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# Abstract

Multiple studies have shown that the mere observation of movements by a robot can affect an observing human’s movement; effects referred to as motor contagions. However, previous studies have either analyzed motor contagions induced during (which we call *on-line* contagions), or induced after (*off-line* contagions) observation of the robot, but never both together. It thus remains unclear whether and how these two contagions differ from each other. Here, in an empirical industrial co-worker setting, we examine the differences in the off-line and on-line contagions induced in participants by the observation of the same movements performed by a human, or a humanoid robot co-worker. We observed that while the off-line contagions predominantly affect the participant’s movement velocity, the on-line contagions affect their movement frequency. Furthermore, the off-line contagions were prominent after observing another human, while the on-line contagions were equally strong with either a human or a humanoid co-worker. These results suggest that actions by a humanoid robot can induce distinct effects on human behaviors, during and after observation.

Does the presence of a robot co-worker influence the performance of humans around it? Studies of motor contagions during human-robot interactions have examined either how the observation of a robot affects a human’s movement velocity, or how it affects the human’s movement variance, but never both together. Performance however, has to be measured considering both task speed (or frequency) as well as task accuracy. Here we examine an empirical repetitive industrial task in which a human participant and a humanoid robot work near each other. We systematically varied the robot behavior, and observed whether and how the performance of a human participant is affected by the presence of the robot. To investigate the effect of physical form, we added conditions where the robot co-worker torso and head were covered, and only the moving arm was visible to the human participants. Finally, we compared these behaviors with a human co-worker, and examined how the observed behavioral affects scale with experience of robots. Our results show that human task frequency, but not task accuracy, is affected by the observation of a humanoid robot co-worker, provided the robot’s head and torso are visible.

# *Acknowledgements*

The acknowledgements and the people to thank go here, don't forget to include your project advisor...

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# Abbreviations

**LAH** List Abbreviations **Here**

# Physical Constants

Speed of Light  $c = 2.997\,924\,58 \times 10^8 \text{ ms}^{-\text{s}}$  (exact)

# Symbols

$a$	distance	m
$P$	power	W ( $\text{Js}^{-1}$ )
$\omega$	angular frequency	$\text{rads}^{-1}$

*For/Dedicated to/To my...*

## Chapter 1

# Bi-directional dual arm object handover

## **1.1 Introduction\***

- perform fluid object handover in a dynamic settings
- Design a planner considering humans field of view, attention, preferences (left/right handed, etc),
- current state (sleeping, sitting, working etc) and the robots field of view, kinematics and dynamics

## **1.2 Robot Control - QP Tasks**

### **1.2.1 Position Task**

### **1.2.2 Orientation Task**

### **1.2.3 COM Task**

### **1.2.4 Vector look at Head Task**

### **1.2.5 Contact Task**



### 1.3 Bi-directional Handover

We formulate the bi-directional human-robot handover as one shot object handover from different starting positions and hand speed and trajectories (of the human). The robot start from half-site and take the object that is handed by the subject in one shot (and vice-versa). A person takes an object and hands it seriously to the robot that must take it (and vice-versa). The subject start and try to give the object from different positions and orientations w.r.t the robot.

two important key features that we want to focus during human humanoid robot object handover is the time of handover and pose of handover.

## 1.4 Notation and Terminology

Let  $\mathcal{M}$  (Mocap) and  $\mathcal{R}$  (Robot) be the two fixed frames that denote both Cartesian coordinate systems and Plücker coordinate systems denoted by  $X$  in the Euclidean space. Both  $\mathcal{M}$  and  $\mathcal{R}$  are defined by their position and orientation of a Cartesian frame, such that  ${}^M X_R$  denotes the Plücker coordinate transform which depends only on the position and orientation of frame  $\mathcal{M}$  relative to frame  $\mathcal{R}$ [1] (see Fig 1.1).

