

Ch3. Crosstalk

2021 Quiz 3.

3. Figure 3 shows two parallel signal lines above a ground plane with the termination resistance $R = 50 \Omega$. Both signal lines are of equal length of 100 cm. One end of the aggressor line is connected to a sinusoidal signal source of 5 V at 1 MHz. The self and mutual distributed inductances and capacitances are given in Table 1.

(a) Calculate the near-end (NE) and far-end (FE) signal voltages (in mV) due to capacitive crosstalk.

(10 marks)

(a) Calculate the NE and FE signal voltages (in mV) due to inductive crosstalk.

(10 marks)

(a) What are the resultant NE and FE signals (in mV) due to both capacitive and inductive crosstalk?

(5 marks)

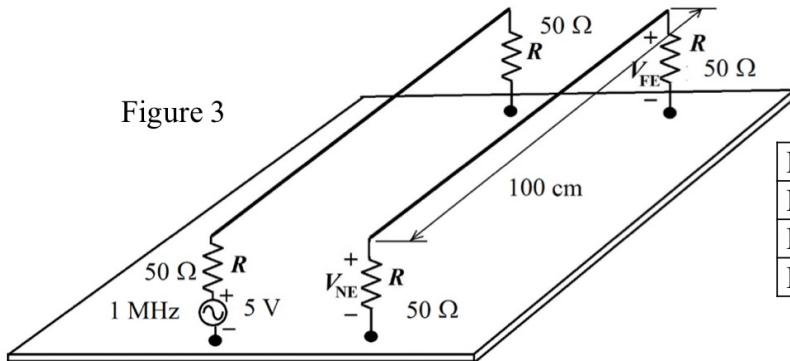


Table 1

Distributed self-capacitance	150 pF/m
Distributed mutual-capacitance	20 pF/m
Distributed self-inductance	300 nH/m
Distributed mutual-inductance	50 nH/m

(a) Capacitive crosstalk :

$$\frac{V_{NE}}{V_G} = \frac{V_{FE}}{V_G} = \frac{j\omega C_{12} R}{4 + j\omega R(4(C_{12} + C) - \omega^2 R^2 C^2 (1 + \frac{2C_{12}}{C}))}$$

At 1 MHz, the $\lambda = \frac{3 \times 10^8}{10^6} = 300 \text{ m}$

the length of conductor (1m) $< \frac{\lambda}{10}$ (30 m), the parallel circuit can be modeled as lumped model.

$$C_{12} = 20 \text{ pF/m} \times 1 \text{ m} = 20 \text{ pF}$$

$$C = 150 \text{ pF/m} \times 1 \text{ m} = 150 \text{ pF}$$

$$\omega = 2\pi f = 6.28 \times 10^6 \text{ rad/s}$$

$$j\omega C_{12} = j125.6 \times 10^{-6} \text{ S}$$

$$j\omega C = j942 \times 10^{-6} \text{ S}$$

$$\begin{aligned} \text{Therefore } \frac{V_{NE}}{V_G} &= \frac{50 \Omega \times j125.6 \times 10^{-6} \text{ S}}{4 + j4 \times 50 \Omega (1067.6 \times 10^{-6} \text{ S}) - (50) \times (942 \times 10^{-6})^2 (1 + 0.2)} \\ &= \frac{j6.28 \times 10^{-3}}{4 + j0.214 - 2.817 \times 10^{-3}} \\ &\approx \frac{j0.00628}{4} = j0.00157 \end{aligned}$$

$$\text{Hence, } V_{NE, \text{cap}} = V_{FE, \text{cap}} = 5 \text{ V} \times j0.00157 = 7.85 \text{ mV}$$

$$(b) L = 300 \text{ nH}/\text{m} \times 1\text{m} = 300 \text{ nH} \quad \rightarrow \quad WL = 1.884 \text{ J}_2$$

$$M_{12} = 50 \text{ nH}/\text{m} \times 1\text{m} = 50 \text{ nH} \quad \rightarrow \quad WM_{12} = 0.314 \text{ J}_2$$

$$\frac{V_{NE, \text{ind}}}{V_G} = -\frac{V_{FE, \text{ind}}}{V_G} = \frac{jwM_2R}{4R^2 + j4wRL - w^2(L^2 - M_2^2)}$$

$$= \frac{j50 \Omega \times 0.314 \Omega}{4 \times 50^2 + j4 \times 50 \times 1.884 - 1.884^2 + 0.314^2}$$

