

## ■ Gaussian MSK

- MSK has three important properties
  - Constant envelope (why?)
  - Relatively narrow bandwidth
  - Coherent detection performance equivalent to that of QPSK
- However, the PSD of the MSK only drops by  $10\log_{10}9 = 9.54$  dB below its midband value at  $fT_b = 0.5$ 
  - The adjacent channel interference is not low enough
- We may modify the PSD with the use of a pre-modulation low-pass filter, hereafter referred to as a pulse shaping filter
  - Frequency response with a narrow bandwidth and sharp cutoff
  - Impulse response with a relatively low overshoot
  - Phase values equal to 0 or  $\pi$  at  $2nT_b$ , or to  $\pm\pi/2$  at  $(2n+1)T_b$

- These desirable features can be achieved by passing a NRZ data stream through a filter defined by a Gaussian function
- Gaussian-filtered MSK (GMSK)

- Let  $W$  be the 3 dB baseband BW of the pulse shaping filter

$$H(f) = \exp\left(-\frac{\log 2}{2} \left(\frac{f}{W}\right)^2\right)$$

- The time domain impulse response of this Gaussian filter is

$$h(t) = \sqrt{\frac{2\pi}{\log 2}} W \exp\left(-\frac{2\pi^2}{\log 2} W^2 t^2\right)$$

- The response of  $h(t)$  to a rectangular pulse of  $U(\frac{-T_b}{2}) - U(\frac{T_b}{2})$  is

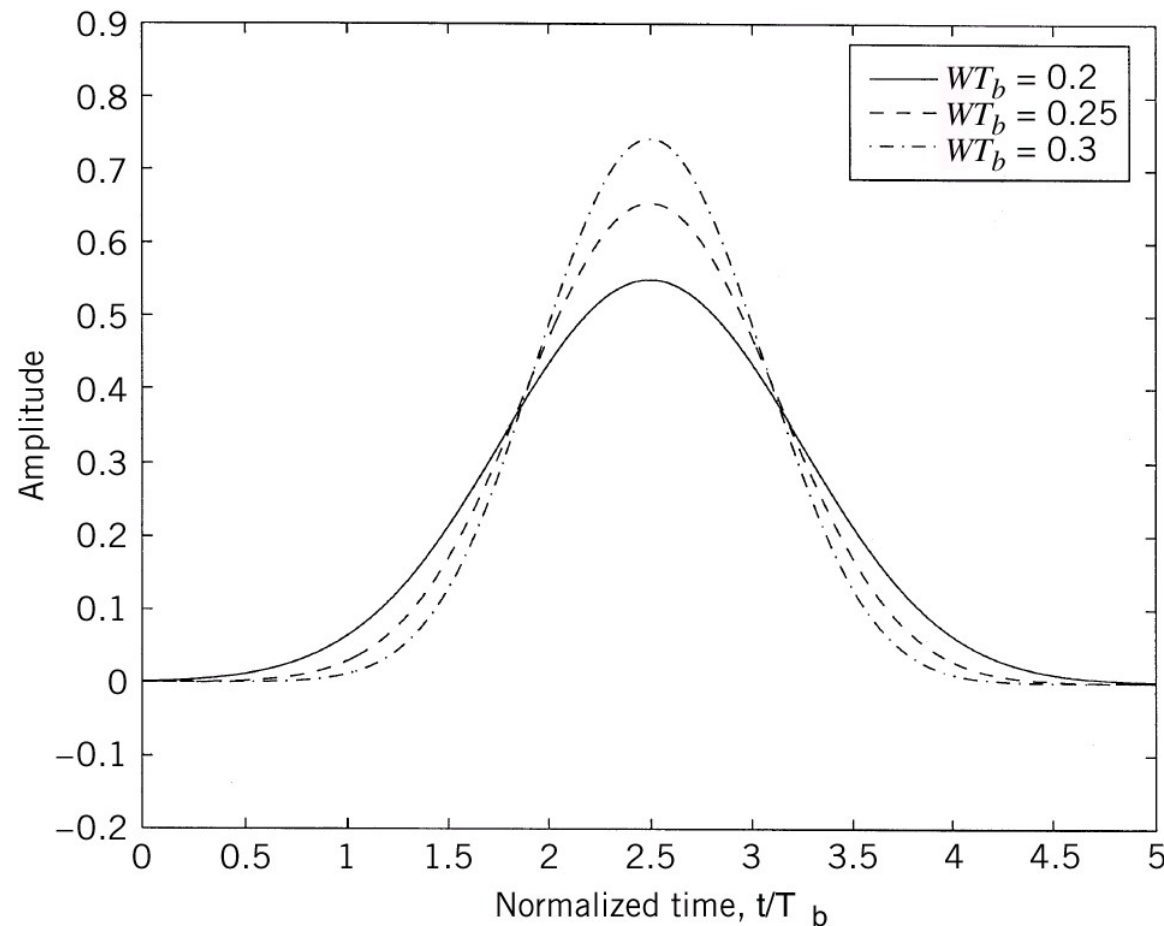
$$g(t) = \sqrt{\frac{2\pi}{\log 2}} W \int_{-T_b/2}^{T_b/2} \exp\left(-\frac{2\pi^2}{\log 2} W^2 (t - \tau)^2\right) d\tau$$

