1 Transfer Function

When we write the transfer function of an arbitrary circuit, it always takes the following form. This is called a "rational transfer function." We also like to factor the numerator and denominator, so that they become easier to work with and plot:

$$H(\boldsymbol{\omega}) = \frac{z(\boldsymbol{\omega})}{p(\boldsymbol{\omega})} = \frac{(j\boldsymbol{\omega})^{N_{z0}}}{(j\boldsymbol{\omega})^{N_{p0}}} \left(\frac{(j\boldsymbol{\omega})^{n}\boldsymbol{\alpha}_{n} + (j\boldsymbol{\omega})^{n-1}\boldsymbol{\alpha}_{n-1} + \dots + j\boldsymbol{\omega}\boldsymbol{\alpha}_{1} + \boldsymbol{\alpha}_{0}}{(j\boldsymbol{\omega})^{m}\boldsymbol{\beta}_{m} + (j\boldsymbol{\omega})^{m-1}\boldsymbol{\beta}_{m-1} + \dots + j\boldsymbol{\omega}\boldsymbol{\beta}_{1} + \boldsymbol{\beta}_{0}} \right)$$

$$= K \frac{(j\boldsymbol{\omega})^{N_{z0}} \left(1 + j\frac{\boldsymbol{\omega}}{\boldsymbol{\omega}_{z1}} \right) \left(1 + j\frac{\boldsymbol{\omega}}{\boldsymbol{\omega}_{z2}} \right) \dots \left(1 + j\frac{\boldsymbol{\omega}}{\boldsymbol{\omega}_{yn}} \right)}{(j\boldsymbol{\omega})^{N_{p0}} \left(1 + j\frac{\boldsymbol{\omega}}{\boldsymbol{\omega}_{p1}} \right) \left(1 + j\frac{\boldsymbol{\omega}}{\boldsymbol{\omega}_{p2}} \right) \dots \left(1 + j\frac{\boldsymbol{\omega}}{\boldsymbol{\omega}_{pm}} \right)}$$

Here, we define the constants ω_z as "zeros" and ω_p as "poles", and N_{z0} , N_{p0} are the number of zeros and poles at $\omega = 0$

2 Bode Plots

Bode plots provide us with a simple and easy tool to plot these transfer functions by hand. Always remember that Bode plots are an approximation; if you want the precisely correct plots, you need to use numerical methods (like solving using MATLAB or IPython).

When we make Bode plots, we plot the frequency on a logarithmic scale, the magnitude on a decibel scale, and the angle in either degrees or radians. We use the decibel because it allows us to break up complex transfer functions into its constituent components. We define the decibel as the following:

$$20\log_{10}(|H(\boldsymbol{\omega})|) = |H(\boldsymbol{\omega})| \text{ [dB]}$$

When making the Bode plot (and plotting using a logarithmic unit), we treat each individual pole and zero independently, and then add them back together at the end. We can use the Bode plot rules to help us plot each of the individual poles and zeros.

$$|H(\omega)| = 10\log\frac{P_{out}}{P_{in}} = 10\log\frac{\frac{V_{out}^2}{R}}{\frac{V_{in}^2}{P_{in}}} = 10\log\frac{V_{out}^2}{V_{in}^2} = 20\log\frac{V_{out}}{V_{in}}$$

2.1 Algorithm

Given a frequency response $H(\omega)$,

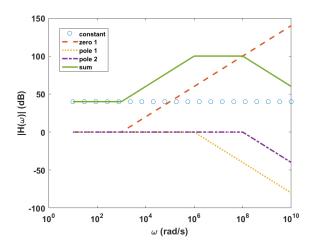
- (a) Break $H(\omega)$ into a product of poles and zeros as in the cheat sheet. Appropriately divide terms to reduce $H(\omega)$ into one of the given forms.
- (b) Draw out the Bode plot for each pole and zero in the product above.
- (c) Add the resulting plots to get the final Bode plot.

