2}$$
 $V_2 = V_c + \frac{V_d}{2}$ $V_o = \frac{R_4}{R_3} (V_2 - V_1)$

Ulazni stepen sa <mark>neinvertujućim</mark> pojačavačima



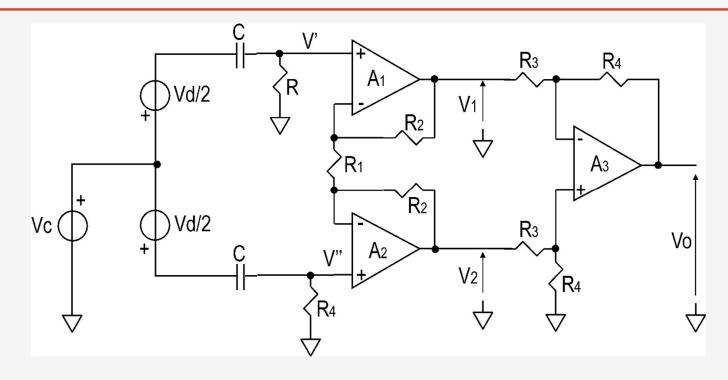
$$V_{1} = \left(1 + \frac{R_{2}}{R_{1}}\right) (V_{c} - \frac{V_{d}}{2}) \quad V_{2} = \left(1 + \frac{R_{2}}{R_{1}}\right) (V_{c} + \frac{V_{d}}{2}) \quad V_{o} = \frac{R_{4}}{R_{3}} (V_{2} - V_{1})$$

Instrumentacioni pojačavač sa tri operaciona pojačavača



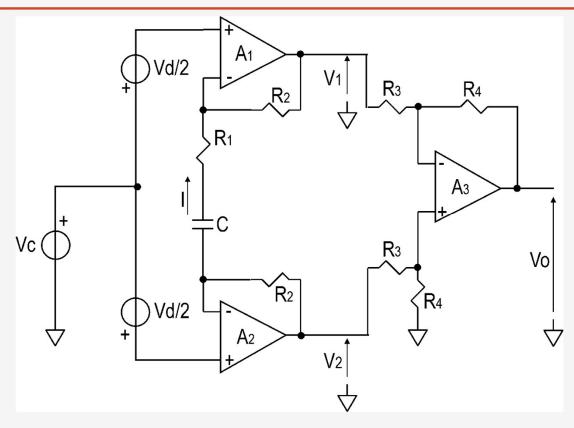
$$I = \frac{V_d}{R_1} \quad V_1 = V_c - (1 + \frac{2R_2}{R_1}) \frac{V_d}{2} \quad V_2 = V_c + (1 + \frac{2R_2}{R_1}) \frac{V_d}{2} \quad V_o = \frac{R_4}{R_3} (V_2 - V_1)$$

Potiskivanje <mark>jednosmerne</mark> komponente diferencijalnog signala na ulazu pojačavača



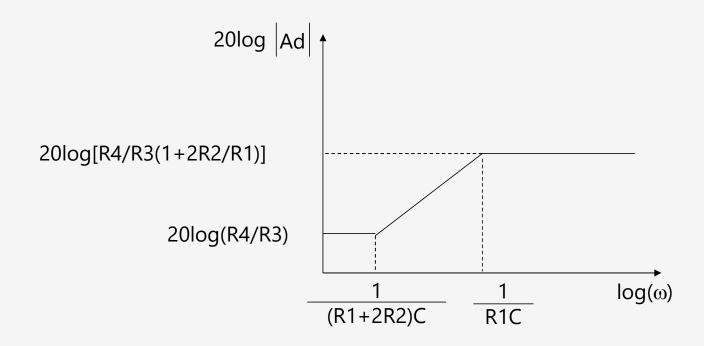
$$V' = \left(V_c - \frac{V_d}{2}\right) \frac{sCR}{1 + sCR} \quad V'' = \left(V_c + \frac{V_d}{2}\right) \frac{sCR}{1 + sCR} \quad V_o = \frac{R_4}{R_3} \left(1 + \frac{2R_2}{R_1}\right) \frac{sCR}{1 + sCR} V_d$$