- The impulse response to  $U(-T_b/2) - U(T_b/2)$  can be expressed as

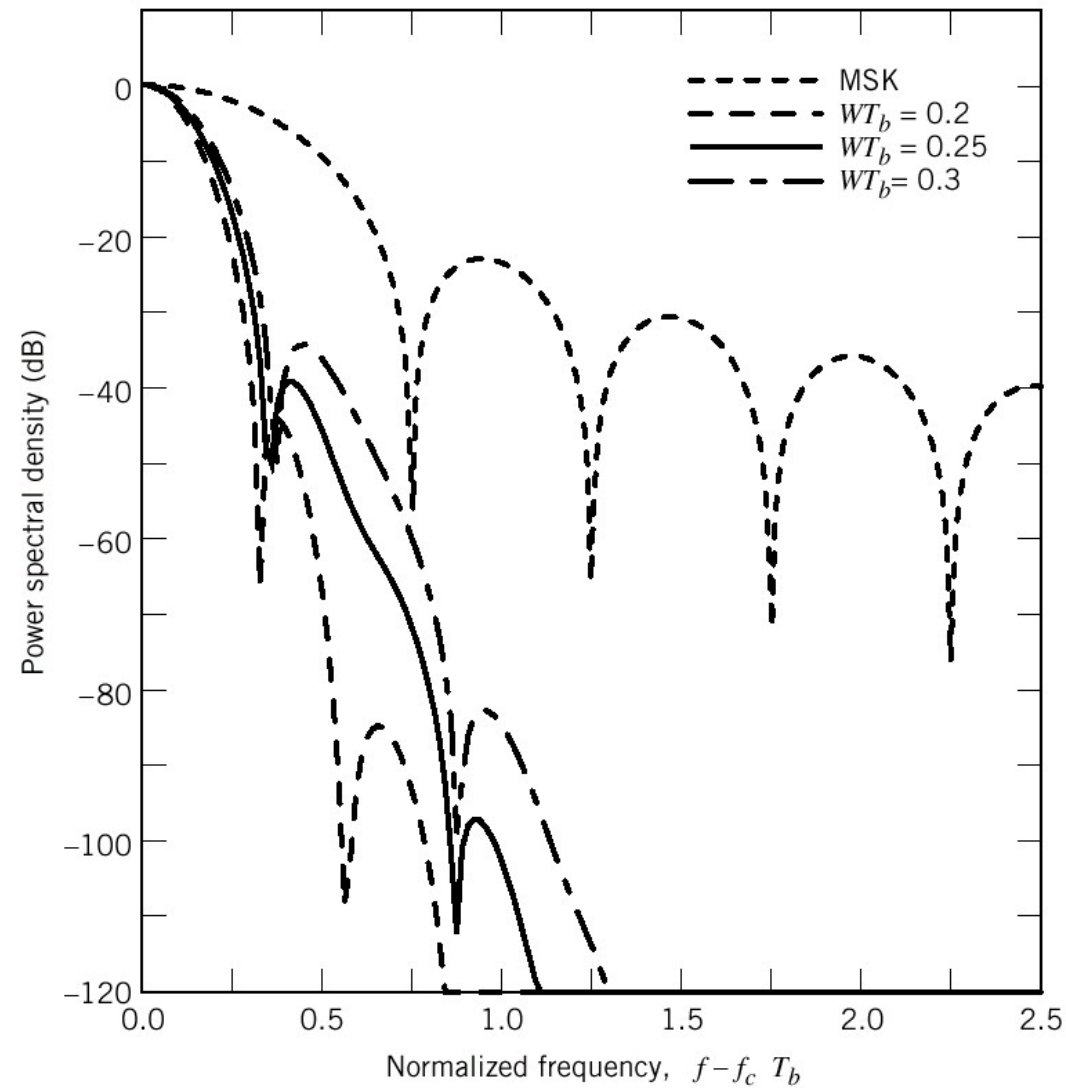
$$g(t) = \frac{1}{2} \left[ \operatorname{erfc} \left( \pi \sqrt{\frac{2}{\log 2}} W T_b \left( \frac{t}{T_b} - \frac{1}{2} \right) \right) - \operatorname{erfc} \left( \pi \sqrt{\frac{2}{\log 2}} W T_b \left( \frac{t}{T_b} + \frac{1}{2} \right) \right) \right]$$