2.2 Example

Plot the magnitude and phase of the following transfer function using the Bode approximation and a numerical solver and compare the two.

$$H(\omega) = \frac{100\left(1 + j\frac{\omega}{1000}\right)}{\left(1 + j\frac{\omega}{10^6}\right)\left(1 + j\frac{\omega}{10^8}\right)}$$

We see 1 zero at $10^3 \frac{\text{rad}}{\text{s}}$, 2 poles at $10^6 \frac{\text{rad}}{\text{s}}$ and $10^8 \frac{\text{rad}}{\text{s}}$, and a constant gain of 100. We start with the constant value, and then move from lowest to highest frequency plotting the poles and zeros as we go. Finally, we add together the plots for each of the individual poles and zeros to give us the final Bode plot.



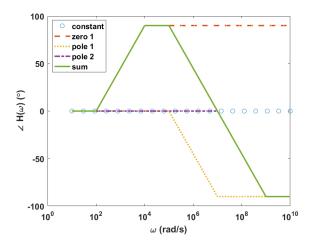


Figure 1: Plotting of the transfer function magnitude using the Bode approximation

Figure 2: Plotting of the transfer function angle using the Bode approximation

Finally, comparing the Bode approximation and the precise value calculated via a computer, we can see the Bode approximation is very similar to the exact answer, except for around the pole and zero frequencies (as expected).

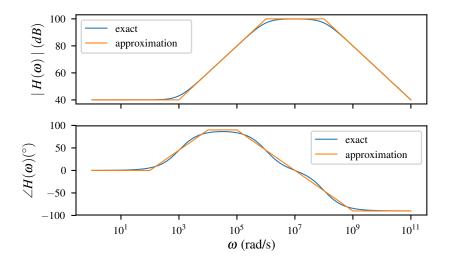
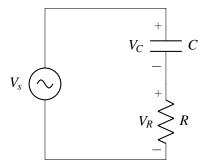


Figure 3: A comparison of Bode vs. exact (numerically computed) answers. Note the agreement between both, except at the pole and zero frequencies.

2.3 Questions

1. Bode Plots of Transfer Functions

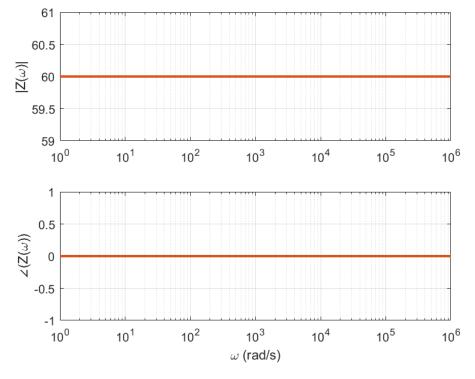
To understand the concept of transfer functions and filters with a concrete example, consider the following simple RC circuit. Let the voltage source V_S be designated as the input phasor, and let V_R and V_C designate the two output voltage phasors. $R = 1 \text{ k}\Omega$ and $C = 1 \mu\text{F}$.



(a) What is the impedance of a $1\,\mathrm{k}\Omega$ resistor? Draw a Bode plot of the impedance of the resistor as a function of frequency. (Don't forget that a Bode plot has both a magnitude plot and a phase plot.)

Answer:

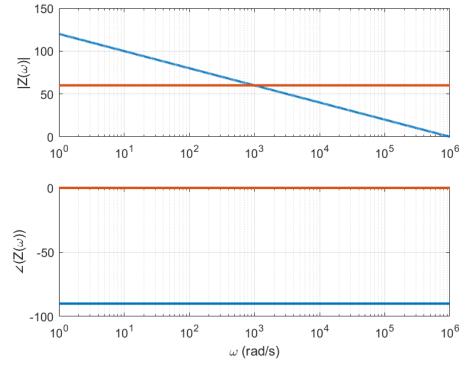
$$Z_R = 1 \mathrm{k}\Omega$$



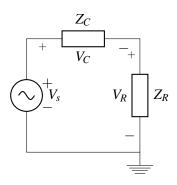
(b) What is the impedance of a 1 μ F capacitor? On the same Bode plot as the last question, sketch the capacitor's impedance as a function of frequency. When is $|Z_C| \gg |Z_R|$ and vice versa? At what ω does $|Z_C| = |Z_R|$? What is this ω called?

Answer:

 $|Z_C|\gg |Z_R|$ approximately when $\omega<\frac{1}{RC}$. $|Z_C|\ll |Z_R|$ approximately when $\omega>\frac{1}{RC}$. This ω is called the corner frequency, or ω_c .



