



State Estimation for Robotics

# Batch Linear Gaussian Estimation

Assignment 1

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## 1 Introduction and Problem Formulation

This report details the application of a **Batch Linear-Gaussian Estimator** to determine the one-dimensional position  $x_k$  of a mobile robot moving along a straight rail. The estimation is achieved by fusing measurements from two primary sources: the robot's onboard **wheel odometry** (providing translational speed,  $u_k$ ) and a **laser rangefinder** (measuring the range  $r_k$  to a fixed cylindrical landmark).

The experiment spans a 280 m journey over approximately 20 minutes of continuous motion. The high-accuracy ground-truth position, obtained from a ten-camera motion capture system (Vicon), is used for noise characterization and performance evaluation. The total dataset comprises  $K = 12709$  synchronous samples.

### 1.1 Modeling Assumptions and Data Pre-processing

To apply the discrete-time linear estimator, the raw, asynchronous sensor data required crucial pre-processing to establish a consistent temporal framework.

#### Temporal Synchronization and Sampling Period

In real-world applications, sensors often acquire data asynchronously and with non-uniform sampling periods (e.g., the nominal 10 Hz laser scans showed variability). To simplify the dynamic model, all data streams (odometry, laser, and ground-truth) were **linearly interpolated** and **synchronized** to a fixed, uniform sampling period  $T$ :

$$T = 0.1 \text{ s} \quad (1)$$

This uniform time step allows for the direct application of the discrete-time state-space equations.

#### Purpose of the 20-Minute Data Acquisition

The extended 20-minute duration of data collection is critical for two main reasons:

1. **Statistical Characterization:** The large number of samples ( $K = 12709$ ) allows for robust analysis, confirming that the sensor errors are close to **zero-mean Gaussian** and enabling the accurate calculation of noise variances ( $\sigma_r^2, \sigma_v^2$ ).
2. **Demonstration of Odometry Drift:** The long trial duration is necessary to clearly expose the inherent flaw in odometry-based estimation: position error grows **unbounded over time** (drift) due to the accumulation of even small biases or process noise ( $\sigma_q^2$ ). The Batch Estimator's main function in this assignment is to use the absolute laser measurements to correct this pronounced long-term drift.

#### State and Observation Models

The system is modeled as a linear discrete-time system, where  $w_k$  is the process noise and  $n_k$  is the exteroceptive sensor noise:

- **Motion Model:**

$$x_k = x_{k-1} + Tu_k + w_k \quad \text{with } w_k \sim \mathcal{N}(0, \sigma_q^2) \quad (2)$$

- **Observation Model (Transformed):** The raw range measurement  $r_k$  is transformed into the observation  $y_k = x_c - r_k$  to directly relate to the robot's position:

$$y_k := x_c - r_k = x_k + n_k \quad \text{with } n_k \sim \mathcal{N}(0, \sigma_r^2) \quad (3)$$

## 1.2 Estimation Framework

The objective is to estimate the full state sequence  $\mathbf{x}_{1:K}$  by solving the **Maximum A Posteriori (MAP)** problem, which, for a Linear-Gaussian system, is equivalent to minimizing the Weighted Least Squares objective function  $J(\mathbf{x}_{1:K})$ . The optimal solution  $\mathbf{x}_{1:K}^*$  is found by solving the linear system  $\mathbf{Hx}^* = \mathbf{b}'$ . The large size of the system ( $K = 12709$ ) and the goal of maintaining computational tractability necessitate the investigation of sparse estimation, as addressed in Question 4.

## 2 Noise Model Assumption and Variances

**Question:** Based on the data above, is the assumption of zero-mean Gaussian noise reasonable? What values of the variances,  $\sigma_q^2$  and  $\sigma_r^2$ , should we use, given  $w_k \sim \mathcal{N}(0, \sigma_q^2)$  and  $n_k \sim \mathcal{N}(0, \sigma_r^2)$ ?

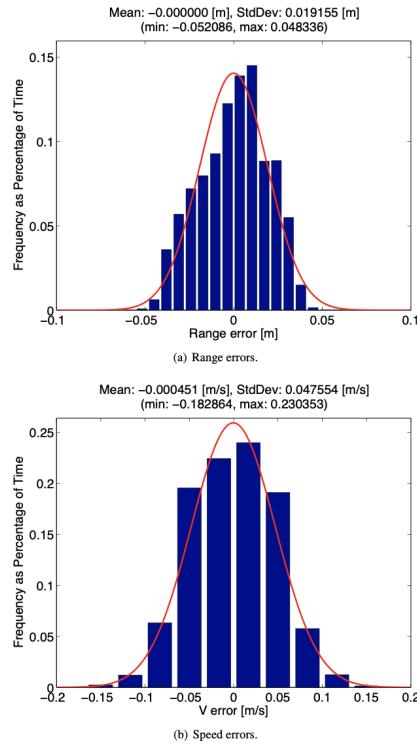
### Reasonableness of the Zero-Mean Gaussian Assumption

The assumption that both the observation noise  $n_k$  and the process noise  $w_k$  are zero-mean Gaussian is **reasonable**.

- **Zero-Mean:** The histograms of the sensor errors (Figure 1) show that the calculated means for both sensor streams are extremely close to zero:
  - Range Error Mean:  $-0.000000$  [m]
  - Speed Error Mean:  $-0.000451$  [m/s]

These values are negligible compared to the spread (standard deviation) of the errors.

