

# Multivariable Feedback Control

## Homework 03 - due Wednesday May 22nd, 2024.

The goal of this homework is to start exploring *MIMO systems*.

**Problem 1** The goal of this first problem is to interpret the steady state behavior of the closed loop controlled SISO system shown in Fig. 1 through the Singular Value Decomposition (interpretation of the singular input and output directions). For the simple plant  $G(s)$  you will solve 2 different control problems.

$$G(s) = \frac{1}{s + 10}$$

- **Spec1** Find  $C_1(s)$  so that the output  $y$  tracks asymptotically any constant reference  $r$ . Let  $(r, d_1, d_2)$  be the inputs and  $(e_y, m)$  the outputs (setting all the other inputs to 0) of the  $2 \times 3$  equivalent MIMO system transfer function  $W_1(s)$ . Interpret the SVD decomposition of the corresponding dc-gain  $W_1(0)$ .
- **Spec2** Find  $C_2(s)$  which guarantees that the output  $y$  will track asymptotically the sinusoidal reference  $r(t) = \sin 10t$ . Let  $(r, n)$  be the inputs and  $(y, m)$  the outputs (setting all the other inputs to 0) of the equivalent  $2 \times 2$  equivalent MIMO system transfer function  $W_2(s)$ . Interpret the SVD decomposition of the corresponding gain matrix  $W_2(j10)$  (you may find useful the command `frd` and `frdata`).

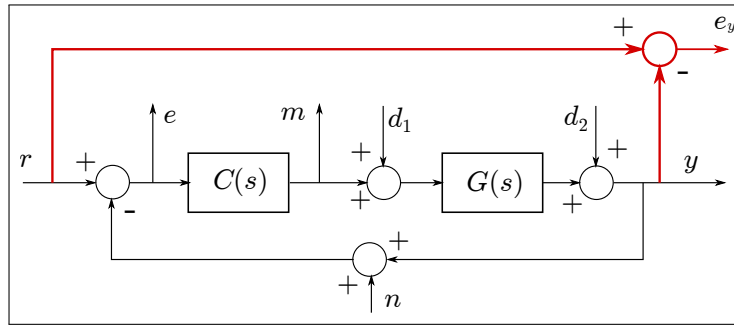


Figure 1: Control system

**Problem 2** Find/create a 2 inputs – 2 outputs (possibly physical) system where it is evident the necessity (advantage) or usefulness of scaling variables in a control problem.

**Problem 3** Consider the three-mass system shown in Fig. 2 and described in terms of the relative displacements  $z_i = \delta_i - \delta_i(0)$ ,  $i = 1, \dots, 3$  by the following set of linear differential equations (see the figure for the definition of the variables  $\delta_i$ ,  $i = 1, \dots, 3$ )

$$\begin{aligned} m_1 \ddot{z}_1 &= -k_0 z_1 - k_1 (z_1 - z_2) - \mu_1 (\dot{z}_1 - \dot{z}_2) - d_1 \dot{z}_1 + f_1 \\ m_2 \ddot{z}_2 &= k_1 (z_1 - z_2) - k_2 (z_2 - z_3) + \mu_1 (\dot{z}_1 - \dot{z}_2) - \mu_2 (\dot{z}_2 - \dot{z}_3) - d_2 \dot{z}_2 \\ m_3 \ddot{z}_3 &= k_2 (z_2 - z_3) + \mu_2 (\dot{z}_2 - \dot{z}_3) - d_3 \dot{z}_3 + f_3 \end{aligned}$$

with parameters  $m_i$  (mass),  $k_i$  (elastic coefficient),  $\mu_i$  (damper coefficient between masses),  $d_i$  (friction with the terrain coefficient),  $f_1$  a control force on the mass  $m_1$  and  $f_3$  a second control force on the mass  $m_3$ . Note the presence of a spring from  $m_1$  to the wall with elastic coefficient  $k_0$

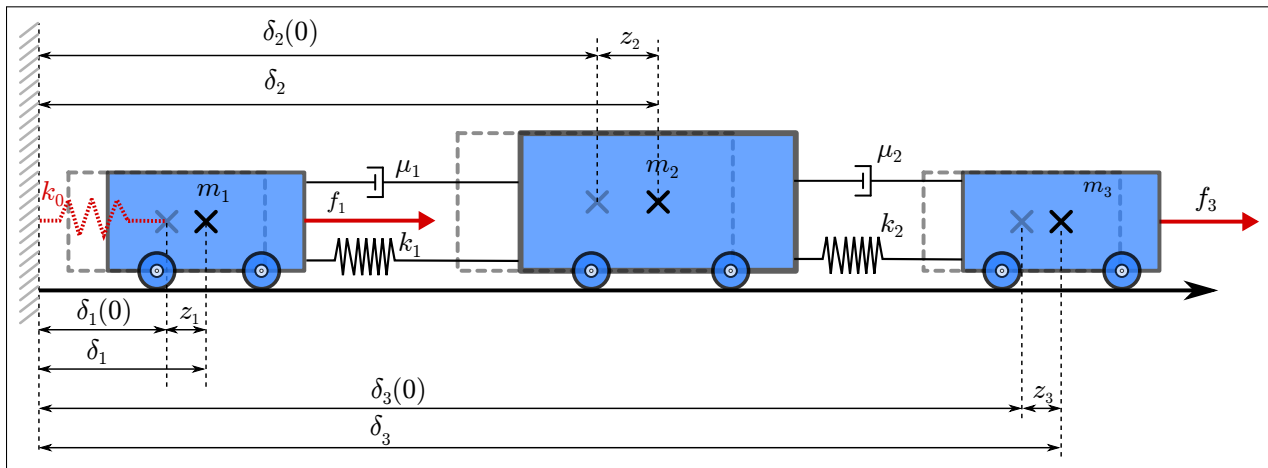


Figure 2: The three-mass system.

Main objectives:

1. Choose a nominal control problem with its performance weights, add measurement noise and a disturbance of your choice on one of the masses and finally build the augmented plant. Find a controller which guarantees this nominal performance.
2. Introduce uncertainties and show the difference between unstructured and structured uncertainty. Verify if the previous controller is also robustly stabilizing. If necessary find a controller using the SSV or see how much more uncertainty you can deal with using the SSV.

Possible values for a standard case (you can explore other situations where there is more or less friction and/or more or less rigid springs and or more differences in the masses):

$$\begin{aligned}
 m_1 &= 1 \text{ kg}, m_2 = 1.5 \text{ kg}, m_3 = 0.5 \text{ kg} \\
 k_0 &= 5 \text{ N/m}, k_1 = 10 \text{ N/m}, k_2 = 100 \text{ N/m} \\
 \mu_1 &= 5 \text{ N.s/m}, \mu_2 = 15 \text{ N.s/m} \\
 d_1 &= 0.1 \text{ N.s/m}, d_2 = 0.2 \text{ N.s/m}, d_3 = 0.1 \text{ N.s/m}.
 \end{aligned}$$