

Thermal Modelling of Thermal Runaway Propagation in Lithium-Ion Battery Systems

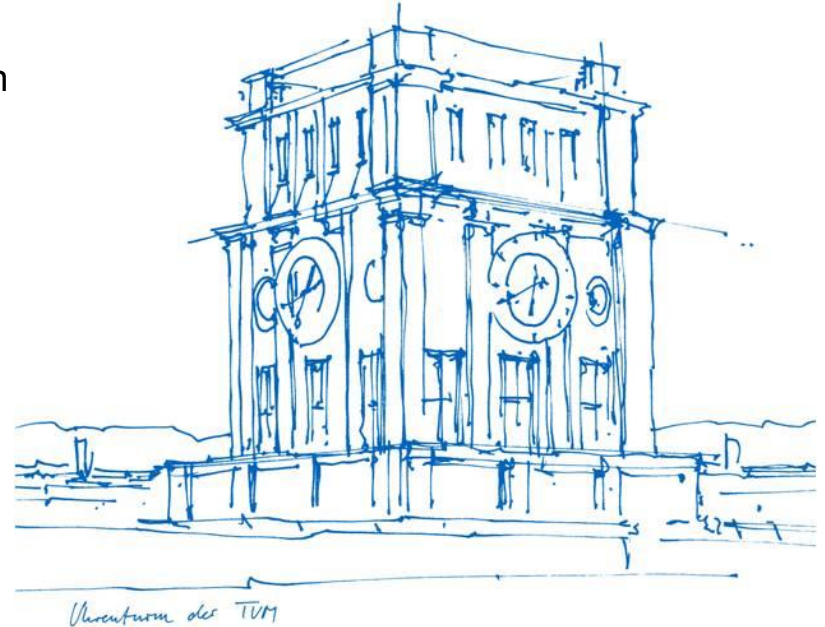
Elisabeth Irene Kolp (M.Sc.), Prof. Dr.-Ing. Andreas Jossen

Technical University of Munich, Germany

Department of Electrical and Computer Engineering

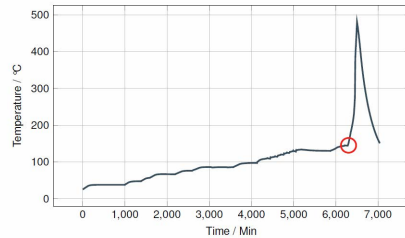
Institute for Electrical Energy Storage Technology

Petten, 8th & 9th March 2018

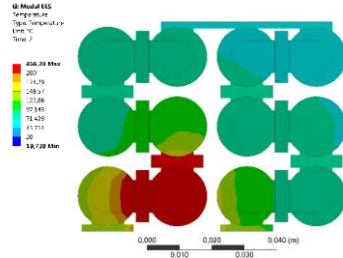


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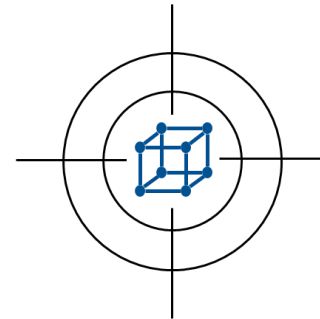
Method to
investigate abusive
behaviour



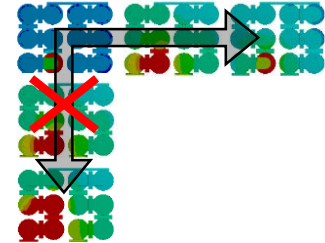
Simulation model for
thermal runaway
propagation (TR-P)



