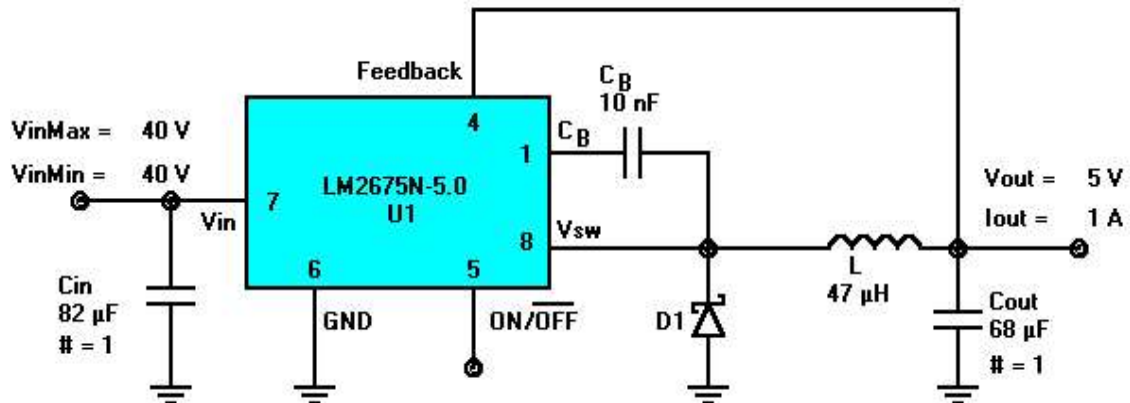




Input filter design for switching power supply:

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Basic step-down simple switcher power supply:



Input parameters

Results

-Maximum input voltage: $V_{input} := 35V$

-Output current: $I_{out} := 10 \cdot A$

-Output voltage: $V_{out} := 5V$

-Output inductor:

inductance: $L_o := 33\mu H$

DC resistance: $R_L := 0.088\Omega$

-Output capacitor: $C_o := 68\mu F$

ESR := 0.09Ω

-Duty cycle: $D := 0.458$

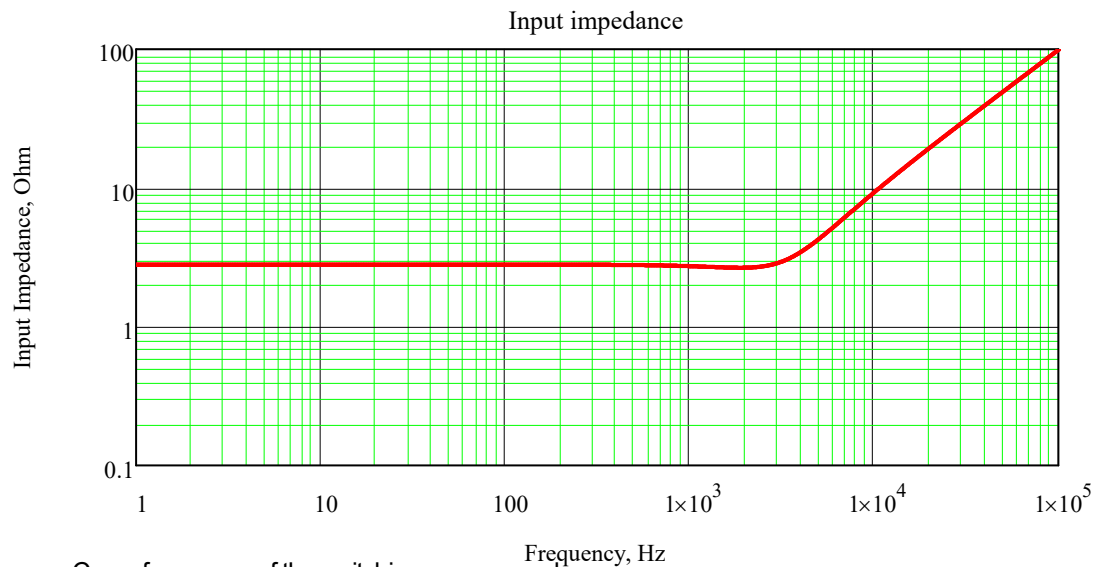
-Output impedance: $R_o := \frac{V_{out}}{I_{out}}$ $R_o = 0.5 \cdot A^{-2} \cdot kg \cdot s^{-3} \cdot m^2$

