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by

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Dissertation

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Doctorate of Philosophy

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August 2015

<Title of dissertation or treatise, double-spaced, and centered>

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The University of Texas at Austin, 2015

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<Abstract: May not exceed 350 words. It should be a continuous description, not disconnected notes or an outline.>

Table of Contents

List of Tablesviii
List of Figuresix
List of Illustrationsx
Chapter 1 Introduction
Chapter 2 Simulation Methods
2.1 Labeling and Mutating Proteins in silico
2.2 Enhanced Molecular Dynamics in Amber03: N-Dimensional Umbrella Sampling and Weighted Histogram Analysis Method3
2.3 Electrostatic Clustering in Vibrational Chromophore Dihedral Space11
2.4 Probe Parameterization for AMOEBA16
2.5 Small Molecule Simulations in AMOEBA
Chapter 3 Electrostatic Field Methods
3.1 Amber03 with Explicit TIP3P Water
3.1.1 Reaction Field Electrostatics
3.1.2 Hybrid Solvent Reaction Field Electrostatics and Solute Coulomb Field
3.2 Amber03 with Poisson-Boltzmann Continuum Solvent30
3.2.1 Reaction Field Method
3.2.2 Grid spacing and size
3.2.3 Box Location
3.3 Amber03 with Poisson-Boltzmann Continuum Solvent and Select Explicit TIP3P Water Molecules
3.3.1 5 Å Water Sphere Around the Vibrational Chromophore31
3.3.2 Single Water Molecule Nearest the Vibrational Chromophore31
3.3.3 Water Molecular Hydrogen Bonding to the Vibrational Chromophore
3.4 AMOEBA32
3.4.1 Poisson-Boltzmann Continuum Solvent32

3.4.2 Explicit AMOEBA Water	32
3.4.3 Charge Penetration Field Corrections	32
Chapter 4 The Role of Electrostatics in Differential Binding of Ra Mutations E30D and K31E Investigated by Vibrational Spec Thiocyanate Probes	ctroscopy of
4.1 Introduction	33
4.2 Results	33
4.3 Discussion	33
Chapter 5 Optimizing Electrostatic Field Calculations with the Ad- Boltzmann Solver to Predict Electric Fields at Protein-Protein Sampling and Focusing	n Interfaces I:
5.1 Introduction	34
5.2 Results	34
5.3 Discussion	34
Chapter 6 Optimizing Electrostatic Field Calculations with the Ad- Boltzmann Solver to Predict Electric Fields at Protein-Protein Explicit Near-Probe and Hydrogen Bonding Water Molecules	in Interfaces II:
6.1 Introduction	35
6.2 Results	35
6.3 Discussion	35
Chapter 7 Electrostatic Fields at Protein-Protein Interfaces: Increa and Various Electrostatic Methods: A Case for Simulating in Fields	Polarizable Force
7.1 Introduction	36
7.2 Results	36
7.3 Discussion	36
Chapter 8 Electrostatic Fields in Small Thiocyanate Molecules w. Generated using the AMOEBA Force Field	
8.1 Introduction	37
8.2 Results	37
8.3 Discussion	37

Appendix (or Appendices)	38
Glossary	39
References	40

List of Tables

Table 2-1: Sample Parameters for Ryckaert Bellemans dihedral potential f	function
used for validating 2D WHAM code	8

List of Figures

Figure 2-1: 2D WHAM Validation	.9
Figure 2-2: PB Solvent Reaction Field vs. Solute Analytic Coulomb Field	13
Figure 2-3: Field Values using Clustering Vs. Field Values using All Frames1	14
Figure 2-4: Correlations and Slopes at Various Cutoff Values	15

List of Code and Parameters

Code and Parameters 2-1: Cyanocysteine AMOEBA Parameters	18
Code and Parameters 2-2: Methyl Thiocyanate AMOEBA Parameters	20
Code and Parameters 2-3: Ethyl Thiocyanate AMOEBA Parameters	22
Code and Parameters 2-4: Hexyl Thiocyanate AMOEBA Parameters	27

Chapter 1 Introduction

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Chapter 2 Simulation Methods

2.1 LABELING AND MUTATING PROTEINS IN SILICO

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2.2 ENHANCED MOLECULAR DYNAMICS IN AMBER03: N-DIMENSIONAL UMBRELLA SAMPLING AND WEIGHTED HISTOGRAM ANALYSIS METHOD

An umbrella sampling strategy was used to obtain a Boltzmann-weighted statistical ensemble of thiocyanate probe orientations for all MD sampling. Through examining simulated protein structures, it became increasingly apparent that a second degree of freedom, χ_1 , was relevant to our probe conformational distributions. Therefore, two different umbrella sampling strategies were tested: one-dimensional sampling about the thiocyanate χ_2 dihedral angle and two-dimensional umbrella sampling about the thiocyanate χ_1 and χ_2 dihedral angles, shown in Figure 2-1. All molecular dynamics were completed using the GROMACS¹ software package at 300 K with the AMBER03² force field and periodic boundary conditions.

Six probe locations on RalGDS were examined: N27C_{SCN}, G28C_{SCN}, N29C_{SCN}, Y31C_{SCN}, K32C_{SCN}, and N54C_{SCN}, in the monomeric state and docked to each GTPase system examined. We have therefore examined all probe locations and mutated constructs for which experimental data are available. Six structures for each system modeled were generated by fixing the thiocyanate χ₂ dihedral angle from 0° to 300° in 60° increments. Each structure was sampled with a dihedral potential that was flat within ± 30° of the fixed-dihedral position and quadratic with a force constant of 1000 kJ mol⁻¹ rad⁻² otherwise. These restraining potentials were carried through for the duration of the system set-up and simulation. Each structure was energy minimized with cut-off electrostatics, solvated with tip3p water³ in a dodecahedron box, charge balanced by randomly replacing the appropriate number of water molecules with sodium or chloride ions using the genion GROMACS utility, and solvent relaxed by sampling for 20 ps with position restraints on all non-solvent heavy atoms with a force constant of 1000 kJ mol⁻¹ nm⁻² using PME^{4,5} electrostatics with a real-space cut-off of 0.9 nm, spacing of 0.12 nm,

and interpolation order 4. Each rotamer of each system was then sampled using the GROMACS stochastic dynamics integrator, constraints on hydrogen-bonds using the LINCS algorithm⁶, and PME electrostatics for 3 ns, recording snapshots every 5 ps, for a total of 18 ns of simulation and 3606 frames for each system.