(c) Now lets look at the impedance voltage divider below. What is the transfer function $H(\omega) = \frac{\tilde{V}_C}{\tilde{V}_S}$?



Answer:

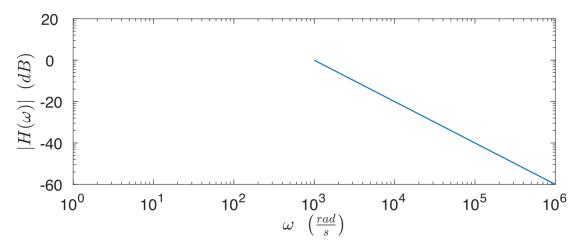
$$H(\omega) = \frac{1}{1 + j\omega RC} = \frac{1}{1 + j\frac{\omega}{10^3}}$$

(d) For the region where $|Z_R| \gg |Z_C|$, what is the approximate function for $|\frac{\tilde{V}_C}{\tilde{V}_S}|$? At what frequencies is our approximation no longer valid? Sketch the approximate function in the appropriate region on a Bode magnitude plot.

Answer:

$$\left| rac{ ilde{V}_C}{ ilde{V}_S}
ight| pprox rac{|Z_C|}{|Z_R|}$$

This is valid for $\omega > \frac{1}{RC}$.

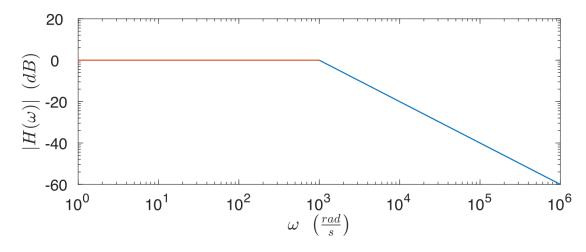


(e) What is the approximate function for $|\frac{\tilde{V_C}}{\tilde{V_S}}|$ when $|Z_C| \gg |Z_R|$? On the same Bode magnitude plot as before, sketch the this approximate function. Where does this function meet your approximation for when $|Z_R| \gg |Z_C|$?

Answer:

$$\left|\frac{\tilde{V}_C}{\tilde{V}_S}\right| \approx 1$$

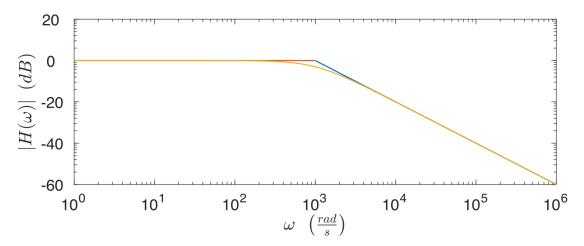
This is approximately valid for $\omega < \frac{1}{RC}$. This meets our other approximation at $\omega = \frac{1}{RC}$.



(f) What is the worst case error for our piecewise approximation? On a log-log plot, does this error appear very large?

Answer:

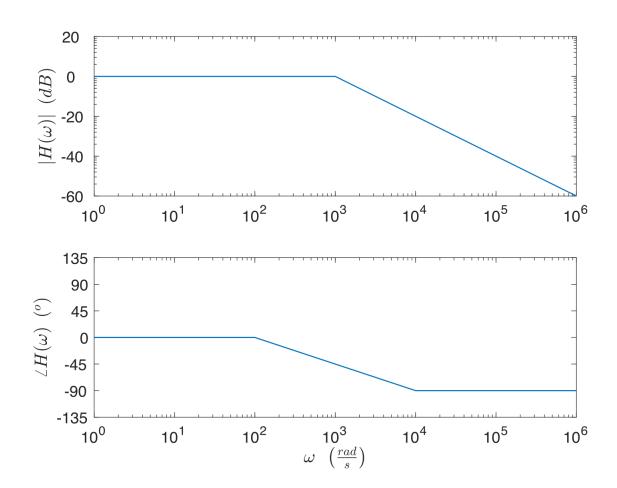
A factor of $\sqrt{2}$ at $\omega = \frac{1}{RC}$. The logarithmic nature of Bode plots means that this error doesn't really affect the general shape of the Bode plot.