$i := 1..2000$ $f_i := 100 \frac{(i-200)}{500}$

$w_i := f_i \cdot \frac{rad}{s}$ $s_i := 2 \cdot \pi \cdot j \cdot w_i$

-Input impedance of the power supply:

$$Z_{i_i} := \left[\left(\frac{R_o + R_L}{D^2} \right) \cdot \left[\frac{1 + s_i \cdot \left[\frac{L_o}{R_o + R_L} + \left(ESR + \frac{R_o \cdot R_L}{R_o + R_L} \right) \cdot C_o \right] + (s_i)^2 \cdot L_o \cdot C_o \cdot \left(\frac{R_o + ESR}{R_o + R_L} \right)}{1 + s_i \cdot (R_o + ESR) \cdot C_o} \right] \right]$$



-Cross frequency of the switching power supply:

$$F_{cross} := 32 \text{ kHz}$$

To meet the noise filtering requirements the input filter has to have the corner frequency around one decade below the bandwidth of the feed back loop of the power supply.

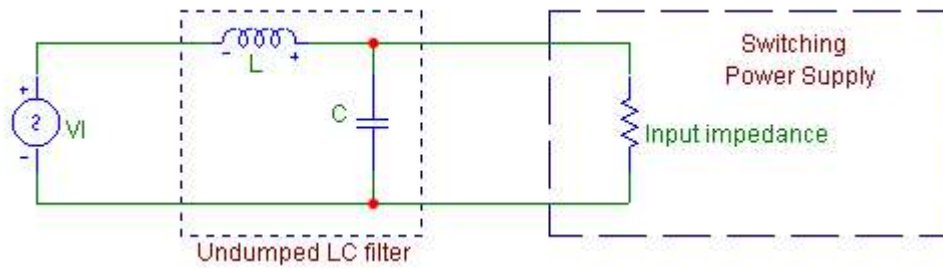
-Cut of frequency of the input filter: $f_c := 5 \text{ kHz}$

-Cut off frequency in radiant: $\omega_c := f_c \cdot 2\pi \quad \omega_c = 3.142 \times 10^4 \cdot s^{-1}$

-Maximum input impedance of the power supply: $R_{in} := 25 \cdot \text{ohm}$

-Input Capacitance of the power supply: $C_{in} := 15 \mu\text{F}$

- UNDUMPED LC FILTER:



-Inductance calculated:

$$L := \frac{1}{\omega_c^2 C} \quad L = 67.547 \cdot \mu\text{H}$$

-Damping factor:

$$\zeta := \frac{L}{2 \cdot R_{in} \cdot \sqrt{L \cdot C}} \quad \zeta = 0.042$$

-Inductor used:

$$L_f := 1 \mu\text{H}$$

$$R_f := 0.030 \cdot \Omega$$

-Capacitor used:

$$C_f := 33 \mu\text{F}$$

$$ESR_{ci} := 0.150 \Omega$$

-Cut off frequency of the filter:

$$f_{c_{filter1}} := \frac{1}{2 \cdot \pi \sqrt{L_f \cdot C_f}} \quad f_{c_{filter1}} = 27.705 \cdot \text{kHz}$$