Each frame was assigned to one of 72 5° bins from -180° to 175° based on the χ_2 dihedral angle. The weighted histogram analysis method (WHAM)^{7,8} was then used to calculate a torsional potential of mean force (PMF) for each of N bins i, which is related to the torsional probability distribution for each bin i (P_i) described by equation (2-1):

$$P_{i} = \frac{e^{-\beta \cdot PMF_{i}}}{\sum_{j=0}^{N} e^{-\beta \cdot PMF_{j}}}, \ \beta = \frac{1}{k_{b}T}$$
 (2-1)

which is the typical Boltzmann distribution function for a state i divided by the partition function, where T is the temperature in Kelvin, k_b is the Boltzmann constant, and PMF_j is the PMF for some state j.

The two-dimensional umbrella sampling was done in much the same way as the one-dimensional sampling, with few minor changes. The χ_1 angle was fixed from 0° to 300° in 30° increments, resulting in 12 structures. Each of these structures then had the χ_2 angle fixed from 0° to 300° in 30°, resulting in 144 total structures. To avoid steric clashes in the starting structures, for each χ_2 rotation, the distance between the center of mass coordinate of each rotated atom and every non-rotated atom was calculated. If a distance was found to be under 1.5 Å, the χ_2 angle was rotated \pm 1.5° from the dihedral center and the distances were recalculated. This was done until all non-bonded atoms were at least 1.5 Å from each rotated atom. Next, two harmonic dihedral restraining potentials were generated for each structure, one for the χ_1 dihedral angle and one for the χ_2 dihedral angle. Following the same set-up strategy used in the one-dimensional

sampling, the system was then energy minimized with cut-off electrostatics and dihedral force constants of 1000 kJ mol⁻¹ rad⁻², solvated in tip3p water in a dodecahedron box, and charge balanced as described above. The system underwent solvent relaxation using PME electrostatics for 20 ps with a force constant of 1000 kJ mol⁻¹ nm⁻² on heavy backbone atoms, dihedral force constants of 150 kJ mol⁻¹ rad⁻², and unrestrained sidechain atoms. Each of the 144 χ_1 - χ_2 rotamers were then sampled for 400 ps using the GROMACS stochastic dynamics integrator with PME electrostatics (again, with a realspace cut-off of 0.9 nm, spacing of 0.12 nm, and interpolation order 4) and dihedral restraining potentials of 70 kJ mol⁻¹ rad⁻², for a total of 57.6 ns of simulation and 11664 frames for each system. It is worth reiterating that each step used a progressively smaller dihedral restraining potential. This was done to ensure that the dihedral angles of the final structure before sampling were as close as possible to the umbrella-sampling window while still allowing nearby residues to relax to orientations that accommodate the inclusion of our probe. Starting with a large restraining potential fixes the probe to a specific location orientation and forcibly moves nearby residues to accommodate the probe to minimize interaction energies. Subsequent weakening of the restraining potential allows the probe to respond to its surroundings in a manner more typical of MD, allowing both the probe as well as the residues near the probe to relax to energy minimized orientations. Without this subsequent weakening, many simulations resulted in dihedral forces becoming larger than the integrator can or is expected to handle, which were usually caused by steric clashes between the probe and side-chain atoms.

A Boltzmann-weighted statistical ensemble of structures obtained from twodimensional sampling was then assembled using WHAM. Each frame was assigned to one of 5184 5° by 5° bins. The bins were assigned based on equation (2-2), where b_1 is the one-dimensional χ_1 bin number, b_2 is the one-dimensional χ_2 bin number, B_i is the total number of bins in degree of freedom i (72 for all two-dimensional sampling done), and i_{index} refers to the subscript on b. Conditional probability was assumed.

$$Bin(b_1, b_2) = \sum_{i=b_1, b_2} B_i^{2-i_{index}} \cdot i$$
 (2-2)

To validate our 2D WHAM code, we examined a Ryckaert-Bellemans dihedral potential, shown in equation (2-3), where ϕ is some angle and n and C_n are some example parameters obtained from the GROMACS manual, shown in Table 2-1. This is a very simple potential function with no contributions from any other source, unlike the potential energy calculation in a protein, which will be influenced by various force field parameters such as bond force constants. However in WHAM, the sources of the potentials are not distinguished, and we are able to use the simple Ryckaert-Bellemans model to validate the code. We constructed the PMF from the sum of the potentials for a given pair of coordinates and the unbiased probability distribution, $p^{\circ}(\chi_1, \chi_2)$, using the ratio of the Boltzmann distribution function to the partition function, shown in equation (2-4), over an array of 2D dihedral angles ranging form -180° to 180°.

$$V_{rb} = \sum_{n=0}^{3} C_n (\cos(\phi - \pi))^n$$
 (2-3)

Next, we constructed the PMF and probability distribution landscapes, shown in Figure 2-1a. We then applied biasing potential windows to each dimension in a manner that mimics the methods used in GROMACS. The biased probability, $p(\chi_1, \chi_2)$, is given by equation (2-5). We then performed a Monte Carlo simulation centered on each of 144 biased windows, each with dimensions of 30° x 30°, with a probability $p(\chi_1, \chi_2)$ of sampling a given pair of dihedral angles, which was then analyzed using our 2D WHAM code to return the unbiased PMF and $p^{\circ}(\chi_1, \chi_2)$.

$$p^{\circ}(\chi_{1}, \chi_{2}) = \frac{e^{-\beta(V_{rb}(\chi_{1}) + V_{rb}(\chi_{2}))}}{\iint e^{-\beta(V_{rb}(\chi_{1}) + V_{rb}(\chi_{2}))} d\chi_{1} d\chi_{2}}$$
(2-4)

$$p(\chi_1, \chi_2) = \frac{e^{-\beta(V_{rb}(\chi_1) + V_1 + V_{rb}(\chi_2) + V_2)}}{\int \int e^{-\beta(V_{rb}(\chi_1) + V_1 + V_{rb}(\chi_2) + V_2)} d\chi_1 d\chi_2}$$
(2-5)

Figure 2-1 shows the analytical PMF and probability distributions (a), WHAM PMF and probability distributions on 144 windows each containing 40 frames (b), WHAM PMF and probability distributions on 144 windows each containing 80 frames (c), WHAM PMF and probability distributions on 144 windows each containing 160 frames (d), and WHAM PMF and probability distributions on 144 windows each containing 1000 frames (e). The major features of the probability distribution become clear after only 40 frames; after 80 frames the probability distributions look very similar to the analytical distribution, and after 160 frames very little improvement is seen. We can also see that the high probability regions, representing the staggered orientations, have PMF landscapes that look like the analytical PMF, although the gauche regions appear to be ill characterized still. After 1000 frames the probability distribution is nearly identical to the analytical distribution and the moderate ranges of the PMF (light blue, > 17.92 kJ mol⁻¹) now quantitatively approach the predictions of the analytical expression. Exact analytical PMF matching of low probability regions is very slow, requiring ≥10000 frames. From these results we conclude that the PMF converges to the analytical expression slowly for regions of low probability and quickly for regions of high probability.

