

RELATIVE STABILITY

- ① For the following second order characteristic equation

$$s^2 + 2\zeta\omega_n s + \omega_n^2 = 0 \quad 0 < \zeta < 1$$

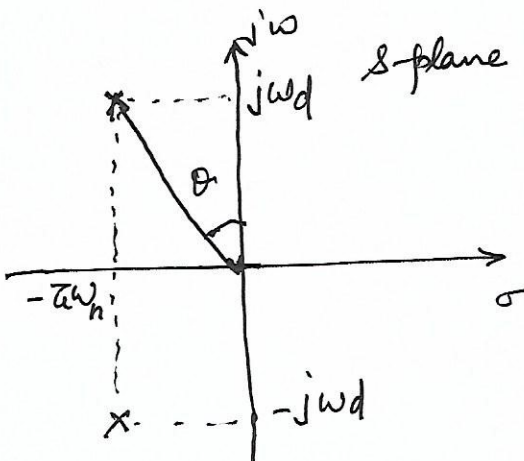
the roots are $-\zeta\omega_n \pm j\omega_n\sqrt{1-\zeta^2}$

② $\sin\theta = \frac{\zeta\omega_n}{\sqrt{(\zeta\omega_n)^2 + \omega_d^2}}$

$\sin^2\theta = \frac{\zeta^2\omega_n^2}{\zeta^2\omega_n^2 + \omega_n^2 - \zeta^2\omega_n^2}$

$\sin^2\theta = \zeta^2$

$\sin\theta = \zeta$



- ③ The angle θ is indicative of the damping ratio ζ .
- ④ As θ becomes smaller so does the value of ζ
- ⑤ Thus if the value of ζ reduces the system tends to become oscillatory and unstable.
- ⑥ In other words if the closed loop poles are located near the $j\omega$ axis the system becomes less stable.
- ⑦ The Nyquist plot can be used as a measure of relative stability of closed loop systems which are open loop stable.

② The stability information for such systems become obvious by inspection of the polar plot of the open loop function $G(s)H(s)$, since this stability criterion is merely the non-encirclement of $(-1, j0)$ point.

ⓧ Consider two different systems whose closed-loop poles are shown in the s -plane (Fig ①)

ⓧ Obviously system A is "more stable" than system B since its dominant closed-loop poles are located comparatively away to the left from the $j\omega$ axis.

ⓧ The open loop frequency response plots for the systems A and B are shown in Fig ②

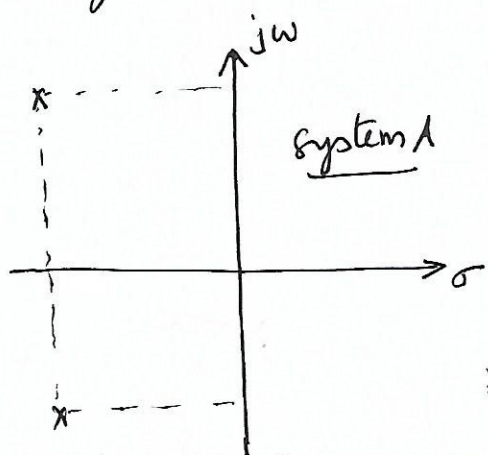


Fig ①

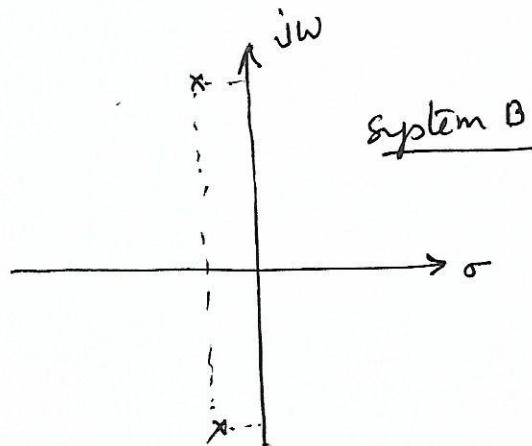


Fig ②

(3)

④ The comparison of the closed loop pole locations of these two systems with their corresponding polar plot reveals that a polar plot moves closer to $(-1, j0)$ point the system behaves relatively less stable and ~~vice~~ vice versa.