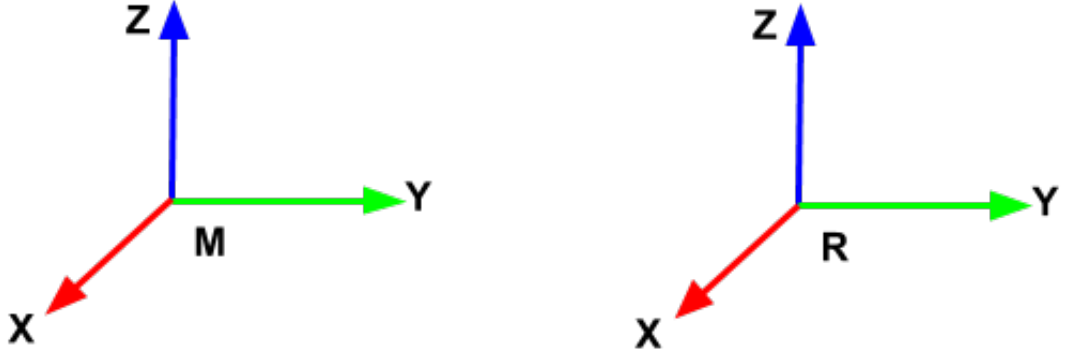


FIGURE 1.1:  $\mathcal{M}$  and  $\mathcal{R}$  Cartesian coordinate systems.

- using QP Orientation Task and Position Task (see 1.2), we get robot end-effector current orientation  ${}^{ef}\mathcal{O}_R \in \mathbb{R}^{3 \times 3}$  and current position  ${}^{ef}\mathcal{P}_R \in \mathbb{R}^3$  respectively in the  $\mathcal{R}$  frame, therefore,

$${}^{ef}X_R = \begin{bmatrix} {}^{ef}\mathcal{O}_R & {}^{ef}\mathcal{P}_R \end{bmatrix} \quad (1.1)$$

- Likewise,  ${}^h\mathcal{O}_M \in \mathbb{R}^{3 \times 3}$  and  ${}^h\mathcal{P}_M \in \mathbb{R}^3$ , denotes the subject's hand  $h$  orientation and position respectively in the  $\mathcal{M}$  frame, obtained from the  $\mathcal{L}$  shape body (see Section 1.5),

$${}^hX_M = \begin{bmatrix} {}^h\mathcal{O}_M & {}^h\mathcal{P}_M \end{bmatrix} \quad (1.2)$$

- ${}^h\mathcal{O}_{ef} \in \mathbb{R}^{3 \times 3}$  and  ${}^h\mathcal{P}_{ef} \in \mathbb{R}^3$ , denotes the subject's hand  $h$  orientation and position respectively in relative to the robot's local  $ef$  (end-effector) frame,

$${}^hX_{ef} = \begin{bmatrix} {}^h\mathcal{O}_{ef} & {}^h\mathcal{P}_{ef} \end{bmatrix} \quad (1.3)$$

- For convenience, we formulate the problem with a common origin  $O$ , such that  $\mathcal{R} \equiv \mathcal{M}$  (both frames are located between the feet of robot HRP2-Kai), we can get

subject's hand pose w.r.t. or relative to robot's end-effector

$${}^hX_{ef} = {}^hX_M{}^{ef}X_R^{-1} \quad (1.4)$$

- otherwise, when  $\mathcal{R} \neq M$

$${}^hX_{ef} = {}^hX_M{}^MX_R{}^{ef}X_R^{-1} \quad (1.5)$$

## 1.5 Subject's Hand Orientation Model

To get the orientation of subject's hand, we placed a rigid body with a shape similar to alphabet  $L$  on wrist of subject's hand(s) as shown in Fig 1.2. The three mocap markers  $A, B$  and  $C$  make up the three vertices of  $\mathcal{L}$  shape body, such that during object handover scenario, vector  $\vec{AB}$  along the longer side and vector  $\vec{BC}$  along the shorter side are set to be parallel with the  $X$ -axis and  $Y$ -axis of the mocap frame  $\mathcal{M}$  respectively. The vectors  $\vec{AB}$  and  $\vec{BC}$  are orthogonal to each other. For simplicity, let  $\hat{x}$  be the unit vector, which is parallel and along the  $X$ -axis and likewise, unit vector  $\hat{y}$  is parallel and along the  $Y$ -axis of the mocap frame  $\mathcal{M}$ , such that