Limitations of
accurate modelling
of TR-P

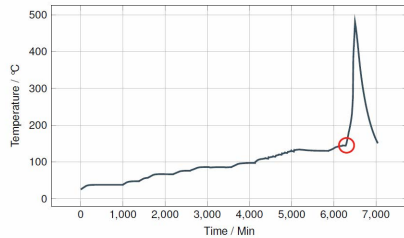


Mitigation strategies
of battery TR-P

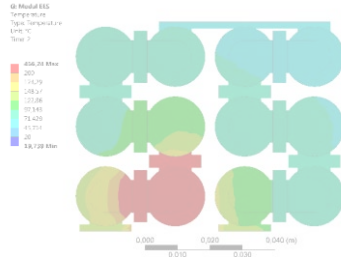


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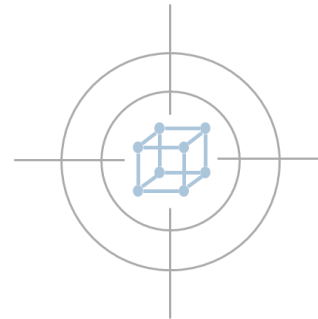
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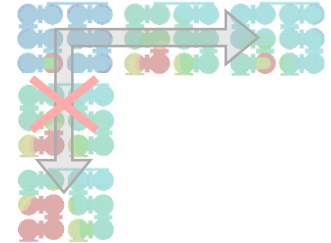
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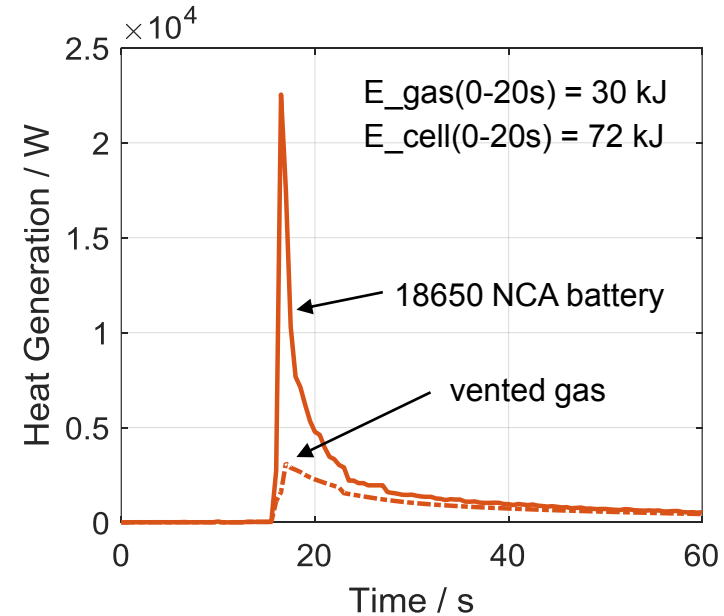


Mitigation strategies
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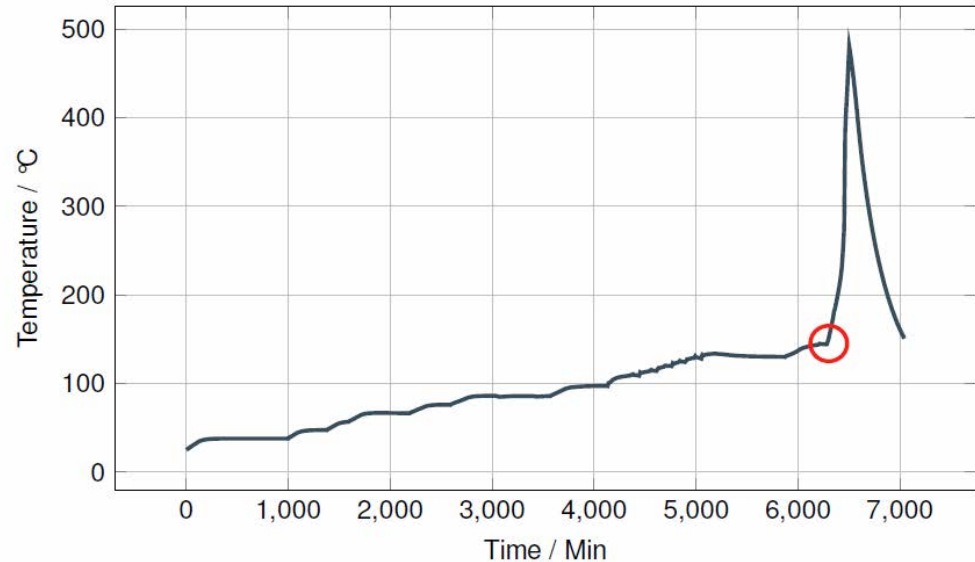
Empirical method to investigate abusive behaviour

Measure heat generation rate of a nail penetrated battery inside a calorimeter



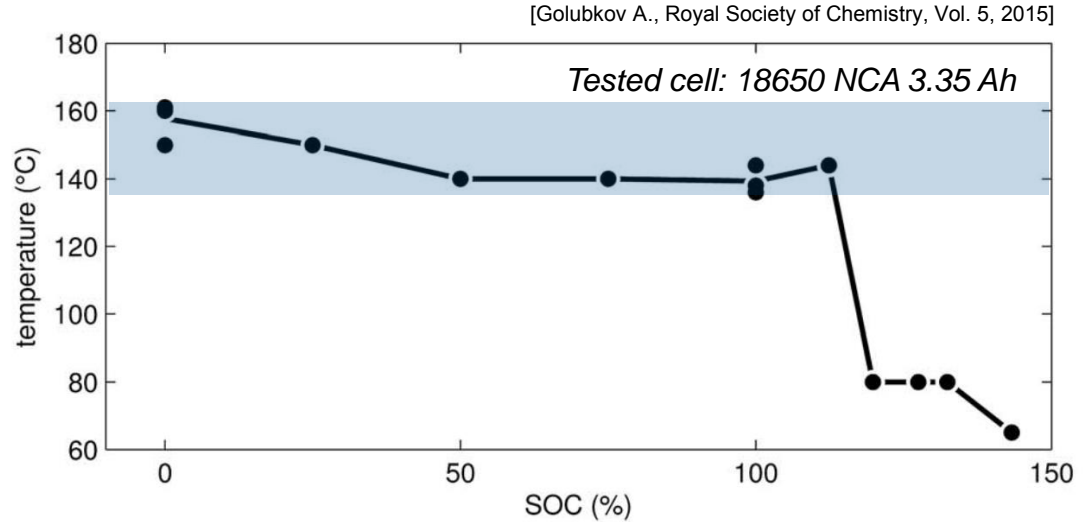
Empirical method to investigate abusive behaviour

Measure trigger temperature of thermal runaway with heat-wait-seek method



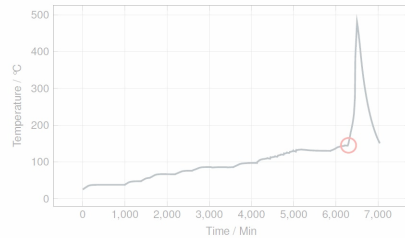
Empirical method to investigate abusive behaviour