Table 2-1: Sample Parameters for Ryckaert Bellemans dihedral potential function used for validating 2D WHAM code

	Constraint (kJ mol ⁻¹)		Constraint (kJ mol ⁻¹)
C_0	9.28	C ₃	-3.06
$\mathbf{C_1}$	12.16	$\mathbf{C_4}$	-26.24
C_2	-13.12		-31.5

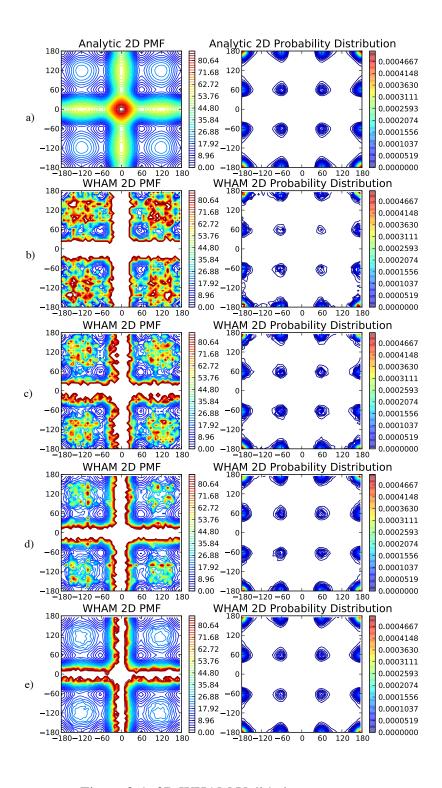


Figure 2-1: 2D WHAM Validation

Comparison between the PMF and probability distributions of a) an analytic Ryckaert-Bellemans dihedral potential and Monte Carlo 2D umbrella sampling for b) 40 frames/biasing window; c) 80 frames/biasing window; d) 160 frames/biasing window; e) 1000 frames/biasing window. Units on the PMF are kJ mol⁻¹.

2.3 ELECTROSTATIC CLUSTERING IN VIBRATIONAL CHROMOPHORE DIHEDRAL SPACE

The largest bottleneck for these sorts of calculations we do are the electrostatics. A single node on Stampede can generate >10 ns of simulation per day. That number can be increased (logarithmically) by using additional nodes. However, the continuum solvent electrostatics calculations take anywhere from 45-60 seconds (APBS) to \$\approx\$ 20 minutes (AMOEBA) per frame. If we keep every 4 ps and collect 250 frames per nanosecond, then the electrostatics require 5-8 ns/day for APBS calculations and approximately 0.3 ns/day for AMOEBA calculations. This can be decreased further by running the serial calculations in parallel. Regardless, it would be convenient to find some method of pruning the total number of frames for continuum electrostatics calculations while ensuring that the average field does not differ significantly from the average using every frame.

For convenience, the vacuum electrostatic field at the nitrile due to solute only was chosen as an indicator of total electrostatic field. In the absence of solvent, this is trivial to calculate for both point charge force fields (Amber03) as well as multipole force fields (AMOEBA). This was chosen because it was 1) intuitive and 2) there is consistently a good correlation between the solute Coulomb field and the PB solvent reaction field, as seen in Figure 2-2,git suggesting that frames which well represent the Coulomb field also well represent the reaction field.

We then took advantage of the weighted averaging over binned data. The Boltzmann weighted average is calculated as in equation (2-6),

$$\langle x \rangle = \sum_{i=1}^{\text{nbins}} \rho_i \sum_{j=1}^{c_i} \frac{x_{ij}}{c_i}$$
 (2-6)

where the probability of being in each bin i is ρ_i , the number of times bin i is visited is c_i , and each value in bin i is x_{ij} for j = 1 to $j = c_i$. There exists some subarray of

values in bin *i* that has k_i values, where $k_i \ge c_i$ entries and $\left| \sum_{j=1}^{k_i} \frac{x_{ij}}{k_i} - \sum_{j=1}^{c_i} \frac{x_{ij}}{c_i} \right| \le \chi$, where χ is

some threshold. As χ approaches 0, k_i approaches c_i , and the subarray is the full array and the averages are identical. Using the a set of test data where umbrella windows were centered every 120 degrees (at 60°, 180°, and 300°, the expected alkane maximum probability torsions) with a flat biasing potential $\pm 60^{\circ}$ of the window center and a force constant of **XXX, the clustered average field for each Ral probe in the monomeric state, docked to each of the four Rap1a mutants and each of the four Ras mutants is plotted against their average field for various values of χ , indicated in the upper-left corner of each subplot, from the full data sets in Figure 2-3. From this, it's clear that the clustered averages are linearly correlated to the full averages. The correlation coefficients and best-fit slopes have also been plotted as a function of the cutoff, χ , in Figure 2-4. Even for a relatively large $\chi = 1$, the clustered correlation coefficient and slope is *very* close to 1.0. In general, as χ approaches zero, the correlation coefficient and slope also approach zero. Moreover, at a $\chi = 0.01$, only approximately 20% of all frames are used, which is a significant decrease in computation requirement. This method also has the advantage of guaranteeing that the property the cluster is based on always has a clustered average nearly identical to the full average, which is a useful sanity check.

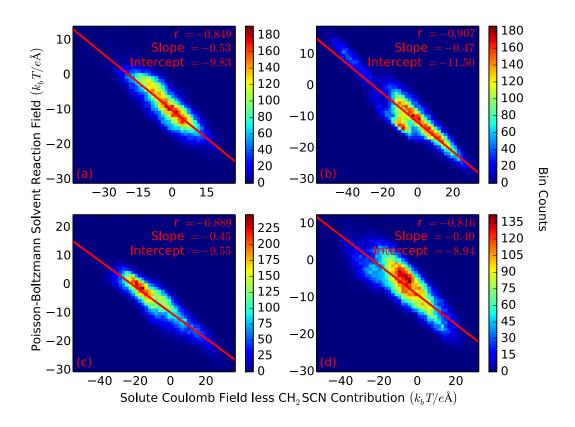


Figure 2-2: PB Solvent Reaction Field vs. Solute Analytic Coulomb Field

Comparison between the analytic Coulomb field at the nitrile bond midpoint due to solute (less the contributions due to the probe itself) (x-axis) and the solvent reaction field at the nitrile bond midpoint (y-axis) using Amber03 point charges for a) Ral $\rm G28C_{SCN}$ monomer; b) Ral $\rm N54C_{SCN}$ monomer; c) Ral $\rm G28C_{SCN}$ docked to wild type Rap; d) Ral $\rm N54C_{SCN}$ docked to wild type Rap. Correlation coefficients (r), slopes (m), and y-intercepts (int), are indicated in the upper-right corner of each figure.