- This pulse shaping function  $g(t)$  is non-causal in that it is nonzero for  $t < -T_b/2$
- For a causal response,  $g(t)$  must be truncated and shifted in time
- The time-bandwidth product  $W T_b$  is a design parameter
- The case of  $W T_b = \infty$  corresponds to the ordinary MSK
- When  $W T_b < 1$ , increasingly more of the transmit power is concentrated inside the passband of the GMSK signal
- An undesirable feature of GMSK is that the modulated signal of NRZ binary data is no longer confined to a single bit interval as in the ordinary MSK, causing inter-symbol interference (ISI)

- The truncated pulse shaping function  $g(t)$  which is shifted in time by  $2.5 T_b$ , and truncated at  $t = \pm 2.5T_b$



□ The PSD of GMSK

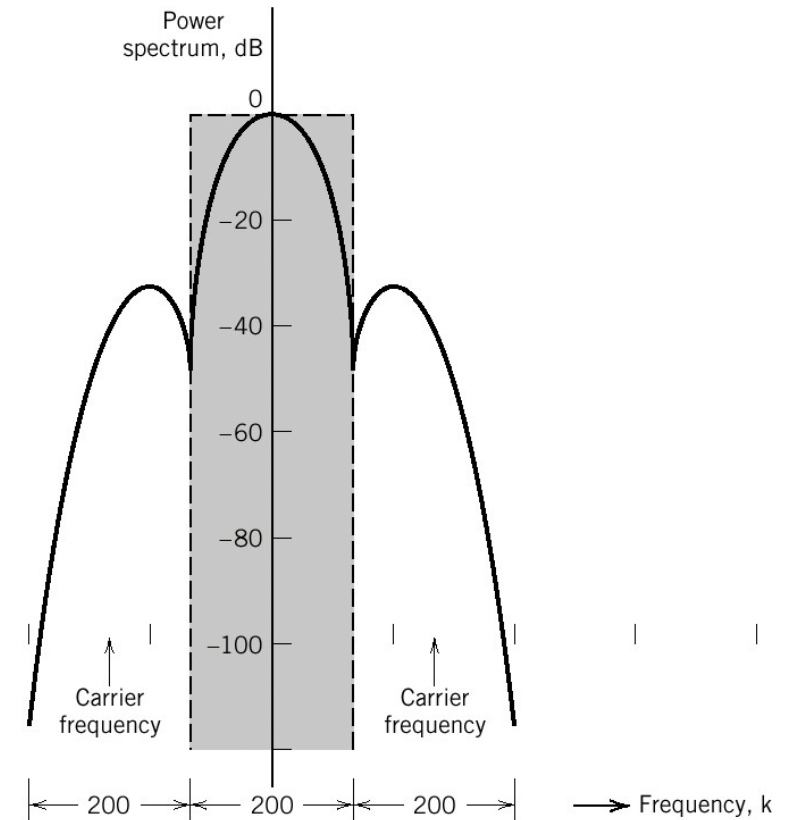
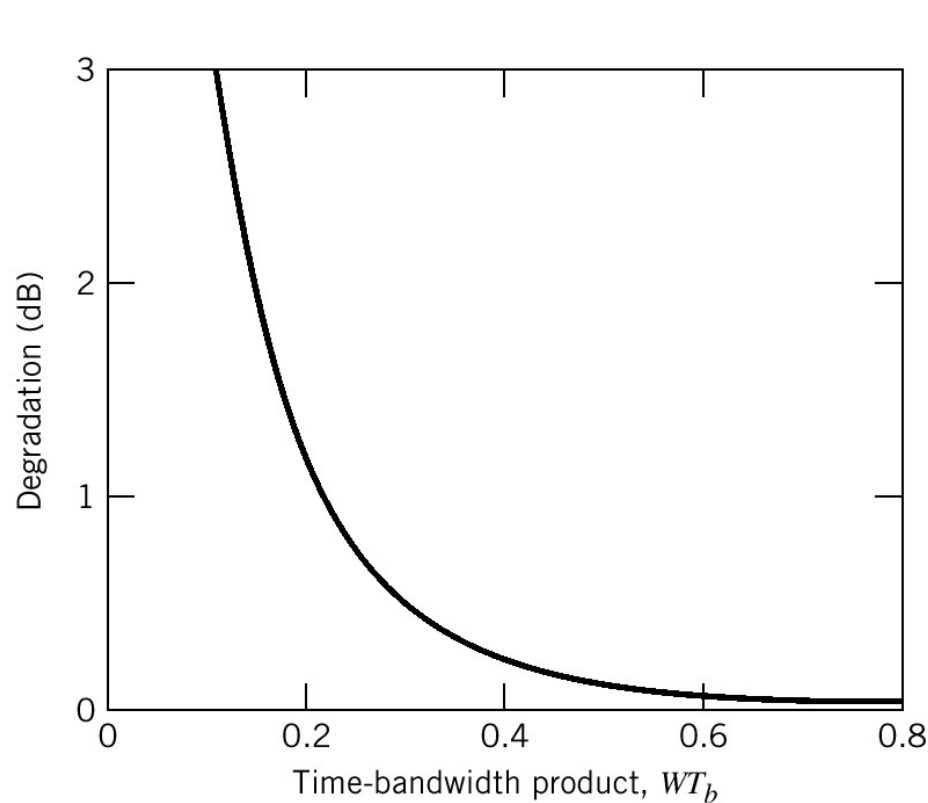


- Therefore, the choice of  $WT_b$  offers a tradeoff between spectral compactness and performance loss
- The BER is hard to derive. Let us express it in terms of the BER of MSK, given by

$$P_e = \frac{1}{2} \operatorname{erfc} \left( \sqrt{\frac{\alpha E_b}{2N_0}} \right)$$