Potiskivanje jednosmerne komponente diferencijalnog signala na ulazu pojačavača

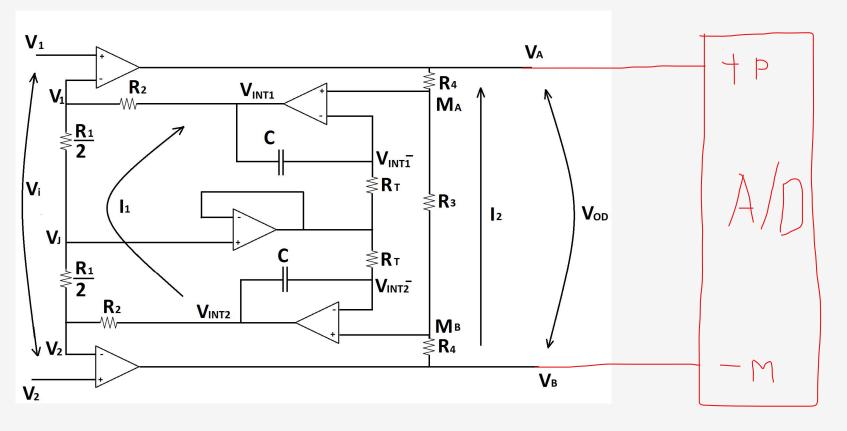


$$I = \frac{V_d}{R_1 + \frac{1}{sC}} \quad V_1 = V_c - (1 + \frac{2R_2}{R_1 + \frac{1}{sC}}) \frac{V_d}{2} \quad V_2 = V_c + (1 + \frac{2R_2}{R_1 + \frac{1}{sC}}) \frac{V_d}{2} \quad V_o = \frac{R_4}{R_3} \frac{1 + sC(R_1 + 2R_2)}{1 + sCR_1} V_d$$

Frekvencijska karakteristika pojačavača

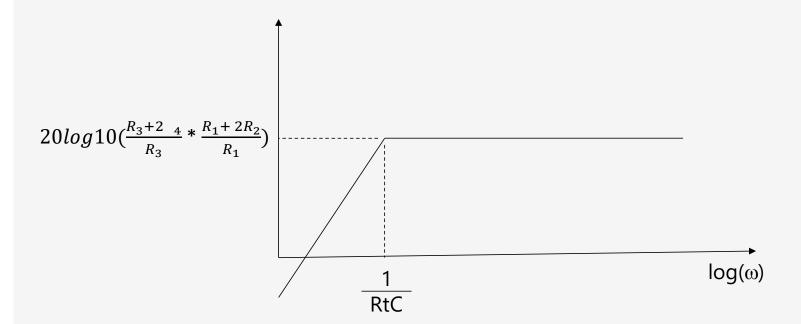


Potiskivanje jednosmerne komponente diferencijalnog signala na ulazu pojačavača

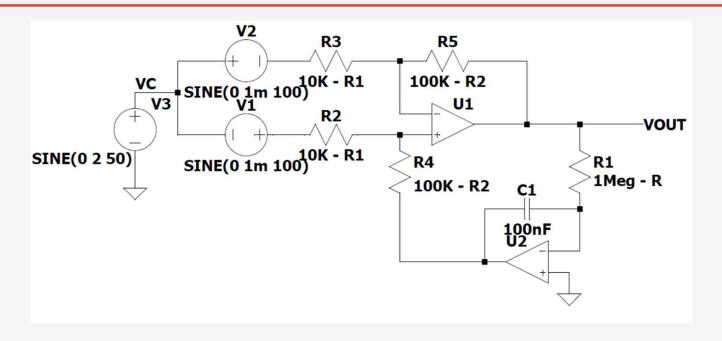


$$\frac{V_{OD}}{V_i}$$
 (s) = $\frac{R_3 + 2R_4}{R_3} * \frac{R_1 + 2R_2}{R_1} * \frac{sRC_T}{1 + sCR_T}$

