#### EE185524

# Quantization and Sampling Theory

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# Digital vs analog controller

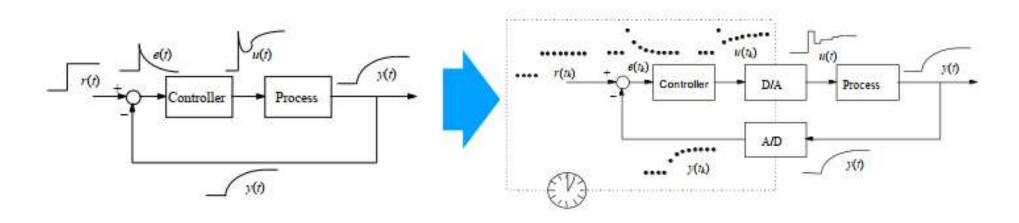
- A digital control system uses digital electronics hardware, usually in the form of a programmed digital computer
- The evolution of microprocessors / embedded systems allowed their use as control elements:
  - > met the stringent performance specifications needed in applications, and
  - ➤ have several advantages over their continuous-time counterparts:
- > Sampling is thus inherent and may be necessary
- For some control system application, better system performance may be achieved by a digital control system design

# Digital controller

➤ More reliable due to its improved noise immunity

- ➤ Need sampling to convert time-varying signals to discrete-time signals
- Quantization?

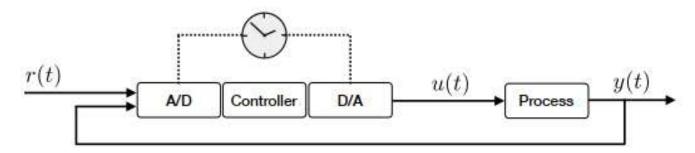
#### Analog vs digital signals

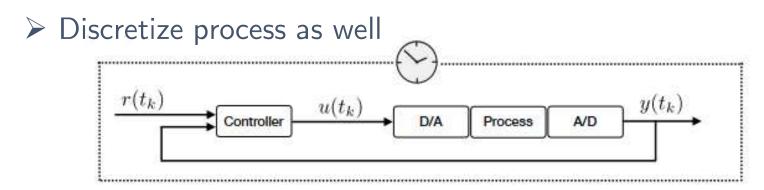


- Reconstruction of analog to digital signal (and vice versa) is only an approximation of the actual signal
- Some signal information might be lost or/and delayed in the process

# Digital controller design

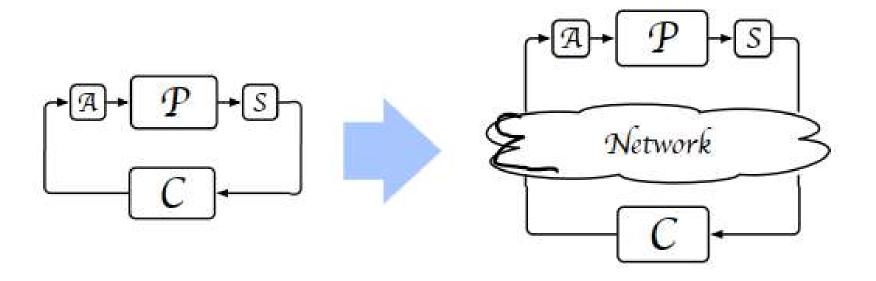
➤ Discretize analog controller (more common)





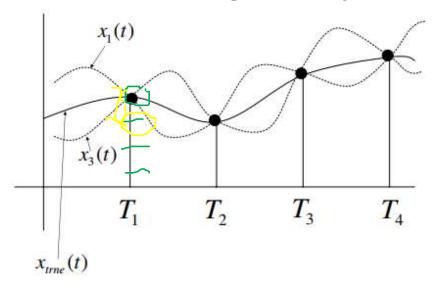
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# Digital control in networked control



#### Sampling

- $\triangleright$  (Usually) takes place in regular intervals, say  $T_s$
- $\triangleright$  Sampling frequency  $f_s = 1/T_s$
- > Generally, cannot reconstruct signals fully from samples