- **Gaussian:** The shape of both histograms closely matches the superimposed red Gaussian curves (Figure 1), confirming that the distribution of errors is well-approximated by a normal distribution.



**Figure 1.6:** Histograms of sensor errors. Red curves are Gaussians with standard deviation fit to the data. Both range and speed have close to zero-mean errors with a spread.

Figure 1: Histograms of sensor errors. Red curves are Gaussians with standard deviation fit to the data. Both range and speed have close to zero-mean errors with a spread.)

## Calculated Variance Values

The required variances,  $\sigma_r^2$  and  $\sigma_q^2$ , are calculated by squaring the corresponding standard deviations found in the dataset analysis (Figure 1).

### Observation Noise Variance ( $\sigma_r^2$ )

The observation noise  $n_k$  is the error in the range measurement. We use the Standard Deviation (StdDev) of the Range Error:

- $\sigma_r = 0.019155 \text{ [m]}$
- $\sigma_r^2 = (0.019155)^2 \approx \mathbf{3.67 \times 10^{-4} \text{ [m}^2]}$

### Process Noise Variance ( $\sigma_q^2$ )

The process noise  $w_k$  relates to the uncertainty in the motion model  $x_k = x_{k-1} + T u_k + w_k$ . This noise results from the error in the measured speed,  $u_k$ . The variance of the process noise is related to the variance of the speed error  $\sigma_v^2$  by the sampling period  $T = 0.1 \text{ s}$ :  $\sigma_q^2 = T^2 \sigma_v^2$ .

- StdDev of Speed Error =  $0.047554 \text{ [m/s]}$
- $\sigma_v^2 = (0.047554)^2 \approx 2.261 \times 10^{-3} \text{ [m}^2/\text{s}^2]$
- $\sigma_q^2 = T^2 \sigma_v^2 = (0.1)^2 \cdot (0.047554)^2 \approx \mathbf{2.26 \times 10^{-5} \text{ [m}^2]}$

### 3 Batch Linear-Gaussian Objective Function

The objective function  $J(x_{1:K}|u_{1:K}, y_{1:K})$  that we seek to minimize is the sum of two components: the cost associated with the **observations** (laser rangefinder) and the cost associated with the **motion model** (odometry).

$$J(x_{1:K}|u_{1:K}, y_{1:K}) = \underbrace{\sum_{k=1}^K \frac{1}{\sigma_r^2} (y_k - x_k)^2}_{\text{Observation Cost (Laser)}} + \underbrace{\sum_{k=2}^K \frac{1}{\sigma_q^2} (x_k - x_{k-1} - Tu_k)^2}_{\text{Motion Cost (Odometry)}} \quad (1.3) \quad (4)$$

Where:

- $y_k = x_c - r_k$  is the transformed observation (the position of the robot inferred from the range measurement  $r_k$  and cylinder center  $x_c$ ).
- $x_k$  is the estimated robot position at timestep  $k$ .
- $Tu_k$  is the commanded motion (displacement) derived from the odometry input  $u_k$  over the sampling period  $T$ .
- $\sigma_r^2$  is the variance of the observation noise,  $n_k \sim \mathcal{N}(0, \sigma_r^2)$ .
- $\sigma_q^2$  is the variance of the process noise,  $w_k \sim \mathcal{N}(0, \sigma_q^2)$ .
- The sum for the motion cost starts at  $k = 2$  because  $x_1$  is the first state, and the first motion transition occurs between  $k = 1$  and  $k = 2$ .

### 4 Derivation of Optimal Position Estimates $\mathbf{x}_{1:K}^*$

The optimal position estimates  $\mathbf{x}_{1:K}^*$  are found by minimizing the Batch Linear-Gaussian objective function  $J(\mathbf{x}_{1:K})$ . Since the system is linear and the noise is Gaussian, the minimum is found by setting the gradient of  $J$  with respect to the state vector  $\mathbf{x}$  to zero:  $\nabla_{\mathbf{x}} J(\mathbf{x}) = \mathbf{0}$ .

#### The Concept of Future Dependence

It is the **global** nature of the Batch Estimator that allows the exploitation of the future dependence. Unlike a sequential estimator (like the Kalman filter), which only operates on the past and present, the Batch Estimator uses the entire dataset simultaneously. This means the optimal position  $x_i^*$  depends on **three** terms in the objective function:

1. The **observation** cost at  $k = i$ .
2. The **incoming motion** cost (linking it to the past,  $x_{i-1}$ ).
3. The **outgoing motion** cost (linking it to the future,  $x_{i+1}$ ).

This three-way linkage is the reason the Information Matrix  $\mathbf{H}$  results in its **tridiagonal** and symmetric structure.

## System of Normal Equations

This minimization procedure yields the system of linear equations (Normal Equations):

$$\mathbf{H}\mathbf{x}^* = \mathbf{b}' \quad (5)$$

The optimal estimate is then given by:

$$\mathbf{x}_{1:K}^* = \mathbf{H}^{-1}\mathbf{b}' \quad (1.4) \quad (6)$$

The elements of the Information Matrix  $\mathbf{H}$  and the Information Vector  $\mathbf{b}'$  are derived from the partial derivatives  $\frac{\partial J}{\partial x_i}$  for  $i = 1$  to  $K$ . Let  $\lambda_r = 1/\sigma_r^2$  and  $\lambda_q = 1/\sigma_q^2$  be the information weights.