Measure trigger temperature of thermal runaway: compare to literature

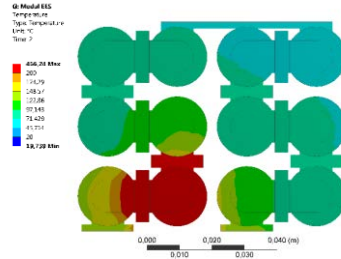


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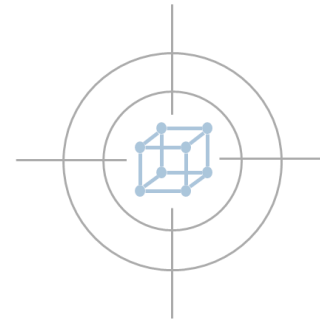
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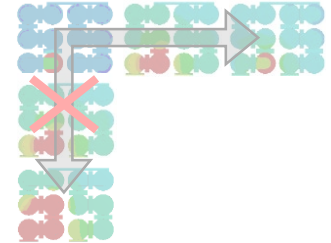
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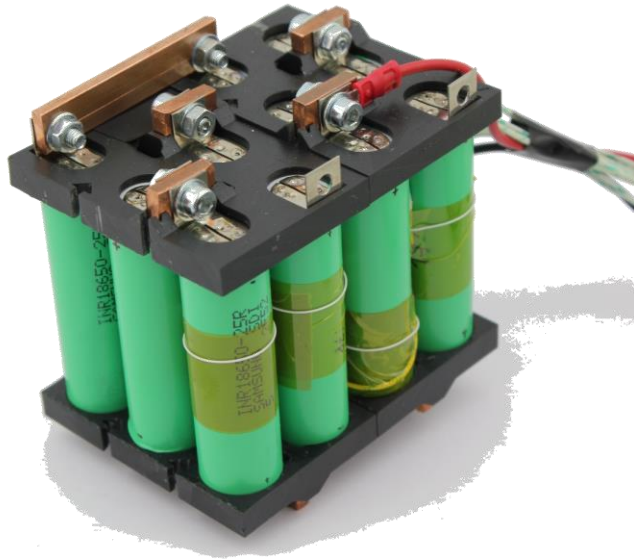


Mitigation strategies
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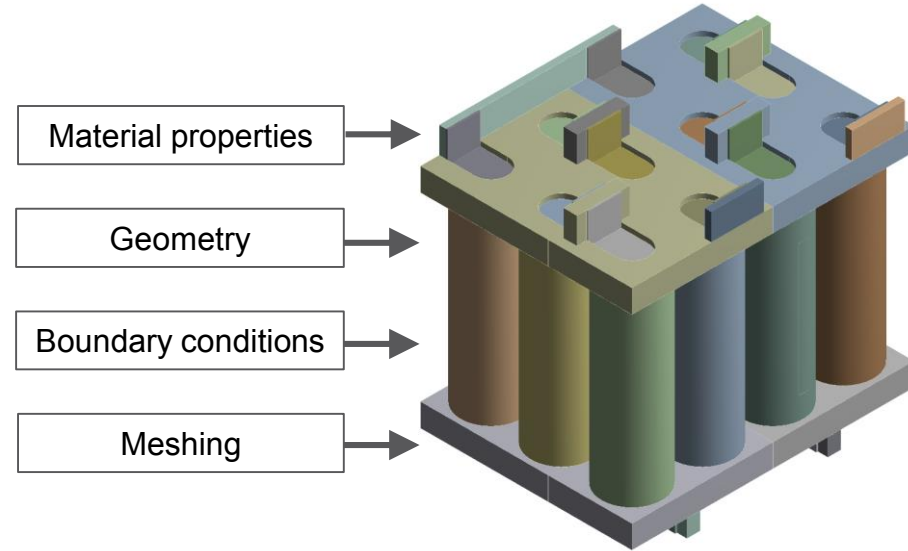


Conductive thermal model for TR propagation

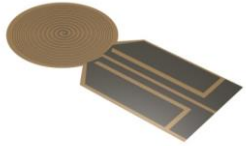
**Lithium-ion battery
module (12s1p)**



**FEM-model of lithium-ion
battery module**



Conductive thermal model for TR propagation



Custom Hot Disk / Literature:

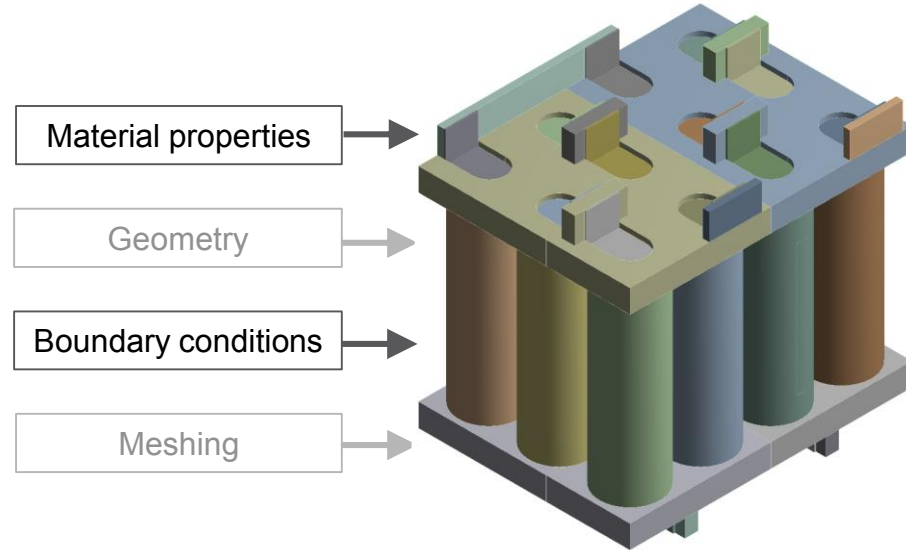
- Heat capacity
- Thermal conductivity (anisotrop)



