

#6 PW 2.32: 4 MVAR minimizes the real power line losses to .336 MW; 4.5 MVAR minimizes the apparent power flow into the feeder to 8.34 MVA.

PW 2.33: See graph attached

PW 2.34: @  $Q_{cap} = 5.0$  MVAR, the load is 10 MW/5 MVAR. we have the least feeder losses at .525 MW & 1.050 MVAR.

@  $Q_{cap} = 5.5$  MVAR, the load is 20 MW/10 MVAR & 7.206 MW is the lowest feeder losses. & 4.413 MVAR, since these are the lowest feeder losses then they must produce the lowest average feeder losses.

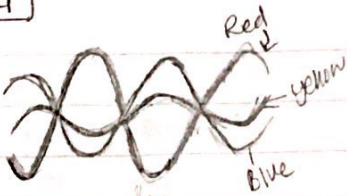
$Q_{cap}$  should be set between 5-5.5 MVAR.

\* I worked with Matt Flynn.

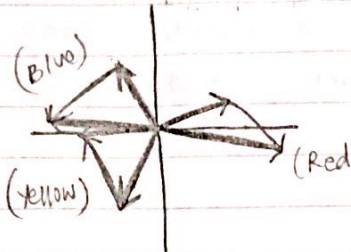
## HW 4

#1

a)



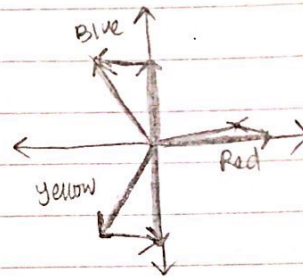
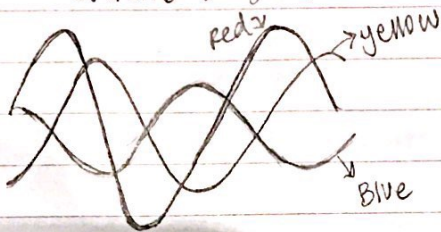
The red component has the highest amplitude, then blue followed by yellow.



The Blue & yellow vectors are in phase with each other.

b)

Current Diagram:



The Blue & yellow currents are out of phase with each other by 180 degrees

c) If I move the relative angle to the right, The magnitude of the red phasor decreases while the magnitude of the yellow & blue components increase.

#2

a) Real power: 137 W

Apparent power: 137 VA

$$b) THD_I = \frac{\sqrt{\sum_{k=2}^{\infty} I_{krms}^2}}{I_{irms}} \times 100 = \frac{\sqrt{(.5A)^2}}{1A} \cdot 100\% = 50\%$$

$$V_{rms} = V_{irms} \sqrt{1 + (THD_V/100)^2} = 276 V$$

$$I_{rms} = (1A) \sqrt{1 + (50/100)^2} = 1.12 A$$

$$P_{avg} = \sum_{k=1}^{\infty} V_{krms} I_{krms} \cos(\phi_k - \theta_k) = (276V)(.5A) \cos(0) + 0 + (0V)(.5A) \cos(0-0)$$

$$P_{avg} = 138 W$$

$$P_{true} = \frac{P_{avg}}{V_{rms} I_{rms}} \left( \frac{1}{\sqrt{1 + (THD_I/100)^2}} \right) = \frac{138 W}{(276V)(1.12A)} \cdot \frac{1}{\sqrt{1 + (50/100)^2}} = .89$$

$$P = (276V)(.5A)(.89) = 122.01 \text{ W}$$

$$S = (276V)(.5A) = 138 \text{ VA}$$

- c) The third harmonic of the current is the only contributor to THD.  
The true p.f. is affected by the harmonics & power transferred to the load.

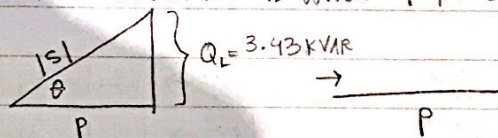


- 3 a) The customer & the neighbors will be concerned because non-linear loads do not present a constant impedance. A non-constant impedance will distort current waveform, causing current harmonics which in turn cause voltage harmonics.
- b) If the source impedance is resistive, there will be less harmonics. If it's inductive the harmonics will be larger.