### 4.1 Information Matrix $\mathbf{H}$

The matrix  $\mathbf{H}$  is a  $K \times K$  symmetric, **tridiagonal** matrix.

- **Elements on the main diagonal ( $H_{i,i}$ ):**

$$H_{i,i} = \begin{cases} \lambda_r + \lambda_q & \text{for } i = 1 \text{ and } i = K \quad (\text{1 motion term}) \\ \lambda_r + 2\lambda_q & \text{for } 1 < i < K \quad (\text{2 motion terms: in and out}) \end{cases} \quad (7)$$

- **Elements on the off-diagonals ( $H_{i,i\pm 1}$ ):**

$$H_{i,i+1} = H_{i+1,i} = -\lambda_q \quad \text{for } 1 \leq i < K \quad (8)$$

$$\mathbf{H} = \begin{bmatrix} \lambda_r + \lambda_q & -\lambda_q & 0 & \dots & 0 \\ -\lambda_q & \lambda_r + 2\lambda_q & -\lambda_q & \dots & 0 \\ 0 & -\lambda_q & \lambda_r + 2\lambda_q & \dots & 0 \\ \vdots & \vdots & \vdots & \ddots & \vdots \\ 0 & 0 & 0 & -\lambda_q & \lambda_r + \lambda_q \end{bmatrix}$$

### 4.2 Information Vector $\mathbf{b}'$

The vector  $\mathbf{b}'$  is a  $K \times 1$  column vector. Let  $f_k = Tu_k$  represent the known odometry displacement.

- **First element ( $b'_1$ ):**

$$b'_1 = \lambda_r y_1 + \lambda_q f_2 \quad (9)$$

- **Intermediate elements ( $b'_i$  for  $1 < i < K$ ):**

$$b'_i = \lambda_r y_i + \lambda_q (f_i - f_{i+1}) \quad (10)$$

- **Final element ( $b'_K$ ):**

$$b'_K = \lambda_r y_K - \lambda_q f_K \quad (11)$$

The final vector  $\mathbf{b}'$  is:

$$\mathbf{b}' = \begin{bmatrix} \lambda_r y_1 + \lambda_q f_2 \\ \lambda_r y_2 + \lambda_q (f_2 - f_3) \\ \lambda_r y_3 + \lambda_q (f_3 - f_4) \\ \vdots \\ \lambda_r y_{K-1} + \lambda_q (f_{K-1} - f_K) \\ \lambda_r y_K - \lambda_q f_K \end{bmatrix}$$

## 5 Batch Estimation with Sparse Observations

The computational bottleneck for  $K = 12709$  is the size of the Information Matrix  $\mathbf{H}$ . The proposed solution is to reduce the dimension of the state vector to be estimated ( $\mathbf{x}_{\text{sparse}}$ ) while incorporating the full odometry information ( $u_{1:K}$ ) into the remaining sparse transitions.

### 5.1 Defining the Sparse System

Let  $M = K/\delta$  be the total number of states to be estimated. The sparse state vector is  $\mathbf{x}_{\text{sparse}} = [x_\delta, x_{2\delta}, \dots, x_{M\delta}]^T$ .

To use all odometry inputs  $u_{1:K}$ , the sequence of  $\delta$  motion steps between  $x_{(m-1)\delta}$  and  $x_{m\delta}$  must be treated as a single, integrated transition.

#### Integrated Odometry Input ( $\tilde{u}_m$ )

The total displacement based on all odometry readings  $u_k$  between the sparse states is summed:

$$\tilde{u}_m = \sum_{j=(m-1)\delta+1}^{m\delta} T u_j \quad (12)$$

#### Integrated Process Noise Variance ( $\sigma_{\tilde{q}}^2$ )

Since the individual process noise terms ( $w_j$ ) are independent, their variances ( $\sigma_q^2$ ) sum up over the  $\delta$  steps:

$$\sigma_{\tilde{q}}^2 = \text{Var} \left( \sum_j w_j \right) = \delta \sigma_q^2 \quad (13)$$

This term captures the degradation of the odometry measurement due to the increased time separation, effectively using the "power" of all intermediate odometry readings.

### 5.2 Modified Objective Function

The modified objective function  $J_{\text{sparse}}$  minimizes the total error using the sparse observations  $y_{m\delta}$  and the integrated motion model:

$$J_{\text{sparse}}(\mathbf{x}_{\text{sparse}}) = \underbrace{\sum_{m=1}^M \frac{1}{\sigma_r^2} (y_{m\delta} - x_{m\delta})^2}_{\text{Sparse Observation Cost}} + \underbrace{\sum_{m=2}^M \frac{1}{\sigma_{\tilde{q}}^2} (x_{m\delta} - x_{(m-1)\delta} - \tilde{u}_m)^2}_{\text{Integrated Motion Cost}} \quad (14)$$

### 5.3 Optimal Position Estimates Expression

The optimal sparse estimates  $\mathbf{x}_{\text{sparse}}^*$  are found by solving the reduced linear system  $\mathbf{H}_{\text{sparse}} \mathbf{x}_{\text{sparse}}^* = \mathbf{b}'_{\text{sparse}}$ , where the matrix dimension is  $M \times M$ .

$$\mathbf{x}_{\text{sparse}}^* = \mathbf{H}_{\text{sparse}}^{-1} \mathbf{b}'_{\text{sparse}} \quad (15)$$

The structure remains tridiagonal, with the key modification being the replacement of the original information weight  $\lambda_q = 1/\sigma_q^2$  with the new sparse weight  $\lambda_{\tilde{q}} = 1/\sigma_{\tilde{q}}^2 = 1/(\delta\sigma_q^2)$ .

