

# An Introduction to Radio Interferometry

1-5 Antenna response function and the Jy/beam unit

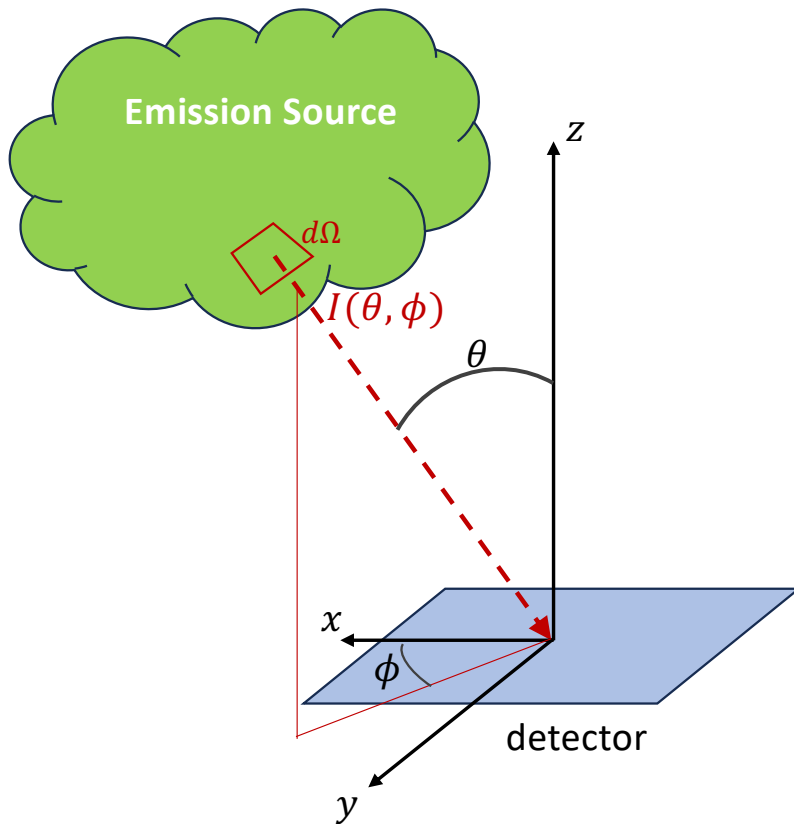


You can find relevant material  
on my personal webpage

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Flux density (incoming energy per unit time, frequency, and area) received by a CCD pixel:

$$F_\nu = \int I_\nu(\theta, \phi) \cos \theta \, d\Omega$$



Flux density (incoming energy per unit time, frequency, and area) received by a CCD pixel:

$$F_\nu = \frac{1}{2} \int I_\nu(\theta, \phi) \cos \theta d\Omega$$

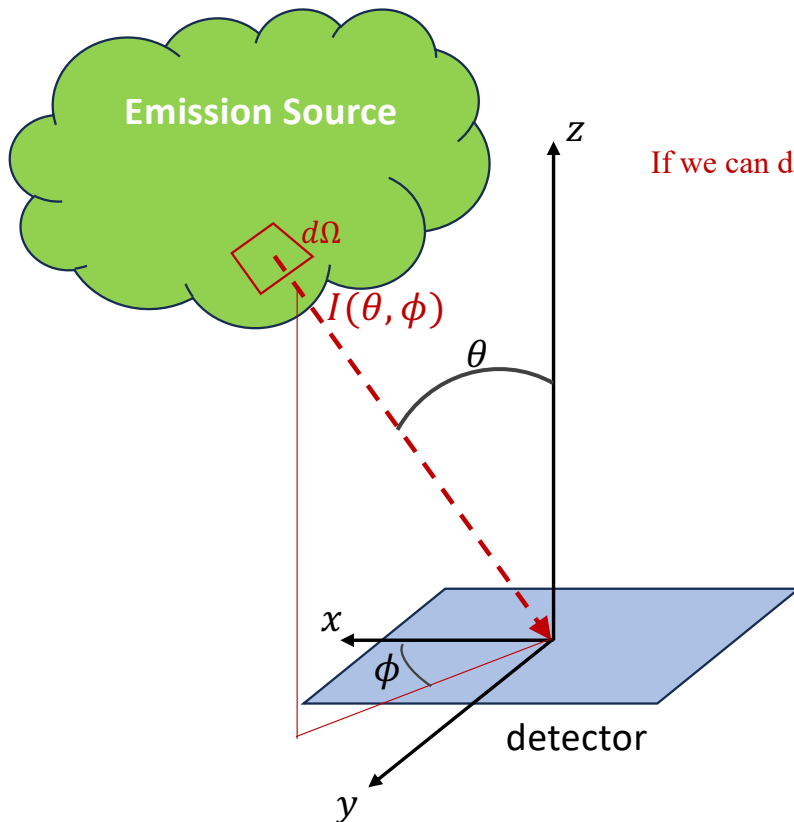
If we can detect one of the two polarizations

