# SURFv6 Design Document

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## 1 Introduction

This document describes the Sampling Unit for RF (SURF) version 6. The SURFv6 is designed to work with a Trenz Electronik TE0835 RFSoC board and interface in an IEEE 1101.1 rack to the Radio Array Carrying Kit (RACK). This document describes the overall design of the SURFv6.

#### 1.1 Definitions

- SURF: Sampling Unit for RF. This document describes this board. This term will be used interchangeably for just the board itself as well as the SURF+TE0835 combined board.
- TURF: Trigger Unit for RF. This is the master trigger and clock distribution system for PUEO.
- TURFIO: Trigger Unit for RF I/O. This board provides the interface between the SURF (via the RACK) and the TURF.
- RACK: Radio Array Carrying Kit. This is the custom backplane by which the SURF units communicate with each other and with the TURFIO.
- RACKbus: The set of signals connecting the SURFv6 to the RACK.
- TE0835: This is the Trenz Electronik RFSoC module. The specific module (ZU47DR, ZU25DR) is unimportant as the SURF is compatible with both.
- U: IEEE 1101.1 standard for vertical spacing. It is equal to 1.75" (44.45 mm). Common increments are 3U, 6U, 9U, etc.
- HP: IEEE 1101.1 standard for horizontal spacing. It is equal to 0.2" (5.08 mm). Common increments are 4HP, 5HP, etc.
- CompactPCI Serial: This is a computer interconnect standard. While the
  electrical interface is not used in the SURF design, the CompactPCI Serial
  Conduction Cooled physical specifications are used to provide a thermal
  design.

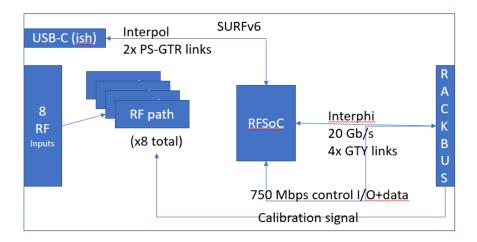


Figure 1: Primary functions of the SURFv6.

- Crate: The SURFv6s are arranged into 2 total crates, H and V polarization, each with 2 RACKs each.
- Phi sector: A phi sector is a set of 4 antennas viewing a common 15 degree range of azimuth. Each SURFv6 covers 2 phi sectors.
- Interphi communication: Communication between 2 SURFv6s in a single crate is interphi communication.
- Interpol communication: Communication between 2 SURFv6s in different crates is interpol communication.
- PL: Programmable Logic. This comprises the FPGA side of the RFSoC.
- PS: Processing System. This comprises the ARM CPU inside the RFSoC.
- Lxx P/N: These signals describe I/Os from the PL.
- MIOxx: These signals describe I/Os from the PS.

#### 1.2 Overview

The SURFv6 is an 8-channel RF digitizer and beamforming trigger module, based on the TE0835 RFSoC module. The *primary* functions of the SURFv6 are covered in Fig. 1. Each SURFv6 needs to digitize the incoming input signals primarily from  $300-1200\,\mathrm{MHz}$ , but with an extended input bandwidth for calibration and bench testing. In addition, a calibration signal needs to be switchable into the RF path to be calibrate timing offsets in the overall system.

The SURFv6 forms a first-level trigger based on the 8 channels it receives, and then forms a *second* level trigger based on data from adjacent phi sectors (i.e. adjacent SURFs). This allows the SURFv6 to form a full 16-channel beamformed trigger to reach the physics design goals. Therefore, the communication between adjacent phi sectors ("interphi communications") is high priority and all 4 available GTY transceivers from the TE0835 are assigned to interphi communications.

In addition, the SURFv6 accommodates the possibility of communication between crates ("interpol communication") for possible LCP/RCP formation and L3 processing. 2x PS-GTR transceivers are dedicated to this communication, using a USB-C connector and cable. Note that the **design goals** for interpol communication require only  $\sim 1\,\mathrm{Gb/s}$  communication, however we overdesign this interface for margin.

