# Visco-elastic Finite difference seismic modeling with simple and effective boundary conditions

B.Arntsen

May 4, 2023

PRELIMINARY VERSION UNDER DEVELOPMENT. CONTAINS ERRORS.

## Elastic equations of motion

Consider an elastic medium characterized by the density  $\rho(\mathbf{x})$ , and lamé parameters  $\lambda(\mathbf{x})$  and  $\mu(\mathbf{x})$  at each spatial point  $\mathbf{x}$ . Now assume that  $u(\mathbf{x})_i$  is the i'th component of the particle displacement and  $\sigma_{ij}$  is the stress tensor and  $c_{ijkl}$  is Hook's tensor. The elastic equations of motion and Hook's law in Cartesian coordinates are given as

$$\rho(\mathbf{x})\partial_t^2 u_i(\mathbf{x},t) = \partial_i \sigma_{ii}(\mathbf{x},t) + f_i(\mathbf{x},t), \tag{1}$$

$$\sigma_{ij}(\boldsymbol{x},t) = c_{ijkl}e_{kl} + q_{ij}. \tag{2}$$

Here  $f_i$  is a driving force, and  $q_{ij}$  is a driving stress. In the isotropic case one has

$$c_{ijkl} = \lambda \delta_{ij} \delta_{kl} + \mu \left( \delta_{ik} \delta_{jl} + \delta_{il} \delta_{jk} \right), \tag{3}$$

giving

$$\rho(\mathbf{x})\partial_t^2 u_i(\mathbf{x},t) = \partial_j \sigma_{ij}(\mathbf{x},t) + f_i(\mathbf{x},t), \tag{4}$$

$$\sigma_{ij}(\boldsymbol{x},t) = \lambda(\boldsymbol{x})e_{kk}\delta_{ij} + 2\mu e_{ij} + q_{ij}. \tag{5}$$

Here  $f_i$  is the i'th component of the driving force, while the strain tensor  $e_{ij}$  is equal to

$$e_{ij} = \frac{1}{2} [\partial_i u_j(\boldsymbol{x}, t) + \partial_j u_i(\boldsymbol{x}, t)]. \tag{6}$$

Writing out the individual components of the equations above, one gets:

$$\rho \partial_t^2 u_x = \partial_x \sigma_{xx} + \partial_y \sigma_{xy} + \partial_z \sigma_{xz} + f_x, 
\rho \partial_t^2 u_y = \partial_x \sigma_{yx} + \partial_y \sigma_{yy} + \partial_z \sigma_{yz} + f_y, 
\rho \partial_t^2 u_z = \partial_x \sigma_{zx} + \partial_y \sigma_{zy} + \partial_z \sigma_{zz} + f_z,$$
(7)

$$\begin{split} \sigma_{xx} &= \lambda \left( e_{xx} + e_{yy} + e_{zz} \right) + 2\mu e_{xx} + q_{xx}, \\ \sigma_{yy} &= \lambda \left( e_{xx} + e_{yy} + e_{zz} \right) + 2\mu e_{yy} + q_{yy}, \\ \sigma_{zz} &= \lambda \left( e_{xx} + e_{yy} + e_{zz} \right) + 2\mu e_{zz} + q_{zz}, \end{split}$$

$$\sigma_{xy} = 2\mu e_{xy} + q_{xy}, 
\sigma_{xz} = 2\mu e_{xz} + q_{xz}, 
\sigma_{yz} = 2\mu e_{yz} + q_{yz}.$$
(8)

## Viscoelastic equations of motion

Using the description in Appendix A, we can write down the viscoe-elastic equations of motion and the constitutive relation. In addition to viscoelastic stress-strain relation we have also introduced time-dependence for the density. The density then shows relaxation in the same way as a viscoelastic medium.

$$\partial_t^2 u_i(\boldsymbol{x}, t) = \rho_u^{-1}(\boldsymbol{x}) \partial_j \sigma_{ij}(\boldsymbol{x}, t) + f_i(\boldsymbol{x}, t),$$

$$+ \chi(\boldsymbol{x}, t) * \partial_j \sigma_{ij}(\boldsymbol{x}, t), \qquad (9)$$

$$\sigma_{ij}(\boldsymbol{x}, t) = \lambda_u e_{kk} \delta_{ij} + 2\mu_u e_{ij} + q_{ij}$$

$$+ \delta_{ij} \phi_{\lambda}(t) * e_{mm} + 2\phi_{\mu}(t) * e_{ij} \qquad (10)$$