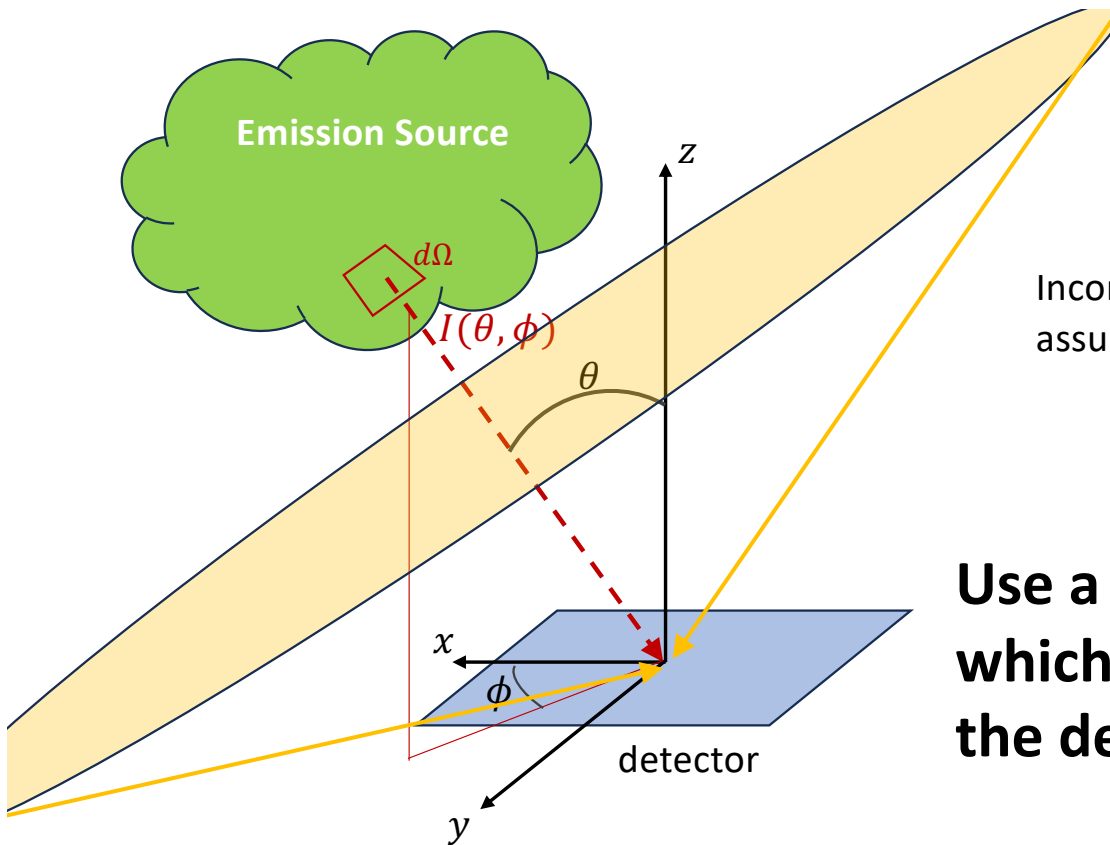
Incoming energy per unit time and frequency (i.e., power if assuming monochromatic light) received by a CCD pixel:

$$P_\nu = \frac{1}{2} A \int I_\nu(\theta, \phi) \cos \theta d\Omega$$

surface area of the detector

We receive more power in a unit of time (i.e., our device is more sensitive to weak signals) when the effective surface area of the detector is larger.



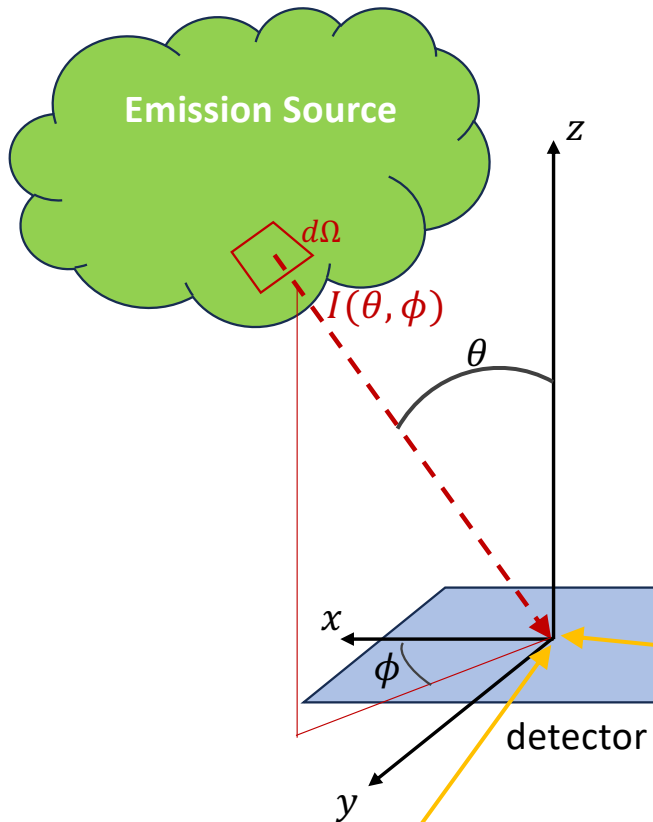


Incoming energy per unit time and frequency (i.e., power if assuming monochromatic light) received by a CCD pixel:

$$P_\nu = \frac{1}{2} A_e \int I_\nu(\theta, \phi) \cos \theta d\Omega$$

**Use a lense to collect light from a larger area, which increases the effective surface area of the detector**

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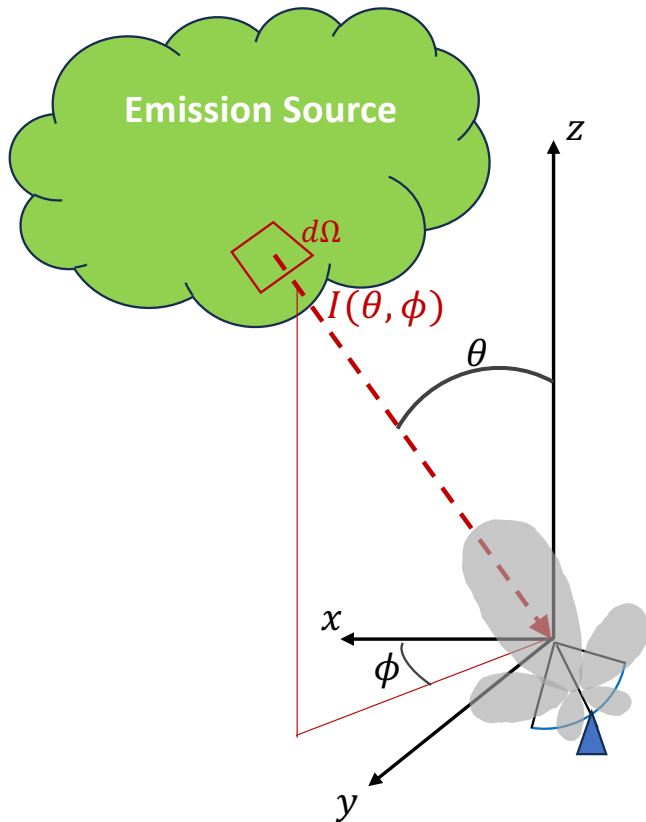


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**Use a reflector to collect light from a larger area, which increases the effective surface area of the detector**

We receive more power in a unit of time (i.e., our device is more sensitive to weak signals) when the effective surface area of the detector is larger.