## 1.3 Operation conditions

The SURFv6 is intended to be as multifunctional as possible: we therefore attempt to accommodate

- Operation in conduction or convection cooled crate, communication with TURFIO (flight conditions)
- Operation in conduction or convection cooled crate, communication via debug cable (no TURFIO)
- Standalone operation outside of a crate

# 2 Physical Dimensions

The SURFv6 is designed as a standard IEEE 1101.1 3U plug-in card, with primary dimensions of  $160 \,\mathrm{mm} \times 100 \,\mathrm{mm}$  and a 5HP front panel area.

The connector interface extends slightly, resulting in a maximum bounding box of the SURFv6 of  $163\,\mathrm{mm}\times100\,\mathrm{mm}$ . Overall physical dimensions are shown in Fig 2. The backplane connector is a Hirose FX23 100-pin floating connector. This connector has a nominal distance from backplane to back of daughtercard of  $10.1\,\mathrm{mm}$ , and a connector mating length of  $1.5\,\mathrm{mm}$ . The IEEE distance from "front attachment plane" to "backplane connector mounting plane" is  $175.24-176.1\,\mathrm{mm}$ . With the  $2.54\,\mathrm{mm}$  front panel gap, this places the nominal distance from front of the board to the backplane as  $172.7-173.56\,\mathrm{mm}$ . Therefore, we extend the connector portion to  $163\,\mathrm{mm}$ , resulting in a board separation distance of  $9.7-10.56\,\mathrm{mm}$ , well within the  $10.1\pm0.75$  allowable range.

In general, component clearance from the top and bottom sides of the board is  $9.4\,\mathrm{mm}$ , however from  $59.5-124.5\,\mathrm{mm}$ , that clearance reduces to  $5\,\mathrm{mm}$  to accommodate the TE0835, and from  $124.5-144\,\mathrm{mm}$  the clearance is  $8.5\,\mathrm{mm}$ . This clearance extends only until  $144\,\mathrm{mm}$ . The component clearances are shown in Fig. 3. Direct contact can be made with the board within this area only.

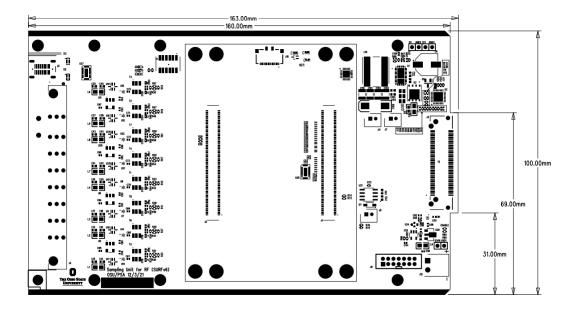


Figure 2: Overall physical dimensions for the SURFv6.

Component clearance ends at 144 mmas no parts beyond that point are expected to have significant power consumption.

Standard IEEE 1101.1 mounting holes are located at  $5.55\,\mathrm{mm}$  from the top and bottom and  $3.57\,\mathrm{mm}$  and  $140.07\,\mathrm{mm}$  from the front of the PCB. IEEE 1101.1 uses the bottom mounting hole for a convection-cooled insertion/extraction handle and the top mounting hole for a front-panel bracket.

#### 2.1 Convection cooled assembly

The SURFv6 can be inserted into any IEEE 1101.1 3U 160 mm Eurocard convection-cooled crate by adding a standard front panel, insertion/extraction handle and front-panel bracket. An example kit would be Schroff P/N #20848-585 with a replacement front panel (e.g. Schroff P/N #30848-300) as a 5HP kit is not available. For operation in a convection cooled crate, a slim 12V DC fan+heatsink is required, powered by connector J8. Power to the fan is only provided when a convection crate is indicated by a floating connection on the \CONVECTION pin on the RACKbus.