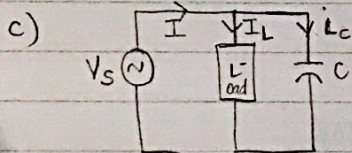
#4 a)  $|S| = (20A)(240V) = 4,800 \text{ VA}$

$$\cos \theta = \frac{3.36 \text{ kW}}{4800 \text{ VA}} = .7 \text{ lagging}$$

b) KVAR should be  $-Q_L$  when p.f. = 1 since  $\sin(\cos^{-1}(1)) = 0$ .



After adding  $Q_C$ ,  $Q_L$  reduces completely.  $Q_{cap} = Q_L = 3.43 \text{ KVAR}$



$$I_L = \frac{P}{V_{RMS} \cos \theta} = \frac{3.36 \text{ kW}}{(240 \text{ V})(1)} = 14 \text{ amps}$$

$$I_C = I - I_L = 20 \text{ A} - 14 \text{ A} = 6 \text{ A}$$

- d) 20 Amps
- e) The capacitor only adds reactance / reduces the reactance of the load. It doesn't change total current.  
Diagram  $\rightarrow$  from part b, we don't have an angle anymore because the power factor is 1. From the triangle, to a flat line as in b.
- f) The best KVAR rating would have been 3.43 KVAR



#5 Power Transfer

a)  $Z = jX$

$$I_{12} = \frac{V_1 - V_2}{Z}$$

$$S_1 = I_{12}^* V_1$$

$$S_2 = I_{12}^* V_2$$

$$P_1 = |S_1| \cos(\theta)$$

$$P_2 = |S_2| \cos(\theta)$$

$$Q_1 = |S_1| \sin(\theta)$$

$$Q_2 = |S_2| \sin(\theta)$$

$$P_{12} = P_1 + P_2$$

$$Q_{12} = Q_1 + Q_2$$

b) For maximum power transfer to occur, one of sources must generate x amount of real power and the other source must consume x amount of real power.

$$c) \quad V_1 = 10 \angle 30^\circ \quad I_{12} = \frac{10 \angle 30^\circ - 10 \angle 0^\circ}{1 \angle 90^\circ} = \frac{8.66 + j5 - (10)}{1 \angle 90^\circ} = \frac{-1.34 + j5}{1 \angle 90^\circ} = \frac{5.176 \angle -75^\circ}{1 \angle 90^\circ}$$

$$V_2 = 10 \angle 0^\circ$$

$$X = 1 \Omega$$

$$I_{12} = 5.176 \angle -165^\circ$$

$$S_1 = [5.176 \angle 165^\circ] [10 \angle 30^\circ] = 51.76 \angle 195^\circ \rightarrow |S_1| = 51.76$$

$$S_2 = [5.176 \angle 165^\circ] [10 \angle 0^\circ] = 51.76 \angle 165^\circ \rightarrow |S_2| = 51.76$$

$$P_1 = (51.76) \cos(195^\circ) = -50 \text{ W}$$

$$P_2 = (51.76) \cos(165^\circ) = -50 \text{ W}$$

$$Q_1 = (51.76) \sin(195^\circ) = -13.39 \text{ VAR}$$

$$Q_2 = (51.76) \sin(165^\circ) = 13.39 \text{ VAR}$$

Yes it all adds up. Machine 1 generates 50 W & supplies reactive power of 13.39 VAR. Machine 2 consumes energy at the rate of 50 W and supplies reactive power of 13.39 VAR. Supplied reactive power is 26.78 VAR which is required by the inductive reactance of  $1 \Omega$ . Since the impedance is purely reactive, no real power is consumed by the impedance, and all the watts generated by machine 1 are transferred to machine 2.



d)  $\delta_1 = 45^\circ$   $V_1 = 10 \angle 45^\circ$   
 $V_2 = 10 \angle 0^\circ$

$$I_{12} = \frac{10 \angle 45^\circ - 10 \angle 0^\circ}{1 \angle 90^\circ} = \frac{10 \cos(45) + j10 \sin(45) - 10}{1 \angle 90^\circ}$$

$$I_{12} = 7.07 + j7.07 - 10 = \frac{-2.92 + j7.07}{1 \angle 90^\circ} = \frac{7.65 \angle -67.55^\circ}{1 \angle 90^\circ}$$

The current's magnitude increases,

while the angle decreases. Machine

1 generates 70.65 watts. while

Machine 2 consumes 70.70 watts.