Incoming energy per unit time and frequency (i.e., power if assuming monochromatic light) received by a CCD pixel:

$$P_v = \frac{1}{2} A_e \int I_v(\theta, \phi) \cos \theta \underbrace{P(\theta, \phi)}_{\text{Response function of the observing device.}} d\Omega$$

Response function of the observing device.

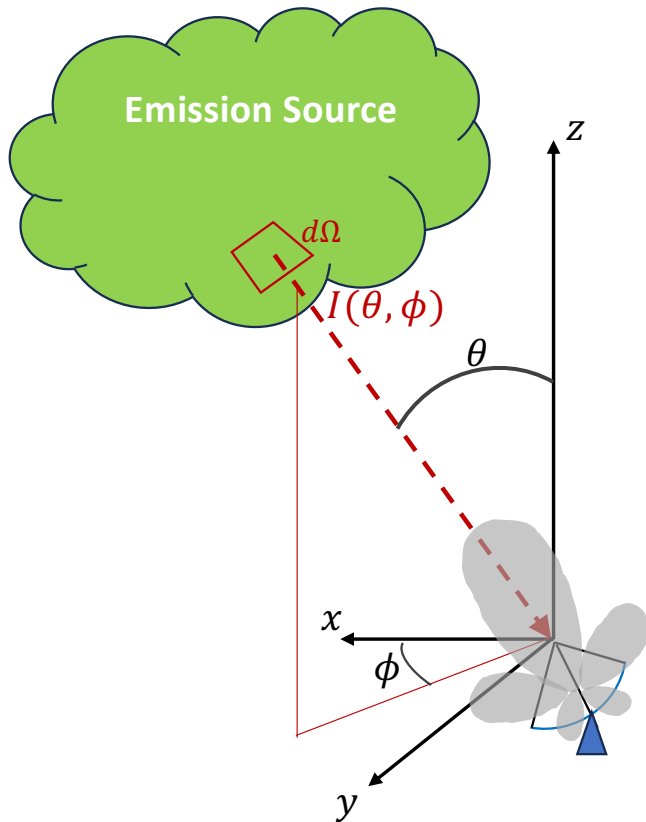
Normalization: peak = 1.0 (i.e., 100% of incoming intensity can be detected.)

**The optics determines the response function.**

**With a telescope, we:**

- (1) Receive light from smaller solid angle(s)**  
(usually, provides better angular resolution)
- (2) Have a bigger collecting area**

We receive more power in a unit of time (i.e., our device is more sensitive to weak signals) when the effective surface area of the detector is larger.



Incoming energy per unit time and frequency (i.e., power if assuming monochromatic light) received by a CCD pixel:

$$P_\nu = A_e \int I_\nu(\theta, \phi) \cos \theta P(\theta, \phi) d\Omega \equiv k T_A$$

Boltzmann constant

Antenna temperature

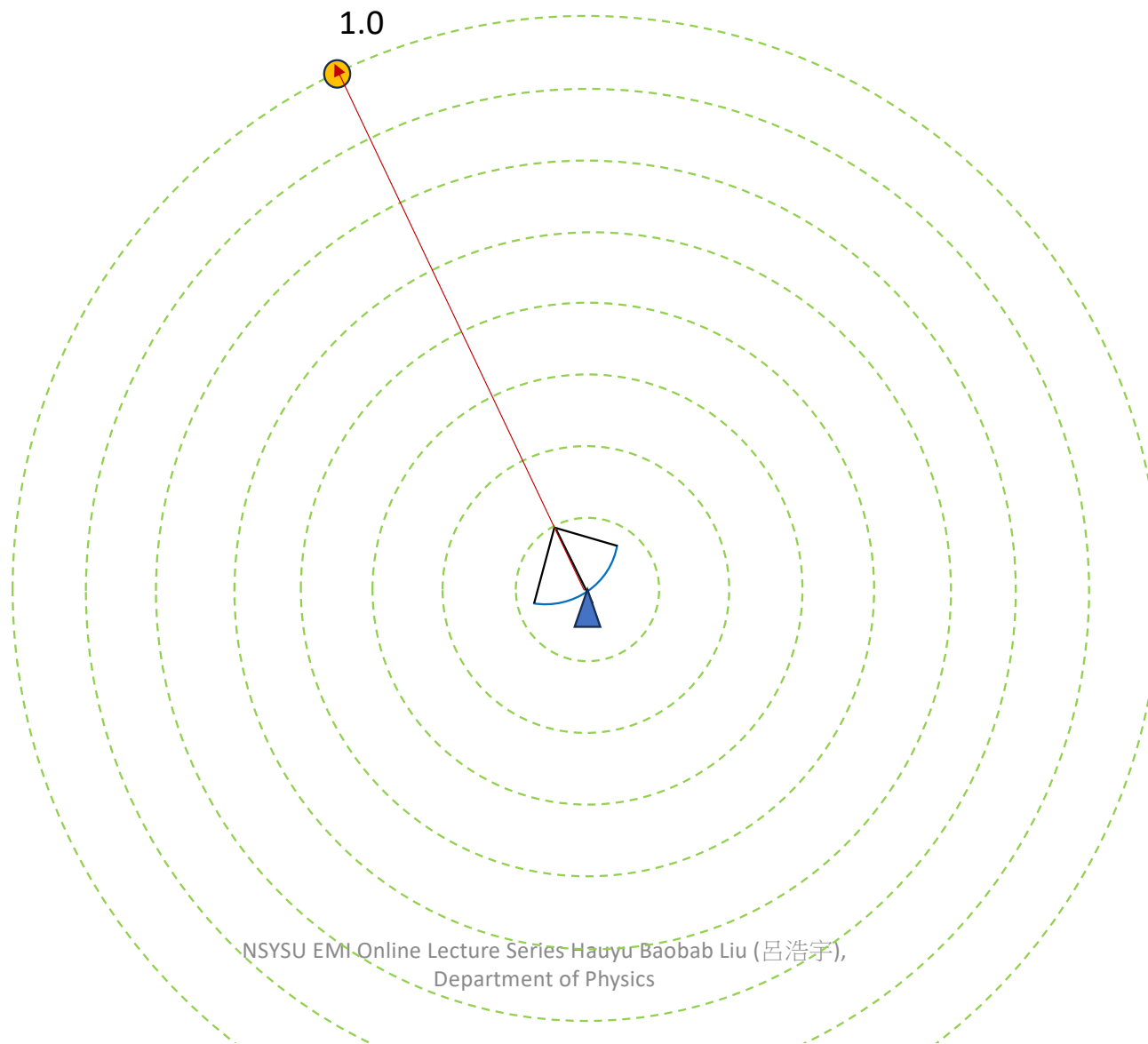
Response function of the observing device.

