

①

## Rotation I

### Moment of inertia tensor

For a rigid body, the velocity of a point at  $\underline{r}$  is given by  $\underline{v} = \underline{\omega} \times \underline{r}$ . Then,

$$\begin{aligned} \underline{J} &= \sum \underline{r} \times \underline{p} \\ &= \sum m \underline{r} \times (\underline{\omega} \times \underline{r}) \\ &= \sum m (r^2 \underline{\omega} - (\underline{\omega} \cdot \underline{r}) \underline{r}) \end{aligned}$$

$$\rightarrow J_i = I_{ij} \omega_j$$

$$\text{, where } I_{ij} = \sum m (r^2 \delta_{ij} - x_i x_j)$$

$$\begin{aligned} \text{Also, } T &= \frac{1}{2} \sum m v^2 \\ &= \frac{1}{2} \sum m (\underline{\omega} \times \underline{r}) \cdot (\underline{\omega} \times \underline{r}) \\ &= \frac{1}{2} \left( \sum m \underline{r} \times (\underline{\omega} \times \underline{r}) \right) \cdot \underline{\omega} \end{aligned}$$

$$\rightarrow T = \frac{1}{2} \underline{J} \cdot \underline{\omega}$$

Now  $\underline{I}$  is a symmetric tensor, so can diagonalise:

$$\underline{I} = \begin{pmatrix} I_1 & 0 & 0 \\ 0 & I_2 & 0 \\ 0 & 0 & I_3 \end{pmatrix}$$

$$\underline{J} = (I_1 \omega_1, I_2 \omega_2, I_3 \omega_3)$$

$$T = \frac{1}{2} (I_1 \omega_1^2 + I_2 \omega_2^2 + I_3 \omega_3^2)$$

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Matrices recap

If  $A$  is a transformation matrix s.t

$$A \vec{e}_i = \vec{e}_i'$$

what is  $A_{ij}$ ?

$$\rightarrow A_{jk} (\vec{e}_i)_k = \vec{e}_i' \cdot \vec{e}_j'$$

$$\rightarrow A_{jk} \delta_{ik} = \vec{e}_i' \cdot \vec{e}_j'$$

$$\rightarrow A_{ji} = \vec{e}_i' \cdot \vec{e}_j'$$

$$\rightarrow A_{ij} = \vec{e}_j' \cdot \vec{e}_i'$$

$$\rightarrow A = \begin{pmatrix} \vec{e}_1' \cdot \vec{e}_1' & \vec{e}_1' \cdot \vec{e}_2' & \vec{e}_1' \cdot \vec{e}_3' \\ \vec{e}_2' \cdot \vec{e}_1' & \vec{e}_2' \cdot \vec{e}_2' & \vec{e}_2' \cdot \vec{e}_3' \\ \vec{e}_3' \cdot \vec{e}_1' & \vec{e}_3' \cdot \vec{e}_2' & \vec{e}_3' \cdot \vec{e}_3' \end{pmatrix}$$

If  $A$  rotates axes, what is  $A_{ij}$ ?

$$\vec{v} = v_i \hat{e}_i = v_j' \hat{e}_j'$$

$$\rightarrow v_k' = v_i \hat{e}_i \cdot \hat{e}_k' = A_{ki} v_i$$

$$\rightarrow A_{ki} = \hat{e}_k' \cdot \hat{e}_i'$$

$$\rightarrow A_{ij} = \hat{e}_i' \cdot \hat{e}_j'$$

$$\rightarrow A = \begin{pmatrix} \vec{e}_1' \cdot \vec{e}_1' & \vec{e}_1' \cdot \vec{e}_2' & \vec{e}_1' \cdot \vec{e}_3' \\ \vec{e}_2' \cdot \vec{e}_1' & \vec{e}_2' \cdot \vec{e}_2' & \vec{e}_2' \cdot \vec{e}_3' \\ \vec{e}_3' \cdot \vec{e}_1' & \vec{e}_3' \cdot \vec{e}_2' & \vec{e}_3' \cdot \vec{e}_3' \end{pmatrix}$$

3

Euler angles

3 rotations of coordinate axes:

- 1) Rotate coordinates about  $z$  by  $\phi$ :  
 $x, y, z \rightarrow x', y', z'$

$$D = \begin{pmatrix} \cos \phi & \sin \phi & 0 \\ -\sin \phi & \cos \phi & 0 \\ 0 & 0 & 1 \end{pmatrix}$$

- 2) Rotate about  $x'$  by  $\theta$ :  
 $x', y', z' \rightarrow x'', y'', z''$

$$C = \begin{pmatrix} 1 & 0 & 0 \\ 0 & \cos \theta & \sin \theta \\ 0 & -\sin \theta & \cos \theta \end{pmatrix}$$

- 3) Rotate about  $z''$  by  $\psi$ :  
 $x'', y'', z'' \rightarrow x''', y''', z'''$

$$B = \begin{pmatrix} \cos \psi & \sin \psi & 0 \\ -\sin \psi & \cos \psi & 0 \\ 0 & 0 & 1 \end{pmatrix}$$

Overall, from  $xyz \rightarrow x'''y'''z'''$ , trans matrix is  
 $A = BCD$ :

$$A = \begin{pmatrix} \cos \phi \cos \psi - \sin \phi \sin \psi \cos \theta & \sin \phi \cos \psi + \cos \phi \sin \psi \cos \theta & \sin \psi \sin \theta \\ -\cos \phi \sin \psi - \sin \phi \cos \psi \cos \theta & \sin \phi \sin \psi - \cos \phi \cos \psi \cos \theta & \sin \psi \cos \theta \\ \sin \phi \sin \theta & -\cos \phi \sin \theta & \cos \theta \end{pmatrix}$$



(4)

Now a general rotation is given by

$$\underline{\omega} = \dot{\phi} \hat{\omega}_\phi + \dot{\theta} \hat{\omega}_\theta + \dot{\psi} \hat{\omega}_\psi$$

$$\hat{\omega}_\phi = (0, 0, 1) \text{ in } xyz$$

$$\rightarrow \hat{\omega}_\phi = (\sin\theta \sin\psi, \sin\theta \cos\psi, \cos\theta) \text{ in } 123$$

$$\hat{\omega}_\theta = (1, 0, 0) \text{ in } x''y''z''$$

$$\rightarrow \hat{\omega}_\theta = (\cos\psi, -\sin\psi, 0) \text{ in } 123$$

$$\hat{\omega}_\psi = (0, 0, 1) \text{ in } 123$$

$$\rightarrow \underline{\omega} = \begin{pmatrix} \dot{\phi} \sin\theta \sin\psi + \dot{\theta} \cos\psi \\ \dot{\phi} \sin\theta \cos\psi - \dot{\theta} \sin\psi \\ \dot{\phi} \cos\theta + \dot{\psi} \end{pmatrix} \text{ in } 123 \quad \text{--- (1)}$$

Euler's rotation eqs

$$L = T - V = \frac{1}{2} \sum_{i=1}^3 I_i \omega_i^2 - V$$

$$E-L: \frac{d}{dt} \left( \frac{\partial T}{\partial \dot{\psi}} \right) - \frac{\partial T}{\partial \psi} = - \frac{\partial V}{\partial \psi} = \tau_\psi \quad \text{--- Euler torque}$$

$$\text{Now } \frac{\partial T}{\partial \dot{\psi}} = \sum_{i=1}^3 \frac{\partial T}{\partial \omega_i} \frac{\partial \omega_i}{\partial \dot{\psi}}, \quad \frac{\partial T}{\partial \psi} = \sum_{i=1}^3 \frac{\partial T}{\partial \omega_i} \frac{\partial \omega_i}{\partial \psi}$$

$$\frac{\partial \omega_1}{\partial \dot{\psi}} = \omega_1$$

$$\frac{\partial \omega_1}{\partial \psi} = 0$$

$$\frac{\partial \omega_2}{\partial \dot{\psi}} = -\omega_1$$

$$\frac{\partial \omega_2}{\partial \psi} = 0$$

$$\frac{\partial \omega_3}{\partial \dot{\psi}} = 0$$

$$\frac{\partial \omega_3}{\partial \psi} = 1$$

⑤

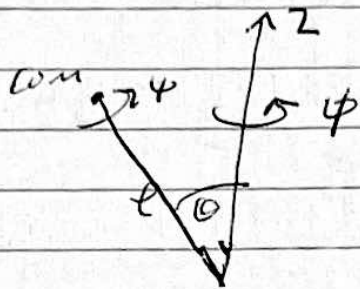
→ E-L become  $I_3 \dot{\omega}_3 - (I_1 - I_2) \omega_1 \omega_2 = C_3$