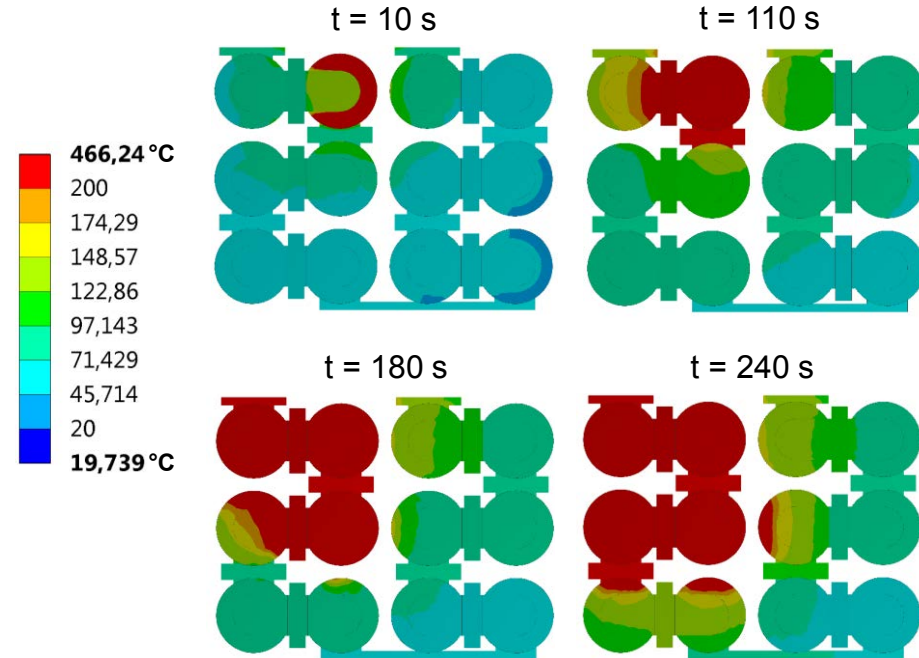
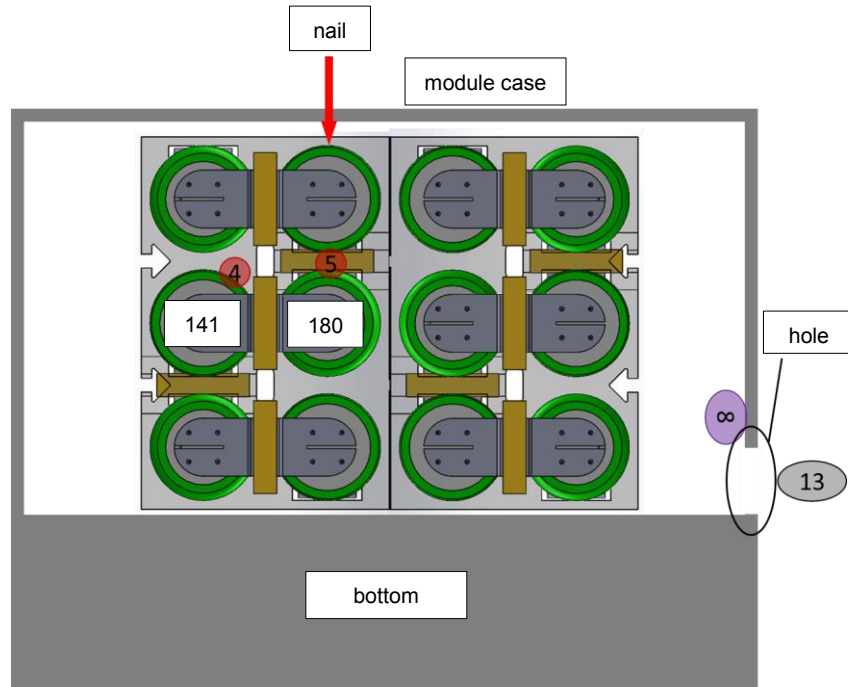
ARC/Calorimeter:

- Heat generation rate
- Heat capacity
- Trigger temperature of thermal runaway

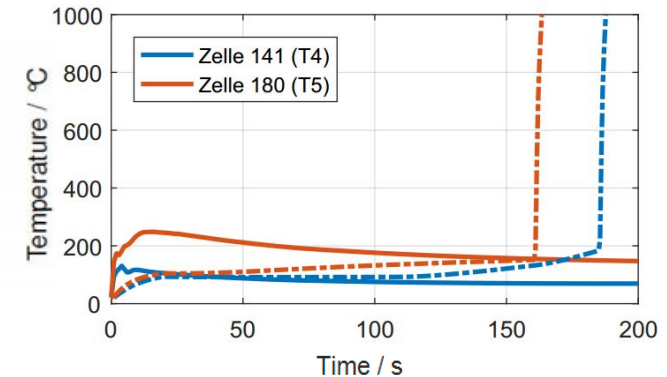
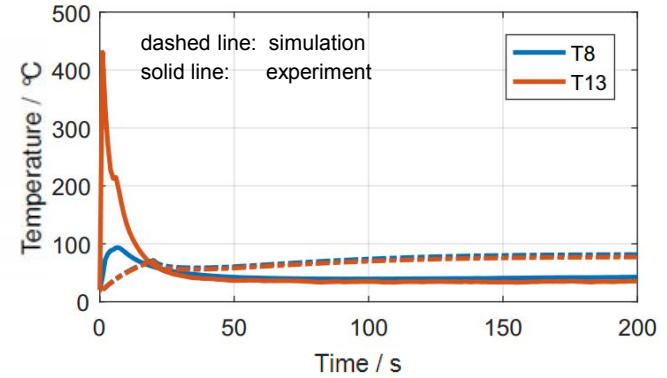
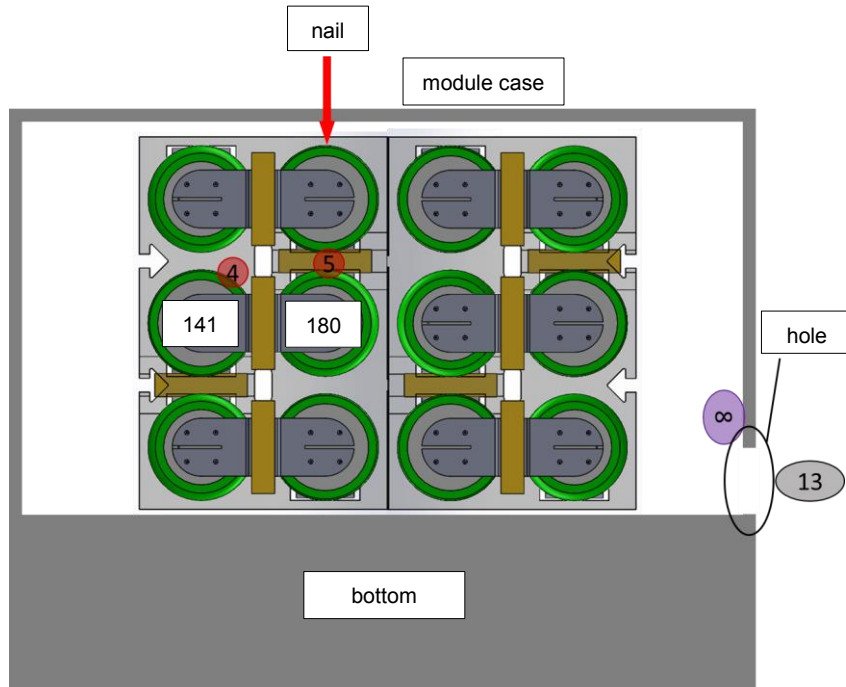
FEM-model of lithium-ion battery module



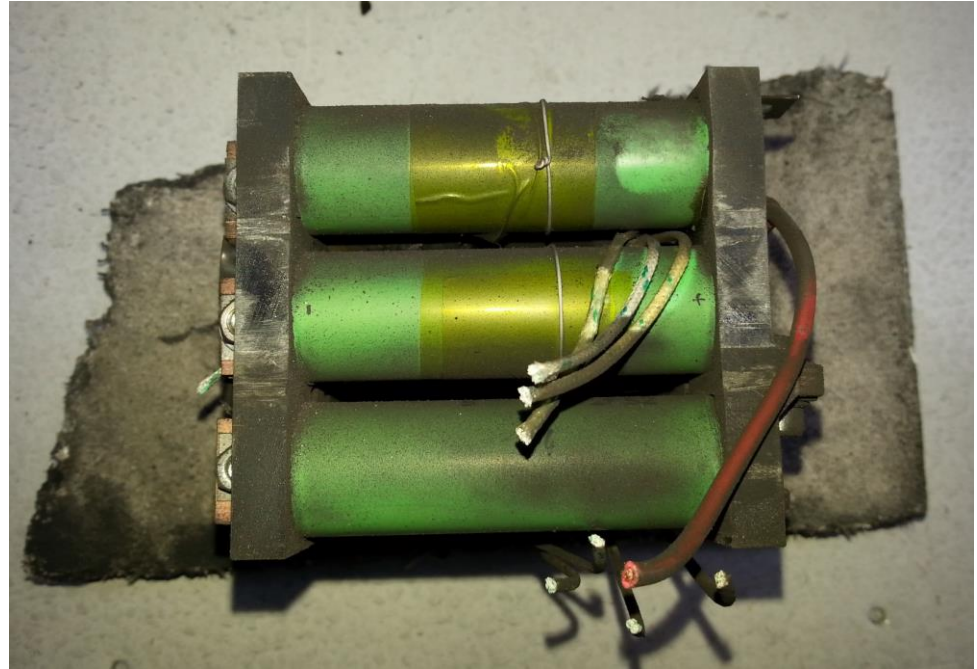
Simulation: 12s1p module nail penetration of a single cell