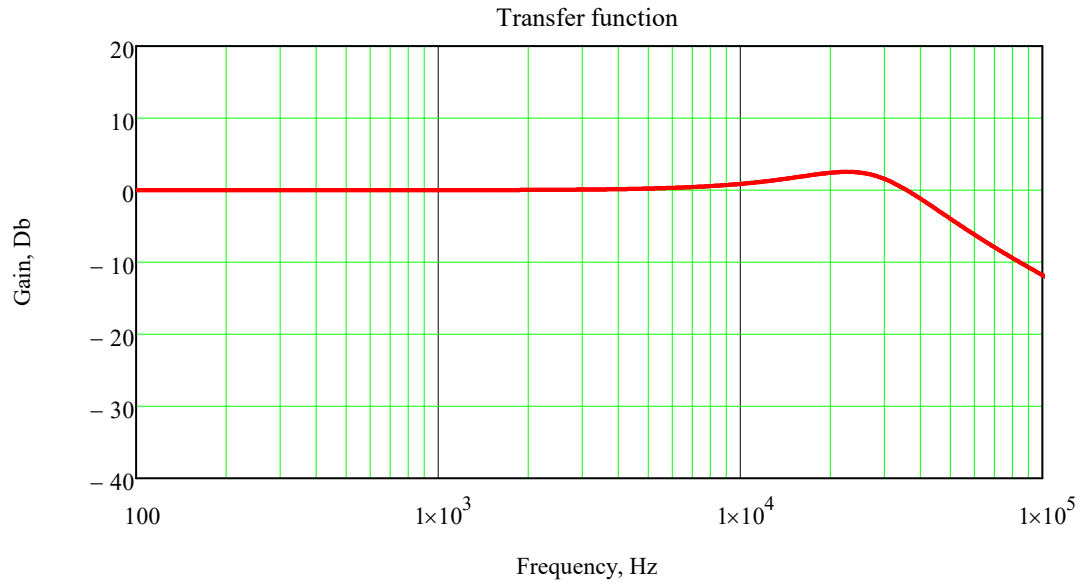
-Transfer function:

$$Z1_i := R_f + s_i \cdot L_f$$

$$Z2_i := ESR_{ci} + \frac{1}{s_i \cdot C_f}$$

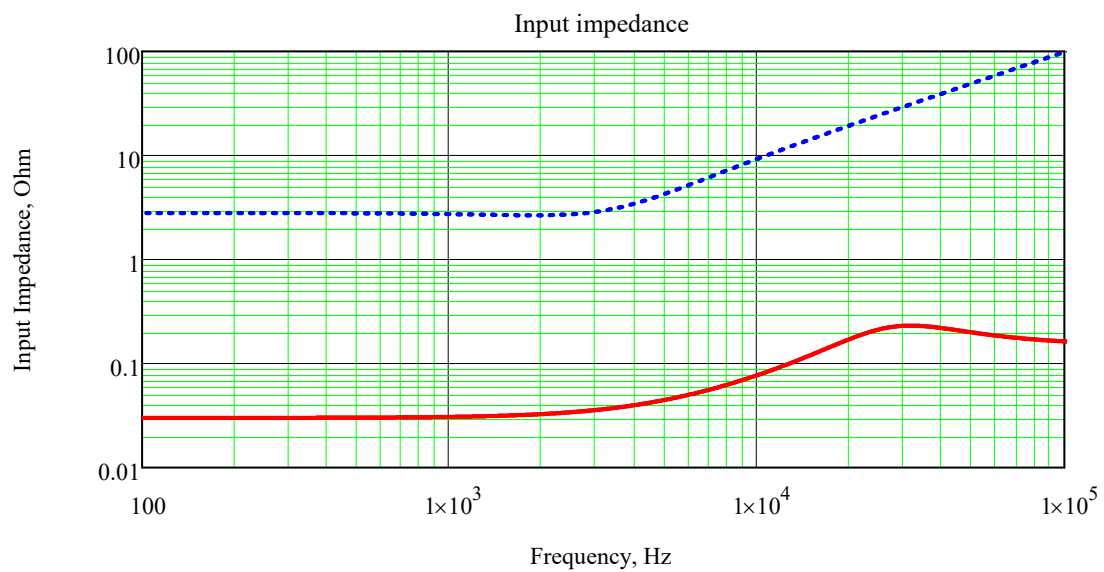
$$Z2eq_i := \frac{Z2_i \cdot R_{in}}{Z2_i + R_{in}}$$

$$\text{Filter}_i := 20 \cdot \log \left(\left| \frac{Z2eq_i}{Z2eq_i + Z1_i} \right| \right)$$