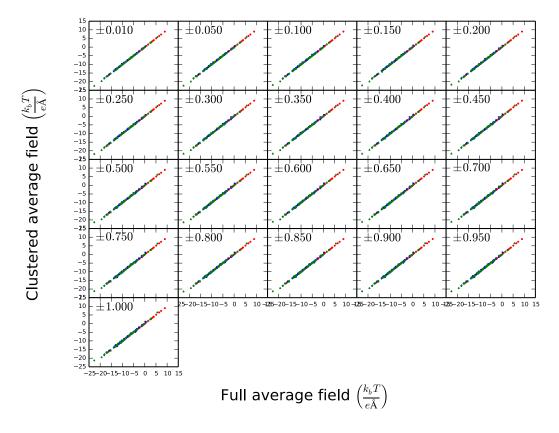


Figure 2-3: Field Values using Clustering Vs. Field Values using All Frames

Average Coulomb electrostatic field (red), solvent reaction field (blue), and the electrostatic field calculated using the AMOEBA force field (green) from clustered frames versus the respective full averages for various cutoff values, χ , indicated in the top left corner of each box.

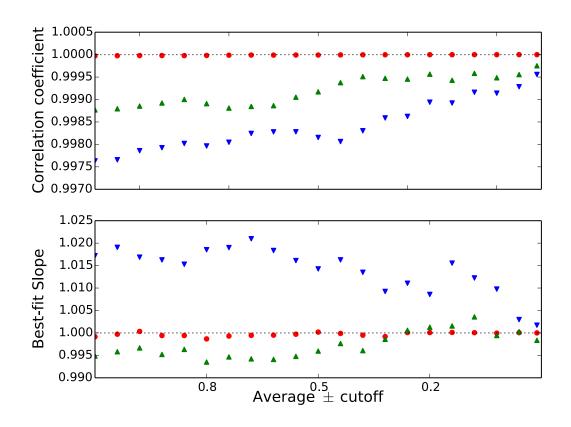


Figure 2-4: Correlations and Slopes at Various Cutoff Values

Correlation coefficients of the Coulomb electrostatic field (red), solvent reaction field (blue), and the electrostatic field calculated using the AMOEBA force field (green) as a function of the cutoff, χ . (Bottom) Best-fit slopes of the Coulomb electrostatic field (red), solvent reaction field (blue), and the electrostatic field calculated using the AMOEBA force field (green) as a function of the cutoff, χ .

2.4 PROBE PARAMETERIZATION FOR AMOEBA

<Body text to begin here.>

										_		_
1.	atom	259	55	CB	"CNC					6	12.011	4
2.	atom	260	56	SG	"CNC					16	32.066	2
3.	atom	261	57	CD	"CNC					6	12.011	2
4.	atom	262	58	NE	"CNC					7	14.007	1
5.	atom	263	59	HB	"CNC	HB"				1	1.008	1
6.												
7.	multipole	259	8	260			-0.152	228				
8.							0.074	107	0.00000	0.31	740	
9.							-0.151	.17				
10.							0.000	900 -	-0.21945			
11.							-0.192	82	0.00000	0.37	962	
12.	multipole	260	259	261			0.330	74				
13.	•						0.443	889	0.00000	0.287	736	
14.							1.223					
15.							0.000		-2.16613			
16.							-0.316		0.00000	0.942	244	
	multipole	261	260	262			0.245		0.00000	0.542		
18.	arcipoic	-01	_00	232			0.064		0.00000	-0.418	300	
19.							0.157		0.00000	0.410		
20.							0.000		0.22633			
20.							0.266		0.00000	-0.383	273	
	multipole	12	8	259			0.128		0.00000	-0.50.	373	
23.	шитстроте	12	0	233			0.025		0.00000	0.070	21.4	
							0.190		0.00000	0.076	714	
24.								-	0 17013			
25.							0.000		0.17012	0.36	262	
26.		262	250	•			-0.015		0.00000	-0.36	163	
	multipole	263	259	8			0.091		0 00000	0 004	200	
28.							-0.071		0.00000	-0.020	080	
29.							-0.160		0 00050			
30.							0.000		-0.02258	0.40		
31.	7	262	264	260			-0.032		0.00000	0.183	319	
	multipole	262	261	260			-0.588			0 04		
33.							-0.005		0.00000	-0.242	238	
34.							0.323					
35.							0.000		0.16836			
36.							-0.082	202	0.00000	-0.493	168	
37.												
	polarize	259			3340		900	263				
	polarize	260			3000		900	261				
	polarize	261			3340		900	260	262			
	polarize	262			0730		900	261				
	polarize	263		0.4	4960	0.3	900	259				
43.												
	vdw	58			3.710		0.10					
	vdw	55			3.786	90	0.10					
	vdw	56			4.005	50	0.35	50				
47.	vdw	57			3.786	90	0.10	60				
48.	vdw	59			2.87	90	0.03	30	0.900			
49.	bond	55	7		323.000	90	1.53	317				
	bond	55	56		235.800	90	1.83	353				
51.	bond	55	59		341.000	90	1.08					
	bond	56	57		235.800	90	1.70	60				
	bond	57	58		450.000	90	1.13	374				
	angle	7	55	56	53.200		109.69					
	angle	7	55	59	42.446		110.80					
	angle	56	55	59	60.246		108.48					
	angle	59	55	59	39.576		108.82					
•	5 -			-	•	17						

```
58. angle
                                  60.0000
                                            108.7411
                 55
59. angle
                 55
                                  80.0000
                                            112.9036
60. angle
                 55
                       7
                                  38.0000
                                            109.5706
                            6
61. angle
                 55
                      56
                           57
                                  60.4300
                                             98.5327
62. angle
                 56
                      57
                                  60.0000
                                            178.6763
                           58
63. strbnd
                  7
                      55
                                             18.7000
                           56
                                  18.7000
64. strbnd
                  7
                      55
                           59
                                  11.5000
                                             11.5000
65. strbnd
                 56
                      55
                           59
                                  11.5000
                                             11.5000
66. strbnd
                 55
                            3
                                  18.7000
                                             18.7000
67. strbnd
                 55
                             1
                                  18.7000
                                             18.7000
68. strbnd
                 55
                       7
                                  11.5000
                                             18.7000
                            6
69. strbnd
                 55
                      56
                           57
                                  -5.7500
                                             -5.7500
70. torsion
                 56
                      55
                            7
   1.010 0.0 1
                  1.230 180.0 2
                                  1.000 0.0 3 # CYS 3 7 8 12
71. torsion
                 56
                      55
                                        -0.160 0.0 1
                                                        1.080 180.0 2
   1.520 0.0 3 # CYS 1 7 8 12
72. torsion
                 56
                      55
                                         0.000 0.0 1
                                                        0.000 180.0 2
                                                                         0.475 0.0 3 #
   CYS 6 7 8 12
73. torsion
                      55
                                         0.000 0.0 1
                                                        0.000 180.0 2
                                                                         0.180 0.0 3 #
   CYS 3 7 8 9
74. torsion
                      55
                                         0.000 0.0 1
                                                        0.000 180.0 2
                                                                         0.500 0.0 3 #
   CYS 1 7 8 9
                                                                         0.299 0.0 3 #
75. torsion
                                         0.000 0.0 1
                                                        0.000 180.0 2
   CYS 6 7 8 9
76. torsion
                  7
                      55
                           56
                                 57
                                       -0.4400 0.0 1 -
   0.2600 180.0 2
                    0.6000 0.0 3 # EtSCN C1 C2 S C
                                        0.0000 0.0 1 0.0000 180.0 2 0.6600 0.0 3 #
77. torsion
                 59
                           56
                                 57
   EtSCN H2 C2 S C
                                         0.929 0.0 1
                                                        0.328 180.0 2
                                                                         0.000 0.0 3 #
78. torsion
   CYS 1 3 7 8
                                         0.000 0.0 1
                                                        0.000 180.0 2
                                                                         0.000 0.0 3 #
79. torsion
   CYS 5 3 7 8
80. torsion
                                         2.576 0.0 1
                                                        1.011 180.0 2
                                                                         0.825 0.0 3 #
                             1
                                  3
   CYS 3 1 7 8
                                                        0.000 180.0 2
                                                                         0.000 0.0 3 #
81. torsion
                                         0.000 0.0 1
   CYS 4 1 7 8
82. torsion
                 55
                      56
                                 58
                                        0.0000 0.0 1 0.0000 180.0 2 0.5000 0.0 3 #
 EtSCN C2 S C N
```