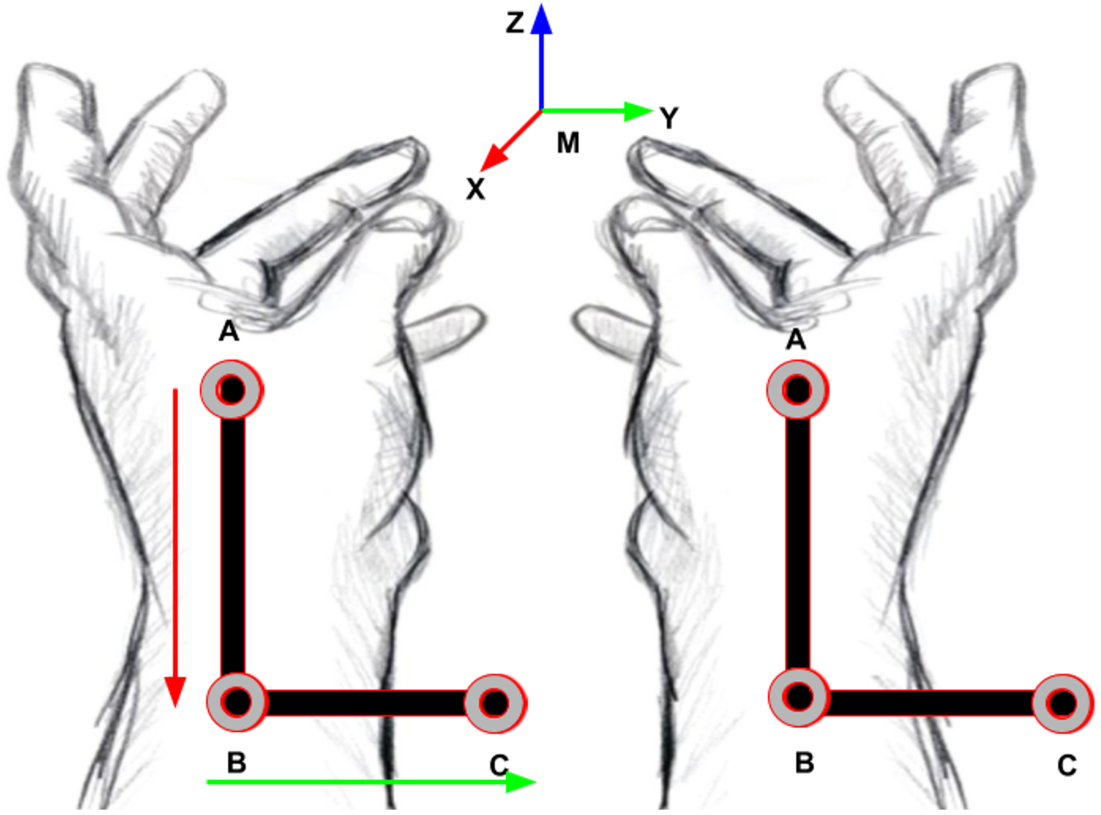


FIGURE 1.2:  $\mathcal{L}$  shape rigid body on the subject's hand(s)

$$\hat{x} = \frac{\vec{AB}}{\|\vec{AB}\|}$$

$$\hat{y} = \frac{\vec{BC}}{\|\vec{BC}\|}$$

Let  ${}^h\mathcal{O}_M$  in equation (1.2) be the column rotation matrix representing the subject's hand orientation in the mocap frame  $\mathcal{M}$  and since  $\hat{x} \in \mathbb{R}^3$  and  $\hat{y} \in \mathbb{R}^3$  are the two orthogonal unit vectors of an  $\mathcal{L}$  shape rigid body on subject's each hand (Fig 1.2), the cross product of them would result in another unit vector  $\hat{z} \in \mathbb{R}^3$  which is orthogonal to both  $\hat{x}$  and  $\hat{y}$ . The direction of the cross product would be given by equation (1.6) using right-hand rule.