**Sparse Information Matrix  $\mathbf{H}_{\text{sparse}}$  ( $M \times M$ )**

$$\mathbf{H}_{\text{sparse}} = \begin{bmatrix} \lambda_r + \lambda_{\tilde{q}} & -\lambda_{\tilde{q}} & 0 & \dots & 0 \\ -\lambda_{\tilde{q}} & \lambda_r + 2\lambda_{\tilde{q}} & -\lambda_{\tilde{q}} & \dots & 0 \\ 0 & -\lambda_{\tilde{q}} & \lambda_r + 2\lambda_{\tilde{q}} & \dots & 0 \\ \vdots & \vdots & \vdots & \ddots & \vdots \\ 0 & 0 & 0 & -\lambda_{\tilde{q}} & \lambda_r + \lambda_{\tilde{q}} \end{bmatrix} \quad (16)$$

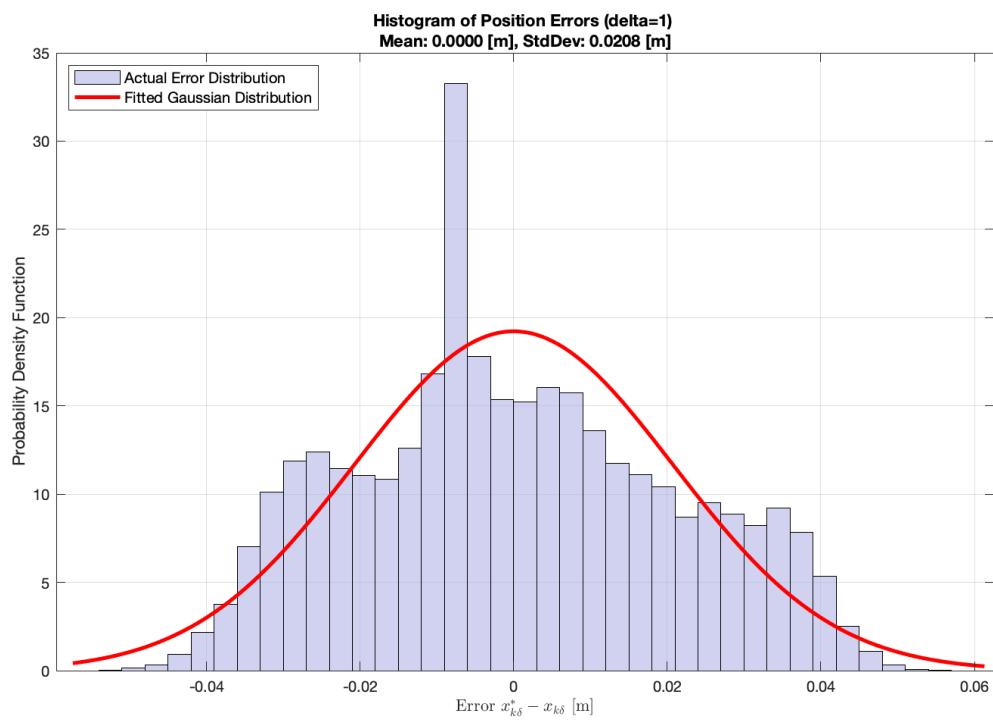
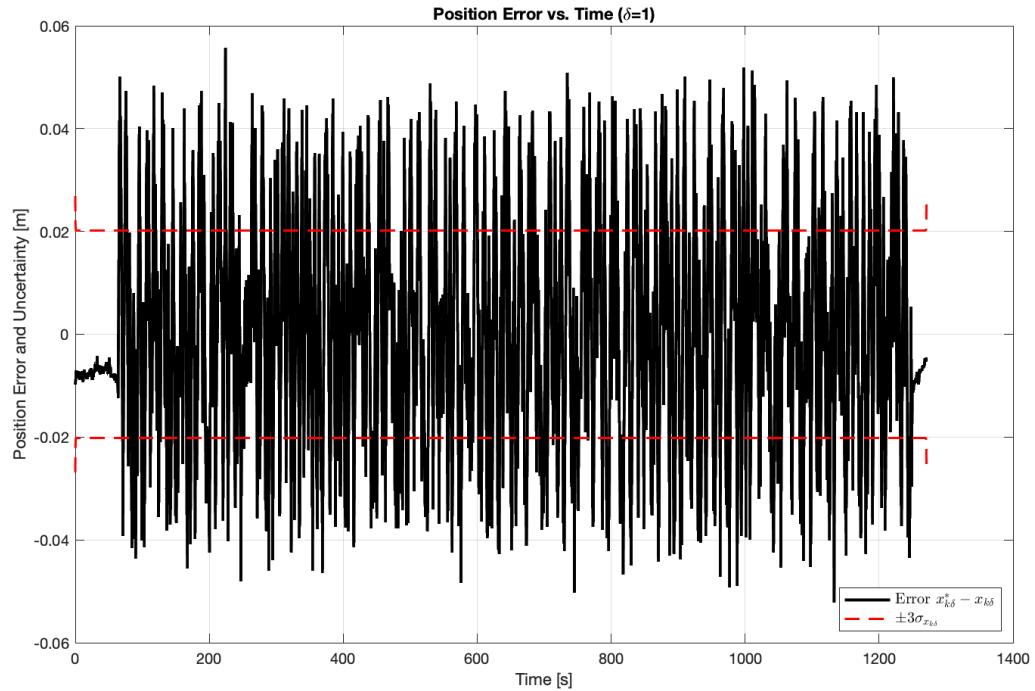
**Sparse Information Vector  $\mathbf{b}'_{\text{sparse}}$  ( $M \times 1$ )**