- Comparing to the BER of MSK, GMSK has a performance degradation of  $10\log_{10}(\alpha/2)$  dB in SNR
- The value of  $\alpha$  depends on  $WT_b$
- For MSK, we have  $WT_b = \infty$ , corresponding to  $\alpha = 2$
- For GSM, we have  $WT_b = 0.3$ , resulting in an SNR degradation of 0.46 dB, corresponding to  $\alpha/2 = 0.9$

- The performance degradation  $10\log_{10}(\alpha/2)$  v.s.  $WT_b$



- For GSM, data rate is 271kb/s, with BW=200kHz for each channel
- 99% of the power is confined to a BW of 250kHz with  $WT_b = 0.3$

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- M-ary FSK

- We have  $s_i(t) = \begin{cases} \sqrt{\frac{2E}{T}} \cos\left(\frac{\pi}{T}(n_c + i)t\right), & 0 \leq t \leq T \\ 0, & \text{elsewhere} \end{cases}$

where  $i = 1, 2, \dots, M$ , and  $f_c = n_c / 2T$

- Since the individual frequencies are separated by  $1/2T$  Hz, we have

$$\int_0^T s_i(t)s_j(t)dt = 0, \quad i \neq j$$

- We thus may use the transmitted signals  $s_i(t)$  themselves as a complete orthonormal set of basis functions, as shown by

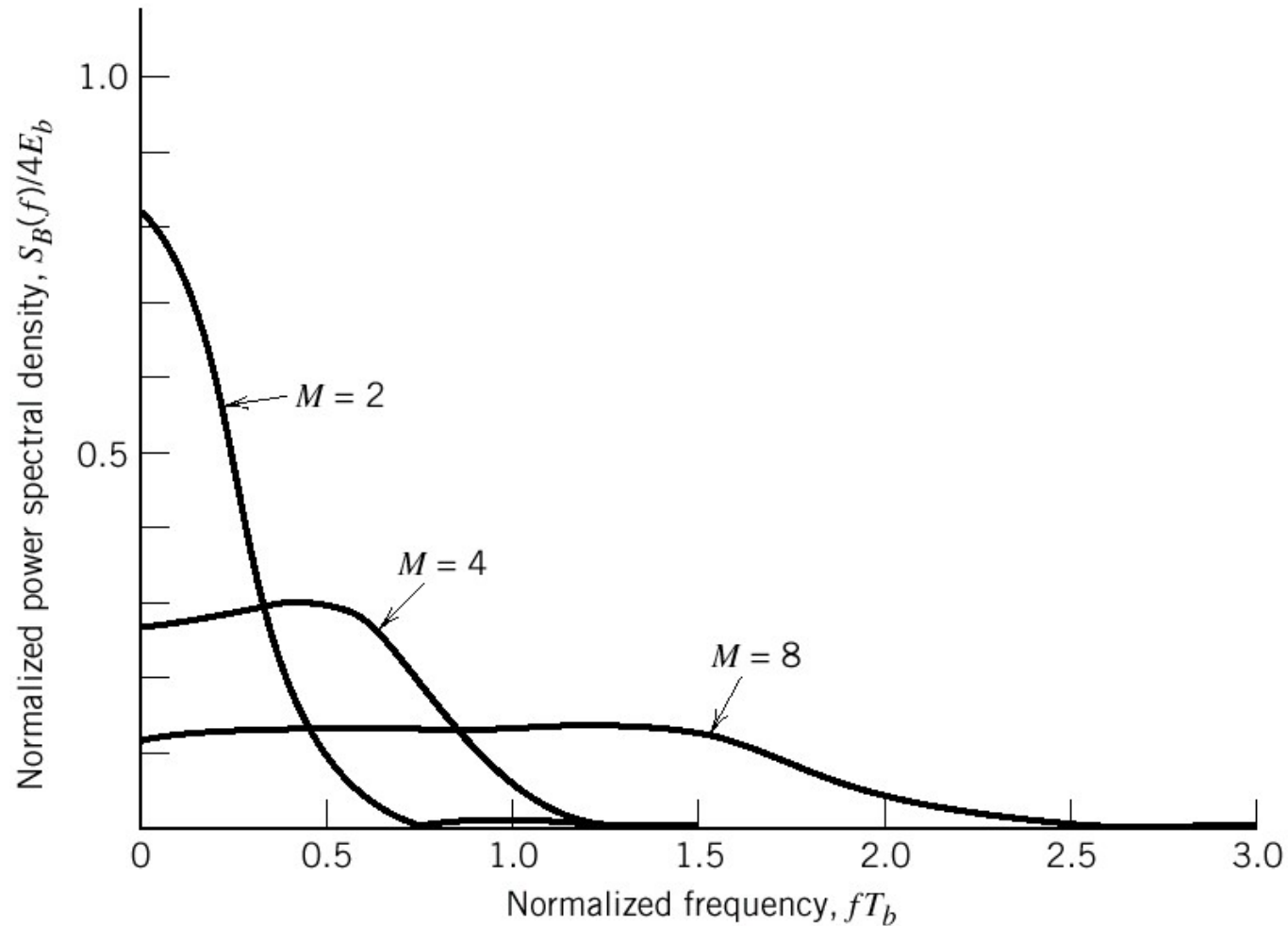
$$\phi_i(t) = \frac{1}{\sqrt{E}} s_i(t), \quad 0 \leq t \leq T, i = 1, 2, \dots, M$$