$$\hat{z} = \hat{x} \times \hat{y} \quad (1.6)$$

To get the orientation of subject's hand we used these unit vectors  $\hat{x}, \hat{y}$  and  $\hat{z}$  as columns of the rotation matrix [2–4]  ${}^h\mathcal{O}_M$  in equation (1.7), such that the unit vectors  $\hat{x}, \hat{y}$  and  $\hat{z}$  represents subject's hand orientation around the *roll – pitch – yaw* axes respectively.

$${}^h\mathcal{O}_M = \begin{Bmatrix} \hat{x} \cdot x & \hat{y} \cdot x & \hat{z} \cdot x \\ \hat{x} \cdot y & \hat{y} \cdot y & \hat{z} \cdot y \\ \hat{x} \cdot z & \hat{y} \cdot z & \hat{z} \cdot z \end{Bmatrix}_{3 \times 3} \quad (1.7)$$

## 1.6 Handover Position Prediction Model

Algorithm 1 explains the procedure of predicting subject's hand position and estimating handover location. Inputs to the prediction model are robot left end-effector pose  ${}^{ef}X_R$  (eq 1.1) in the robot frame and subject's hand mocap markers positions  ${}^h\mathcal{P}_M$  (eq 1.2) in the mocap frame of reference.

Note that for simplicity, we formulated the problem with a common origin  $O$ , such that  $\mathcal{R} \equiv M$ , also from onwards by  ${}^h\mathcal{P}_M$  we meant position of the point  $A$  on the  $\mathcal{L}$  shape body as the subject's hand marker position as shown in Fig 1.2.

The prediction model behavior can be tuned by two initially required constant time periods,  $t_{observe}$  —a predefined time period required to observe the motion of subject's hand and  $t_{predict}$  —required to predict the subject's hand position in advance.

In order for handover between human subject and robot HRP2-Kai to be smooth and fluent, the robot needs to estimate the position of handover location in advance during both cases when robot act as receiver or when robot acts as giver, therefore we formulate the motion of subject's hand as a constant velocity based linear motion model (see Algorithm 1) to predict the handover position continuously. The robot observes subject's hand for a predefined time period  $t_{observe}$  and estimates the subject's hand direction and position based on the subject's hand velocity using equations (1.8) and (1.9) during the predefined time period.

$${}^h\bar{\mathcal{V}}_M = \frac{1}{t_{observe}} \sum_{j=1}^{j=t_{observe}} f'({}^h\mathcal{P}_M(j))/dt \quad (1.8)$$

$${}^h\mathcal{P}_M(t_{predict}) = {}^h\bar{\mathcal{V}}_M \cdot t_{predict} + {}^h\mathcal{P}_M(t_{observe}) \quad (1.9)$$

The prediction model then updates and converges itself over time and in doing so update the robot's end-effector position towards the subject's hand, upon condition if updated position is within the end-effector's constraint workspace, see Fig XXX.

Using equations 1.7 and 1.9 we get the orientation and translation components of  ${}^hX_M$  in 1.2, and recalling equations 1.4 and 1.5, the updated translation component of plücker transformation  ${}^hX_{ef}$ , which provides the predicted position of subject's hand

with respect to robot end-effector in the robot coordinate system is given by 1.10, the relative orientation component of  ${}^hX_{ef}$  is discussed in next Section 1.7.