$$\approx \frac{j15.7}{10000 + j376.8} \approx \frac{j15.7}{10^4} = j0.00157$$

$$\Rightarrow V_{NE, \text{ind}} = -V_{FE, \text{ind}} = j7.85 \text{ mV}$$

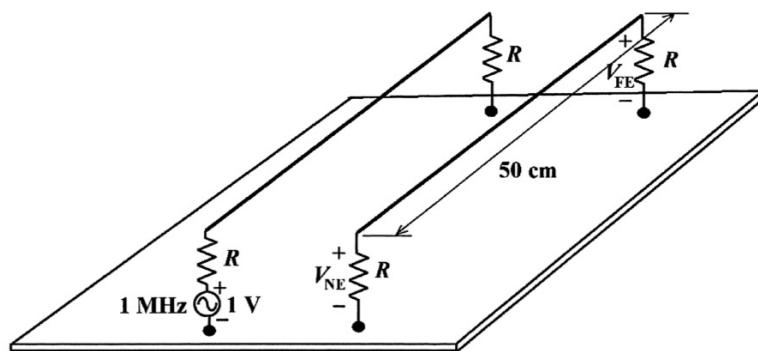
$$V_{FE, \text{IND}} = -j7.85 \text{ mV}$$

(c)

$$V_{NE} = V_{NE, \text{cap}} + V_{NE, \text{ind}} = j15.7 \text{ mV}$$

$$V_{FE} = V_{NE, \text{cap}} + V_{FE, \text{ind}} = 0$$

2. (a) Figure 3 on page 3 shows two parallel signal lines that share the same ground plane. The measured distributed parameters of the two signal lines are given in Table 1 on page 3. All the termination resistance $R = 100 \Omega$. The near-end and far-end crosstalk signal voltages of the victim line are denoted as V_{NE} and V_{FE} , respectively.
- Calculate V_{NE} and V_{FE} due to capacitive coupling. (4 Marks)
 - Repeat part (i) for inductive coupling. (4 Marks)
 - Calculate resultant V_{NE} and V_{FE} due to both capacitive and inductive couplings. (2 Marks)

**Figure 3****Table 1**

Distributed self-capacitance	30 pF/m
Distributed mutual-capacitance	5 pF/m
Distributed self-inductance	50 nH/m
Distributed mutual-inductance	5 nH/m

(i) At 1 MHz, the wavelength is $\frac{3 \times 10^8}{10^6} = 300 \text{ m}$
 The length of conductor (0.5 m) $< \frac{1}{10}$ (30 m), hence, the lumped model can be applied.

$$C_{12} = 5 \text{ pF/m} \times 0.5 \text{ m} = 2.5 \text{ pF}$$

$$C = 30 \text{ pF/m} \times 0.5 \text{ m} = 15 \text{ pF}$$

$$wC_{12} = 2\pi \times 10^6 \times 2.5 \times 10^{-12} = 15.7 \times 10^{-6} \text{ S}$$

$$wC = 2\pi \times 10^6 \times 15 \times 10^{-12} = 94.25 \times 10^{-6} \text{ S}$$

$$\begin{aligned} \frac{V_{NE, CAP}}{V_G} &= \frac{V_{FE, CAP}}{V_G} = \frac{jwC_{12}R}{4 + j4wR(C_{12} + C) - w^2R^2C(1 + \frac{2C_{12}}{C})} \\ &= \frac{j1.57 \times 10^{-3}}{4 + j0.044 - 1.18 \times 10^{-4}} \\ &\approx \frac{j1.57 \times 10^{-3}}{4} = j3.925 \times 10^{-4} \Rightarrow V_{NE, CAP} = V_{FE, CAP} = 0.385 \text{ mV} \end{aligned}$$

$$\begin{aligned}
 (ii) \quad M_{12} &= 5 \text{nH/m} \times 0.5 \text{m} = 2.5 \text{nH} \\
 L &= 50 \text{nH/m} \times 0.5 \text{m} = 25 \text{nH} \\
 wM_{12} &= 2\pi \times 10^6 \times 2.5 \times 10^{-9} = 1.571 \times 10^{-2} \text{JL} \\
 wL &= 2\pi \times 10^6 \times 25 \times 10^{-9} = 0.1571 \text{JL}
 \end{aligned}$$

$$\begin{aligned}
 \frac{V_{NE, IND}}{V_G} &= -\frac{V_{FE, IND}}{V_G} = \frac{jwM_{12}R}{4R^2 + j4wRL - w^2(L^2 - M_{12}^2)} \\
 &= \frac{j1.571}{4 \times 10^4 + j62.84 - 0.0244} \\
 &\approx j3.925 \times 10^{-5}
 \end{aligned}$$