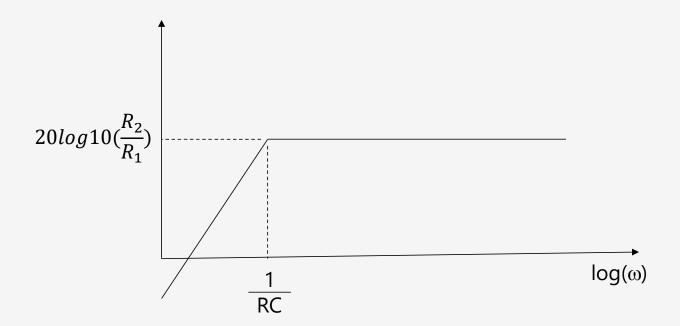
Frekvencijska karakteristika pojačavača



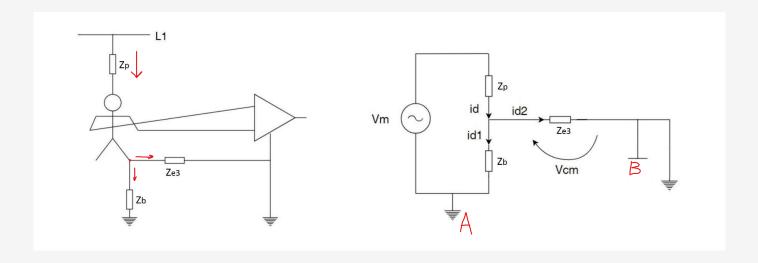
Potiskivanje jednosmerne komponente diferencijalnog signala u diferencijalnom pojačavaču



$$\frac{V_o(s)}{V_i(s)} = \frac{R_2}{R_1} \frac{sRC}{1 + sRC}$$



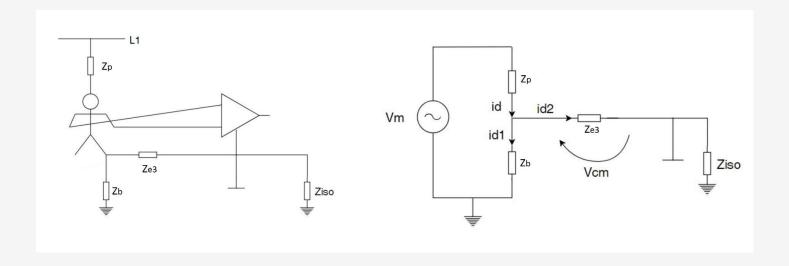
Treća elektroda - uzemljena



$$Z_{e3} \ll Z_b \to i_{d2} \approx i_d$$

$$V_{cm} = Z_{e3}i_d$$

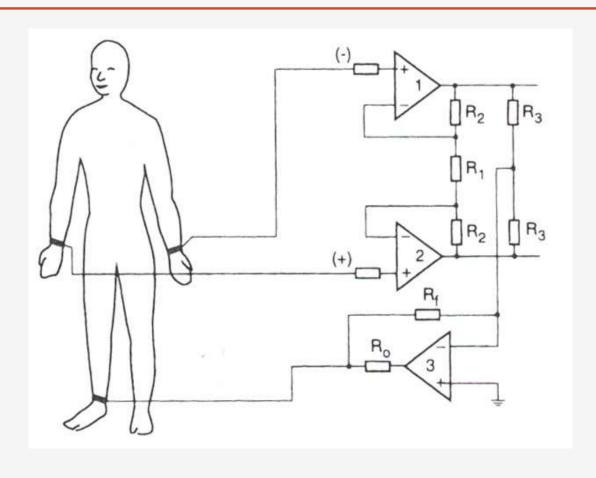
Treća elektroda – spojena na masu izolovanog pojačavača



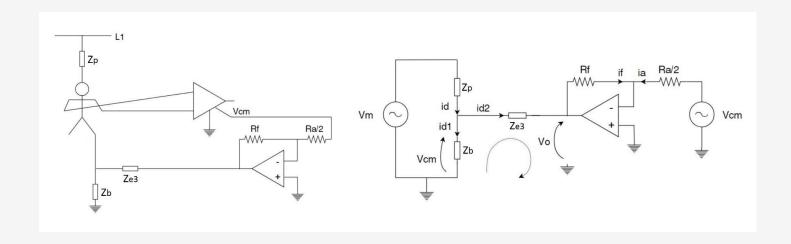
$$i_{d2} = i_d \frac{Z_b}{Z_b + Z_{e3} + Z_{iso}}$$
 $V_{cm} = i_{d2} Z_{e3}$