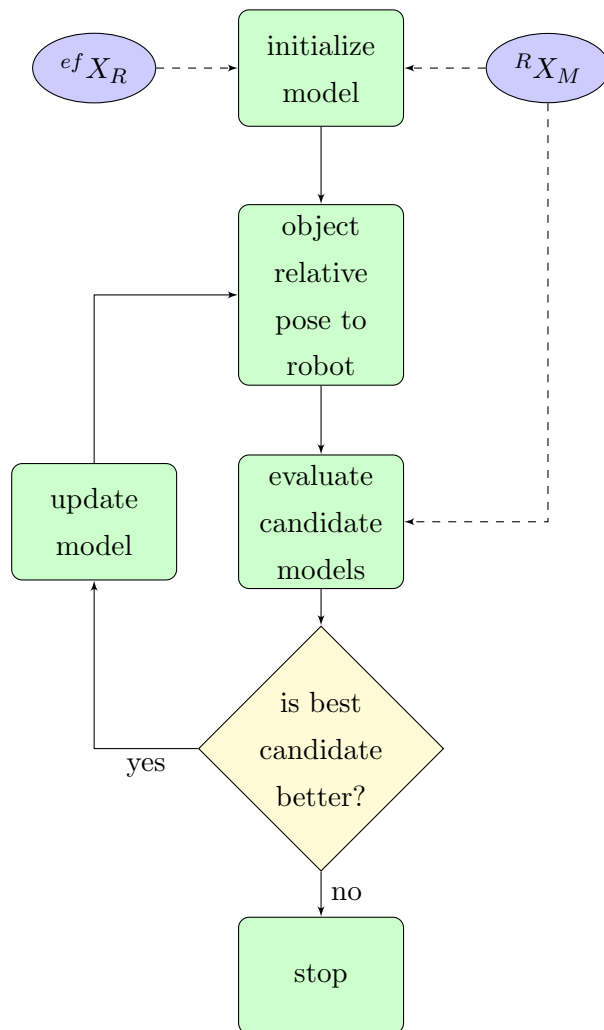
$${}^hX_{ef}(t_{predict}) = {}^hX_M^M X_R^{ef} X_R^{-1} \quad (1.10)$$

where,  ${}^MX_R$  is the Plücker coordinate transform frame  $\mathcal{M}$  relative to frame  $\mathcal{R}$ , if  $\mathcal{R} \neq \mathcal{M}$ .

Finally, the handover location is estimated as the subject's hand predicted position when the following conditions satisfy (1.11), that is when the subject's hand velocity is minimum and robot end-effector is closest to the subject's hand.

$$\left. \begin{aligned} & \left\| {}^h\vec{\mathcal{V}}_M \right\| \leq 1e^{-2} \\ & \left\| ({}^h\mathcal{P}_{ef}(t_{predict}) - {}^{ef}\mathcal{P}_R) \right\| \leq 1e^{-2} \end{aligned} \right\} \quad (1.11)$$