Writing out the individual components of the equations above, one gets:

$$\partial_t^2 u_x = \rho_u^{-1} \left[ \partial_x \sigma_{xx} + \partial_y \sigma_{xy} + \partial_z \sigma_{xz} \right] + f_x,$$

$$= +\chi * \left[ \partial_x \sigma_{xx} + \partial_y \sigma_{xy} + \partial_z \sigma_{xz} \right],$$

$$\partial_t^2 u_y = \rho_u^{-1} \left[ \partial_x \sigma_{yx} + \partial_y \sigma_{yy} + \partial_z \sigma_{yz} \right] + f_y,$$

$$= \chi * \left[ \partial_x \sigma_{yx} + \partial_y \sigma_{yy} + \partial_z \sigma_{yz} \right]$$

$$\partial_t^2 u_z = \rho_u^{-1} \left[ \partial_x \sigma_{zx} + \partial_y \sigma_{zy} + \partial_z \sigma_{zz} \right] + f_z,$$

$$= \chi * \left[ \partial_x \sigma_{zx} + \partial_y \sigma_{zy} + \partial_z \sigma_{zz} \right].$$
(11)

$$\begin{array}{rcl} \sigma_{xx} & = & \lambda_u \left( e_{xx} + e_{yy} + e_{zz} \right) + 2\mu_u e_{xx} + q_{xx} \\ & + & \phi_{\lambda} * \left[ e_{xx} + e_{yy} + e_{zz} \right] + 2\phi_{\mu}(t) * e_{xx}, \\ \sigma_{yy} & = & \lambda_u \left( e_{xx} + e_{yy} + e_{zz} \right) + 2\mu_u e_{yy} + q_{yy} \\ & + & \phi_{\lambda} * \left[ e_{xx} + e_{yy} + e_{zz} \right] + 2\phi_{\mu}(t) * e_{yy}, \\ \sigma_{zz} & = & \lambda_u \left( e_{xx} + e_{yy} + e_{zz} \right) + 2\mu_u e_{zz} + q_{zz} \\ & + & \phi_{\lambda} * \left[ e_{xx} + e_{yy} + e_{zz} \right] + 2\phi_{\mu}(t) * e_{zz}, \\ \sigma_{xy} & = & 2\mu_u e_{xy} + q_{xy} + 2\phi_{\mu}(t) * e_{xy}, \\ \sigma_{xz} & = & 2\mu_u e_{xz} + q_{xz} + 2\phi_{\mu}(t) * e_{xz}, \end{array}$$

$$\sigma_{yz} = 2\mu_u e_{yz} + q_{yz} + 2\phi_{\mu}(t) * e_{yz}. \tag{12}$$

#### Viscoelastic velocity-stress formulation

Using the velocity  $v_i = \dot{u}_i$ , one gets

$$\partial_{t}v_{x} = \rho_{u}^{-1} \left[ \partial_{x}\sigma_{xx} + \partial_{y}\sigma_{xy} + \partial_{z}\sigma_{xz} \right] + f_{x}, 
= +\chi * \left[ \partial_{x}\sigma_{xx} + \partial_{y}\sigma_{xy} + \partial_{z}\sigma_{xz} \right], 
\partial_{t}v_{y} = \rho_{u}^{-1} \left[ \partial_{x}\sigma_{yx} + \partial_{y}\sigma_{yy} + \partial_{z}\sigma_{yz} \right] + f_{y}, 
= \chi * \left[ \partial_{x}\sigma_{yx} + \partial_{y}\sigma_{yy} + \partial_{z}\sigma_{yz} \right] 
\partial_{t}v_{z} = \rho_{u}^{-1} \left[ \partial_{x}\sigma_{zx} + \partial_{y}\sigma_{zy} + \partial_{z}\sigma_{zz} \right] + f_{z}, 
= \chi * \left[ \partial_{x}\sigma_{zx} + \partial_{y}\sigma_{zy} + \partial_{z}\sigma_{zz} \right].$$
(13)

$$\dot{\sigma}_{xx} = \lambda_{u} \left( \dot{e}_{xx} + \dot{e}_{yy} + \dot{e}_{zz} \right) + 2\mu_{u}\dot{e}_{xx} + \dot{q}_{xx}, 
+ \phi_{\lambda} * \left[ \dot{e}_{xx} + \dot{e}_{yy} + \dot{e}_{zz} \right] + 2\phi_{\mu}(t) * \dot{e}_{xx}, 
\dot{\sigma}_{yy} = \lambda_{u} \left( \dot{e}_{xx} + \dot{e}_{yy} + \dot{e}_{zz} \right) + 2\mu_{u}\dot{e}_{yy} + \dot{q}_{yy} 
+ \phi_{\lambda} * \left[ \dot{e}_{xx} + \dot{e}_{yy} + \dot{e}_{zz} \right] + 2\phi_{\mu}(t) * \dot{e}_{yy}, 
\dot{\sigma}_{zz} = \lambda_{u} \left( \dot{e}_{xx} + \dot{e}_{yy} + \dot{e}_{zz} \right) + 2\mu_{u}\dot{e}_{zz} + q_{zz}, 
+ \phi_{\lambda} * \left[ \dot{e}_{xx} + \dot{e}_{yy} + \dot{e}_{zz} \right] + 2\phi_{\mu}(t) * \dot{e}_{zz}, 
\dot{\sigma}_{xy} = 2\mu_{u}\dot{e}_{xy} + q_{xy} + 2\phi_{\mu}(t) * \dot{e}_{xy}, 
\dot{\sigma}_{xz} = 2\mu_{u}\dot{e}_{xz} + q_{xz} + 2\phi_{\mu}(t) * \dot{e}_{xz}, 
\dot{\sigma}_{yz} = 2\mu_{u}\dot{e}_{yz} + q_{yz} + 2\phi_{\mu}(t) * \dot{e}_{yz}.$$
(14)