#### 2.2 Conduction cooled assembly

The SURFv6 is designed to be assembled into a CompactPCI Serial (CPCI-S) Conduction Cooled Assembly (CCA) for use in a conduction-cooled crate meeting these specifications. The CPCI-S conduction-cooled specification restricts

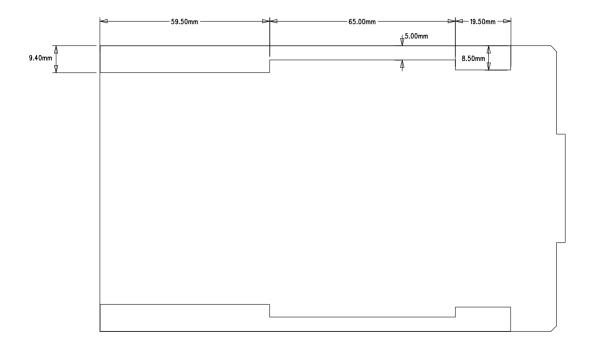


Figure 3: Component keepout area for the SURFv6. Dimensions are identical top and bottom. Direct contact with the board can be made in this area only.

the maximum height of the PCB+heatsink to 14.5 mmon the top side ("side 1"), and a maximum height of the PCB+heatsink on the rear side ("side 2") of 4 mm. The through-hole pins of the RF connector on the SURFv6 slightly exceed this distance (4.4 mm), however the heatsinks for all boards are cleared in this area preventing an interference issue.

# 3 Features

The SURFv6 is designed to the following features.

- 8 ADC inputs with a 3 dB bandwidth of  $90-1400\,\mathrm{MHz}$  and an insertion loss of  $1.75\,\mathrm{dB}$ , flat to  $\pm 0.5\,\mathrm{dB}$  over  $100-1200\,\mathrm{MHz}$
- Calibration inputs available for all channels, from either an FPGA derived impulse or a backplane input
- Backplane connection to PUEO Radio Array Carrying Kit (RACK) via a Hirose FX23 100-pin floating connector, also providing power
- Fan power connector for benchtop use
- Auxiliary power connector for benchtop use
- Inter-polarization connection utilizing a USB-C connector
- $9-15\,\mathrm{V}$  input range
- Overvoltage, undervoltage, and overcurrent protection
- 8 DAC outputs and additional Zynq MPSoC gigabit transceivers (Ethernet, DisplayPort, etc.) available on daughterboard connector
- Gigabit Ethernet available via FFC cable

# 4 Power Supply

The SURFv6 is designed to be powered by a nominal +12V supply, with an acceptable range of  $9-15\,V$ . The SURFv6 can be powered either from the backplane (via J3) or via a dedicated connector for benchtop testing (J12). The J12 input is a 3.5 mm pitch 2-pin terminal block header, with many mating options. By default, power to the SURF is disabled and must be enabled via backplane. This can be overridden with connector J14: closing pins 1-2 will force ENABLE high and turn on the SURF. J14 should not be installed when inserted into a crate.

Parameter	Value	Notes
Undervoltage lockout	$9.5 - 10.17\mathrm{V}$	corresponds to single-battery voltage as well
Overvoltage lockout	$15.58 - 16.50\mathrm{V}$	corresponds to single-battery voltage as well
Current limit	$3.43 - 3.92 \mathrm{A}$	corresponds to $>30\mathrm{W}$ at abs. min V
Output ramp time	$3.8 - 6.93 \mathrm{ms}$	
Nominal inrush current	$0.23 - 0.39 \mathrm{A}$	based on $100\mu\mathrm{F}$ load capacitance
Current limit during inrush	$1.3 - 1.71 \mathrm{A}$	~70% margin
Maximum FET power in fault	$24.134 - 26.141\mathrm{W}$	Not max load power! During fault, FET limited to this power
Fault time	$140 - 196.84 \mu \mathrm{s}$	Results in 80.22% FET thermal margin

Table 1: Design parameters for SURFv6.

## 4.1 Input protection

The SURFv6 has undervoltage, overvoltage, and overcurrent protection, as well as a soft-start current draw and FET temperature protection during fault conditions. The SURFv6 does **not** have reverse current protection. Therefore, **great care** should be taken when connecting the auxiliary power input! Polarity is marked on the connector.