### 1.6.1 Block Diagram: Position Prediction Model\*





### 1.6.2 Algorithm: Position Prediction Model

---

**Algorithm 1:** linear prediction model - Position

---

**Input:**  ${}^M X_R, {}^{ef} X_R, mocapData$

**Output:**  ${}^h wp_{ef}$  // predicted waypoints

**Data:** Initial require:  $t_{observe} = 10ms, t_{predict} = 100ms, i = dt = 5ms$

```

1  $i += dt$  // increments as per controller run-time (dt)
2 if  $(i \% t_{observe}) == 0$  then
3   for  $j = 1$  to  $t_{observe}$  do
4      ${}^h \mathcal{P}_M = mocapData.handMarker(i - t_{observe} + j)$ 
5      ${}^h \bar{\mathcal{V}}_M = \frac{1}{t_{observe}} \sum_{j=1}^{j=t_{observe}} f'({}^h \mathcal{P}_M(j)) / dt$ 

    /* predict subject's hand handover position at  $t_{predict}$  */
6      ${}^h \mathcal{P}_M(t_{predict}) = {}^h \bar{\mathcal{V}}_M \cdot t_{predict} + {}^h \mathcal{P}_M(t_{observe})$ 
7      ${}^h X_M = \begin{bmatrix} {}^h \mathcal{O}_M & {}^h \mathcal{P}_M \end{bmatrix}$ 

    /* transform handover position relative to robot end-effector */
8      ${}^h X_{ef}(t_{predict}) = {}^h X_M {}^M X_R {}^{ef} X_R^{-1}$ 

    /* way points between subject hand and robot end-effector handover location */
9     Function generateWp( ${}^{ef} \mathcal{P}_R, {}^h \mathcal{P}_{ef}(t_{predict}), t_{predict}$ ):
10      for  $k = 0$  to  $t_{predict}$  do
11         ${}^h wp_{ef}(k) = [{}^h \mathcal{P}_{ef}(t_{predict}) - {}^{ef} \mathcal{P}_R] \cdot (\frac{k}{t_{predict}}) + {}^{ef} \mathcal{P}_R$ 
12      return  ${}^h wp_{ef}$ 

```

---

## 1.7 Relative Orientation Model

The translation component of  ${}^{ef}X_R$  in the equation (1.1) is updated based on the predicted position of subject's hand (see Section 1.6) while the orientation component is updated based on the relative orientation of subject's hand (see Section 1.5).

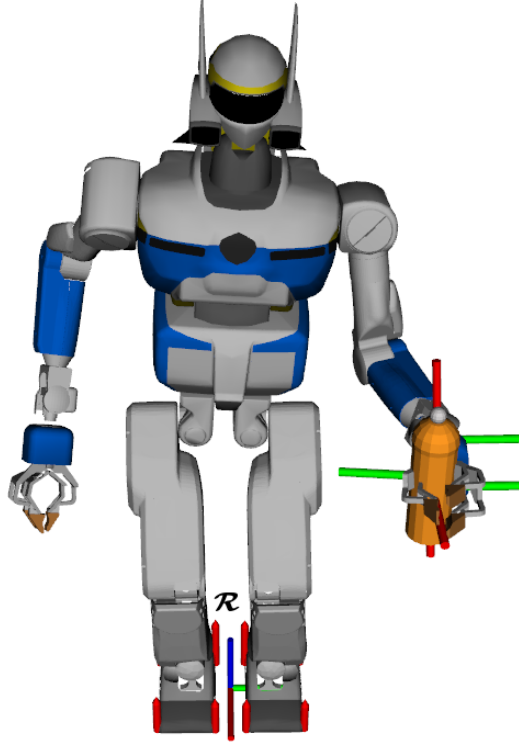


FIGURE 1.3: Robot HRP2-Kai (left end-effector) holding object with fixed orientation during handover in the robot frame  $\mathcal{R}$

Since our robot HRP2-Kai lacks conventional anthropomorphic hands, but instead it has gripper alike hands. For relative orientation model to work, we were required to know the fixed initial orientation of the robot end-effector, in which object handover is feasible between human and robot HRP2-Kai, irrespective of the subject's hand orientation, therefore consider a possible scenario where the robot end-effector orientation is fixed throughout the handover cycle (transfer of object from human to robot and return to human), irrespective of the condition where robot is a giver or receiver. Let  ${}^{efInit}\mathcal{O}_R$  denote the initial and fixed orientation of the robot end-effector in the robot frame  $\mathcal{R}$  during such human robot object handover scenarios as shown in Fig 1.3, and Fig 1.4, where,  ${}^{efInit}\mathcal{O}_R \subset {}^{ef}\mathcal{O}_R$ .

