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Problem 1) Jacobians

1.4) In the given configuration, the rank of the spatial manipulator Jacobian is 5.

So in the given configuration, there is a kinematic singularity and J^s is not invertible.

Hence, we cannot find a set of joint velocities $\dot{\theta}$, that can move the end-effector in the way mentioned in the question.

$$v^s = J^s \dot{\theta}$$

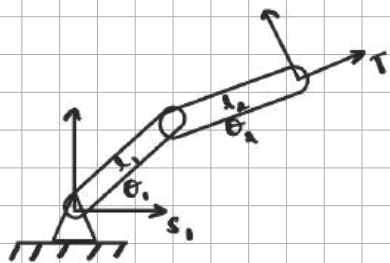
$$\Rightarrow \dot{\theta} = (J^s)^{-1} v^s$$

Since $\text{rank}(J^s) = 5 < 6$, J^s is not invertible \Rightarrow we cannot find a solution for $\dot{\theta}$ using inverse velocity kinematics.

In HW3, we had to write an optimization function and find a "numerical" solution to the problem as opposed to an analytical solution.

This is consistent with the conclusion from above, stating that a singularity does exist in the home configuration.

Problem 2) Statics



$$2.1) \quad g_{s,l_1} = \begin{bmatrix} \cos\theta_1 & -\sin\theta_1 & 0 & 0 \\ \sin\theta_1 & \cos\theta_1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$g_{l_1,l_2} = \begin{bmatrix} \cos\theta_2 & -\sin\theta_2 & 0 & l_1 \\ \sin\theta_2 & \cos\theta_2 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$g_{l_2,t} = \begin{bmatrix} 1 & 0 & 0 & l_2 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

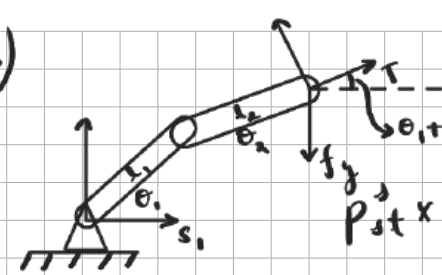
$$g_{st} = g_{s,l_1} g_{l_1,l_2} g_{l_2,t} = \begin{bmatrix} \cos(\theta_1+\theta_2) & -\sin(\theta_1+\theta_2) & 0 & l_1\cos(\theta_1+\theta_2)+l_2\cos\theta_1 \\ -\sin(\theta_1+\theta_2) & \cos(\theta_1+\theta_2) & 0 & l_2\sin(\theta_1+\theta_2)+l_1\sin\theta_1 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

2.2) When $\theta_2 = 0/\pi$, the body manipulator Jacobian becomes:

$$J^b = \begin{bmatrix} 0 & 0 \\ l_2 & l_2 \\ 0 & 0 \\ 0 & 0 \\ 1 & 1 \end{bmatrix} \quad \text{and this matrix has rank 1 due to its columns being linearly dependant.}$$

So, when $\theta_2 = 0, \pi, 2\pi$ etc., there is a kinematic singularity, wherein we will not be able to compute joint velocities analytically for a given v^b or v^d of the end-effector.

2.3)



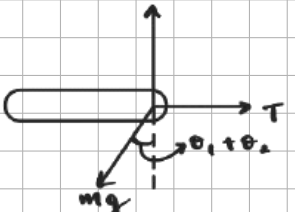
$$f_{st}^s = [0 \ -mg \ 0]^T$$

$$p_{st}^s = [l_1 \cos \theta_1 + l_2 \cos(\theta_1 + \theta_2), l_1 \sin \theta_1 + l_2 \sin(\theta_1 + \theta_2), 0]^T$$

$$p_{st}^s \times f_{st}^s = [0, 0, -mg(l_2 \cos(\theta_1 + \theta_2) + l_1 \cos \theta_1)]$$

$$F_t = Ad(g_{st})^T F_s$$

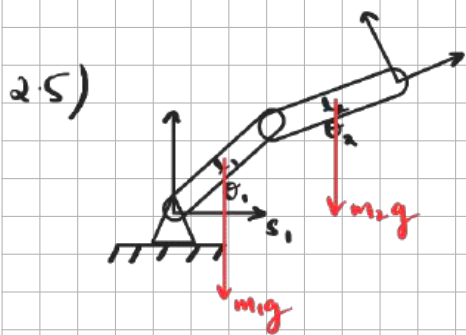
or simply computing in tool frame:



$$f = [-mg \sin(\theta_1 + \theta_2) \quad -mg \cos(\theta_1 + \theta_2) \quad 0]^T$$

$$\tau = [0 \ 0 \ 0]^T$$

$$\Rightarrow F_t = [-mg \sin(\theta_1 + \theta_2) \quad -mg \cos(\theta_1 + \theta_2) \quad 0 \ 0 \ 0 \ 0]^T$$



$$f_2^s = [0, -m_2 g, 0]^T$$

$$p_2^s = [l_1 \cos \theta_1 / 2, l_1 \sin \theta_1 / 2, 0]^T$$

$$\Rightarrow \tau_2^s = p_2^s \times f_2^s = [0, 0, -m_2 g l_1 \cos \theta_1 / 2]^T$$

$$f_1^s = [0, -m_1 g, 0]^T$$

$$p_1^s = [l_1 \cos \theta_1 + l_2 \cos(\theta_1 + \theta_2) / 2, l_1 \sin \theta_1 + l_2 \sin(\theta_1 + \theta_2) / 2, 0]^T$$

$$\Rightarrow \tau_1^s = p_1^s \times f_1^s = [0, 0, -m_1 g (l_2 \cos(\theta_1 + \theta_2) / 2 + l_1 \cos \theta_1)]^T$$

$$F_{1s} = [f_1^T \ \tau_1^T]^T; \quad F_{2s} = [f_2^T \ \tau_2^T]^T$$

$$F_s = F_{1s} + F_{2s}$$

F_t can be computed using the relation:

$$F_t = Ag(g_{st})^T F_s$$