Generative:  $I_1 \dot{\omega}_1 - (I_2 - I_3) \omega_2 \omega_3 = C_1$

$I_2 \dot{\omega}_2 - (I_3 - I_1) \omega_3 \omega_1 = C_2$

$I_3 \dot{\omega}_3 - (I_1 - I_2) \omega_1 \omega_2 = C_3$

Symmetric top w point fixed



$\dot{\phi}$  = 'Precession'

$\dot{\psi}$  = 'Nutation'

using ①, can write

$$L = \frac{1}{2} I_1 (\dot{\phi}^2 \sin^2 \theta + \dot{\psi}^2) + \frac{1}{2} I_3 (\dot{\phi} \cos \theta + \dot{\psi})^2 - M g l \cos \theta$$

$p_\psi = I_3 (\dot{\psi} + \dot{\phi} \cos \theta) = I_3 \omega_3 = I_1 a = \text{const} \dots \textcircled{2}$

$p_\phi = (I_1 \sin^2 \theta + I_3 \cos^2 \theta) \dot{\phi} + I_3 \dot{\psi} \cos \theta = I_1 b = \text{const} \dots \textcircled{3}$

Can see that  $\frac{\partial L}{\partial t} = 0$ , so  $H = E = T + V$  is const.

$$\frac{1}{2} I_1 (\dot{\phi}^2 \sin^2 \theta + \dot{\psi}^2) + \frac{1}{2} I_3 (\dot{\phi} \cos \theta + \dot{\psi})^2 + M g l \cos \theta = E \dots \textcircled{4}$$

Now, solve for  $\dot{\psi}, \dot{\phi}$  in ②, ③ to get

$$\dot{\phi} = \frac{b - a \cos \theta}{\sin^2 \theta} \dots \textcircled{5}$$

$$\dot{\psi} = \frac{I_1}{I_3} a - \frac{\cos \theta (b - a \cos \theta)}{\sin^2 \theta} \dots \textcircled{6}$$

⑥

⑤, ⑥ into ④)

$$\frac{1}{2} \dot{\theta}^2 + \frac{mgl \cos \theta}{I_1} + \frac{1}{2} \frac{(b - a \cos \theta)^2}{\sin^2 \theta} = \frac{E'}{I_1} \dots (7)$$

where  $E' = E - \frac{1}{2} I_3 \omega_3^2$

Now, make dimensionless. Choose  $t \sim \frac{1}{b} I_1$  define

$$p = \frac{mgl}{I_1 b^2} \dots (8), \quad \xi = \frac{a}{b} \dots (9), \quad \varepsilon = \frac{E'}{I_1 b^2} \dots (10)$$

$$(7): \frac{1}{2} \left( \frac{d\theta}{dt'} \right)^2 + p \cos \theta + \frac{(1 - \xi \cos \theta)^2}{2 \sin^2 \theta} = \varepsilon \dots (11)$$

Let  $u = \cos \theta$

$$\rightarrow (11): \left( \frac{du}{dt'} \right)^2 = 2(1 - u^2)(\varepsilon - pu) - (1 - \xi u)^2 = f(u) \dots (12)$$

Note, allowed values of  $u$  are  $-1 \leq u \leq 1$

$$f(-1) = -(\varepsilon + 1)^2 < 0$$

$$f(1) = -(\varepsilon - 1)^2 < 0$$

$\Rightarrow$  To, must have one real root for  $u > 1$

$\Rightarrow$  must have 0, 1 or 2 real roots for  $-1 < u < 1$

0 roots  $\Rightarrow f(u) < 0 \quad \forall u \in [-1, 1] \Rightarrow$  not allowed  
 w 1 or 2 roots.