In order to correctly transform desired subject's hand orientation into robot end-effector frame, we further utilize the equation (1.10). We take advantage of the QP's Orientation Task (see subsection 1.2.2) and calculate the task error  $e$  between *current* subject's hand

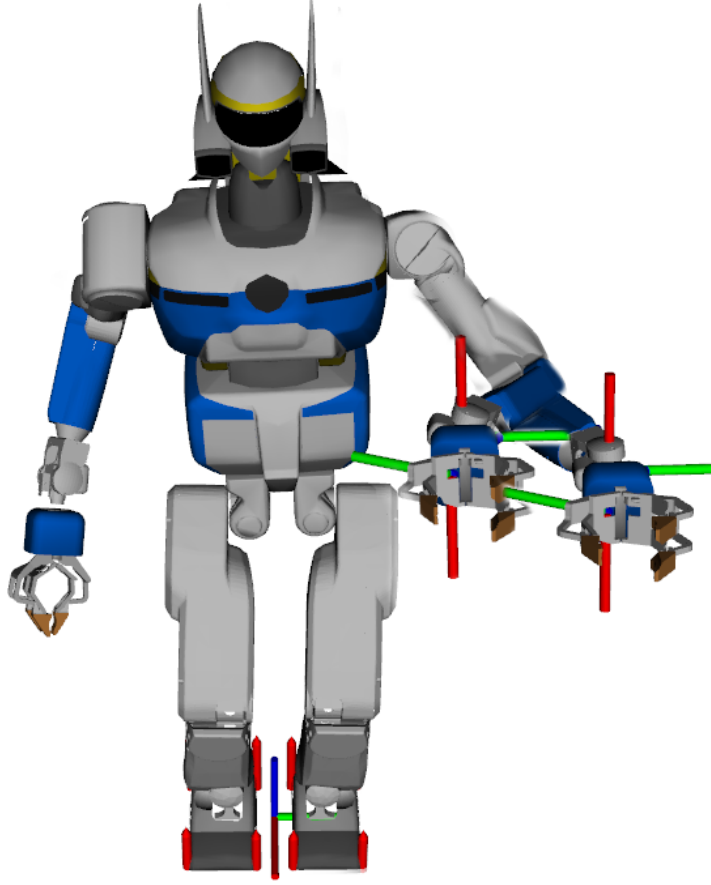


FIGURE 1.4: Robot HRP2-Kai (left end-effector) fixed orientation during two handover trials in the robot frame  $\mathcal{R}$

and *fixed* robot end-effector orientations, the resulting orientation from the Orientation Task is the desired robot end-effector orientation relative to the subject's hand orientation, see Fig 1.5, therefore, using fixed orientation component  $^{efInit}\mathcal{O}_R$ , of equation (1.1) and current subject's hand orientation  $^h\mathcal{O}_M$  from equation (1.7) derived in Section 1.5, we further modify equation (1.10).

$$\begin{bmatrix} {}^h\mathcal{O}_{ef} & {}^h\mathcal{P}_{ef} \end{bmatrix} = \begin{bmatrix} {}^h\mathcal{O}_M & {}^h\mathcal{P}_M \end{bmatrix} \begin{bmatrix} {}^M\mathcal{O}_R & {}^M\mathcal{P}_R \end{bmatrix} \begin{bmatrix} {}^{efInit}\mathcal{O}_R & {}^{ef}\mathcal{P}_R \end{bmatrix}^{-1} \quad (1.12)$$