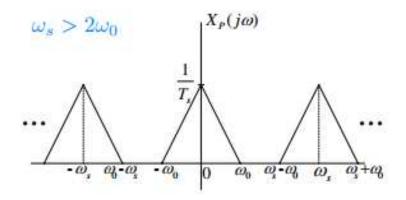
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#### Sampling criterion

 $\succ x_c(t)$  can be uniquely determined by its samples  $x_c(nT_s)$  if the sampling angular frequency is at least twice as big as  $\omega_0$ :

$$\omega_{S} = \frac{2\pi}{T_{S}} > 2\omega_{0}$$

➤ Nyquist angular frequency: minimum sampling angular frequency

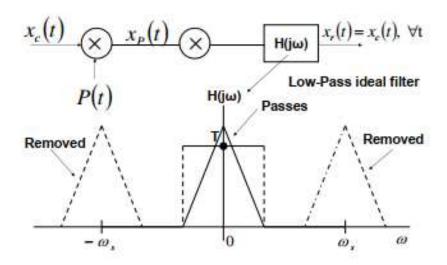


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#### Reconstruction

- ➤ D/A conversion
- > Requires a low-pass filter w/ cut-off frequency:

$$\omega_0 < \omega_c < \omega_s - \omega_0$$

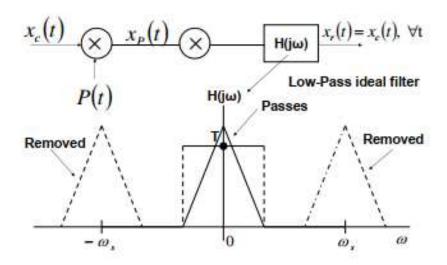


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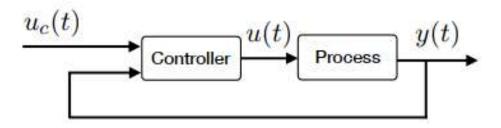
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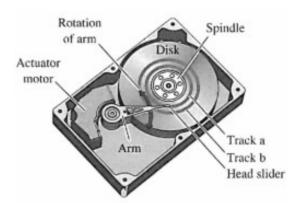


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#### Example

 $\triangleright$  Consider a plant with TF  $G(s) = \frac{k}{Js^2}$ 

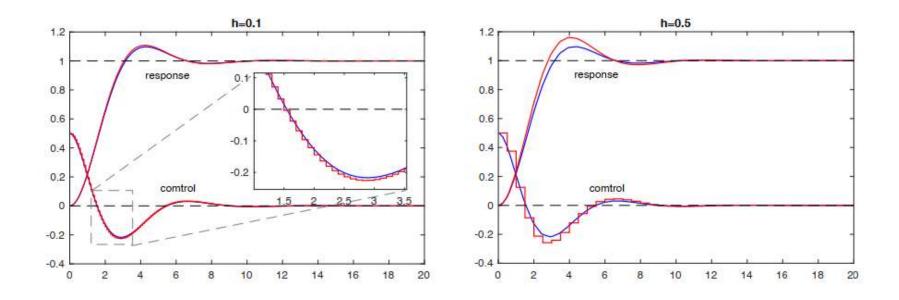




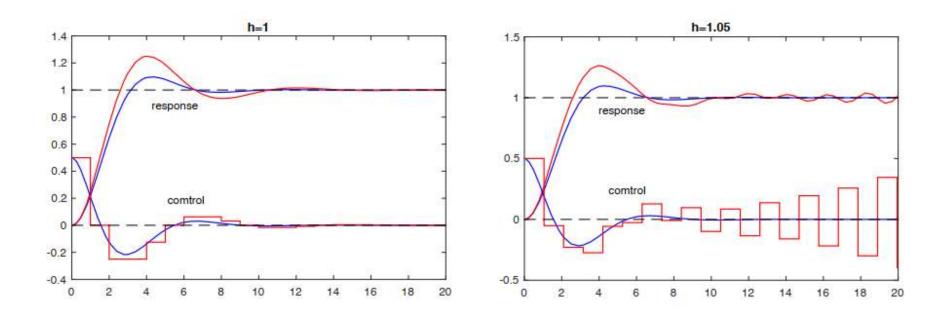
- Suppose controller  $U(s) = K \frac{b}{a} U_c(s) K \frac{(s+b)}{s+a} Y(s)$
- > Derivative is approximated w/ a difference