$$V_{cm} = \frac{Z_b}{Z_b + Z_{e3} + Z_{iso}} Z_{e3} i_d$$

DRL kolo - Driven Right Leg



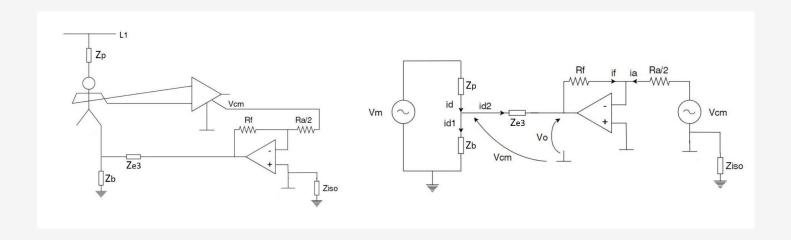
DRL kolo kod uzemljenog pojačavača Driven Right Leg



$$\frac{2V_{cm}}{R_a} + \frac{V_o}{R_f} = 0 V_o = -\frac{2R_f}{R_a}V_{cm} V_{cm} = V_o + Z_{e3}i_{d2} Z_b \gg Z_{e3} \to i_{d2} \approx i_d$$

$$V_{cm} = V_o + Z_{e3}i_d \qquad V_{cm} = -\frac{2R_f}{R_a}V_{cm} + Z_{e3}i_d \qquad V_{cm}\left(1 + \frac{2R_f}{R_a}\right) = Z_{e3}i_d \qquad V_{cm} = \frac{1}{\left(1 + \frac{2R_f}{R_a}\right)}Z_{e3}i_d$$

DRL kolo kod izolovanog pojačavača Driven Right Leg



$$i_{d2} \approx i_d \frac{Z_b}{Z_b + Z_{e3} + Z_{iso}} \quad \frac{2V_{cm}}{R_a} + \frac{V_o}{R_f} = 0 \qquad V_o = -\frac{2R_f}{R_a}V_{cm} \quad V_{cm} = V_o + Z_{e3}i_{d2}$$

$$V_{cm} = -\frac{2R_f}{R_a}V_{cm} + Z_{e3}i_{d2} \qquad V_{cm} = \frac{Z_{e3}}{\left(1 + \frac{2R_f}{R_a}\right)}i_{d2} \qquad V_{cm} = \frac{1}{\left(1 + \frac{2R_f}{R_a}\right)}\frac{Z_b}{Z_b + Z_{e3} + Z_{iso}}Z_{e3}i_{d3}$$

Komercijalni pojačavači – AD8232 Analog Devices

FEATURES

Fully integrated single-lead ECG front end

Low supply current: 170 µA (typical)

Common-mode rejection ratio: 80 dB (dc to 60 Hz)

Two or three electrode configurations

High signal gain (G = 100) with dc blocking capabilities

2-pole adjustable high-pass filter

Accepts up to ±300 mV of half cell potential Fast restore feature improves filter settling

Uncommitted op amp

3-pole adjustable low-pass filter with adjustable gain

Leads off detection: ac or dc options Integrated right leg drive (RLD) amplifier Single-supply operation: 2.0 V to 3.5 V

Integrated reference buffer generates virtual ground

Rail-to-rail output Internal RFI filter 8 kV HBM ESD rating

Shutdown pin

20-lead, 4 mm \times 4 mm LFCSP and LFCSP_SS package

Qualified for automotive applications

APPLICATIONS

Fitness and activity heart rate monitors

Portable ECG

Remote health monitors

Gaming peripherals

Biopotential signal acquisition

FUNCTIONAL BLOCK DIAGRAM

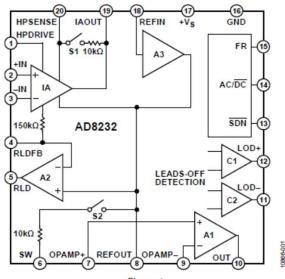


Figure 1.

Komercijalni pojačavači – AD8232 Analog Devices