Input protection is provided by the ADM1278 hot-swap controller chip. Note that the SURFv6 should not be plugged in live, although it is likely that no damage will occur. The ADM1278 has PMBus communication for voltage and current reporting as well as fault detection. Each SURFv6 has its own I2C address provided by the backplane to identify which slot it is inserted into.

Parameters for the ADM1278 were developed on the ADM1278 worksheet. The ADM1278 device is currently listed as NRND (it became NRND early 2022) but device availability is high. Design parameters are shown in Tab. 1.

Note that the ADM1278 has two separate current limits - one that applies during startup (determined ISTART, the current limit during inrush), while the voltage is ramping, and one that applies during normal operation. Starting up into a dead short therefore produces significantly less peak current (during fault) than normal operating. Note that the high margin on the ISTART current limit is designed to allow increasing the  $+12\,\mathrm{V}$  output capacitance if needed. Up to  $220\,\mu\mathrm{Fload}$  capacitance can be tolerated by this design with good margins.

#### 4.1.1 Enable polarity and default state

The SURFv6 was designed to accommodate both ADM1278 ENABLE polarities. The "ENABLE" pin on the RACKbus is *always* positive polarity. Negative polarity (which is the default assembly variant) is accommodated by assemblying U39 and R99 and **removing** R98. Positive polarity is accommodated by removing U39/R99 and installing R98 (as a 0-ohm resistor). Closing pins 1-2 on J14 will place the ADM1278 VCAP onto the FET.

# 4.2 TE0835 supply (+5V)

The Trenz TE0835 RFSoC is supplied via a high-efficiency 12 V to 5 V regulator, an LT8648. Component values were determined and simulated using LTPower-Cad with the project in design folder, with a target maximum load of 6 A. The efficiency exceeds 97.4% beyond 2 A. Note that this efficiency includes inductor and capacitor losses. Output is 4.98 V with  $\pm 10\,\mathrm{mV}$  ripple (0.2%). Note that the LT8648S design uses the default loop compensation, rather than the "LT-powerCAD Suggested Compensation" as the "suggested" compensation is quite sensitive to the ESR of the bulk filtering capacitor. Loop parameters for the default compensation have sufficient stability and margin (80 deg phase margin, -11.27 dB gain margin). However, pads were made available for all possible loop compensation options.

The LT8648 bulk input capacitor is a high-temperature solid polymer aluminum capacitor. At operating temperatures below 65C expected lifetime is 200K hours. The low ESR of the input capacitor implies that heat generated inside the capacitor will be minimal (10 – 20 mW). Ceramic input capacitors were chosen for a total of  $27\,\mu\text{F}$  at 12VDC bias, reducing the ripple seen by the bulk capacitor at a 6A maximum load to 1340 mA, well below the bulk capacitor maximum of 3300 mA.

The LT8648 was chosen for its extremely high efficiency combined with the extremely low emissions.

## 4.3 Calibration amp supply

The calibration amplifier (an ADL5544) is provided a  $4.75\,\mathrm{V}$  supply via a MAX8873. Input power to the MAX8873 is filtered through an NFM21PC105B1A3D, providing 30 dB of filtering at the  $400\,\mathrm{kHz}$  DC-DC switching frequency. Along with the  $30\,\mathrm{dB}$  PSRR of the MAX8873, this should reduce the  $10\,\mathrm{mV}$  supply ripple to microvolt-levels.

#### 4.4 Fan power supply

In a convection crate, the TE0835 consumes enough power that an active cooling solution is needed. This is provided via a +12V fan connector, switched by a DS4560 load-switch. The fan is deactivated when the  $\overline{CONDUCTION}$  pin is pulled low by the backplane, indicating a conduction cooled crate. Note that the fan is obviously also not installed in this case, so the disabling of the supply isn't strictly necessary, but it prevents a live high-current voltage on a pin.