$$\frac{x(t+h)-x(t)}{(h)} = -ax(t) + (a-b)y(t)$$

# Example



# Example



#### Quantization

- The process of mapping input values from a large set (often continuous) to output values in a (countable) smaller set
- > Output: fixed-point words (8-bit, 16-bit, and 24-bit)



➤ An A/D converter produces these binary representation of the sampled signals at each sample time

# Fixed-point number representation

 $\triangleright$  A n-bit fixed-point binary number N

$$N = \sum_{j=-m}^{n-1} b_j 2^j = b_{n-1} 2^{n-1} + \dots + b_0 2^0 + b_{-1} 2^{-1} + \dots + b_{-m} 2^{-m}$$
Integer portion

Decimal portion

$$= (b_{n-1}b_{n-2} \dots b_0 \odot b_{-1} \dots b_{-m})_2, \qquad b_j \in (0,1)$$

$$\downarrow \qquad \qquad \downarrow$$

$$MSB \qquad \text{Binary point} \qquad \mathsf{LSB}$$

#### Quantization error

> Depends on the type of arithmetic and type of quantization used

$$-\frac{q}{2} \le e \le \frac{q}{2}$$

where  $q := 2^{-C}$ , C being the number of bits

- ➤ More level → lower noise
- > Typically, original signal is much larger than LSB

#### Quantizer

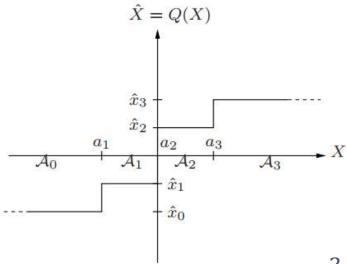


- > Samples  $X = X_N^1$  into a k-bit index, then produces approximation  $\widehat{X}_1^N$
- > Example: Scalar quantizer

ightharpoonup Encoder:  $X \in A_i \to I$ , Decoder:  $I \to \hat{X} = \hat{x}_i$ 

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#### Quantizer



- $\triangleright$  MSE quantization distortion:  $D = \mathbb{E}[(X \hat{X})^2]$
- > Signal-to-quantization-noise ratio:  $SQNR = \frac{\mathbb{E}[X^2]}{\mathbb{E}[(X-\hat{X})^2]}$

# Uniform quantization

$$ightharpoonup$$
 Step size  $\Delta = \frac{2V}{2^k} = 2^{1-k}V$ 

- $\triangleright$  Quantization error  $\tilde{X} = X Q(X)$ 
  - $Y \in [-V, V] \rightarrow$  "granular region"
  - $\triangleright |X| > V \rightarrow \text{"overload"}$
- Quantization noise:

$$D = \int_{-V}^{V} (x - Q(x))^2 f(x) dx + \int_{x=|V|} (x - Q(x))^2 f(x) dx$$

Granular distortion

Decimal portion

-V

 $\hat{X} = Q(X)$ 

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#### Quantization for nonuniform distribution

> Distortion is given by

Distortion is given by
$$D = \sum_{i=0}^{K-1} \int_{A_i} (x - x_i)^2 f(x) dx$$

➤ Optimal encoding:

$$a_i = \frac{\hat{x}_{i-1} + \hat{x}_i}{2} \qquad (OE)$$

$$= \sum_{i=0}^{K-1} \int_{a_i}^{a_{i+1}} (x - x_i)^2 f(x) dx \qquad \qquad \hat{x}_i = \frac{\int_{a_i}^{a_{i+1}} x f(x) dx}{\int_{a_i}^{a_{i+1}} f(x) dx}$$
 (OD)