(g) Approximately what is the phase of $\frac{\tilde{V}_C}{\tilde{V}_S}$ at $\omega = 0, \frac{1}{10RC}, \frac{1}{RC}, \frac{10}{RC}, \frac{1000}{RC}$? Connect the dots and sketch a plot of phase vs. time in a phase plot below your magnitude plot to complete your Bode plot for $\frac{\tilde{V}_C}{\tilde{V}_S}$.

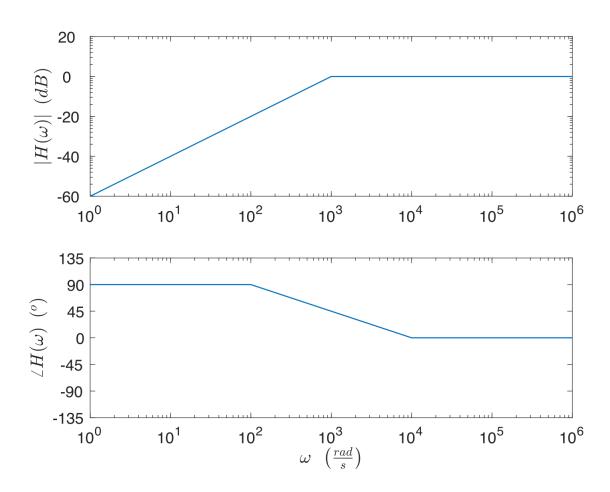
Answer:

$$0^{\circ}, 0^{\circ}, -45^{\circ}, -90^{\circ}, -90^{\circ}$$



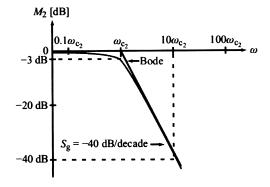
(h) Draw the Bode plot for $\left|\frac{\tilde{V}_R}{\tilde{V}_S}\right|$.

Answer:



2. Bode Plots

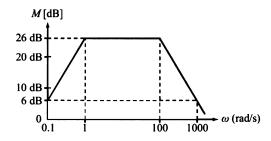
(a) Derive a transfer function that would result in the following Bode plot.



Answer:

$$H(\omega) = \frac{1}{\left(1 + \frac{j\omega}{\omega_c}\right)^2}$$

(b) Derive a transfer function that would result in the following Bode plot.

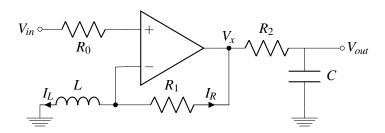


Hint: $20\log_{10} 2 = 6$

Answer:

$$H(\omega) = \frac{j20\omega}{(1+j\omega)\left(1+\frac{j\omega}{100}\right)}$$

3. Bode Plots and Phasors



We found the transfer function of this circuit to be:

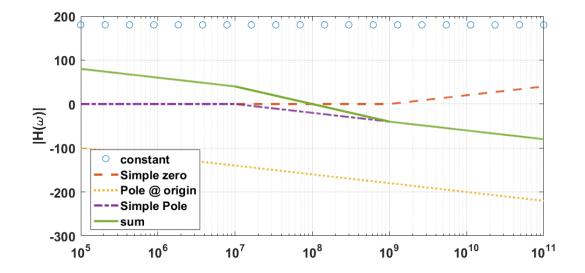
$$H(\omega) = \frac{R_1}{L} \frac{1 + j\omega \frac{L}{R_1}}{(j\omega)(1 + j\omega R_2 C)}$$

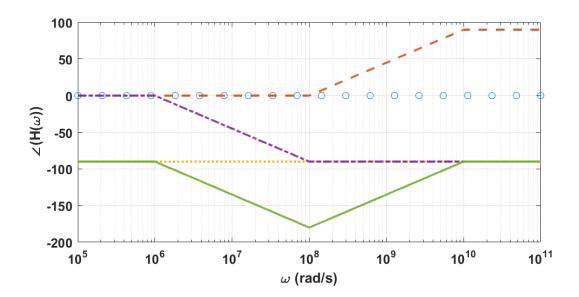
Using the following values:

$$R_0 = 100 \,\Omega, R_1 = 1 \,\mathrm{k}\Omega, L = 1 \,\mathrm{\mu H}, R_2 = 100 \,\mathrm{k}\Omega, C = 1 \,\mathrm{pF}$$

Plot its magnitude and phase Bode plots.