-Filter output impedance:

$$Z_{f_i} := \left| \frac{Z_{1_i} \cdot Z_{2_i}}{Z_{1_i} + Z_{2_i}} \right|$$



— Filter output impedance

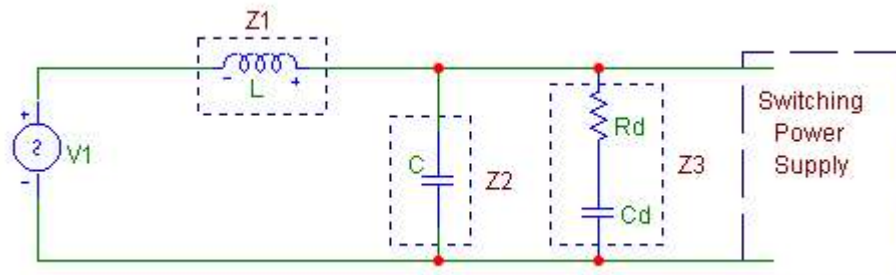
--- Power supply input impedance

In order to avoid oscillations it is important to keep the peak output impedance of the filter below the input impedance of the converter.

The two curves should not overlap.

-PARALLEL DAMPED FILTER:

In most of the cases a parallel damped filter meet easily the damping and impedance requireme



The purpose of R_d is to reduce the output peak impedance of the filter at the cutoff frequency. The capacitor C_d blocks the DC component of the input voltage.

-Damping resistance:

$$R_d := \sqrt{\frac{L_f}{C_f}} \quad R_d = 0.174 \cdot \text{A}^{-2} \cdot \text{kg} \cdot \text{s}^{-3} \cdot \text{m}^2$$

$$C_d := 4 \cdot C_f \quad C_d = 132 \cdot \mu\text{F}$$

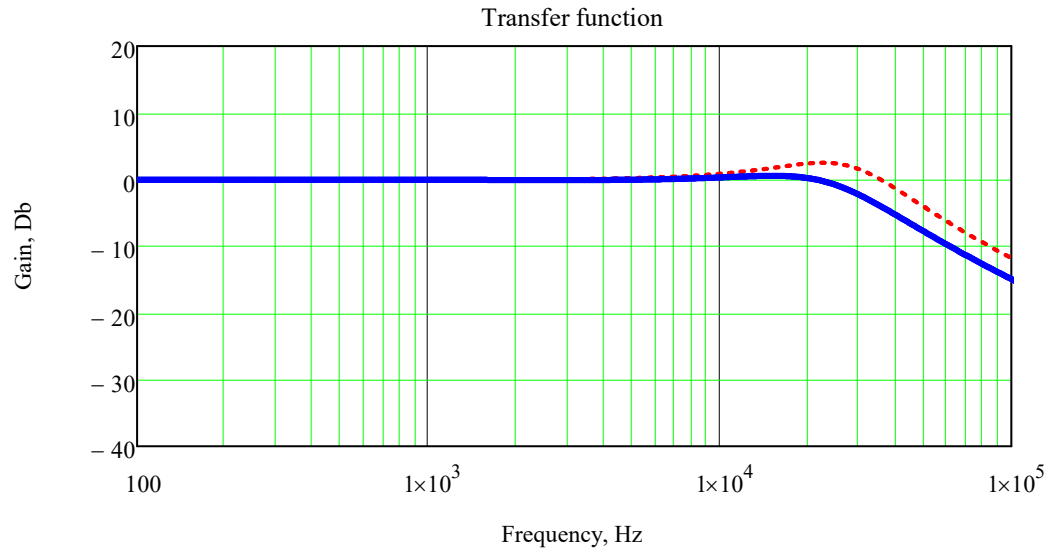
$$\text{ESR}_{cd} := 0.200 \Omega$$

$$Z_{3i} := \frac{1}{s_i \cdot C_d} + \text{ESR}_{cd} + R_d$$

$$Z_{3eq2i} := \frac{Z_{2eq1i} \cdot Z_{3i}}{Z_{2eq1i} + Z_{3i}}$$

-Transfer function:

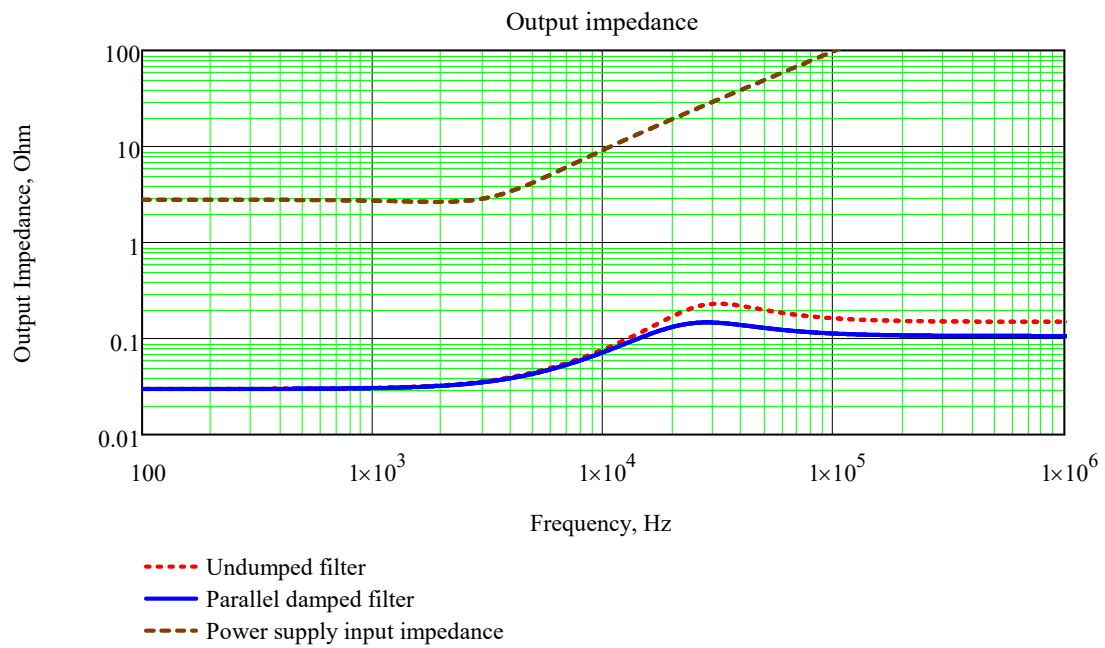
$$\text{Filter}_{2i} := 20 \cdot \log \left(\left| \frac{Z_{3eq2i}}{Z_{3eq2i} + Z_{1i}} \right| \right)$$



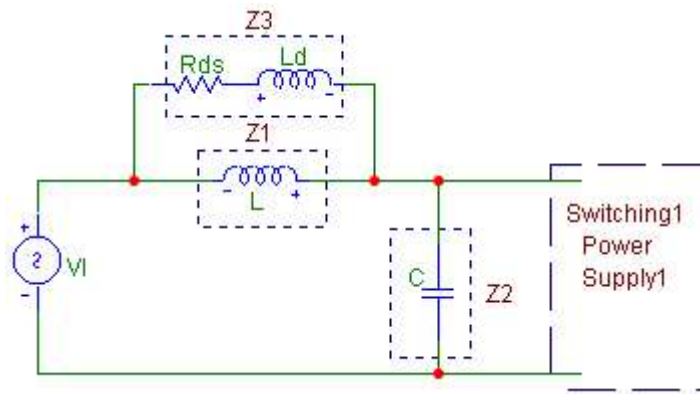
---- Undumped Filter
— Parallel damped filter