⑦

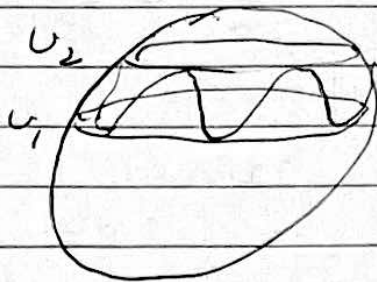
Locus of figure axis

Let  $v_1$  and  $v_2$  be roots of  $f(u)$  in  $[-1, 1]$  and  $v' = \frac{1}{\Sigma}$ . From ②

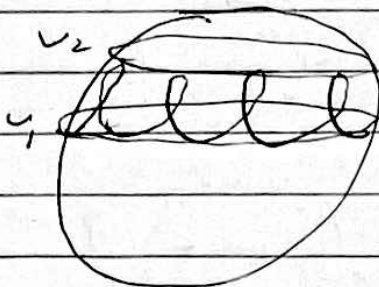
$$\frac{d\phi}{dt'} = \frac{1 - \frac{v}{v'}}{1 - v^2} \quad \text{--- (13)}$$

Remember,  $f(u)$  must be nonnegative always, so  $v_1 \leq v \leq v_2 \Rightarrow$  figure axis remains between two bounding circles always.

- 1) If  $v' > v_2$ , then since  $v \in [v_1, v_2]$ ,  $v \leq v'$  always, so from (13),  $\frac{d\phi}{dt'} > 0$  always  $\Rightarrow$  unidirectional precession

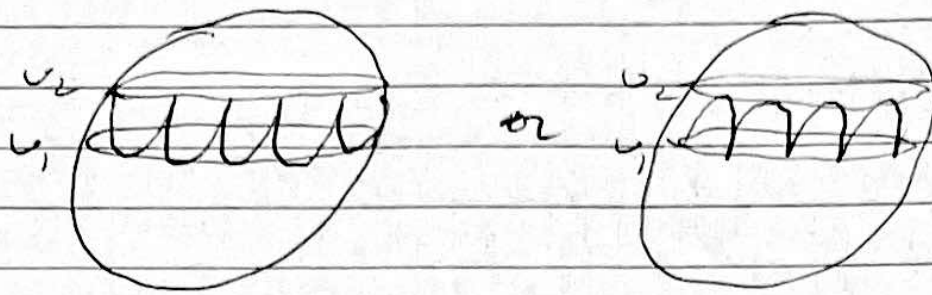


- 2) If  $v_1 \leq v' \leq v_2$ , at  $v = v_2$ ,  $\frac{d\phi}{dt'} \leq 0$  and at  $v = v_1$ ,  $\frac{d\phi}{dt'} > 0$ :



- 3) If  $v' = v_1$  or  $v_2$ , at  $v_1$  or  $v_2$ , both  $\dot{\theta} = 0$  and  $\dot{\phi} = 0$ :

(8)



~~First~~ First pic above is actually  $v_0 = v_2$  and is  $\dot{\theta}(0) = \dot{\phi}(0) = 0$ .

~~With~~ A  $v_0$ ,  $\dot{\theta}(0) = \dot{\phi}(0) = 0$  into (3):

$$b = \frac{I_3}{I_1} \dot{\phi} v_0$$

But (2):  $a = \frac{I_1}{I_1} \dot{\phi}$

$$\Rightarrow \text{~~From~~ } v' = \frac{1}{\Sigma} = \frac{b}{a} = v_0 = v_2$$

Fast top and  $\dot{\theta}(0) = \dot{\phi}(0) = 0$

Around  $\dot{\theta}(0) = \dot{\phi}(0) = 0$  and

$$\frac{1}{2} I_3 \omega_3^2 \gg \text{negl} \dots (14) \quad (\text{Fast top})$$

Putting  $v = v_0$  into (2) and using  $f(v_0) = 0$  and  $\Sigma = \frac{1}{v_0}$ , get

$$\Sigma = p v_0 \dots (15)$$

(15) into (2)

$$f(v) = 2p(v - v_0) \left( v^2 - \frac{1}{2pv_0^2} v + \frac{1}{2pv_0} - 1 \right)$$