Code and Parameters 2-1: Cyanocysteine AMOEBA Parameters

	_					.				_		_	
1.	atom	271	67	H1	"MeSCN					1	1.008		1
2.	atom	272	68	C1	"MeSCN					6	12.01		4
3.	atom	273	69	S	"MeSCN					.6	32.06		2
4.	atom	274	70	C	"MeSCN					6	12.01		2
5.	atom	275	71	N	"MeSCN	I N"				7	14.00	7	1
6.													
7.	multipole	272	273	271		-0.	22754						
8.						0.	00000	0.000	90 -0	.024	.49		
9.						0.	72145						
10.						0.	00000	0.7214	45				
11.						0.	00000	0.000	00 -1	.442	.90		
12.	multipole	273	272	274		0.	33074						
13.						0.	44389	0.0000	90 O	.287	36		
14.						1.	22369						
15.						0.	00000	-2.1663	13				
16.						-0.	31636	0.000	90 O	.942	44		
17.	multipole	274	273	275			24556						
18.				_			06457	0.000	a - 0	.418	00		
19.							15740		. •	0			
20.							00000	0.2263	33				
21.							26601	0.000		.383	73		
	multipole	271	272	273			07989						
23.	шатегроте	_,_	_,_	2,3			02678	0.000	aa -a	.314	.73		
24.							66454	0.000			, ,		
25.							00000	-0.0099	28				
26.							17231	0.000		.654	56		
	multipole	275	274	273			58843	0.000	0	.054	.50		
28.	шатстротс	275	2/4	213			00512	0.000	aa _a	.242	38		
29.							32332	0.000		•	.50		
30.							00000	0.1683	36				
31.							08202	0.000		.491	68		
32.													
	polarize	271		0.	4960	0.3900	27	2					
	polarize	272			3340	0.3900							
	polarize	273			3000	0.3900							
	polarize	274			3340	0.3900							
	polarize	275			0730	0.3900							
38.	•	_,,			0,50	0.3300		•					
	vdw	68			3.7806) 0	.1060						
	vdw	69			4.0056		.3550						
	vdw	70			3.7806		.1060						
	vdw	67			2.8700		.0330	a	900				
	vdw	71			3.7100		.1050	0.					
	bond	68	69		235.8006		.8209						
	bond	68	67		341.0000		.0794						
	bond	69	70		235.8000		.7068						
	bond	70	71		450.0006		.1373						
	angle	69	68	67	60.2400		.5747						
	angle	67	68	67	39.5706		.6263						
	angle	68	69	70	60.4300		.4461						
	angle	69	70	70	60.0000		.9042						
	strbnd	69	68	67			.5000						
	strbnd	68	69	70	11.5000 -5.7500		.7500						
	torsion	67	68	69		.0000		0.0000	180 0	2	0.6600	00	2
			69	70									
55.	torsion	68	69	10	71 6	.0000	ד ט.ט	0.0000	T80.0	_	0.5000	0.0	3