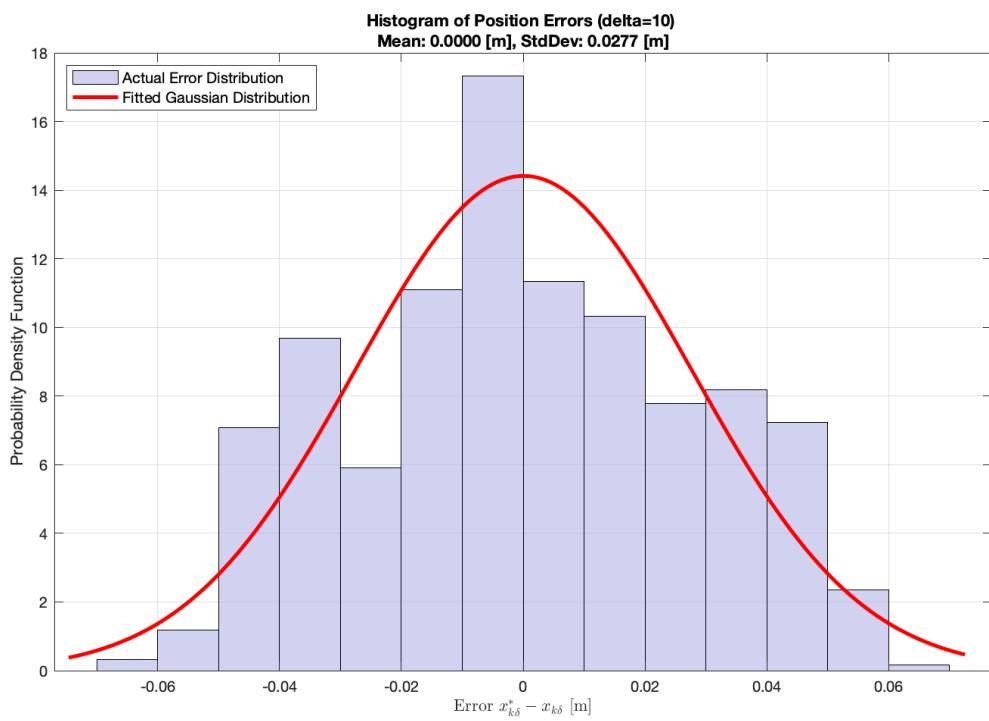
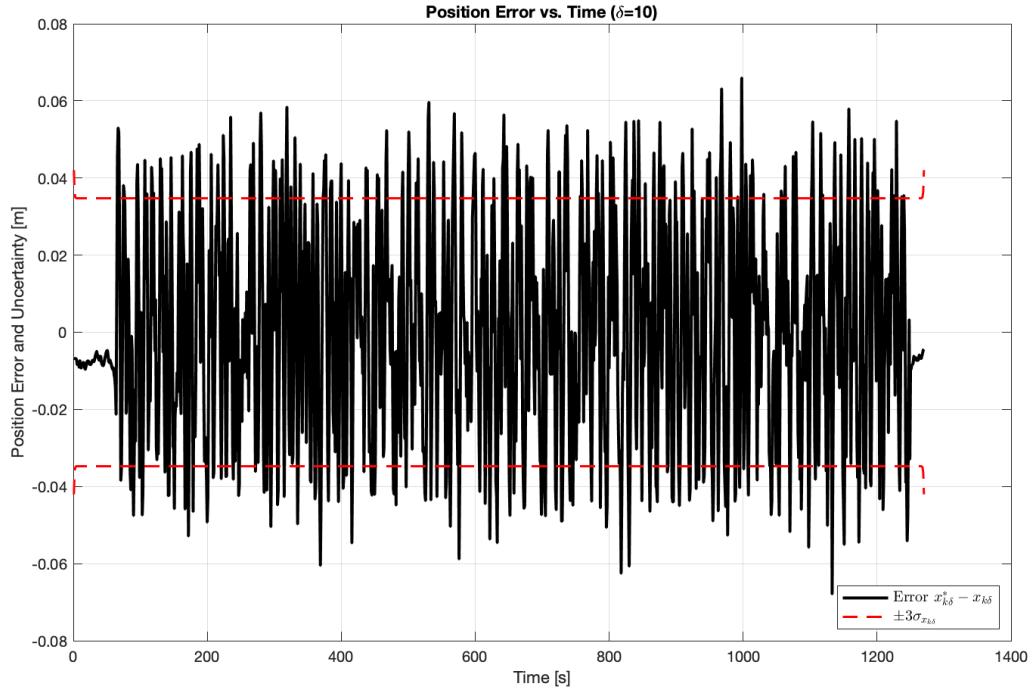
Let  $\tilde{f}_m = \tilde{u}_m$ .