Experiment: 12s1p module nail penetration of a single cell



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Experiment: 12s1p module nail penetration of a single cell



Results:

- Conductive thermal model approach cannot describe the TR-P of experiment
- Heat release of gas and direction of gas flow have a strong influence on TR-P

➡ Implementing gas flow / venting necessary

➡ CFD model

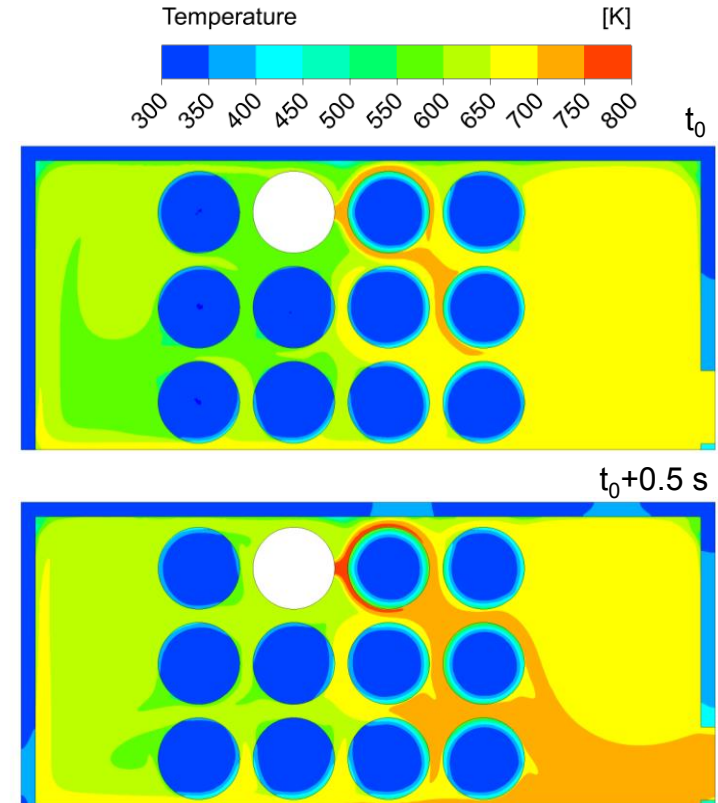
1st CFD model approach for TR propagation

Model assumptions:

- 2D, k- ϵ model for turbulence
- $v_{\text{fluid,inlet}} = 215 \text{ m/s}$ [Coman P.T., JoP 307 (2016)]
- $T_{\text{fluid,inlet}} = \text{measured data}$
- Vent position extracted from module experiment
- Gas = similar specs like hydrogen

Neglected:

- Cell connector \rightarrow heat transfer via solid bodies
- Heat generation of nail penetrated cell



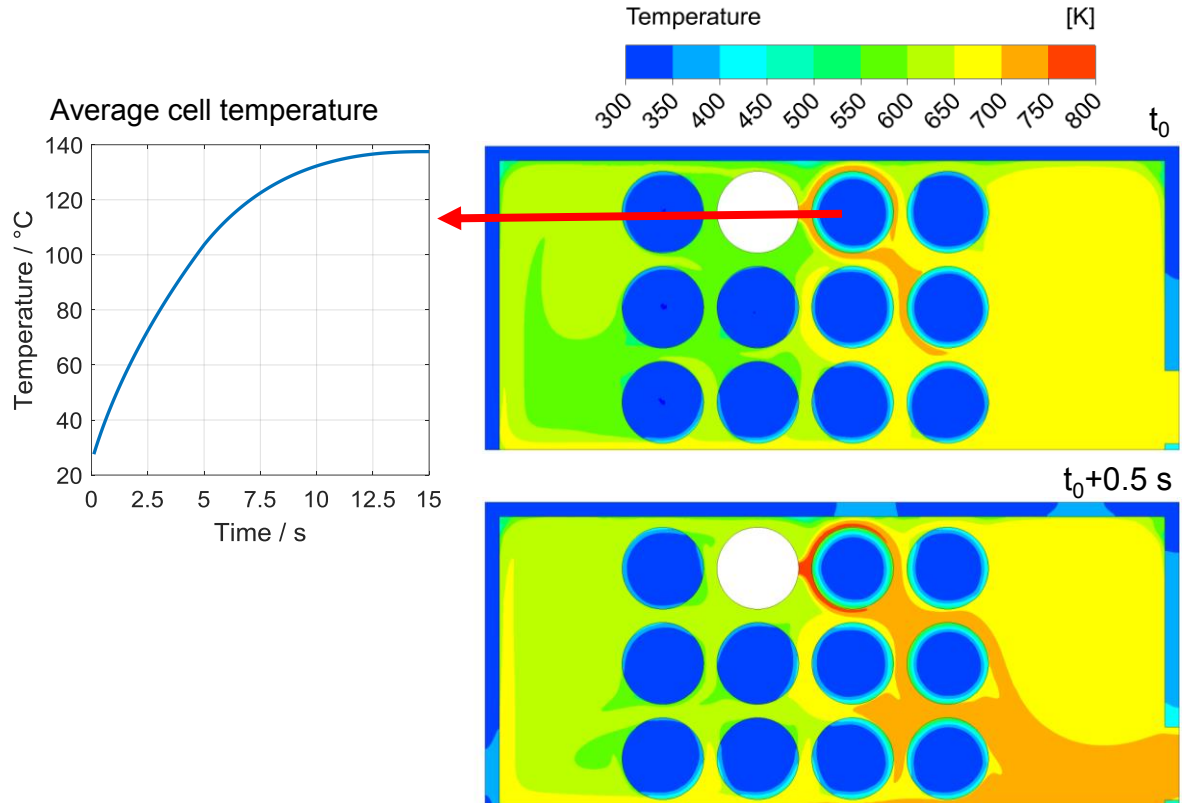
1st CFD model approach for TR propagation