Code and Parameters 2-2: Methyl Thiocyanate AMOEBA Parameters

49. 50. 51. 52. 53.	polarize polarize polarize polarize	267 268 269 270 60 62		0.496 3.306 1.334 1.073	90 10		266 269 268 269 1040 1060	270			
49. 50. 51. 52.	polarize polarize polarize polarize	267 268 269 270		3.300 1.334	90 10 30	0.3900 0.3900 0.3900	269 268 269	270			
49. 50. 51.	polarize polarize polarize polarize	267 268 269		3.300 1.334	90 10	0.3900 0.3900	269 268	270			
49. 50.	polarize polarize polarize	267 268 269		3.300 1.334	90 10	0.3900 0.3900	269 268	270			
49.	polarize polarize	267 268		3.300	90	0.3900	269				
	polarize	267									
48.					()	" JUU	266				
	polarize	266		1.334		0.3900	264				
	polarize	265		0.496		0.3900	264				
	polarize	264		1.334		0.3900	265				
44.											
43.						-0.0	8202	0.00000	-0.49	168	
42.							0000	0.16836			
41.							2332				
40.							0512	0.00000	-0.24	238	
	multipole	270	269	268			8843				
38.							6601	0.00000	-0.38	373	
37.							0000	0.22633			
36.							5740				
35.							6457	0.00000	-0.41	800	
	multipole	269	268	270			4556				
33.	7	262	262	270			1636	0.00000	0.94	244	
32.								-2.16613	0.0	244	
31.							2369	2 16612			
30.							4389	0.00000	0.28	/36	
	multipole	268	266	269			3074	0 00000	0 20	726	
	mul+inolo	260	266	260				טטטטט. ט	-0.09	Z 1 3	
28.							0032	0.00000	-0.09	210	
27.							0000	0.02253			
26.							6966	5.00000	-0.00	TJJ	
25.		200	204	200			1969	0.00000	-0.08	459	
	multipole	265	264	266			8187	5.00000	-0.03		
23.							0070	0.00000	-0.03	653	
22.							0000	0.01348			
21.							2305	0.00000	-0.05	+13	
20.	шатстроте	207	200	207			92 44 9077	0.00000	-0.03	413	
	multipole	267	266	264			9244	0.00000	0.55	213	
18.							8743	0.00000	0.35	219	
17.								-0.08487			
16.							6732	0.00000	0.13	1001	
15.		200	204	200			6819	0.00000	0.15	997	
	multipole	266	264	268			3503	0.00000	0.50	0.70	
13.							0000	0.00000	0.50	030	
12.								-0.25019			
11.							5019	0.00000	0.32	J+1	
10.		204	200	203			0000	0.00000	0.32	541	
9.	multipole	264	266	265		_a 1	8333				
8.	a com	2,0	30	14	LCJCN				,	14.007	_
7.	atom	270	66	N	"EtSCN				7	14.007	1
6.	atom	269	65	C	"EtSCN				6	12.011	2
5.	atom	268	64	S	"EtSCN				16	32.066	2
4.	atom	267	63	H2	"EtSCN				1	1.008	1
3.	atom	266	62	C2	"EtSCN				6	12.011	4
2.	atom	265	61	H1	"EtSCN				1	1.008	1
1.	atom	264	60	C1	"EtSCN	L C1"			6	12.011	4

```
55. vdw
                  64
                                    4.0050
                                                0.3550
56. vdw
                  65
                                    3.7800
                                                0.1060
57. vdw
                  63
                                    2.8700
                                                0.0330
                                                             0.900
58. vdw
                  61
                                    2.9800
                                                0.0240
                                                             0.920
59. vdw
                  66
                                    3.7100
                                                0.1050
60. bond
                  60
                                  345.3000
                                                1.5227
                       62
61. bond
                  60
                       61
                                  341.0000
                                                1.0855
62. bond
                  62
                       64
                                  323.0000
                                                1.8329
63. bond
                  62
                       63
                                  341.0000
                                                1.0809
64. bond
                  64
                       65
                                  235.8000
                                                1.7068
65. bond
                  65
                       66
                                  450.0000
                                                1.1376
66. angle
                  62
                       60
                            61
                                   42.4400
                                              111.1890
67. angle
                  61
                       60
                            61
                                   39.5700
                                              108.4478
68. angle
                  60
                       62
                            64
                                   53.2000
                                              114.3035
69. angle
                  60
                       62
                            63
                                   42.4400
                                              111.8003
70. angle
                  64
                       62
                            63
                                   60.2400
                                              108.0491
71. angle
                  63
                       62
                            63
                                   45.5700
                                              107.8321
72. angle
                  62
                       64
                            65
                                   60.4300
                                               99.8280
73. angle
                  64
                       65
                             66
                                   60.0000
                                              179.1383
74. strbnd
                  62
                       60
                            61
                                   11.5000
                                               11.5000
75. strbnd
                  60
                       62
                             64
                                   18.7000
                                               18.7000
76. strbnd
                                               11.5000
                  60
                       62
                            63
                                   11.5000
77. strbnd
                  64
                       62
                            63
                                   11.5000
                                               11.5000
78. strbnd
                  62
                       64
                            65
                                   -5.7500
                                               -5.7500
79. torsion
                  61
                       60
                            62
                                          0.0000 0.0 1
                                                         0.0000 180.0 2
                                                                          0.4750 0.0 3
                                          0.0000 0.0 1 0.0000 180.0 2
                                                                          0.2990 0.0 3
80. torsion
                  61
                       60
                            62
                                  63
                                         -0.4400 0.0 1 -0.2600 180.0 2
                                                                          0.6000 0.0 3
81. torsion
                  60
                       62
                             64
                                  65
82. torsion
                                          0.0000 0.0 1 0.0000 180.0 2
                                                                          0.6600 0.0 3
                  63
                       62
                            64
                                  65
83. torsion
                                          0.0000 0.0 1 0.0000 180.0 2
                  62
                       64
                            65
                                  66
                                                                          0.5000 0.0 3
```

Code and Parameters 2-3: Ethyl Thiocyanate AMOEBA Parameters

1.	atom	276	72	C1	"HxSCN	C1"		6	12.011	4
2.	atom	277	73	C2	"HxSCN			6	12.011	4
3.	atom	278	74	H1	"HxSCN			1	1.008	1
4.	atom	279	75	C3	"HxSCN			6	12.011	4
5.	atom	280	76	H2	"HxSCN			1	1.008	1
		281		H3				1		1
6.	atom		77		"HxSCN				1.008	
7.	atom	282	78	C4	"HxSCN			6	12.011	4
8.	atom	283	79	C5	"HxSCN			6	12.011	4
9.	atom	284	80	H4	"HxSCN			1	1.008	1
	atom	285	81	H5	"HxSCN			1	1.008	1
	atom	286	82	C6	"HxSCN			6	12.011	4
	atom	287	83	H6	"HxSCN			1	1.008	1
	atom	288	84	S	"HxSCN			16	32.066	2
	atom	289	85	C	"HxSCN	C"		6	12.011	2
15.	atom	290	86	N	"HxSCN	N"		7	14.007	1
16.										
17.	multipole	279	282	277		-0.12665				
18.						0.16365	0.00000	0.143	302	
19.						0.06092				
20.						0.00000	-0.43628			
21.						-0.27661	0.00000	0.375	36	
22.	multipole	276	277	278		-0.15938				
23.	•					0.00000	0.00000	0.267	734	
24.						-0.20136				
25.						0.00000	-0.20136			
26.						0.00000	0.00000	0.402	772	
	multipole	283	282	286		-0.11656	0.00000	0.101	-,_	
28.	шатегроте	203		200		0.24230	0.00000	0.092	285	
29.						0.15205	0.00000	0.052	_05	
30.						0.00000	-0.43470			
31.						-0.43635	0.00000	0.282	265	
	multipole	282	279	283		-0.11327	0.00000	0.202	_05	
33.	шатстроте	202	213	203		0.22022	0.00000	0.084	170	
34.						0.15602	0.00000	0.002	+/3	
35.						0.00000	-0.44910			
36.								0 202	200	
	m1++m.o.1.o	277	270	276		-0.36114	0.00000	0.293	000	
	multipole	277	279	2/6		-0.12195	0.00000	0 15-	705	
38.						0.19367	0.00000	0.157	795	
39.						-0.01138	0 24202			
40.						0.00000	-0.31282	0.30	120	
41.		200	202	200		-0.22362	0.00000	0.324	120	
	multipole	286	283	288		-0.18161				
43.						0.04843	0.00000	0.185	545	
44.						-0.01034				
45.						0.00000	-0.10804	_		
46.						-0.18618	0.00000	0.118	338	
	multipole	280	277	279		0.05998				
48.						0.00441	0.00000	-0.076	536	
49.						0.04595				
50.						0.00000	0.03338			
51.						-0.00973	0.00000	-0.079	933	
					^	2				