Get roots of quadratic. Define

$$I = \frac{1}{2pv_0^2} = \frac{I_1 a^2}{2 \text{negl}} = \frac{I_3}{I_1} \frac{\frac{1}{2} I_3 \omega_3^2}{\text{negl}}$$



(9)

(14) means  $I \gg 1$ . Quadratic is then

$$v^2 - Iv - (1 - Iv_0) = 0$$

$$\rightarrow v_{\pm} = \frac{I}{2} \left( 1 \pm \left( 1 - \frac{4v_0}{I} + \frac{4}{I^2} \right)^{\frac{1}{2}} \right)$$

$$\rightarrow v_{\pm} \approx \frac{I}{2} \left( 1 \pm \left( 1 - \frac{2v_0}{I} + \frac{2(1-v_0^2)}{I^2} \right) \right)$$

$$v_+ \approx I \gg 1 \text{ so not allowed}$$

$$v_- \approx v_0 - \frac{1-v_0^2}{I}$$

$$\text{so } v_+ = v_- \approx v_0 - \sin^2 \theta \frac{I_1}{I_3} \frac{2\pi\hbar}{I_3 \omega_3^2} \quad (16)$$

1)  $|v_+ - v_-|$  gives extent of nutation. If  $\omega_3$  increases, nutation decreases.

Frequency of nutation: Energy eq:

$$\dot{\psi}^2 = 2p(v - v_0) \left( v^2 - \frac{1}{2pv_0^2} v + \frac{1}{2pv_0} - 1 \right) \quad (17)$$

If (14) is satisfied,  $v$  is close to  $v_0$  i.e.  
 $v = v_0 + x$ , where  $x \ll v_0$

means  $\frac{d}{dt} \rightarrow (17): \dot{x}^2 = -2p \sin^2 \theta_0 x + 2p(2v_0 - I)x^2 + O(x^3)$

$$\rightarrow \frac{d^2 x}{dt^2} + 2p(I - 2v_0)x = -p \sin^2 \theta_0$$

$$\text{But } t' = bt$$

$$\rightarrow \ddot{x} + 2b^2 p I x = -b^2 p \sin^2 \theta_0 \quad (18)$$

(10)

$$\rightarrow \omega^2 = 2b^2, I = a^2$$

$$\rightarrow \omega = a = \frac{I_2}{I_1} \omega_2 \dots (19)$$

2) To larger  $\omega_2$  means faster rotation.

$$\text{Precession: } \dot{\phi} = \frac{b(1-\epsilon\omega)}{1-\omega^2} \quad (20)$$

$$\text{Let } \omega = \omega_0 + \epsilon, \quad \epsilon \ll \omega_0$$

$$\rightarrow \dot{\phi} \approx -\frac{a\epsilon}{\sin^2 \theta_0}$$

Solve (18) w B.C.:  $x(0) = 0, \dot{x}(0) = 0$

$$\rightarrow \cancel{\dot{x}} x(t) = -\frac{\sin^2 \theta_0}{2I} (1 - \cos(at))$$

$$\rightarrow \dot{\phi} \approx \frac{a}{2I} (1 - \cos(at)) = \frac{a}{I} \sin^2\left(\frac{at}{2}\right)$$

$$\rightarrow \langle \dot{\phi} \rangle = \frac{a}{2I} = \frac{\omega_2}{I_2 \omega_2} \dots (21)$$

3) To larger  $\omega_2$  means slower precession.

1), 2), 3) are the relevant conclusions.

Initial conds for pure precession

Want to find initial conds which lead to  $\Theta = 0 \forall t$  and just pure precession.

$\rightarrow \omega_0$  must be a double root, so  $f(\omega_0) = 0$  and  $\frac{df}{d\omega} \bigg|_{\omega_0} = 0$ .