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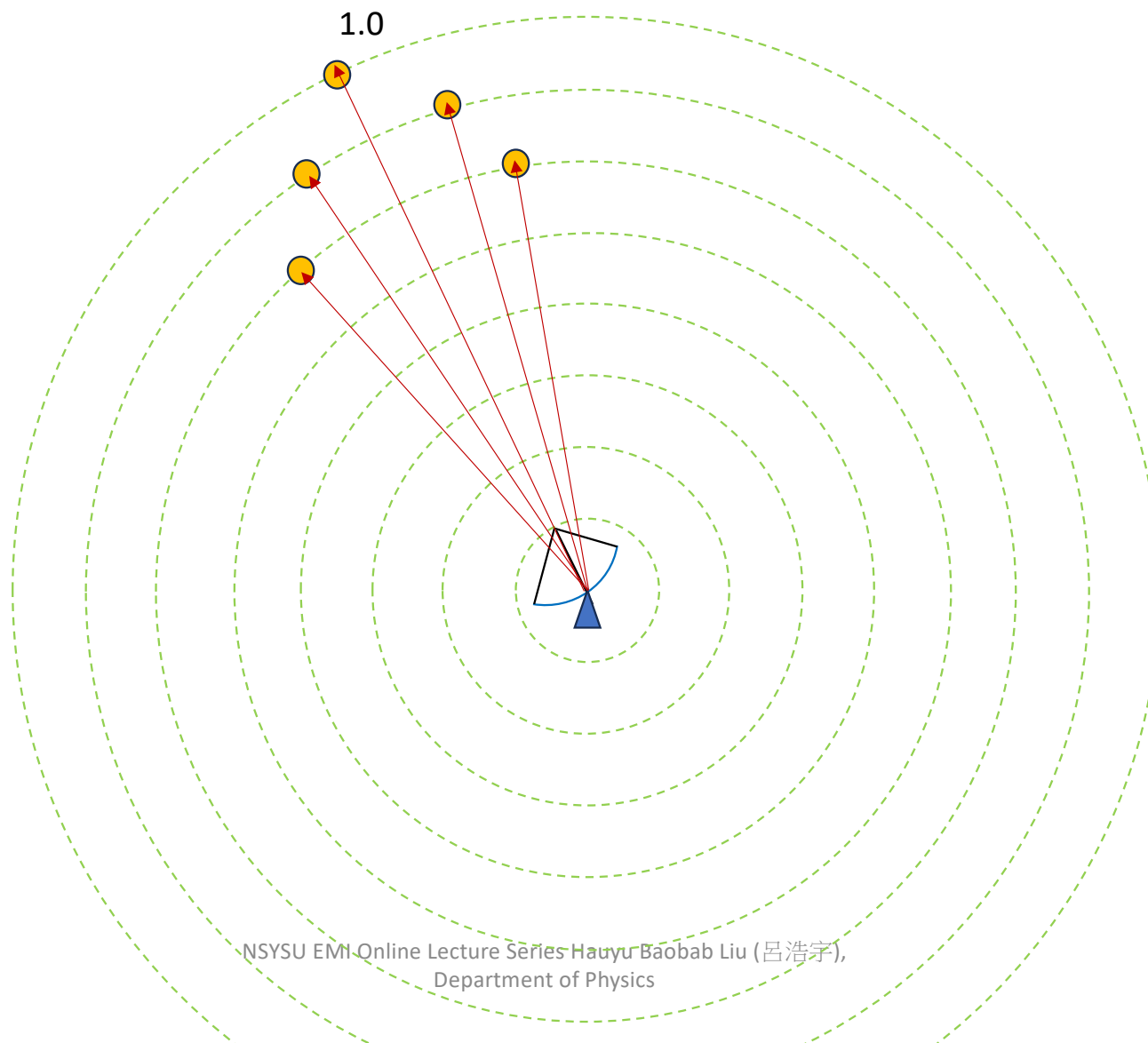
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