Answer:





2.4 Extra Practice

1. Transfer Function

Create a Bode plot of the following transfer function:

$$H(\omega) = \frac{1}{10} \frac{((j\omega)^2 + 110j\omega + 1000)(j\omega + 10000)}{(j\omega + 1000)((j\omega)^2 + 101j\omega + 100)}$$

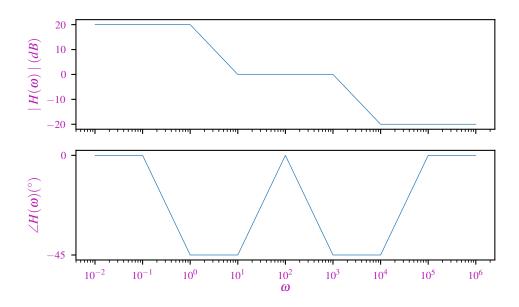
Answer:

First of all, we decompose the second-order terms:

$$H(\omega) = \frac{1}{10} \frac{((j\omega) + 100)(j\omega + 10))(j\omega + 10000)}{(j\omega + 1000)((j\omega) + 100)(j\omega + 1))} = \frac{1}{10} \frac{(j\omega + 10)(j\omega + 10000)}{(j\omega + 1000)(j\omega + 1)}$$

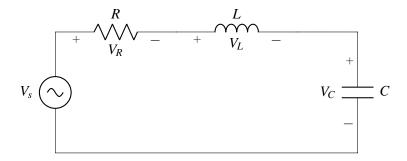
Then, we convert it to the normal form:

$$H(\omega) = \frac{10}{1} \frac{(\frac{j\omega}{10} + 1)(\frac{j\omega}{10000} + 1)}{(\frac{j\omega}{1000} + 1)(j\omega + 1)}$$



2. RLC Circuit

In this question, we will take a look at an electrical systems described by second order differential equations and analyze it using the phasor domain. Consider the circuit below where V_s is a sinusoidal signal, L = 1 mH, and C = 1 nF:



(a) Transform the circuit into the phasor domain. Answer:

$$Z_{R} = R$$

$$Z_{L} = j\omega L$$

$$Z_{C} = \frac{1}{j\omega C}$$

(b) Solve for the transfer function $H_C(\omega) = \frac{\widetilde{V}_C}{\widetilde{V}_s}$ in terms of R, L, and C.

Answer:

 \widetilde{V}_C is a voltage divider where the output voltage is taken across the capacitor.

$$\widetilde{V}_C = \frac{Z_C}{Z_R + Z_L + Z_C} \widetilde{V}_s$$

$$H_C(\omega) = \frac{Z_C}{Z_R + Z_L + Z_C} = \frac{\frac{1}{j\omega C}}{R + j\omega L + \frac{1}{j\omega C}}$$

Multiplying the numerator and denominator by $j\omega C$ gives

$$H_C(\omega) = \frac{1}{(j\omega)^2 LC + j\omega RC + 1}$$

(c) Solve for the transfer function $H_L(\omega) = \frac{\widetilde{V}_L}{\widetilde{V}_s}$ in terms of R, L, and C.

 \widetilde{V}_L is a voltage divider where the output voltage is taken across the inductor.

$$\widetilde{V}_L = \frac{Z_L}{Z_R + Z_L + Z_C} \widetilde{V}_s$$

$$H_L(\omega) = \frac{Z_L}{Z_R + Z_L + Z_C} = \frac{j\omega L}{R + j\omega L + \frac{1}{i\omega C}}$$

Multiplying the numerator and denominator by $j\omega C$ gives

$$H_L(\omega) = \frac{(j\omega)^2 LC}{(j\omega)^2 LC + j\omega RC + 1}$$

(d) Solve for the transfer function $H_R(\omega) = \frac{\widetilde{V}_R}{\widetilde{V}_s}$ in terms of R, L, and C.