-Filter output impedance:

$$Z_{f2_i} := \left| \frac{Z_{1_i} \cdot Z_{3eq2_i}}{Z_{1_i} + Z_{3eq2_i}} \right|$$



-SERIES DAMPED FILTER:



$$s_r := \frac{1}{2 \cdot \pi \cdot \sqrt{L_f \cdot C_f}}$$

-Series inductor: $n_3 := \frac{2}{15}$

$$L_d := L_f \cdot n_3 \quad L_d = 0.133 \cdot \mu\text{H}$$

-Series damping resistance:

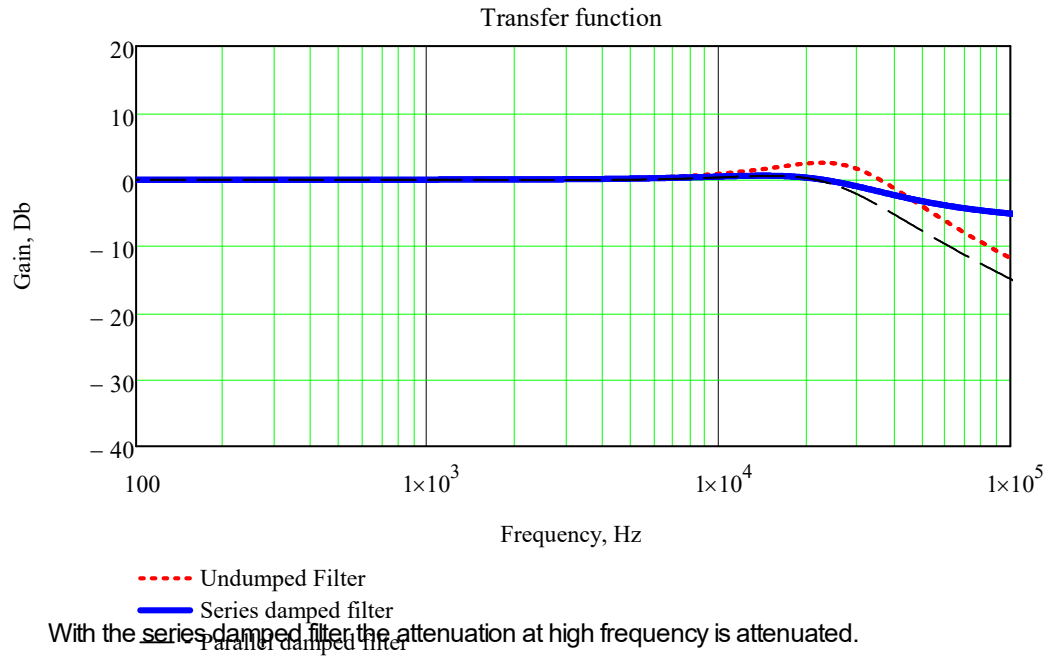
$$R_{ds} := \frac{\sqrt{L_f}}{\sqrt{C_f}} \quad R_{ds} = 0.174 \cdot \text{A}^{-2} \cdot \text{kg} \cdot \text{s}^{-3} \cdot \text{m}^2$$