	multipol	e 284	282	279	0.0	96214			
53.					0.0	2649	0.00000	-0.05387	
54.					0.0	1977			
55.					0.0	00000	0.03305		
56.					-0.0	00324	0.00000	-0.05282	
57.	multipol	e 281	279	282	0.0	95805			
58.					0.0	00916	0.00000	-0.05550	
59.					0.0	33877			
60.					0.0	00000	0.02937		
61.						06123	0.00000	-0.06814	
	multipol	e 285	283	282		7555			
63.	arczpoz	203	203	202		91936	0.00000	-0.04776	
64.						25942	0.0000	0.01770	
65.						00000	0.03376		
								0 00310	
66.		- 270	276	277		01589	0.00000	-0.09318	
	multipol	e 278	276	277		95847		0.40450	
68.						01125	0.00000	-0.10159	
69.						96569			
70.						00000	0.03435		
71.						33952	0.00000	-0.10004	
	multipol	e 287	286	283	0.0	7235			
73.						92117	0.00000	-0.04358	
74.					0.0	94575			
75.					0.0	0000	0.03869		
76.					-0.0	91006	0.00000	-0.08444	
77.	multipol	e 288	286	289	0.	33074			
78.	·				0.4	14389	0.00000	0.28736	
79.					1.	22369			
80.					0.0	90000 -	-2.16613		
81.						31636	0.00000	0.94244	
	multipol	e 289	288	290		24556	0.0000	0.00	
83.	arczpor	203	200	230		26457	0.00000	-0.41800	
84.						15740	0.00000	0.41000	
85.						00000	0.22633		
86.								0 20272	
		- 200	200	200		26601	0.00000	-0.38373	
	multipol	e 290	289	288		58843	0 00000	0 24220	
88.						00512	0.00000	-0.24238	
89.						32332			
90.						00000	0.16836		
91.					-0.0	08202	0.00000	-0.49168	
92.									
	polarize			1.3340		277	278		
	polarize			1.3340		276	280		
	polarize			0.4960		276			
	polarize			1.3340	0.3900	281			
97.	polarize	280		0.4960		277			
98.	polarize	281		0.4960		279			
	polarize			1.3340		284			
100.		olarize	28		1.3340	0.3900	285		
101.		olarize	28		0.4960	0.3900	282		
102.		olarize	28		0.4960	0.3900	283		
103.		olarize	28		1.3340	0.3900	287		
104.		olarize	28		0.4960	0.3900	286		
105.		olarize	28		3.3000	0.3900			
106.		olarize	28		1.3340	0.3900		290	
								230	
107.		olarize	29		1.0730	0.3900	289		
108.	•								
					2.4				