#### 4.5 PSBATT supply

The SURFv6 provides the low-voltage PSBATT (used to power the onboard RTC if used) via a simple series voltage reference. Current consumption of PSBATT by the RTC is  $\sim 3\,\mathrm{uA}$ , well under the current limit of the reference. Note that because PSBATT is not actually battery-backed, the RTC will fail after a power cycle.

# 5 RF Inputs

The SURFv6 RF inputs pass through a high-pass section, a low-pass section, a calibration switch, and finally a wideband balun before arriving at the TE0835 inputs.

#### 5.1 High pass filter

The high pass filter is designed as an extremely simple 3rd order tee-style (minimum inductor) Butterworth filter with a 90 MHz cutoff. This cutoff was intentionally made significantly lower than the PUEO design so that variation in the filter cutoff will have no effect on the observed band.

#### 5.2 Low pass filter

The low pass filter used was a Mini-Circuits LFCG-1000+ with a 3dB cutoff of 1370 MHz. The low-pass filter functionally acts primarily as an antialiasing filter, offering roughly 20 dB of rejection above Nyquist (1500 MHz).

#### 5.3 Calibration switch

The RF switch used for the calibration switch is a SKY13323. Note that the isolation of this switch is  $\sim 27\,\mathrm{dB}$ , which while high, may still allow some signal leakage in. Therefore the calibration amplifier should be turned off when the normal signal path is in use. Signal leakage into the calibration path should be unimportant if the calibration signal is strong enough. The SKY13323 is driven with a high-range (3.3 V) output from the FPGA, giving an OP1dB point well above the amplifier compression point.

#### 5.4 Wideband balun

The wideband balun selected was a Mini-Circuits TCM2-43X+. This part is footprint-compatible with several other baluns from Mini-Circuits as well. The TCM2-43X+ was specifically chosen because unlike the balun used on the Trenz baseboard (a TCM2-33WX+), the TCM2-43X+ has a decreasing insertion loss with frequency, allowing it to compensate for the gain slope of the filters. In addition, the return loss is constant within the band, showing fewer artifacts when combined with the filters and switch. The downside is a slightly higher insertion loss.

## 5.5 Full path simulation

To simulate the full RF path, an ideal balun was used to convert the differential signal back to single-ended. Note that the ~0.05 dB "kink" visible near ~380 MHz is due to the SKY13323 S-parameter data. This appears to be a measurement artifact, as no kink is visible in the datasheet and below this frequency,



Figure 4: Simulated RF insertion loss for the SURFv6. Note that the "kink" near 380 MHz is due to the SKY13323 S-parameter data.

the return loss of the unconnected input is an unphysical positive value and phases make a rapid unphysical jump and immediately return to their previous values. Insertion loss is flat to within  $\pm 0.5\,\mathrm{dB}$  over the PUEO band, and group delay is flat to within  $\pm 0.25\,\mathrm{ns}$ .

# 6 Calibration path

A common "CAL" input comes from the RACK backplane and is sent through another SKY13323 switch, with the other input being the output of a differential signal from the FPGA (an impulse test). This CAL input is amplified via an ADL5544, then split 8 ways via an EP4RKU+ in combination with SBTC-2-20+ power splitters (resulting in a total loss of ~16 dB, or roughly equal to the input from the backplane).