Results:

- $t > 0$; $T_{\text{fluid}} \gg T_{\text{initial}}$
- $t > 0$; $T_{\text{outlet}} \gg T_{\text{initial}}$
- $t > 0$; $T_{\text{cells}} \gg T_{\text{initial}}$
- Direction of gas flow

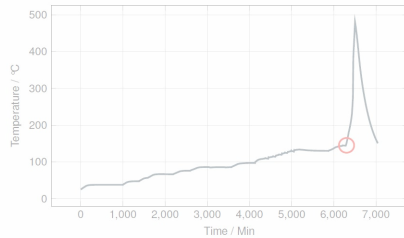
Problem:

- 3D CFD simulation is time consuming
- Uncertain input parameters
- Experiment (nail penetration) not suitable

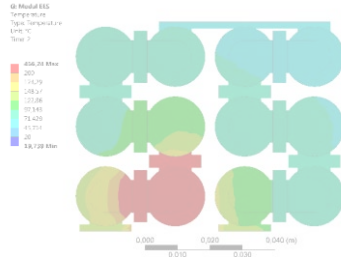


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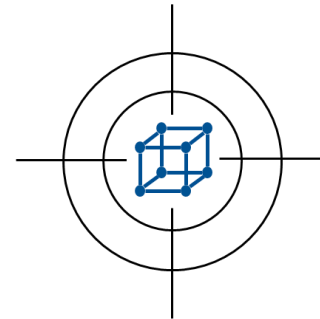
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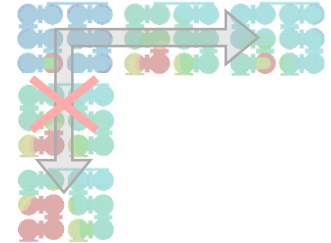
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Limitations of
accurate modelling
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Mitigation strategies
of battery TR-P



Limitations of accurate of modelling TR-P

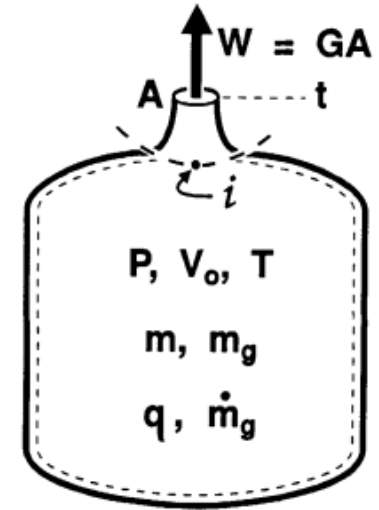
General:

- Temperature dependent material properties for $> 100\text{ }^{\circ}\text{C}$ not available
- 3D-CFD simulation is time consuming

Understanding and describing venting by a model needs accurate data on

- Vent size and vent position
- Heat release, mass rate, velocity of vented gas

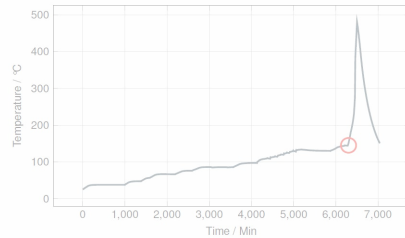
➔ Missing information makes it hard to simulate TR-P with simplified thermal models, especially if venting gas occurs



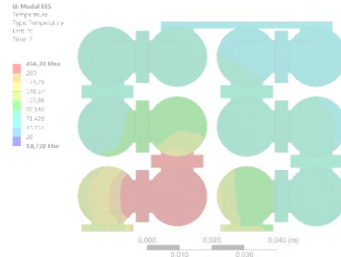
venting model
[Leung J.C., AiChE, Vol. 38, No. 5, 1992]