MEASUREMENT OF RELATIVE STABILITY

①

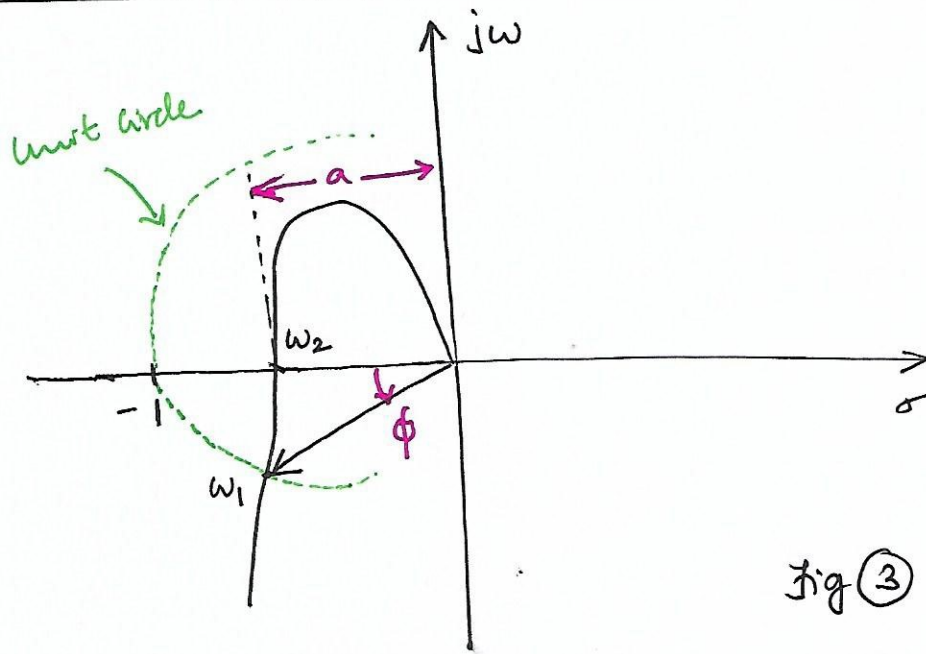


Fig (3)

- ① Above Fig shows a typical $G(j\omega)H(j\omega)$ plot which crosses the negative real axis at a frequency $\omega = \omega_2$ with an intercept of 'a'.
- ② Let a unit circle centred at the origin intersect the $G(j\omega)H(j\omega)$ plot at a frequency $\omega = \omega_1$ and let the phasor $G(j\omega_1)H(j\omega_1)$ make an angle ' ϕ ' with the negative real axis, measured positively in counterclockwise direction.
- ③ As $G(j\omega)H(j\omega)$ locus approaches $(-1, j0)$ point, the relative stability reduces. Simultaneously the value of 'a' approaches unity and that of ϕ tends to zero.
- ④ The relative stability could thus be measured in terms of intercept a and/or the angle ϕ .

GAIN MARGIN

①

- ② It is the factor by which the system gain can be increased to drive it to the verge of instability.
- ③ In Fig (3) it is seen that at $\omega = \omega_2$ the phase angle $\angle G(j\omega)H(j\omega)$ is 180° and $|G(j\omega)H(j\omega)| = a$.
- ④ If the gain of the system is increased by a factor $\frac{1}{a}$ then $|G(j\omega)H(j\omega)|_{\omega=\omega_2}$ becomes $a \times \frac{1}{a} = 1$ and hence the $G(j\omega)H(j\omega)$ plot will pass through $(-1, j0)$ point, driving the system to the verge of instability.
- ⑤ Thus GAIN MARGIN (GM) may be defined as the reciprocal of the gain at the frequency at which the phase angle becomes 180° .
- ⑥ The frequency at which the phase angle is 180° is called the phase cross-over frequency.
- ⑦ $GM = \frac{1}{a}$. In decibels the $GM = 20 \log \frac{1}{a}$
 $GM = -20 \log a \text{ dB}$
- ⑧ Since 'a' is less than 1 for a stable system, GM is positive