$$Z3s_i := R_{ds} + s_i \cdot L_d$$

$$Z13_i := \frac{Z1_i \cdot Z3s_i}{Z1_i + Z3s_i}$$

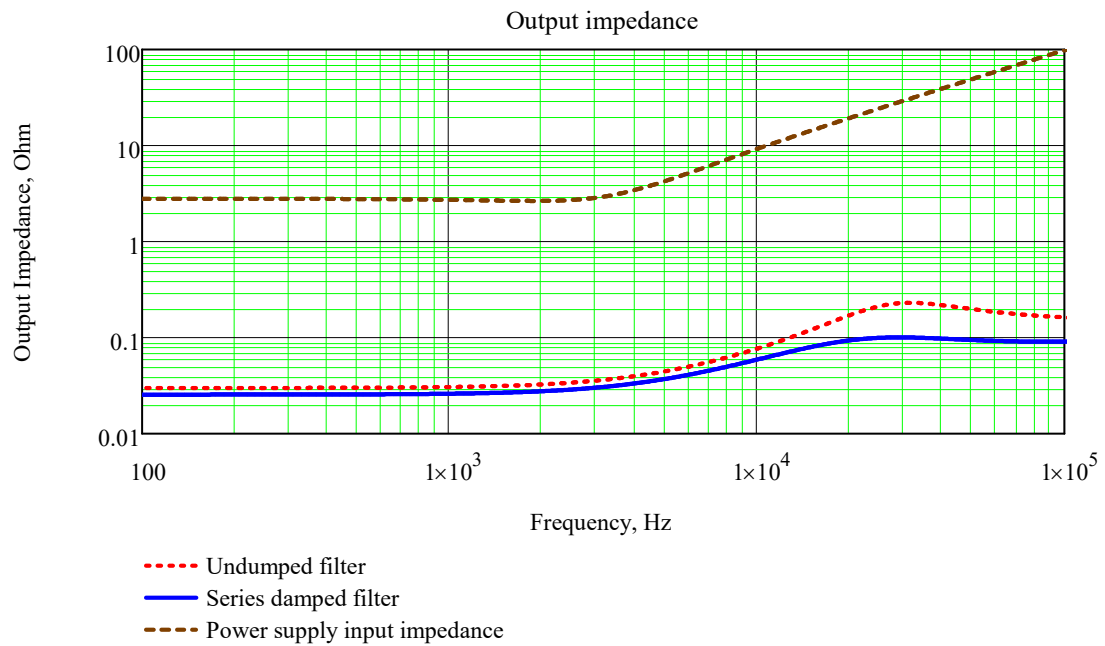
-Transfer function:

$$\text{Filter3}_i := 20 \cdot \log \left(\left| \frac{Z2_i}{Z2_i + Z13_i} \right| \right)$$

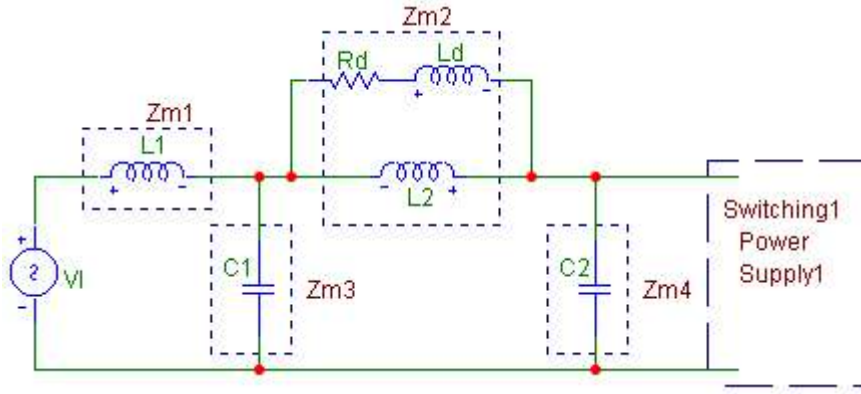


-Filter output impedance:

$$Z_{f3_i} := \left| \frac{Z2_i \cdot Z13_i}{Z2_i + Z13_i} \right|$$



-MULTIPLE FILTER SECTIONS:



-First LC filter:

$$L1 := \frac{Lf}{4} \quad L1 = 0.25 \cdot \mu H \quad RL1 := 0.1 \Omega$$

$$C1 := \frac{Cf}{4} \quad C1 = 8.25 \cdot \mu F \quad ESRc1 := 0.120 \Omega$$

$$fm1 := \frac{1}{2 \cdot \pi \cdot \sqrt{L1 \cdot C1}} \quad fm1 = 110.821 \cdot kHz$$