- The optimum receiver consists of a bank of  $M$  matched filters



- ❑ The receiver makes decisions based on the largest matched filter output in accordance with the ML decision rule
- ❑ The exact BER is difficult to derive, while can be bounded from above by  $P_e \leq \frac{1}{2}(M - 1)\text{erfc}\left(\sqrt{\frac{E}{2N_0}}\right)$   
since the minimum distance in M-ary FSK is  $\sqrt{2E}$
- ❑ For  $M = 2$ , i.e. BFSK, the bound becomes an equality
- The PSD of M-ary FSK depends on the frequency assigned to each value of  $M$ 
  - ❑ When the spacing is uniform with a deviation  $k = 0.5$ , that is when frequencies are separated from each other by  $1/2T$  Hz, the PSD is plotted in the next page

- The PSD of M-ary FSK, for  $k = 0.5$



- The bandwidth efficiency of M-ary FSK
  - The adjacent frequencies need only be separated from each other by  $1/2T$  to maintain orthogonality
  - We, thus, define the channel bandwidth required to transmit M-ary FSK as  $B = M / 2T$
  - Recall that  $T$  is equal to  $T_b \log_2 M$
  - Let  $R_b = \frac{1}{T_b}$ , then  $B = \frac{R_b M}{2 \log_2 M}$
  - The bandwidth efficiency of an M-ary signal is thus given by

$$\rho = \frac{R_b}{B} = \frac{2 \log_2 M}{M}$$

- Increasing the number of M tends to decrease the bandwidth efficiency of M-ary FSK

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## ■ Lab 4

- ❑ Redo Lab3-2 by changing the RC filter with a RRC filter
- ❑ Generate a series of binary random numbers
- ❑ Modulate the binary numbers with MSK, given that the carrier frequency  $f_c$  is 1 MHz, and the symbol energy  $E$  is 10dB and the symbol frequency is 1KHz
- ❑ Demodulate the transmitted signal using the method on p.p. 100
- ❑ Draw and compare the BERs with the theoretical values
- ❑ Redo the above procedure with GMSK when  $WT_b = 0.3$ 
  - Using the pulse shaping filter on pp. 113
  - Draw the phase trellis of GMSK and compare it with that of MSK

- HW2 (due on 4/21)
  - For FSK: 6.20, 6.21, 6.22, 6.23, 6.26, and 6.28