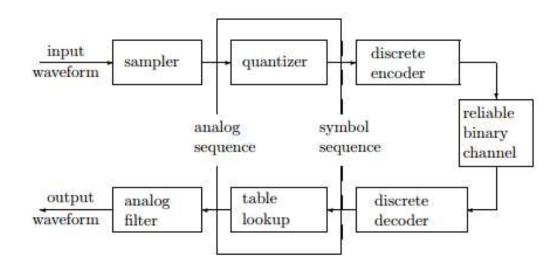
$$\hat{x}_{i} = \frac{\int_{a_{i}}^{a_{i+1}} x f(x) dx}{\int_{a_{i}}^{a_{i+1}} f(x) dx}$$
(OD)

(assuming pdf known)

#### Lloyd-Max algorithm

- $\triangleright$  Iteratively computes quantization variables  $\hat{x}_i$  and  $a_i$
- $\triangleright$  Assumption: f(x) known,  $a_0 = -V$ ,  $a_k = V$
- > Steps:
  - $\triangleright$  Step 1: Assume a value for  $\hat{x}_0$
  - $\triangleright$  Step 2: Find  $a_1$  from (OE)
  - $\triangleright$  Step 3: Find  $\hat{x}_2$  from (OD)
  - > ... etc.

# Quantization in communication systems



#### Sustained oscillations and deadband effects

- ➤ When digital controllers are implemented with finite word length, sustained oscillations may appear at the controller output
- Consider the controller described by difference equation

$$y[k] = ay[k-1] + x[k]$$
 where  $a = 0.5$ ,  $x[k] = 0.75\delta[k]$ ,  $y[-1] = 0$ 

> If the controller equation implemented with infinite word, then  $y[k] = 0.75(0.5)^k$ 

100

#### Sustained oscillations and deadband effects

- If the controller equation implemented with 3-bit word, then  $y_q[k] = Q\left[0.5y_q[k-1]\right] + 0.75\delta[k]$
- ightharpoonup ..... stops at  $y_q[k] = 0.125$

# Interplay between sampling and quantization error

Quantization error may not be ignored

- For example, consider a controller w/ TF  $G(s) = \frac{10^4}{s+1}$
- > Discretization w/ impulse invariant approximation

$$G(z) = \frac{10^4}{1 + e^{-h}z^{-1}}$$

- $G(z) = \frac{10^4}{1 + e^{-h}z^{-1}}$   $\Rightarrow \text{Thus}$
- > Thus,

$$\sum_{m=0}^{\infty} g^{2}[m] = 10^{8} \sum_{m=0}^{\infty} e^{-2hm} = 10^{8} (1 + e^{-2h} + \dots) = \frac{10^{8}}{1 - e^{-2h}}$$

# Interplay between sampling and quantization error

Quantization error may not be ignored

➤ Variance of output:

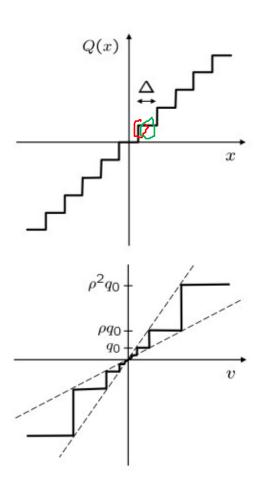
$$var(y_e) = var(e) \sum_{m=0}^{\infty} g^2[m] = \left(\frac{2^{-2C}}{12}\right) \left(\frac{10^8}{1 - e^{-2}}\right)$$

- $\triangleright$  If C fixed: decreasing h increases variance of output noise
- $\triangleright$  If h fixed: increasing C decreases variance of output noise

#### Which quantizers?

Since a finite bits are transmitted, quantizers should be **designed** 

- ➤ Uniform quantizers: divide space into equal sections
- Logarithmic quantizers: provide a finer quantization near the origin
- Dynamic scaling: a smaller scaling factor provides a fine quantization near origin; a larger one ensures large number fall within domain of quantization