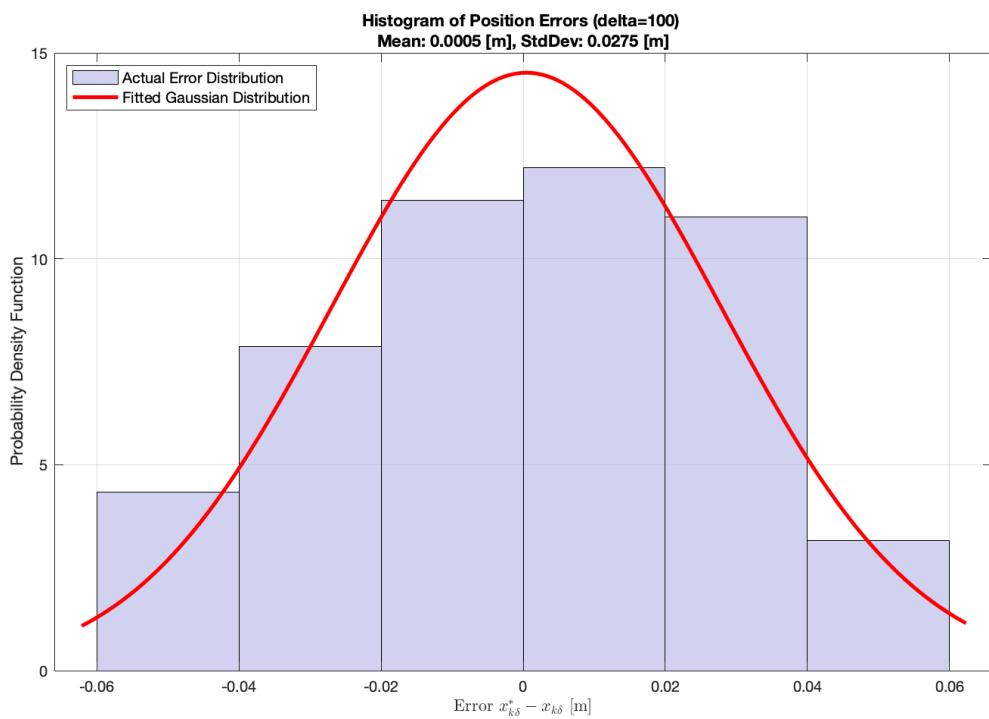
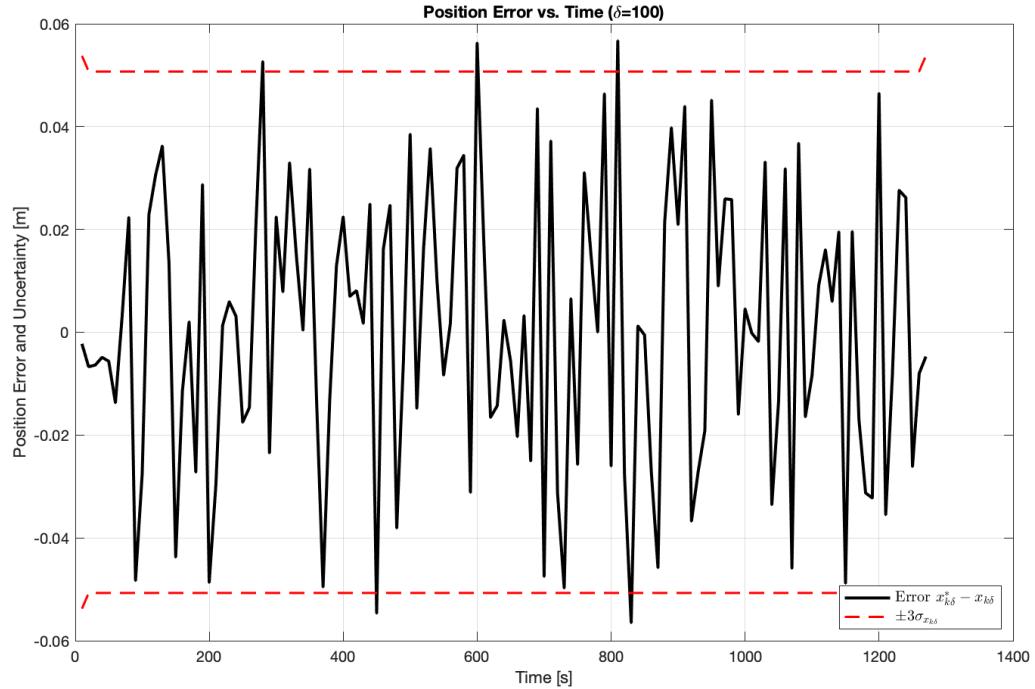
$$\mathbf{b}'_{\text{sparse}} = \begin{bmatrix} \lambda_r y_\delta + \lambda_{\tilde{q}} \tilde{f}_2 \\ \lambda_r y_{2\delta} + \lambda_{\tilde{q}} (\tilde{f}_2 - \tilde{f}_3) \\ \vdots \\ \lambda_r y_{(M-1)\delta} + \lambda_{\tilde{q}} (\tilde{f}_{M-1} - \tilde{f}_M) \\ \lambda_r y_K - \lambda_{\tilde{q}} \tilde{f}_M \end{bmatrix}$$