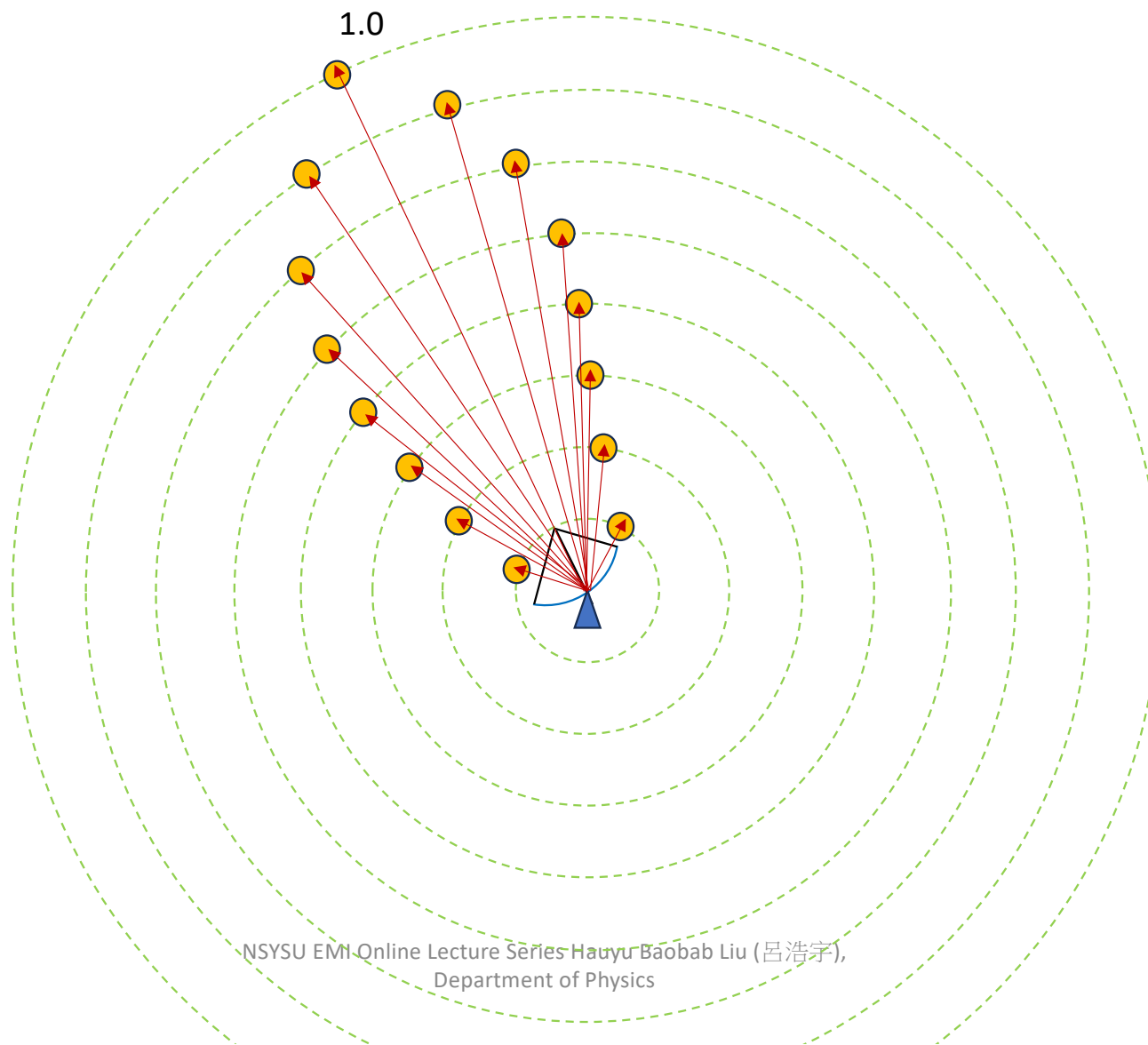
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