# 7 Backplane interface (RACKbus)

Left Name	Left #	Right #	Right Name
ENABLE	1	51	CAL
GND	2	52	GND
DOUT+	3	53	RX
DOUT-	4	54	TX
GND	5	55	GND
CIN+	6	56	COUT+
CIN-	7	57	COUT-
GND	8	58	GND
RXCLK+	9	59	TXCLK+
RXCLK-	10	60	TXCLK-
GND	11	61	GND
TIN+	12	62	TOUT+
TIN-	13	63	TOUT-
\CONDUCTION	14	64	\ALERT
TCK	15	65	TDO
TMS	16	66	TDI
GND	17	67	3.3VSB
PSYNC	18	68	
	19	69	
	20	70	
	21	71	
EXT CLK P	22	72	
EXT CLK N	23	73	
GND	24	74	GND
U0RX+	25	75	D0TX+
U0RX-	26	76	D0TX-
GND	27	77	GND
U0TX+	28	78	D0RX+
U0TX-	29	79	D0RX-
GND	30	80	GND
U1RX+	31	81	D1TX+
U1RX-	32	82	D1TX-
GND	33	83	GND
U1TX+	34	84	D1RX+
U1TX-	35	85	D1RX-
GND	36	86	GND
U2RX+	37	87	D2TX+
U2RX-	38	88	D2TX-
GND	39	89	GND
U2TX+	40	90	D2RX+
U2TX-	41	91	D2RX-
GND	42	92	GND
U3RX+	43	93	D3TX+
U3RX-	44	94 11	D3TX-
GND	45	95	GND
U3TX+	46	96	D3RX+
U3TX-	47	97	D3RX-
GND	48	98	GND
A0	49	99	SDA
A1	50	100	SCL

#### 7.1 TURF interface

The interface to the TURF (via the TURFIO) consists of source-synchronous high speed (750 Mbps) serial links. Data is transmitted via DOUT+/-, and commands are received and responded to on CIN+/-, COUT+/- respectively. RXCLK+/- and TXCLK+/- complete the source-synchronous interfaces.

The system clock is provided on EXT CLK P/N.

# 7.2 Interphi comms

U[3:0]RX/TX+/- (increasing phi communication) and D[3:0]RX/TX+/- (decreasing phi communication) comprise the interphi communication system. Note that the "up/down" here is arbitrary, it's really just to opposite sides on the backplane.

Interphi links are required to reach a total throughput of 20 Gb/s. Since the interphi system comprises 4 total links, each link therefore *must* reach 5 Gb/s. This should be reachable with minimal effort, however higher throughputs (and thus fewer links) are preferred if possible. This may require using blind or backdrilled vias to eliminate stubs in the L1-L3 transition, and will be investigated in a second production run.

The MGT links are operated from a reference clock of 125 MHz, derived from the input 7.8125 MHz system clock.

MGT connections are routed on layer 3 as stripline.

#### 7.3 Auxiliary trigger chain

To accomodate a secondary low-level trigger for the LF instrument, a trigger chain (TIN+/- and TOUT+/-) is formed to combine low-level trigger outputs from the TE0835s. Note that while nominally a loss of a single TE0835 breaks the chain, this problem can be mitigated since the trigger chain could be reconfigured to wrap around the ends of the crate.

#### 7.4 Single-ended control signals

- A0/A1: Address pins to identify the slot. These address pins have 3 possible values (open, resistor to ground, or ground). Combined with the backplane identification (left/right) that gives 18 total possibilities (only 14 are needed).
- SDA/SCL/\ALERT : SMBus interface pins.
- PSYNC: Power system synchronization clock.
- ENABLE: Allows disabling power to all TE0835s. This is always positive logic.
- 3.3VSB: standby low current 3.3V supply

Clock #	TE0835 name	SURFv6 name	Frequency	Purpose
0A	unused	unused		
0	$CLKC_P/N$	ACLK0_P/N	$187.5\mathrm{MHz}$	ADC 0/1 clock
1	$CLKB_P/N$	ACLK1_P/N	$187.5\mathrm{MHz}$	ADC 2/3 clock
2	CLKA_P/N	$ACLK2_P/N$	$187.5\mathrm{MHz}$	ADC 4/5 clock
3	CLKD_P/N	ACLK3_P/N	$187.5\mathrm{MHz}$	ADC 6/7 clock
4	$\text{CLKE}_{P/N}$	PLCLK_P/N(*)	$187.5\mathrm{MHz}$	Logic clock
5	CLKF_P/N	unused (*)		
6	$B128\_CLK0\_P/N$	_	$125\mathrm{MHz}$	MGT clock
7	$B129\_CLK0\_P/N$	_	$125\mathrm{MHz}$	MGT clock
8	$CLK8_P/N$	_	$7.8125\mathrm{MHz}$	PL_SYSREF
9	$PSMGT_{100MHz}P/N$	_	$125\mathrm{MHz}$	PS MGT clock
9A	$CLK0A\_100MHz\_P/N$	SYSREFCLK_P/N	$7.8125\mathrm{MHz}$	Analog SYSREF

Table 2: Clock outputs of the Si5395 clock generator on the TE0835. CLKE/F - marked with (\*) - can also be routed as DAC clocks. Note that clocks 9 and 9A do not match their TE0835 frequency names. This is unimportant and only represents the original usage in the TE0835 base project.