400					2 0200	0 1010		
109.	vdw	75			3.8200	0.1010		
110.	vdw	72			3.8200	0.1010		
111.	vdw	79			3.8200	0.1010		
112.	vdw	78			3.8200	0.1010		
113.	vdw	73			3.8200	0.1010		
114.	vdw	82			3.7800	0.1060		
115.	vdw	84			4.0050	0.3550		
116.	vdw	85			3.7800	0.1060		
117.	vdw	76			2.9800	0.0240	0.940	
118.	vdw	80			2.9800	0.0240	0.940	
119.	vdw	77			2.9800	0.0240	0.940	
120.	vdw	81			2.9800	0.0240	0.940	
121.	vdw	74			2.9600	0.0240	0.920	
122.	vdw	83			2.8700	0.0330	0.900	
123.	vdw	86			3.7100	0.1050		
124.	bond	75	78		453.0000	1.5299		
125.	bond	75	73		453.0000	1.5298		
126.	bond	75	77		341.0000	1.0885		
127.	bond	72	73		323.0000	1.5282		
128.	bond	72	74		341.0000	1.0863		
129.	bond	79	78		453.0000	1.5312		
130.	bond	79	82		345.3000	1.5276		
131.	bond	79	81		341.0000	1.0866		
132.	bond	78	80		341.0000	1.0879		
133.	bond	73	76		341.0000	1.0878		
		82						
134.	bond		84		235.8000	1.8351		
135.	bond	82	83		341.0000	1.0810		
136.	bond	84	85		235.8000	1.7063		
137.	bond	85	86	70	450.0000	1.1375		
138.	angle	78	75	73	48.2000	113.1072		
139.	angle	78	75	77	38.0000	109.3223		
140.	angle	73	75	77	38.0000	109.2787		
141.	angle	77	75	77	39.5700	106.3036		
142.	angle -	73	72	74	42.4400	111.1869		
143.	angle	74	72	74	39.5700	107.7267		
144.	angle	78	79	82	48.2000	111.5264		
145.	angle	78	79	81	38.0000	109.6162		
146.	angle	82	79	81	38.0000	109.5120		
147.	angle	81	79	81	39.5700	106.9493		
148.	angle	75	78	79	48.2000	112.7564		
149.	angle	75	78	80	38.0000	109.3923		
150.	angle	79	78	80	38.0000	109.3217		
151.	angle	80	78	80	39.5700	106.4572		
152.	angle	75	73	72	48.2000	112.9179		
153.	angle	75	73	76	38.0000	109.3170		
154.	angle	72	73	76	38.0000	109.3845		
155.	angle	76	73	76	45.5700	106.3035		
156.	angle	79	82	84	53.2000	109.0812		
157.	angle	79	82	83	42.4400	111.1744		
158.	angle	84	82	83	60.2400	108.2095		
159.	angle	83	82	83	39.5700	108.8985		
160.	angle	82	84	85	60.4300	99.5693		
161.	angle	84	85	86	60.0000	179.0730		
162.	strbnd	78	75	73	18.7000	18.7000		
163.	strbnd	78	75	77	11.5000	18.7000		
164.	strbnd	73	75	77	11.5000	18.7000		
165.	strbnd	73	72	74	11.5000	11.5000		
100.	3 CT 011U	, ,	, _	, 4	11.5000	11.7000		

```
166.
           strbnd
                        78
                             79
                                  82
                                        18.7000
                                                    18.7000
167.
                        78
                             79
                                         11.5000
                                                    18.7000
           strbnd
                                   81
168.
                        82
                             79
                                  81
                                        11.5000
                                                    18.7000
           strbnd
169.
           strbnd
                        75
                             78
                                   79
                                         18.7000
                                                    18.7000
170.
                        75
                             78
                                        11.5000
                                                    18.7000
           strbnd
                                  80
                        79
                                         11.5000
                                                    18.7000
171.
           strbnd
                             78
                                   80
172.
                        75
                             73
                                  72
                                        18.7000
                                                    18.7000
           strbnd
173.
           strbnd
                        75
                             73
                                   76
                                         11.5000
                                                    18.7000
174.
           strbnd
                        72
                             73
                                  76
                                        11.5000
                                                    18.7000
175.
           strbnd
                        79
                             82
                                   84
                                         18.7000
                                                    18.7000
176.
                        79
                             82
                                  83
                                        11.5000
                                                    11.5000
           strbnd
177.
           strbnd
                        84
                             82
                                   83
                                         11.5000
                                                    11.5000
178.
           strbnd
                        82
                             84
                                  85
                                        -5.7500
                                                    -5.7500
                        73
                                        79
                                                0.576 0.0 1
179.
           torsion
                             75
                                   78
  0.017 180.0 2
                    2.031 0.0 3
           torsion
                        73
                             75
                                  78
                                                0.000 0.0 1
                                                              0.000 180.0 2
                                                                               0.000
180.
                                        80
  0.0 3
                        77
                             75
                                   78
                                        79
                                                0.000 0.0 1
                                                              0.000 180.0 2
                                                                               0.000
181.
           torsion
  0.0 3
182.
           torsion
                        77
                             75
                                   78
                                        80
                                                0.000 0.0 1
                                                              0.000 180.0 2
                                                                               0.000
  0.0 3
183.
           torsion
                        78
                             75
                                   73
                                        72
                                                0.484 0.0 1
                                                              0.014 180.0 2
                                                                               2.221
  0.0 3
184.
                        78
                             75
                                   73
                                        76
                                                0.000 0.0 1
                                                              0.000 180.0 2
                                                                               0.000
           torsion
  0.0 3
185.
           torsion
                        77
                             75
                                   73
                                        72
                                                0.000 0.0 1
                                                              0.000 180.0 2
                                                                               0.000
   0.0 3
186.
           torsion
                        77
                             75
                                   73
                                        76
                                                0.000 0.0 1
                                                              0.000 180.0 2
                                                                               0.000
  0.0 3
187.
           torsion
                        74
                             72
                                   73
                                        75
                                               0.0000 0.0 1 0.0000 180.0 2 0.3410
  0.0 3
188.
           torsion
                        74
                             72
                                  73
                                        76
                                               0.0000 0.0 1 0.0000 180.0 2 0.2990
  0.0 3
                             79
                                        75
                                                0.364 0.0 1 -
189.
           torsion
                        82
                                   78
  0.024 180.0 2
                    1.958 0.0 3
190.
           torsion
                        82
                             79
                                   78
                                        80
                                                0.000 0.0 1 0.000 180.0 2
                                                                               0.000
  0.0 3
191.
           torsion
                        81
                             79
                                   78
                                        75
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  0.0 3
192.
           torsion
                        81
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                                                0.000 0.0 1
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  0.0 3
193.
           torsion
                        78
                             79
                                   82
                                        84
  0.688 0.0 1 0.489 180.0 2
                                  1.957 0.0 3
194.
           torsion
                        78
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195.
           torsion
                        81
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196.
           torsion
                        81
                                  82
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  0.0 3
                        79
                             82
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197.
           torsion
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   2.643 0.0 1 0.709 180.0 2
                                  1.072 0.0 3
198.
           torsion
                        83
                             82
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                                                0.000 0.0 1
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  0.0 3
199.
                        82
                                               0.0000 0.0 1 0.0000 180.0 2 0.5000
           torsion
                             84
                                  85
                                        86
   0.0 3
```

Code and Parameters 2-4: Hexyl Thiocyanate AMOEBA Parameters

2.5 SMALL MOLECULE SIMULATIONS IN AMOEBA

Chapter 3 Electrostatic Field Methods

- 3.1 AMBER03 WITH EXPLICIT TIP3P WATER
 - 3.1.1 Reaction Field Electrostatics
 - 3.1.2 Hybrid Solvent Reaction Field Electrostatics and Solute Coulomb Field

3.2 AMBER03 WITH POISSON-BOLTZMANN CONTINUUM SOLVENT

3.2.1 Reaction Field Method

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3.2.2 Grid spacing and size

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3.2.3 Box Location

3.3 AMBER03 WITH POISSON-BOLTZMANN CONTINUUM SOLVENT AND SELECT EXPLICIT TIP3P WATER MOLECULES

3.3.15 Å Water Sphere Around the Vibrational Chromophore

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3.3.2 Single Water Molecule Nearest the Vibrational Chromophore

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3.3.3 Water Molecular Hydrogen Bonding to the Vibrational Chromophore

3.4 AMOEBA

3.4.1 Poisson-Boltzmann Continuum Solvent

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3.4.2 Explicit AMOEBA Water

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3.4.3 Charge Penetration Field Corrections

Chapter 4 The Role of Electrostatics in Differential Binding of RalGDS to Rap Mutations E30D and K31E Investigated by Vibrational Spectroscopy of Thiocyanate Probes

4.1 Introduction

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4.2 RESULTS

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4.3 DISCUSSION

Chapter 5 Optimizing Electrostatic Field Calculations with the Adaptive Poisson-Boltzmann Solver to Predict Electric Fields at Protein-Protein Interfaces I: Sampling and Focusing

5.1 Introduction

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5.2 RESULTS

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5.3 DISCUSSION

Chapter 6 Optimizing Electrostatic Field Calculations with the Adaptive Poisson-Boltzmann Solver to Predict Electric Fields at Protein-Protein Interfaces II: Explicit Near-Probe and Hydrogen Bonding Water Molecules

6.1 Introduction

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6.2 RESULTS

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6.3 DISCUSSION

Chapter 7 Electrostatic Fields at Protein-Protein Interfaces: Increased Sampling Time and Various Electrostatic Methods: A Case for Simulating in Polarizable Force Fields

7.1 Introduction

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7.2 RESULTS

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7.3 DISCUSSION

Chapter 8 Electrostatic Fields in Small Thiocyanate Molecules with Ensembles Generated using the AMOEBA Force Field

8.1 Introduction

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8.2 RESULTS

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8.3 DISCUSSION

Appendix

Glossary

This page is optional—must be placed in this order if it is included in the dissertation. If you don't want to include a glossary, then delete the entire page and the following page break.

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