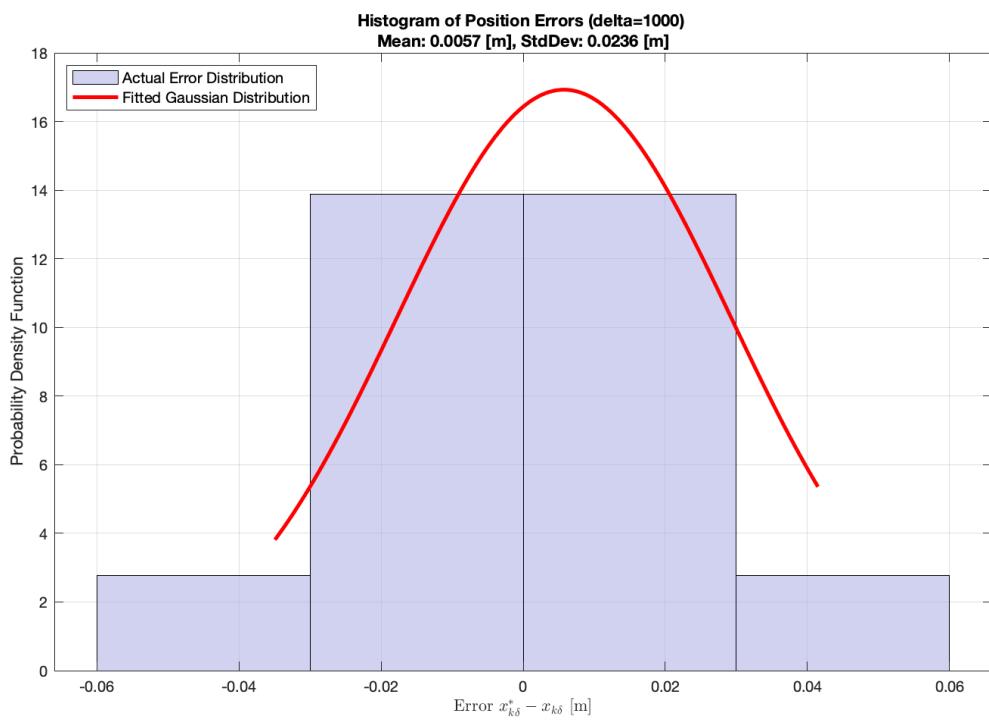
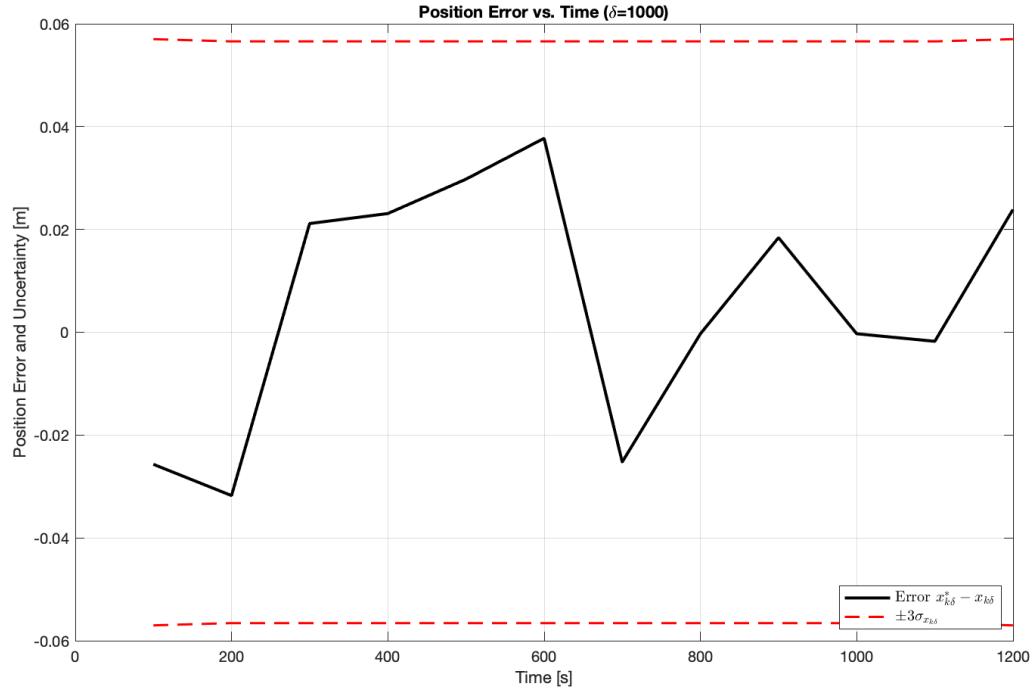
## 6 Conclusion and Analysis of Sparse Estimation

This assignment successfully implemented the **Batch Linear-Gaussian Estimator** to fuse odometry and laser rangefinder data for one-dimensional position estimation. The key findings relate to the trade-off between estimation accuracy, theoretical uncertainty, and computational cost, as explored by varying the state sampling interval,  $\delta$ .









## 6.1 Key Findings on $\delta$ Variation

The analysis confirmed that the integration of odometry information across  $\delta$  timesteps, coupled with sparse laser corrections, allows for significant reduction in the problem size ( $M = K/\delta$ ) while retaining the necessary information to correct the odometry drift.