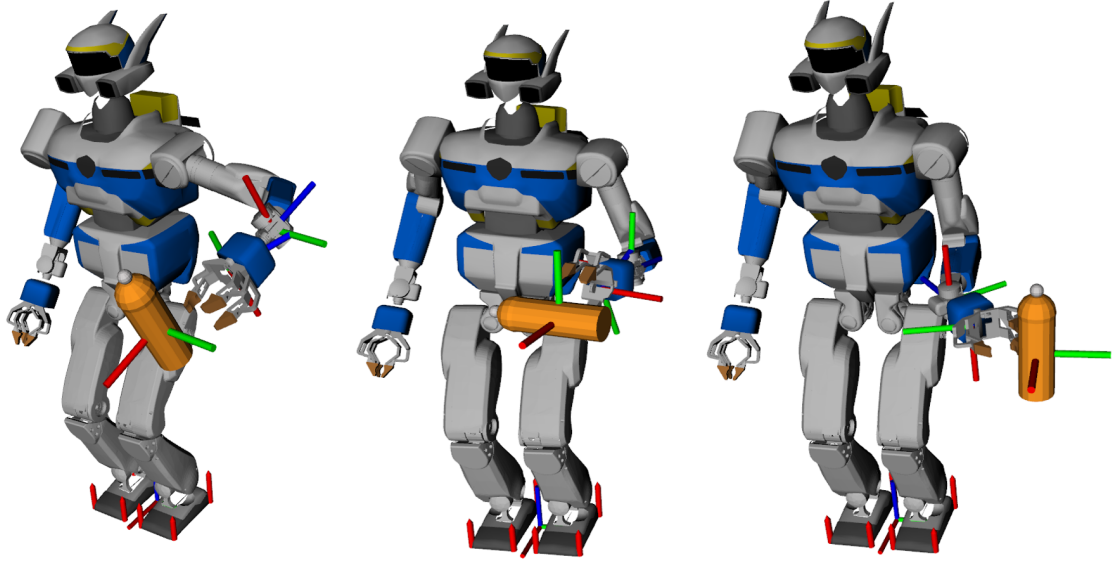


FIGURE 1.5: Robot HRP2-Kai (left end-effector) holding object in multiple possible orientations during handover trials in the robot frame  $\mathcal{R}$

## 1.8 Force Control

Chapter 12 FORCE CONTROL// robot dynamics and control book

we came up we two methods to solve this problem, one highlights simplicity and other highlights efficiency but when used together we get reliability and safest solution possible.

### 1.8.1 Mocap Marker Based

The HRP2-Kai gripper hands are equipped with 6-axis The object marker pose given by  ${}^{obj}X_M$  in the mocap frame  $\mathcal{M}$ .

### 1.8.1.1 Finite State Machine

### 1.8.1.2 Algorithm: Gripper Force Control

---

**Algorithm 2:** Force Based Gripper Controller
 

---

**Input:**  $\mathcal{F}_w$  // EF wrist worldWrenchWithoutGravity

**Output:**  $\mathcal{F}_{pull}, T_{new}$  // Pull force, new threshold based on object mass

```

1  $i++$  // increments as per controller run-time (5ms)
2 if subject hand is near robot then
    /* when SUBJECT holds the object */
3     if  $\mathcal{F}_w.norm() < 1.0$  // gripper is empty
4     then
5          $\mathcal{F}_{zero} = \mathcal{F}_w$  // wrench offset
6     else if  $\mathcal{F}_w.norm() > 2.0$  then
7          $\mathcal{F}_{load} = \mathcal{F}_w$  // wrench with object
    /* when ROBOT holds the object */
8     Function CheckPullForce(axis $\forall x,y,z$ ):
9          $objectMass = \mathcal{F}_{load}/9.81$  // get object mass
10         $\mathcal{F}_{inert} = objectMass * efAce$  // efAce using gripper markers
11         $\mathcal{F}_{pull} = |(\mathcal{F}_w - \mathcal{F}_{inert})|$ 
12         $T_{new} = \mathcal{F}_{load} + T_{old}$  //  $T_{old}$  set to min by user
13        if  $\mathcal{F}_{pull} > T_{new} \forall x,y,z$  then
14             $openGripper$  // release object
15 else
16     if ( $i \% 200$ ) then
17          $\mathcal{F}_{load} = |(\mathcal{F}_w - \mathcal{F}_{zero})|$  //  $\forall x,y,z$  average over time

```

---

## **1.9 both hands individual- adding another hand**

the switching is based on the function which uses hysteresis to compute relative position of object between subject's hand and robot end-effectors

## **1.10 both hands together- using hands together**

### **1.10.1 Force Control changes**

## **1.11    add a step-walk & native stablizer**



## **1.12 repeat handover with step-walk**

## **1.13 experiments**

## **1.14    quantitative analysis**

## **1.15 Results**

## **1.16 Discussion**

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