#### Memory functions

We now define so-called memory variables by including the time convolution into one set of variables:

$$\gamma_{\lambda}^{l}(t) = \frac{1}{\Delta \lambda_{l}} \phi_{\lambda}^{l} * [\dot{e}_{xx} + \dot{e}_{yy} + \dot{e}_{zz}]$$
 (15)

$$\gamma_{ij}^{l}(t) = \frac{1}{\Delta\mu_{l}} \phi_{\mu}^{l} * [\dot{e}_{ij}],$$
(16)

$$\theta_{kij}^{l}(t) = \frac{1}{\Delta \rho_{l}^{-1}} \chi^{l} * \partial_{k}[\sigma_{ij}], \tag{17}$$

Here

$$\Delta \rho_l^{-1} = \rho_u^{-1} \left( 1 - \frac{\tau_{\epsilon l}^{\rho}}{\tau_{\sigma l}^{\rho}} \right), \tag{18}$$

$$\Delta \lambda_l = \lambda_u \left( 1 - \frac{\tau_{el}^{\lambda}}{\tau_{\sigma l}^{\lambda}} \right), \tag{19}$$

$$\Delta \mu_l = \mu_u \left( 1 - \frac{\tau_{el}^{\mu}}{\tau_{\sigma l}^{\rho}} \right). \tag{20}$$

This gives the expressions for the  $\gamma$  functions as:

$$\gamma_{\lambda}^{l} = \left[ \frac{\exp(-t/\tau_{\sigma l}^{\lambda})}{\tau_{\sigma l}^{\lambda} \sum_{l=1}^{N} \frac{\tau_{\sigma l}^{\lambda}}{\tau_{\sigma l}^{\lambda}}} \right] [\dot{e}_{xx} + \dot{e}_{yy} + \dot{e}_{zz}], \tag{21}$$

$$\gamma_{ij}^{l} = \left[ \frac{\exp(-t/\tau_{\sigma l}^{\mu})}{\tau_{\sigma l}^{\mu} \sum_{l=1}^{N} \frac{\tau_{e l}^{\mu}}{\tau_{\sigma l}^{\mu}}} \right] \dot{e}_{ij}, \tag{22}$$

$$\theta_{kij}^{l} = \left[ \frac{\exp(-t/\tau_{\sigma l}^{\rho})}{\tau_{\sigma l}^{\rho} \sum_{l=1}^{N} \frac{\tau_{el}^{\rho}}{\tau_{\sigma l}^{\rho}}} \right] \partial_{k} \sigma_{ij}. \tag{23}$$

and also

$$\begin{split} \gamma_{\lambda}(t) &=& \sum_{l=1}^{N} \gamma_{\lambda}^{l}, \\ \gamma_{ij}(t) &=& \sum_{l=1}^{N} \gamma_{ij}^{l}, \\ \theta_{kij}(t) &=& \sum_{l=1}^{N} \theta_{ij}^{l}. \end{split}$$

This gives the final form of the viscoelastic equations

$$\begin{array}{lll} \partial_t v_x & = & \rho_i^{-1} \left( \partial_x \sigma_{xx} + \partial_y \sigma_{xy} + \partial_z \sigma_{xz} \right) + f_x, \\ & + & \sum_{l=0}^N \theta_{xxx}^l \Delta \rho_l^{-1} + \sum_{l=0}^N \theta_{yxy}^l \Delta \rho_l^{-1} + \sum_{l=0}^N \theta_{zxz}^l \Delta \rho_l^{-1}, \\ \partial_t v_y & = & \partial_x \sigma_{yx} + \partial_y \sigma_{yy} + \partial_z \sigma_{yz} + f_y, \\ & + & \sum_{l=0}^N \theta_{xyx}^l \Delta \rho_l^{-1} + \sum_{l=0}^N \theta_{yyy}^l \Delta \rho_{ll}^{-1} + \sum_{l=0}^N \theta_{zyz}^l \Delta \rho_{ll}^{-1}. \end{array}$$