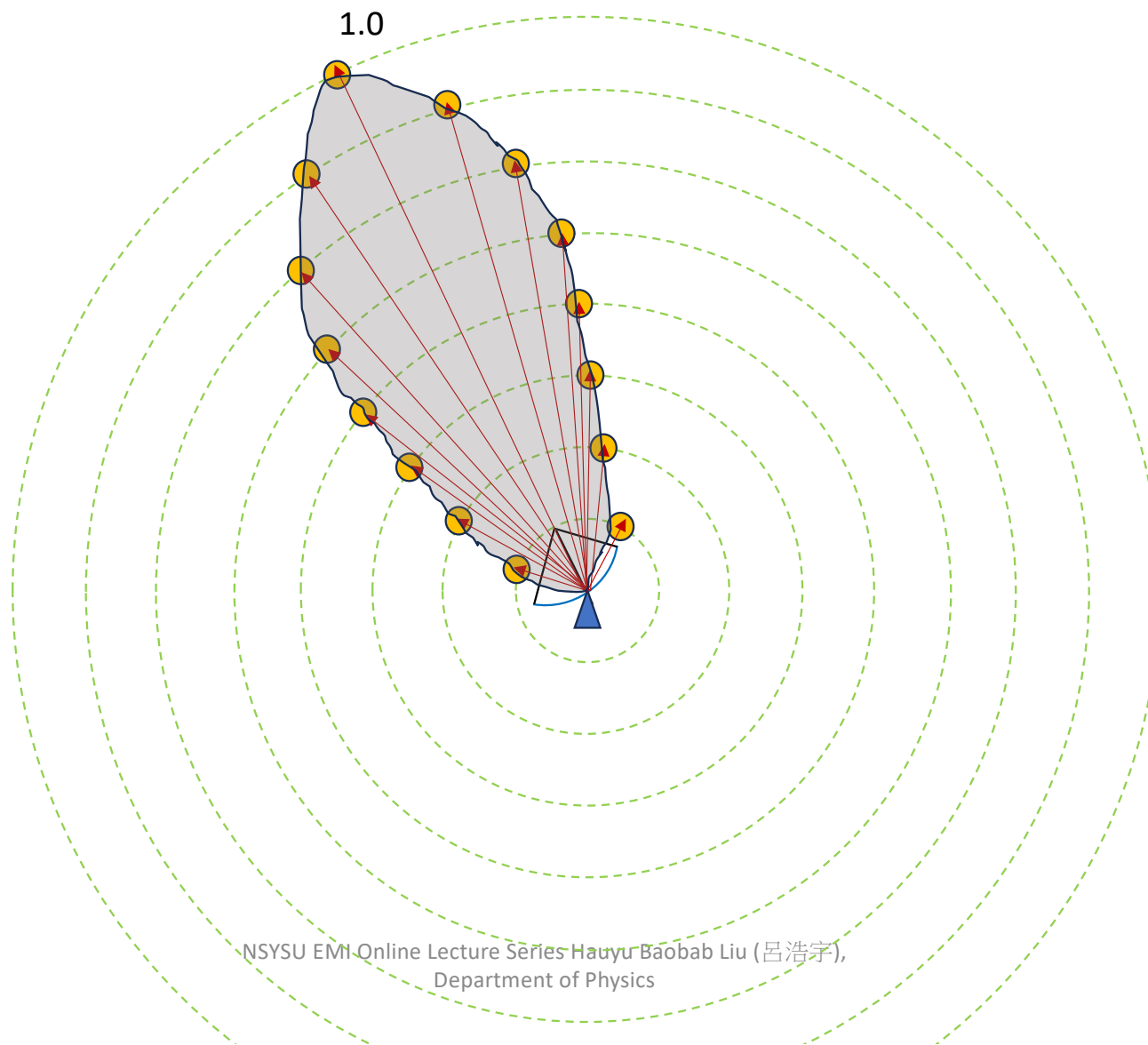
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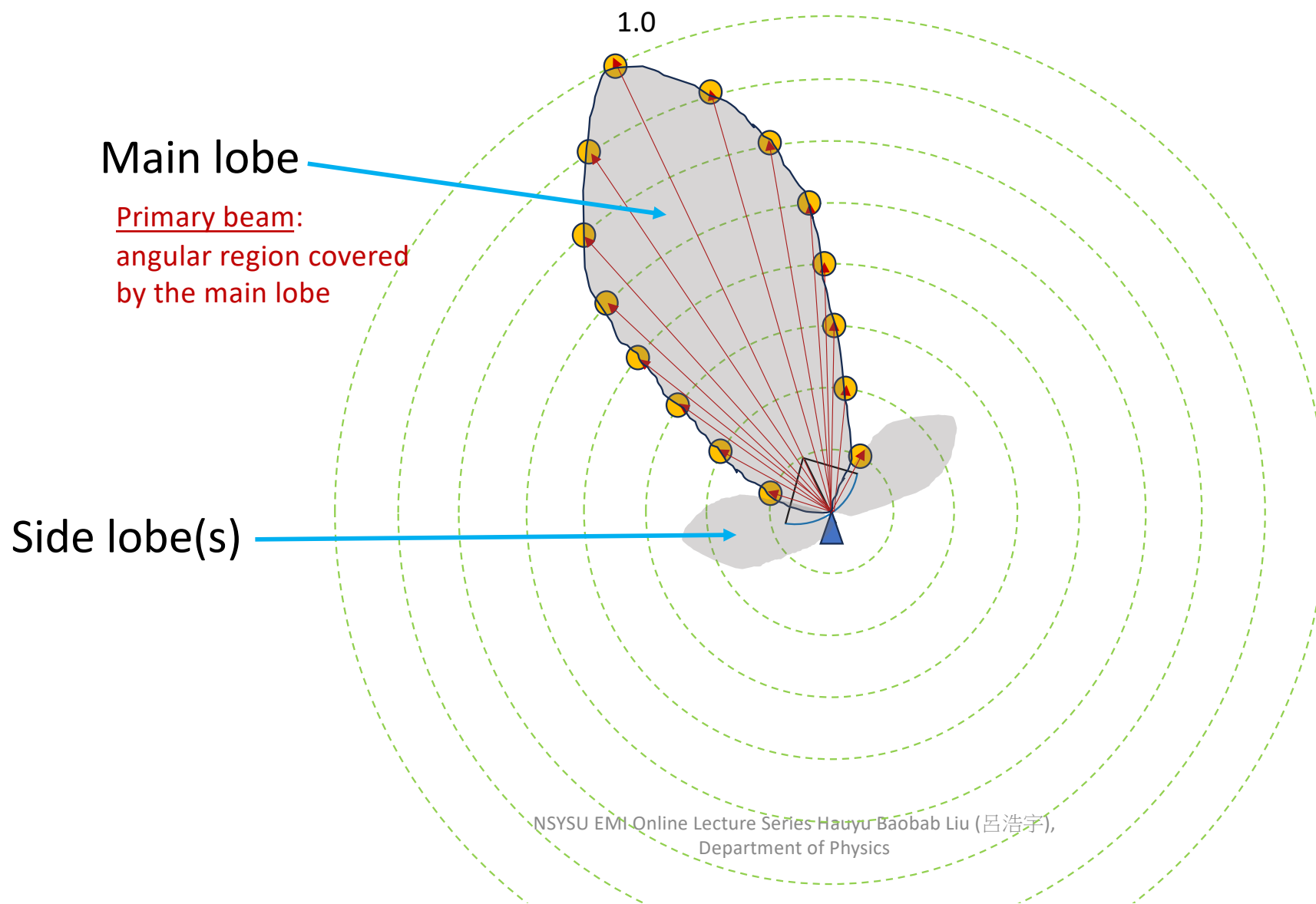