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Using  $f(v) = 2(1-v^2)(\epsilon - pv) - (1-\gamma v)^2$

$$f(v_0) = 0: \quad \epsilon - pv_0 = \frac{(1-\gamma v_0)^2}{2(1-v_0^2)} \quad \dots (21)$$

$$\frac{df}{dv}\bigg|_{v_0} = 0: \quad 2v_0(\epsilon - pv_0) + p(1-v_0^2) - \gamma(1-\gamma v_0) = 0 \quad \dots (22)$$

Using (21):

$$(1-\gamma v_0)(v_0(1-\gamma v_0) - \gamma(1-v_0^2)) + p(1-v_0^2)^2 = 0$$

$$\text{Use } 1-\gamma v_0 = \frac{\dot{\phi} \sin^2 \theta_0}{b}$$

$$\rightarrow \frac{\dot{\phi} \sin^2 \theta_0}{b} \left( \frac{\dot{\phi} \sin^2 \theta_0 \cos \theta_0}{b} - \gamma \sin^4 \theta_0 \right) + p \sin^4 \theta_0 = 0$$

$$\rightarrow \frac{I_3 \omega_j \dot{\phi}}{I_1} - \dot{\phi}^2 \cos \theta_0 = \frac{\mu s l}{I_1} \quad \dots (23)$$

(23) is a general eq for  $\dot{\phi}$ .

There are real solutions to (23), i.e. pure precession is possible if

$$\omega_j > \omega_{jc} = \frac{2}{I_3} \sqrt{\mu s l I_1 \cos \theta_0} \quad \dots (24)$$

~~For~~ If  $\omega_j > \omega_{jc}$ , can choose  $\omega_j$  and  $\theta_0$  to get desired precession rate.

If precession slow, neglect  $\dot{\phi}^2$  term in (23)

$$\rightarrow \dot{\phi} = \frac{\mu s l}{I_3 \omega_j}$$

Can also get this result if  $\omega_j \gg \omega_{jc}$ :



(12)

sol of (22):

$$\dot{\phi} = \frac{I_3 \omega_3}{2I_1 \cos \theta_0} \left( 1 \pm \left( 1 - \frac{4\mu_3 l I_1 \cos \theta_0}{I_3^2 \omega_3^2} \right)^{\frac{1}{2}} \right)$$

If  $\omega_3 \gg \omega_{sc}$ ,

$$\dot{\phi} \approx \frac{I_3 \omega_3}{2I_1 \cos \theta_0} \left( 1 \pm \left( 1 - \frac{2\mu_3 l I_1 \cos \theta_0}{I_3^2 \omega_3^2} \right) \right)$$

$$\left. \begin{aligned} \rightarrow \dot{\phi}_- &= \frac{\mu_3 l}{I_3 \omega_3} \\ \dot{\phi}_+ &= \frac{I_3}{I_1 \cos \theta_0} \omega_3 \end{aligned} \right\} (24)$$

 $v=1$  is a root of  $f(v)$ (1) at  $t=0$ :  $v(0)=1$ ,  ~~$\dot{v}(0)=0$~~  $\rightarrow \Sigma = p \dots (25)$ 

$$\rightarrow E - \frac{1}{2} I_3 \omega_3^2 = \mu_3 l$$

(25) into (2):  $\Sigma = 1$  and so

$$f(v) = (1-v)^2 [2p(1+v) - 1]$$

 $\rightarrow v=1$  is a double root, other root is

$$v_1 = \frac{1}{2p} - 1 = \frac{I_1 b^2}{2\mu_3 l} - 1 = \frac{I_1 a^2}{2\mu_3 l} - 1$$

$$\rightarrow v_1 = \frac{I_3^2 \omega_3^2}{2\mu_3 l I_1} - 1$$

If  $v_1 > 1$ , i.e. if  $\omega_3 > \omega_{sc} = \frac{2}{I_3} \sqrt{\mu_3 l I_1}$ ,  
top remains vertical

(13)

If  $w_3 < w_{3c}$ , top mutates between  $v_2 = 0$  and  $v_1 = \frac{1}{2p} - 1 \neq v_2$ .

If  $w_3 > w_{3c}$  initially and  $\theta_0 = 0$ , friction slows  $w_3$  to  $< w_{3c}$ , so top starts to mutate (nibble).