Answer

 V_R is a voltage divider where the output voltage is taken across the resistor.

$$\widetilde{V}_R = \frac{Z_R}{Z_R + Z_L + Z_C} \widetilde{V}_s$$

$$H_R(\omega) = \frac{Z_R}{Z_R + Z_L + Z_C} = \frac{R}{R + j\omega L + \frac{1}{j\omega C}}$$

Multiplying the numerator and denominator by $j\omega C$ gives

$$H_R(\omega) = \frac{j\omega RC}{(j\omega)^2 LC + j\omega RC + 1}$$

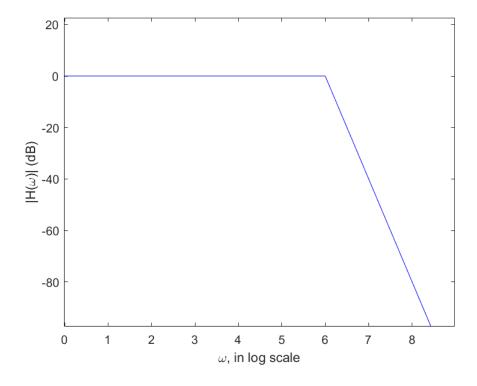
(e) Sketch the bode plot for H_C . Let $R = 2k\Omega$. Answer: From part (a) we have,

$$H_C(\omega) = \frac{1}{(j\omega)^2 LC + (j\omega)RC + 1}$$

$$= \frac{1}{10^{-12}(j\omega)^2 + 2 \times 10^{-6}(j\omega) + 1}$$

$$= \frac{1}{\frac{(j\omega)^2}{(10^6)^2} + \frac{2(j\omega)}{10^6} + 1}$$

Hence, we have two poles at $\omega_p = 10^6$ and $\zeta = 1$, and hence we will have a 40 dB/dec drop off at ω_p . With these parameters, we have the following plot:



 \mathbf{S}

	- 		1 1 1 1 1 1 1 1 1	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		1 1 1 1 1 1 1	
		 			}		
}		 	╌┼╌┼┼┼┼┼	╌┽╌╌┼╌┼┼┼	 	┼╌┼╌┼╌┼ ┼	
		 -			 	 	
	- 		 	- 	 	 	
		ttt-			!		
		ttt-	-†-†-†-†		t 	†-†-†-†††	
II-III		iltt-			!	T-T-T-T-T-T	
						 	
		III	-1-111111		[[
					II		
			-1-1-1-1-111		[[T-1-1111	
						┆ ╌┼╌┼╌┼┼┼	
		IITT	77777777		[[T-T-T-T7T	
			77777				
					il		
		<u> </u>			Ш		
		<u> </u>		<u> </u>	<u> </u>		<u> </u>
		<u> </u>			<u> </u>		
		 			ļļļļ	+-+-+-	
<u> </u>		 			 		<u> </u> -
L		 			 	<u> </u>	
	1 1 1 1 1 1 1 1	il i i					
		 			 		
		 	-4-4-4444		 	1-1-1-11	
		ili-	1 1 1 1 1 1 1 1		11 1 1	1 1 1 1 1 1 1	
1 1 1 1 1 1 1 1 1 1 1	1 1 1 1 1 1 1 1				+++		
			-+-+-++++				
						<u> </u>	
					 		
					 		

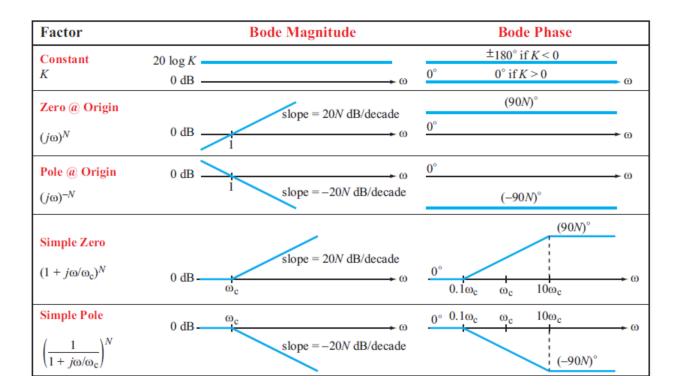


Figure 4: Bode Plot Cheat Sheet