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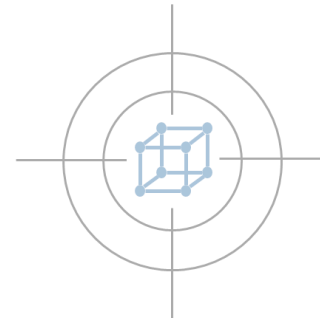
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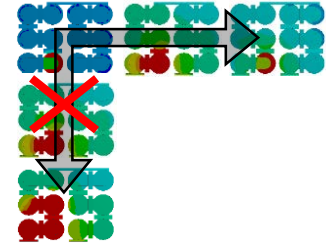
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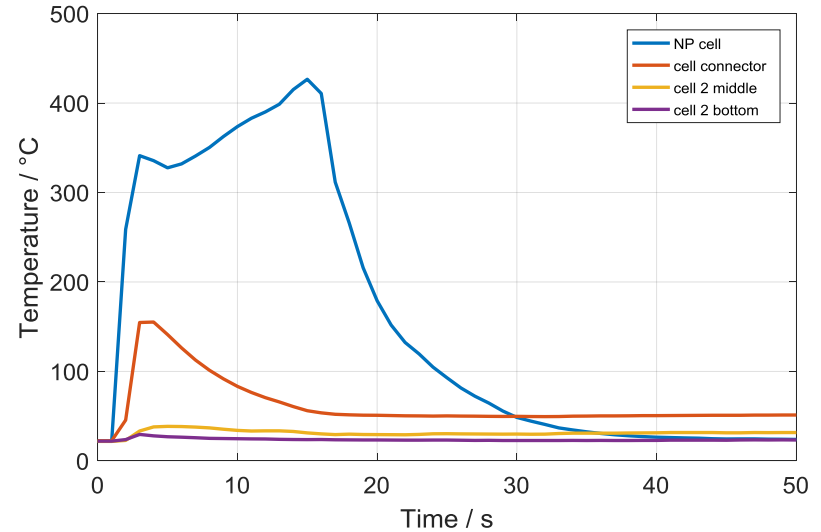
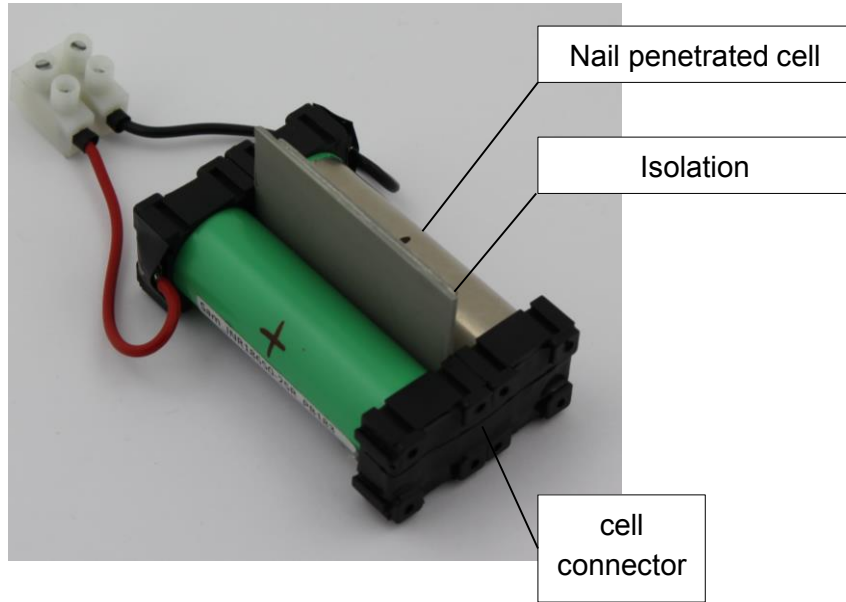
Limitations of
accurate modelling
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Mitigation strategies
of battery TR-P



Experimental results of a 2s1p module for nail penetration of a single cell



- In the beginning rapid temperature increase of cell connector due to opened burst
- Isolation prevents TR-P

Mitigation strategies of battery TR-P

Ideas:

- Increase **trigger temperature** of thermal runaway (by changing separator)
PE, PP/PE/PP, PE-based with ceramic coating
- Use of **electrical fuses** → reduce released electric energy during internal short circuit
e.g. Tesla uses wire bonding which act as fuses too
- Increase **heat dissipation** of battery module
by lower ambient temperature or increased thermal capacity e.g. phase-change-material
- Additional **thermal resistance** between cells
- **Protect** neighbor cells **of venting gas** (define predetermined breaking points on cell)

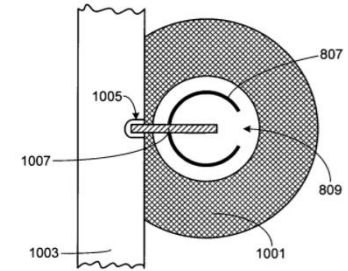


FIG. 10

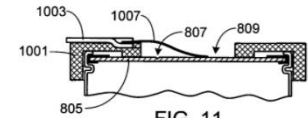


FIG. 11

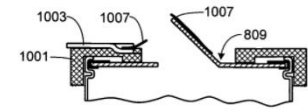
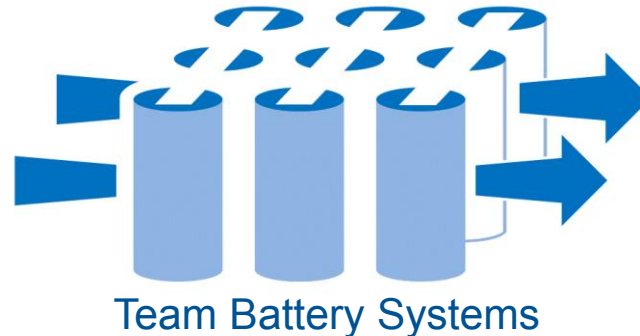


FIG. 12

[Tesla Motors Inc., 2010, patent US8241772 B2]

Summary

- Venting gas during TR can have a strong influence on TR-P inside a battery module
 - Conductive thermal models cannot represent TR-P if venting occurs inside a (half-)closed battery module
 - Approach to implement heat transfer by gas looks promising and shows qualitativ the TR-P behavior
- ➡ More information on physical properties and behavior of venting gas during TR are necessary
- ➡ Standardised abuse testing regarding TR-P by venting gas is required



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