$$\begin{aligned}
 V_{NE, IND} &= j3.925 \times 10^{-5} \times 1V = j0.03925 \text{mV} \\
 V_{FE, IND} &= -V_{NE, IND} = -j0.03925 \text{mV}
 \end{aligned}$$

$$(iii) \quad V_{NE} = V_{NE, CAP} + V_{NE, IND} = j0.43175 \text{mV}$$

$$V_{FE} = V_{FE, CAP} + V_{FE, IND} = j0.35325 \text{mV}$$

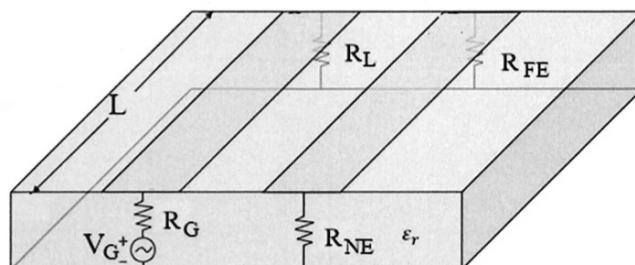
2. (a) Figure 3 on page 3 shows two parallel microstrip lines of length $L = 10 \text{ cm}$ on a printed circuit board (PCB). The substrate material of the PCB has relative permittivity $\epsilon_r = 4.5$. The measured distributed parameters of the two parallel microstrip lines are given in Table 1 on page 3. The aggressor line is driven by a 10 MHz sinusoidal signal source with a source voltage $V_G = 5 \text{ V}$ and a source resistance $R_G = 1 \text{k}\Omega$, which is terminated by a load resistance $R_L = 1 \text{k}\Omega$. Both the near-end and the far-end of the victim line are terminated by amplifiers with input resistance $R_{NE} = R_{FE} = 1 \text{k}\Omega$.

- (i) Compute the near-end and the far-end signal voltages due to capacitive and inductive crosstalk.

(7 Marks)

- (ii) If either the near-end or far-end signal voltage due to crosstalk exceeds 20 mV, it will interfere with the operation of the amplifier. Do you expect an interference issue?

(3 Marks)

**Figure 3****Table 1**

Distributed self-capacitance	30 pF/m
Distributed mutual-capacitance	5 pF/m
Distributed self-inductance	50 nH/m
Distributed mutual-inductance	5 nH/m

(a) At 10 MHz, the wavelength is $\lambda = \frac{C}{f\sqrt{\epsilon_r\mu_r}} = \frac{3 \times 10^8}{10\sqrt{4.5 \times 1}} = 14.14 \text{ m}$
The length of the conductor (0.1 m) < $\frac{\lambda}{10}$ (1.414 m), the lump model can be applied.

$$C_{12} = 5 \text{ pF/m} \times 0.1 \text{ m} = 0.5 \text{ pF}$$

$$M_{12} = 5 \text{ nH/m} \times 0.1 \text{ m} = 0.5 \text{ nH}$$

$$V_{NE, CAP} = \frac{I_N}{2} \cdot R_{NE} = \frac{1}{2} \times \frac{jw C_{12} V_G R_L}{R_G + R_L} \times R_{NE} = \frac{1}{2} \times \frac{j \times 2\pi \times 10^7 \times 0.5 \times 10^{-12} \times 5 \text{ V} \times 10^3}{2 \times 10^3} \times 10^3$$

$$= j39.27 \text{ mV}$$

$$V_{FE, CAP} = V_{NE, CAP} = j39.27 \text{ mV}$$

$$V_{NE, IND} = \frac{V_N}{2} = \frac{jw M_{12} V_G}{2 \times (R_G + R_L)} = \frac{j \times 2\pi \times 10^7 \times 0.5 \times 10^{-12} \times 5 \text{ V}}{2 \times 2 \times 10^3} = j0.03927 \text{ mV}$$

$$V_{FE, IND} = -V_{NE, IND} = -j0.03927 \text{ mV}$$

$$V_{NE} = V_{NE, CAP} + V_{NE, IND} = j(39.27 + 0.03927) \approx j39.27 mV$$

$$V_{FE} = V_{FE, CAP} + V_{FE, IND} = j(39.27 - 0.03927) \approx j39.27 mV$$

(ii) It exists an interference issue. Because $|V_{NE}| = 39.27 mV > 20 mV$.