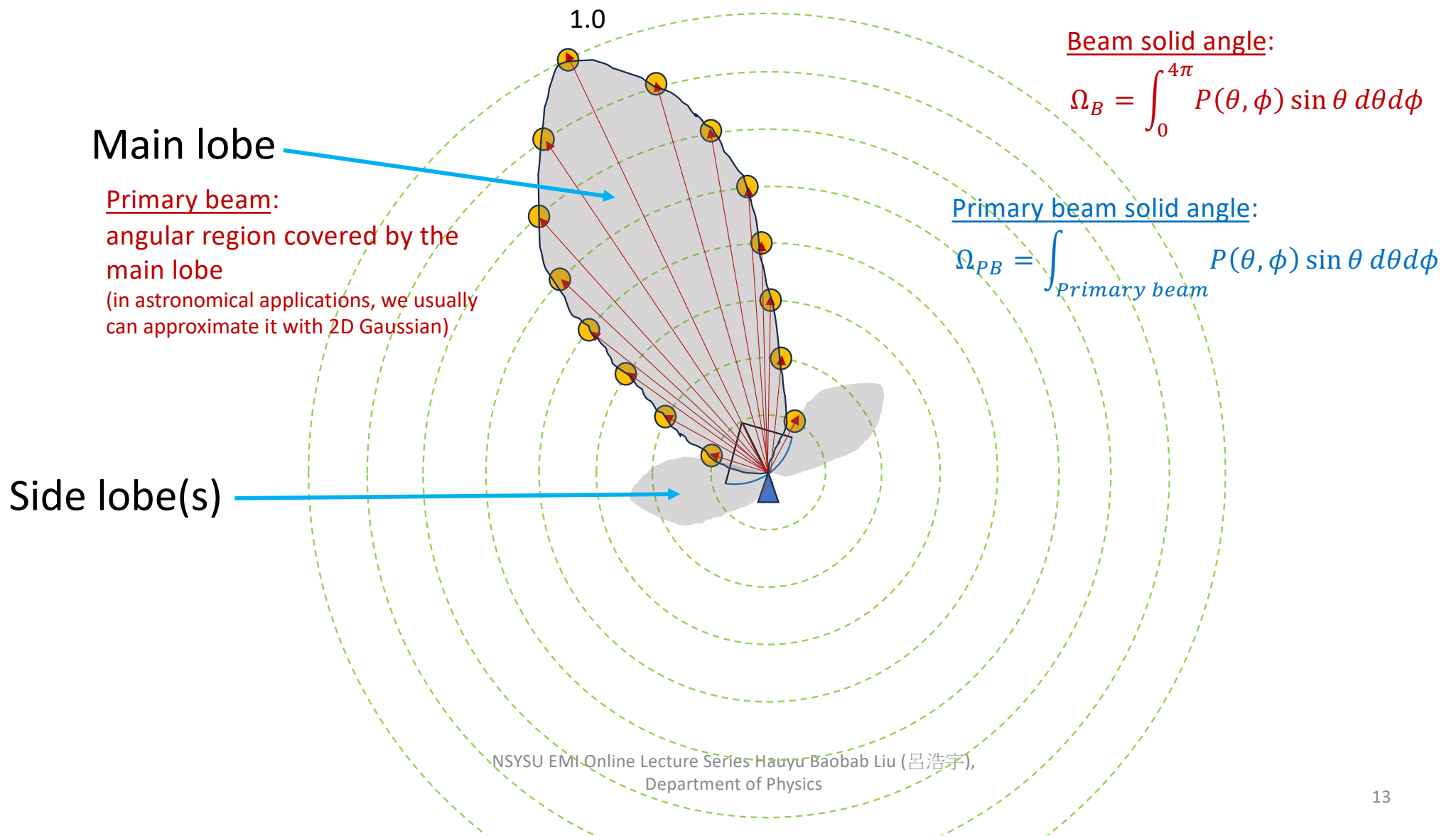












## Example: 2D Gaussian beam

with Full width at half maximum (FWHM)  $\theta_a$  and  $\theta_b$  in the major and minor axes  
(the relation between Gaussian standard deviation  $\sigma$  and FWHM  $\theta$

$$\theta = 2\sqrt{2\ln 2}\sigma \sim 2.35\sigma$$

$$P = e^{\left(\frac{-\xi^2}{2\sigma_a^2} + \frac{-\eta^2}{2\sigma_b^2}\right)} = e^{\left[4\ln 2 \left(\frac{-\xi^2}{(2\sqrt{\ln 2}\sigma_a)^2} + \frac{-\eta^2}{(2\sqrt{\ln 2}\sigma_b)^2}\right)\right]} = e^{\left[4\ln 2 \left(\frac{-\xi^2}{(\theta_a)^2} + \frac{-\eta^2}{(\theta_b)^2}\right)\right]}$$

$$\Omega_B = \int e^{\left[4\ln 2 \left(\frac{-\xi^2}{(\theta_a)^2} + \frac{-\eta^2}{(\theta_b)^2}\right)\right]} d\xi d\eta = \frac{\pi\theta_a\theta_b}{4\ln 2}$$

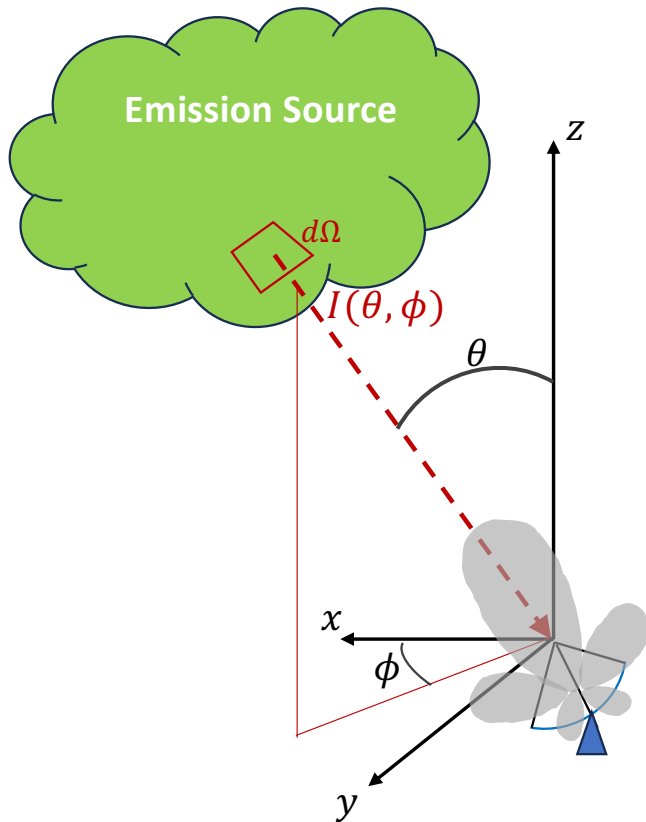
$$\int_{-\infty}^{\infty} e^{-ax^2} dx = \sqrt{\frac{\pi}{a}}$$

Beam solid angle:

$$\Omega_B = \int_0^{4\pi} P(\theta, \phi) \sin \theta d\theta d\phi$$

Primary beam solid angle:

$$\Omega_{PB} = \int_{\text{Primary beam}} P(\theta, \phi) \sin \theta d\theta d\phi$$



Incoming energy per unit time and frequency (i.e., power if assuming monochromatic light) received by a CCD pixel:

$$P_v = A_e \int I_v(\theta, \phi) \cos \theta P(\theta, \phi) d\Omega \equiv k T_A$$

Boltzmann constant

Antenna temperature

Response function of the observing device.