- **Computational Efficiency:** Increasing  $\delta$  from 1 to 1000 drastically reduced the dimension of the matrix  $\mathbf{H}_{\text{sparse}}$  (from  $12709 \times 12709$  to  $12 \times 12$ ). This confirms that the sparse batch method is an effective technique for addressing the potential computational intractability of full batch estimation ( $K = 12709$ ).
- **Odometry Drift Correction:** For large  $\delta$  (e.g.,  $\delta = 1000$ ), the estimation error in the time domain plots showed a characteristic pattern of **growth (drift)** followed by a sharp **correction** upon receiving the sparse laser measurement  $y_{k\delta}$ . For small  $\delta$  (e.g.,  $\delta = 1$  or 10), the corrections are frequent enough to virtually eliminate this long-term drift.
- **Uncertainty Scaling:** The size of the predicted uncertainty envelope ( $\pm 3\sigma_{x_{k\delta}}$ ) is directly controlled by the integrated motion noise,  $\sigma_{\tilde{q}}^2 = \delta\sigma_q^2$ . The uncertainty envelope expands proportionally as  $\delta$  increases, demonstrating that the model correctly predicts the reduced precision when relying heavily on long-term odometry.

## 6.2 Statistical Validation (Consistency Check)

The histogram analysis provides statistical validation of the estimator's consistency:

- **Gaussianity:** For all four  $\delta$  cases, the histogram of the errors ( $x_{k\delta}^* - x_{k\delta}$ ) retained a distribution closely matching a zero-mean Gaussian function. This is expected and confirms that the final estimates  $\mathbf{x}_{\text{sparse}}^*$  obey the properties of a Linear-Gaussian system.
- **Consistency:** The actual spread of the errors closely matches the theoretical spread predicted by the average value of the diagonal elements of the covariance matrix  $\mathbf{H}_{\text{sparse}}^{-1}$ . This correspondence validates that the assumed noise models ( $\sigma_r^2, \sigma_q^2$ ) accurately represent the true uncertainty of the system.

In summary, the experiment revealed a critical trade-off between the theoretical performance (tightness of uncertainty bounds) and the practical reliability (consistency) of the estimator.

The full batch solution, which utilized the laser measurement at every timestep ( $\delta = 1$ ), yielded the lowest average position error and the tightest uncertainty bounds. However, this solution was judged to be **inconsistent** (or overly optimistic).

- The observed error frequently exceeded the theoretical  $\pm 3\sigma$  envelope.
- This occurred because the high frequency of the laser constraints ( $\delta = 1$ ) minimized the influence of the process noise variance ( $\sigma_q^2$ ) in the information matrix ( $\mathbf{H}$ ).
- Consequently, the estimator's calculated uncertainty ( $\mathbf{H}^{-1}$ ) became unrealistically small, failing to account for the full magnitude of the real system errors.

The sparse batch solutions ( $\delta = 10, 100, 1000$ ) demonstrated a more robust behavior. By reducing the frequency of the absolute laser anchor, the estimator was forced to rely more

heavily on the motion model and its associated  $\sigma_q^2$  for propagation over longer intervals.

- The theoretical uncertainty bounds ( $\pm 3\sigma$ ) became wider, reflecting a more realistic assessment of the accumulated error.
- Critically, the observed error predominantly remained within these wider bounds, meaning these solutions achieved **consistency**.
- This approach, particularly for  $\delta = 10$  or  $\delta = 100$ , strikes a near-optimal balance between **accuracy and reliability**, while achieving a significant reduction in computational load, making it the most practical strategy for large-scale, long-duration estimation.

## 7 (Extra) Observability and Sensor Roles

The distinction between the odometer as an input ( $u_k$ ) and the laser rangefinder as an output/observation ( $y_k$ ) is fundamental in estimation theory, dictated by their functional roles in the system's dynamic model.

### 7.1 Non-Observability of Standalone Sensors

**Odometer-Only Model (Non-Observable):** When only the odometry measurements ( $u_k$ ) are used, the system is **non-observable** with respect to the absolute position. The odometer provides information solely about the **relative displacement** ( $x_k - x_{k-1}$ ), without establishing a fixed reference (an absolute anchor). It only defines the velocity, without any connection info with the robot position.

- **Mathematical Consequence:** This ambiguity means an arbitrary constant translation ( $\Delta c$ ) applied to the entire estimated trajectory ( $x_{1:K}$ ) results in the same minimum cost, as the relative differences are unchanged.
- **Least Squares Result:** This leads to a **singular (non-invertible) Information Matrix ( $H$ )**, as the system possesses a non-zero null space (a constant vector  $v = [1, 1, \dots, 1]^T$ ), preventing a unique solution  $x_{1:K}^*$ .

**Laser-Only Model (Uncertainty Growth):** Using only the laser rangefinder ( $y_k$ ) provides a measurement of the **absolute position** (relative to the known cylinder  $x_c$ ). However, without the motion model:

- The estimation lacks the necessary dynamic constraint to link successive states  $x_{k-1}$  and  $x_k$ .
- The lack of coupling causes the overall estimated covariance (uncertainty) to become less constrained over time, leading to a **growing uncertainty envelope**, even though each individual measurement  $y_k$  has a bounded error.

### 7.2 Necessity of Sensor Fusion

The core strength of the Batch Estimator lies in **sensor fusion**, where the two measurements act as complementary constraints:

- The **Odometer** provides the **dynamic coupling** between states, ensuring the trajectory is smooth and constrained by the laws of motion.
- The **Laser** provides the **absolute anchor**, which is critical for removing the non-observable translation ambiguity and preventing the estimation error (drift) from the odometer from accumulating indefinitely.

This fusion renders the system **fully observable** and yields a robust, non-singular solution.