-Second LC filter:

$$L2 := 7 \cdot L1 \quad L2 = 1.75 \cdot \mu H \quad RL2 := 0.1 \Omega$$

$$C2 := 4 \cdot C1 \quad C2 = 33 \cdot \mu F \quad ESRc2 := 0.120 \Omega$$

$$fm2 := \frac{1}{2 \cdot \pi \cdot \sqrt{L2 \cdot C2}} \quad fm2 = 20.943 \cdot kHz$$

$$Rd4 := \sqrt{\frac{L1}{C2}} \quad Rd4 = 0.087 \cdot A^{-2} \cdot kg \cdot s^{-3} \cdot m^2$$

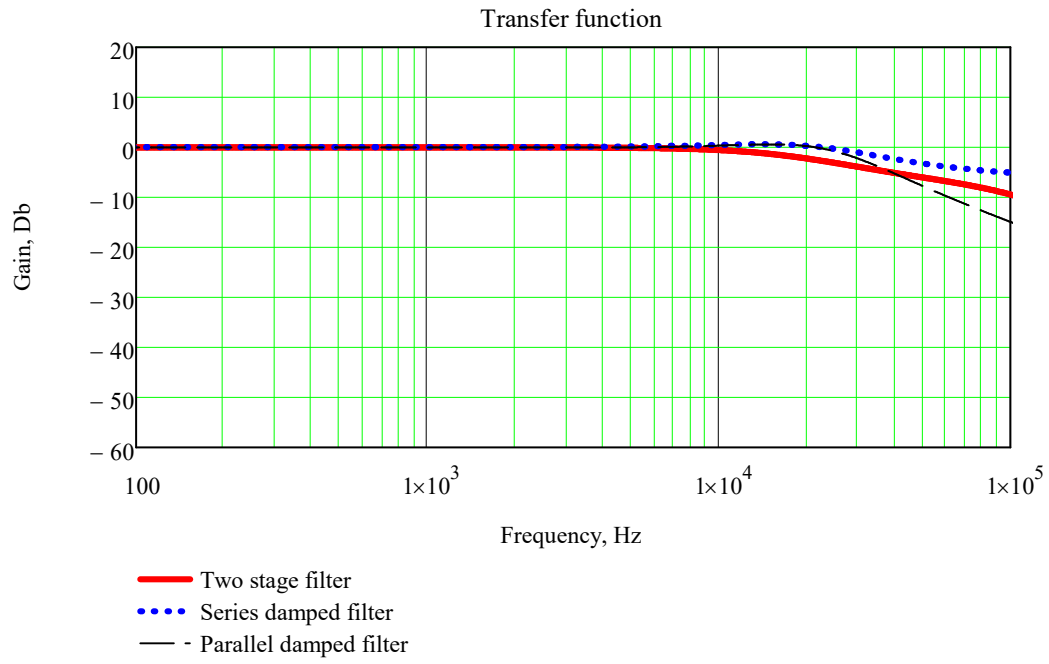
$$Ld4 := \frac{L1}{8}$$

$$Zm1_i := s_i \cdot L1 + RL1 \quad Zm2_i := \frac{1}{s_i \cdot C1} + ESRc1$$

$$Zm3_i := \frac{(Rd4 + s_i \cdot Ld4) \cdot (s_i \cdot L2 + RL2)}{(Rd4 + s_i \cdot Ld4) + s_i \cdot L2 + RL2} \quad Zm4_i := \frac{1}{s_i \cdot C2} + ESRc2$$

-Transfer function:

$$\text{Filter4}_i := 20 \cdot \log \left(\left| \frac{\frac{Zm4_i}{\frac{Zm1_i Zm2_i}{Zm1_i + Zm2_i} + Zm3_i + Zm4_i} \cdot \frac{Zm2_i}{Zm1_i + Zm2_i}}{1} \right| \right)$$



-Filter output impedance:

$$Zf4_i := \left| \frac{\frac{Zm4_i \cdot \frac{Zm1_i Zm2_i}{Zm1_i + Zm2_i} \cdot Zm3_i}{\frac{Zm1_i Zm2_i}{Zm1_i + Zm2_i} + Zm3_i + Zm4_i}}{1} \right|$$