#### Into control system...

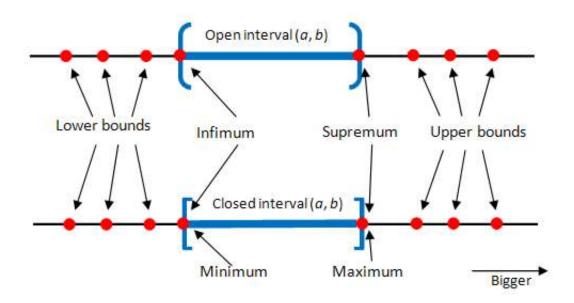
$$x[k+1] = Ax[k] + Bu[k] + w[k]$$
$$y[k] = Cx[k] + v[k]$$

- ➤ **Objective**: Identify the trade-off between the unstable modes of the system and the channel's rate to guarantee stability
- > **Solution**: Consider second moment stability:

$$\sup_{k \in \mathbb{N}} \mathbb{E}(||X_k||^2) < \infty$$

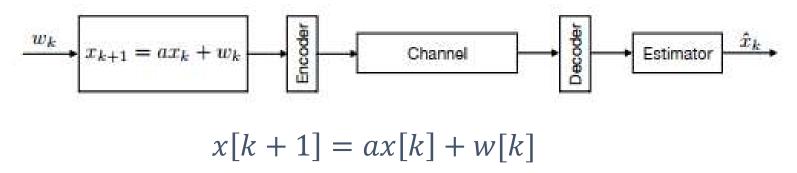
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# Into control system...



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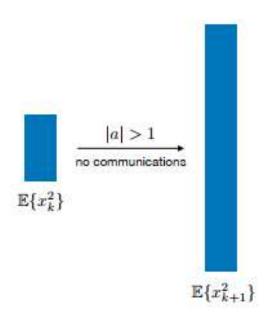
Remote state estimation:



w[k] Gaussian w/ zero mean and variance  $\sigma_w^2$ :  $\mathbb{E}\{x_{k+1}^2\} = a^2 \mathbb{E}\{x_k^2\} + \sigma_w^2$ 

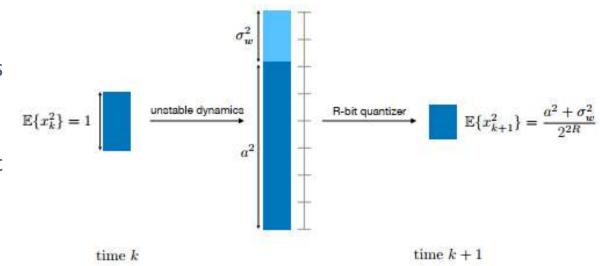
Unstable if |a| > 1

#### Data rate theorem



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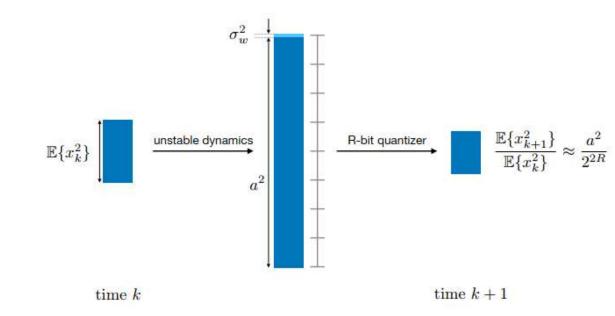
- The noise and bandwidth limitations of the channels are captured by modeling channels capable of transmitting only *R* bits in each time slot
- ➤ By transmitting enough bits at each time step, we can ensure the uncertainty decreases



#### Data rate theorem

- $ightharpoonup \mathbb{E}\{x_k^2\}$  grows larger each time
- Thus, (second moment) stability can be achieved if

$$\frac{a^2}{2^{2R}} < 1$$



#### Conclusion

- ➤ Needs to carefully choose the sampling for stability and performance
- > The finer the quantization, the better
- ➤ How much information is needed to be communicated by the quantizer in order to achieve a certain control objective?