Normalization: peak = 1.0 (i.e., 100% of incoming intensity can be detected.)

$$\frac{P_v}{A_e} = \int I_v(\theta, \phi) \cos \theta P(\theta, \phi) d\Omega \sim \int I_v(\theta, \phi) P(\theta, \phi) d\Omega$$

$\theta \rightarrow 0 \Rightarrow \cos \theta \rightarrow 1$

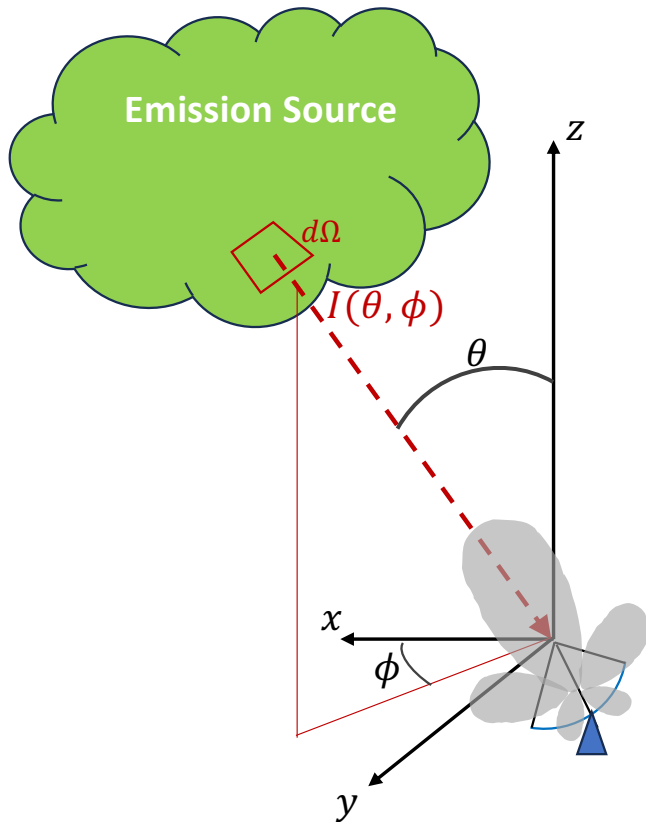
If  $I_v(\theta, \phi)$  is approximately constant over the beam

$$\frac{P_v}{A_e} = \sim I_v \int P(\theta, \phi) d\Omega = I_v \Omega_B = 1 \text{ Jy}$$

Solid angle in Sr unit

Flux density

Intensity in Jy Sr<sup>-1</sup> unit



Incoming energy per unit time and frequency (i.e., power if assuming monochromatic light) received by a CCD pixel:

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If  $I_v(\theta, \phi)$  is approximately constant over the beam

$$\frac{P_v}{A_e} = \sim I_v \int P(\theta, \phi) d\Omega = I_v \Omega_B = I_v^{Jy/beam} \times 1 = 1 Jy$$

Flux density

Intensity in Jy Sr<sup>-1</sup> unit

changing unit

Intensity in Jy beam<sup>-1</sup> unit

Solid angle in Sr unit

Solid angle in beam unit



# Converting $I_\nu^{Jy/beam}$ to $T_B$ (assuming 2D Gaussian beam)

Rayleigh-Jean limit  
(see lecture Unit 1-4)

$$\begin{aligned}
 T_B &= \frac{\lambda^2}{2k} I_\nu = \frac{\lambda^2}{2k} \left( \frac{F_\nu}{\Omega_B} \right) = \frac{\lambda^2}{2k} \left( \frac{F_\nu}{1 \text{ beam}} \right) \left( \frac{1 \text{ beam}}{\Omega_B} \right) \\
 &= \frac{\lambda^2}{2k} I_\nu^{Jy/beam} \frac{1 \text{ beam}}{\Omega_B} \quad \leftarrow \text{(see page 14 for the form of } \Omega_B) \\
 &= \frac{\lambda^2}{2 \cdot 1.38 \cdot 10^{-23}} I_\nu^{Jy/beam} \frac{4 \ln 2}{\pi \theta_a \theta_b} \\
 \Rightarrow T_B &= 3.2 \cdot 10^{22} \frac{\lambda^2}{\theta_b \theta_b} I_\nu^{Jy/beam}
 \end{aligned}$$

# The key information when we look up data archive

1. Target source name/coordinates
2. Ranges of observing frequency
3. Frequency resolution, angular resolution ( $\theta_a \times \theta_b$ ; *P. A.*)
4. The rms noise level in terms of  $T_B$  or  $I_\nu^{Jy/beam}$
5. Polarization (X, Y, R, L)
6. Maximum recoverable angular scale (only relevant in interferometric observations)

1. An observational device can be characterized with a response function  $P(\theta, \phi)$  that the maximum is normalized to 1.0. The form of  $P(\theta, \phi)$  is related to the geometry of the optics.

2. Solid angle of Gaussian primary beam:

$$\Omega_{PB} = \int_{Primary\ beam} P(\theta, \phi) \sin \theta d\theta d\phi = \frac{\pi \theta_a \theta_b}{4 \ln 2}$$

where  $\theta_a, \theta_b$  are the FWHM of the Gaussian in the major and minor axes.

3. The conversion between brightness temperature and the intensity in Jansky per beam unit:  $T_B = 3.2 \cdot 10^{22} \frac{\lambda^2}{\theta_b \theta_b} I_\nu^{Jy/beam}$