• RX/TX: Asynchronous slow-control interface

• \CONDUCTION: Identifies type of crate.

• TCK/TMS/TDI/TDO: JTAG interface.

# 8 Clocking system

The TE0835 contains a Silicon Labs 12-output clock generator which takes either an internal clock or an external reference clock. One of these clocks is unconnected. It should be sadly noted that the unused clock was not routed back to the feedback input, and therefore the Si5395 cannot be operated in zero-delay mode. There will therefore be some unknown propagation delay between the common system clock and the sampling clock of the ADCs. However, this delay can be measured (independent of the ADCs) using a similar setup to the phase scanner present in the SURFv5 and TISC firmware to sub-10 ps precision. This is because the FPGA will have both the input clock (from the TURFIO, via TXCLK\_P/N) and the output clock (via PL\_SYSREF). If this arrangement proves unworkable, a second revision of the SURFv6 would be necessary with its own Si5395 onboard (which would allow the onboard Si5395 to be shut down).

The outputs from the Si5395 are shown in Table 2. Note that the clocks must be configured differently between internal  $(10\,\mathrm{MHz}$  input) and external  $(7.8125\,\mathrm{MHz}$  input).

Protocol	Line rate	Notes
PCIe	$5.0 \; \mathrm{GT/s} \; \mathrm{per} \; \mathrm{lane}$	Fixed lanes: must use lanes 0 for single, $0/1$ for double
SATA	6.0  Gb/s per lane	SATA0=lane 0, SATA1=lane 1
USB 3.0	$5.0~\mathrm{Gb/s}$	USB0=lane 0/1/2, USB1=lane 3
SGMII	1  Gb/s per lane	Any lane is usable
DisplayPort	(n/a)	Transmit only. DP1=lane0/2, DP0=lane1/3

Table 3: Functions available in the PS-GTR transceivers.

# 9 Inter-polarization communication

The inter-polarization communication ("interpol") is an *optional* communication method between SURFv6s located in different crates. It is designed on a "best effort" basis.

Because all 8 FPGA logic MGTs (the GTY transceivers) are taken, any interpolarization communication must occur using the remaining PS MGTs, which are restricted to operate using fixed protocols: USB 3.0, PCI Express, SGMII, SATA, and DisplayPort. The protocols supported by the PS-GTR transceivers are shown in Table . Note that **all** data in the interpol communication must come via the ARM CPUs in the Zynq.

Two PS MGTs are routed to a USB-C connector on the front panel via two differential pair exchange switches to accommodate the USB-C connector reversal function. USB-C cables are unoriented, however, because of the lane requirements imposed by the Zynq (in Tab. 3) the exchange switches are required to ensure that, for instance, if PCIe protocol is used that lane 0 is connected to lane 0. Two PI3DBS16222 exchange switches are used instead of a single for ease of routing, especially near the USB connector. Note that due to the switch arrangement the two switches must be set *opposite* each other, so two control lines (USB\_SW0/USB\_SW1) are used. This leaves half of the PI3DBS16222 exchange switches unused.

Using the PI3DBS16222 switches, if a USB 3.1 cable is used (containing 2 SuperSpeed pairs), any possible legal protocol combination can be used. The PUEO Concept Study Report baselines  $\sim 1\,\mathrm{Gb/s}$  throughput (if communication is used at all), which could be accomplished via a single SGMII Ethernet link.