Machine 1 supplies +29.33 VARs

& Machine 2 supplies 29.21 VARs.

The powers (reactive & real) do not

completely cancel out.

$$I_{12} = 7.65 \angle -157.55^\circ$$

$$S_1 = (7.65 \angle 157.55^\circ)(10 \angle 45^\circ) = 76.5 \angle 202.55^\circ$$

$$S_2 = (7.65 \angle 157.55^\circ)(10 \angle 0^\circ) = 76.5 \angle 157.55^\circ$$

$$P_1 = 76.5 \cos(202.55^\circ) = -70.65 \text{ W}$$

$$P_2 = 76.5 \cos(157.55^\circ) = -70.70 \text{ W}$$

$$Q_1 = 76.5 \sin(202.55^\circ) = -29.33 \text{ VAR}$$

$$Q_2 = 76.5 \sin(157.55^\circ) = 29.21 \text{ VAR}$$

e)  $V_1 = 8.36 \angle 30^\circ$   $V_2 = 4.18 \angle 0^\circ$

$$I_{12} = \frac{8.36 \angle 30^\circ - 4.18 \angle 0^\circ}{1 \angle 90^\circ} = \frac{7.24 + j4.18 - 4.18}{1 \angle 90^\circ}$$

Everything changes except for the reactance.

$$I_{12} = \frac{3.06 + j4.18}{1 \angle 90^\circ} = \frac{5.18 \angle 53.79^\circ}{1 \angle 90^\circ} = 5.18 \angle 36.94^\circ$$

$$S_1 = (5.18 \angle 88.94^\circ)(8.36 \angle 30^\circ) = 43.3 \angle 118.94^\circ$$

$$S_2 = (5.18 \angle 88.94^\circ)(4.18 \angle 0^\circ) = 21.65 \angle 88.94^\circ$$

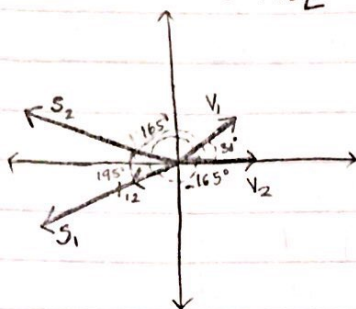
$$P_1 = 43.3 \cos(118.94^\circ) = -20.95 \text{ W}$$

$$P_2 = 21.65 \cos(88.94^\circ) = .4 \text{ W}$$

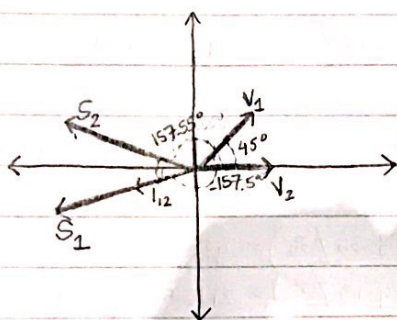
$$Q_1 = 43.3 \sin(118.94^\circ) = 37.89 \text{ VAR}$$

$$Q_2 = 21.65 \sin(88.94^\circ) = 21.65 \text{ VAR}$$

f) Part c:  $V_1 = 10 \angle 30^\circ$   $V_2 = 10 \angle 0^\circ$   $I_{12} = 5.176 \angle -165^\circ$   
 $S_1 = 51.76 \angle 195^\circ$   $S_2 = 51.76 \angle 165^\circ$



Part d:  $V_1 = 10 \angle 45^\circ$   $V_2 = 10 \angle 0^\circ$   $I_{12} = 7.65 \angle -157.55^\circ$   
 $S_1 = 76.5 \angle 202.55^\circ$   $S_2 = 76.5 \angle 157.55^\circ$



Part e:  $V_1 = 8.36 \angle 30^\circ$   $V_2 = 4.18 \angle 0^\circ$   $I_L = 5.18 \angle 88.94^\circ$   
 $S_1 = 43.3 \angle 118.94^\circ$   $S_2 = 21.65 \angle 88.94^\circ$