Cable detection is done using a Type C controller, either a PI5USB30216, a TUSB320, or a FUSB303B, all of which are pin-compatible. Type C roles (source or sink) can be forced using switches 5/6 on the S1 DIP switch if autonegotiation fails. USB inputs are protected via ESD8104 diode arrays.

The USB type-C "SBU" pins are routed as a differential pair to the auxiliary connector J6 and optionally to the L7\_P/N test points (and thus to the FPGA). They are labelled as USB\_GP0/GP1. These connections are routed with no expected use case at the moment.

As a side note, while it might be possible to implement DisplayPort over the USB-C connector via alt mode, the required bias/AC coupling is not provided.

Note: USB cable orientation might be fixed between SURFv6s if Type-C

locking cables are used. In this case the switch controls (USB\_SW[1:0]) can be fixed. If issues arise with the type-C controller (or using the USB-C input as a proper USB connector), the connector can therefore be used as simply a high-performance differential pair link.

## 9.1 USB devices

To accommodate the possibility of USB device connection (via the ARM CPU), a DPS1113 VBUS switch is used to drive +5V onto the USB connector when connected as a USB source. See the PI5USB30216 datasheet. This is not considered a critical use case.

# 10 Auxiliary connectors

The TE0835 has significant resources that are not nominally required for the SURFv6, however it makes sense to make them available for either testing or special purposes. This is done via 2 auxiliary connectors: first, Ethernet signals (PHY\_MDIO[3:0]+/-, as well as the LED outputs) are made available on a flat-flex cable connector (J10) which can be accessed via a Molex Premo-Flex LVDS (0150121) cable. Second, an "aux" connector (J6) contains a number of auxiliary signals on an FX12B-60P board-to-board connector.

The aux connector contains:

- 8 DAC outputs
- 2 PS-MGT RX/TX pairs
- 2 general purpose differential pairs (L1 P/N and L16 P/N)
- MIO signals needed to implement DisplayPort on the PS-MGT signals (CPLD IO2/IO3 and MIO27/MIO30)
- 3 general purpose I/Os (L6 N, L7 N, and L7 P)

CPLD\_IO2/IO3 are outputs from a programmable logic chip (a Lattice MachXO2) on the TE0835. CPLD\_IO3 is nominally used as a Power Good signal, and CPLD\_IO2 is a user signal. However both of these can be reconfigured as needed.

The last 3 GPIOs are also available on test points. L7 $_{
m P/N}$  are also routed as a differential pair, however the test points act as stubs.

## 11 SDIO interface

To facilitate booting from an SD card and matching the TEB0835, a micro-SD socket was placed on the rear of the SURFv6, interfaced to the FPGA using a TXS02612 level converter, matching the TEB0835. One difference is that we do not supply 3.3V to the micro-SD socket unless a card is detected. Cards

are powered via the 3.3V CPLD voltage rail present on the TE0835, which is current-limited to 300 mA, however virtually no loads on either board exist for this rail - the main draw is a CTS626 which is used as a spare MGT clock. This is not considered a critical use case, as the final system will boot from QSPI flash.

# 12 DIP switch

The TE0835 uses a 4-pole DIP switch to configure both the JTAG access and boot settings. The SURFv6 keeps those but the order changes. Therefore the settings are listed again here.

Switch #	Signal Name	Description
1	CPLD_JTAGEN	When ON, selects CPLD JTAG
2	CPLD_IO2	\PROGRAM
3	CPLD_IO1	\BOOT1
4	CPLD_IO0	\BOOT0
5	USB_SNK	When ON=USB sink
6	USB_SRC	When ON=USB source

Note: switching both  $\overline{5}$  and  $\overline{6}$  on will result in undefined behavior.

## 12.1 Boot modes

\BOOT1 and \BOOT0 produce different booting modes for the TE0835.

Boot mode	SW#4 State	SW#3 State
JTAG	ON	ON
QSPI Flash	ON	OFF
SD Card	OFF	OFF

Once firmware is completed, the basic boot mode should be QSPI flash (SW#4 ON, SW#3 OFF).