$$\partial_{t}v_{z} = \partial_{x}\sigma_{zx} + \partial_{y}\sigma_{zy} + \partial_{z}\sigma_{zz} + f_{z},$$

$$+ \sum_{l=0}^{N} \theta_{xzx}^{l} + \sum_{l=0}^{N} \theta_{yzy}^{l} + \sum_{l=0}^{N} \theta_{zzz}^{l}.$$

$$\dot{\sigma}_{xx} = \lambda_{u} \left(\dot{e}_{xx} + \dot{e}_{yy} + \dot{e}_{zz}\right) + 2\mu_{u}\dot{e}_{xx} + \dot{q}_{xx}$$

$$+ \sum_{l=1}^{N} \gamma_{\lambda}^{l} \Delta \lambda_{l} + 2\sum_{l=1}^{N} \gamma_{xx}^{l} \Delta \mu_{l},$$

$$(24)$$

$$\dot{\sigma}_{yy} = \lambda_u \left( \dot{e}_{xx} + \dot{e}_{yy} + \dot{e}_{zz} \right) + 2\mu_u \dot{e}_{yy} + \dot{q}_{yy},$$

$$+ \sum_{l=1}^{N} \gamma_{\lambda}^l \Delta \lambda_l + 2 \sum_{l=1}^{N} \gamma_{yy}^l \Delta \mu_l,$$

$$\dot{\sigma}_{zz} = \lambda_u \left( \dot{e}_{xx} + \dot{e}_{yy} + \dot{e}_{zz} \right) + 2\mu_u \dot{e}_{zz} + \dot{q}_{zz}$$

$$+ \sum_{l=1}^{N} \gamma_{\lambda}^l \Delta \lambda_l + 2 \sum_{l=1}^{N} \gamma_{zz} \Delta \mu_l,$$

$$\dot{\sigma}_{xy} = 2\mu \dot{e}_{xy} + 2\sum_{l=1}^{N} \gamma_{xy}^{l} \Delta \mu_{l} + \dot{q}_{xy},$$

$$\dot{\sigma}_{xz} = 2\mu \dot{e}_{xz} + 2\sum_{l=1}^{N} \gamma_{xz}^{l} \Delta \mu_{l} + \dot{q}_{xz},$$

$$\sigma_{xz} = 2\mu e_{xz} + 2\sum_{l=1}^{N} \gamma_{xz}^* \Delta \mu_l + q_{xz}.$$

$$\dot{\sigma}_{yz} = 2\mu \dot{e}_{yz} + 2\sum_{l=1}^{N} \gamma_{yz}^{l} \Delta \mu_l + \dot{q}_{yz},$$

$$\begin{array}{rcl}
\dot{e_{xx}} &=& \partial_x v_x, \\
\dot{e_{yy}} &=& \partial_y v_y, \\
\dot{e_{zz}} &=& \partial_z v_z, \\
\dot{e_{xy}} &=& \frac{1}{2} (\partial_x v_y + \partial_y v_x), \\
\dot{e_{xz}} &=& \frac{1}{2} (\partial_x v_z + \partial_z v_y), \\
\dot{e_{yz}} &=& \frac{1}{2} (\partial_y v_z + \partial_z v_y).
\end{array} \tag{26}$$

(25)

## Integration of memory functions

The memory functions obeys approximately the relations

$$\gamma_{\lambda}^{l}(t) = \exp(-\frac{\Delta t}{\tau_{\sigma}^{\lambda l}})\gamma_{\lambda}^{l}(t - \Delta t) + \left(\frac{\Delta t}{\tau_{\sigma l}^{\lambda} \sum_{l=1}^{N} \frac{\tau_{\epsilon l}^{\lambda}}{\tau_{\sigma l}^{\lambda}}}\right) (\dot{e}_{xx} + \dot{e}_{yy} + \dot{e}_{zz}),$$

$$\gamma_{ij}^{l}(t) = \exp(-\frac{\Delta t}{N\tau_{\sigma l}^{\mu}})\gamma_{ij}^{l}(t - \Delta t) + \left(\frac{\Delta t}{\tau_{\sigma l}^{\mu} \sum_{l=1}^{N} \frac{\tau_{\epsilon l}^{\mu}}{\tau_{\sigma l}^{\mu}}}\right) \dot{e}_{ij}.$$

$$\theta_{kij}^{l}(t) = \exp(-\frac{\Delta t}{N\tau_{\sigma l}^{\rho}})\theta_{kij}^{l}(t - \Delta t) + \left(\frac{\Delta t}{\tau_{\sigma l}^{\rho} \sum_{l=1}^{N} \frac{\tau_{\epsilon l}^{\rho}}{\tau_{\sigma l}^{\mu}}}\right) \partial_{k}\sigma_{ij}.$$
(27)

Defining the quantities

$$\alpha_1^l = \exp(-\frac{\Delta t}{\tau^{\lambda_l}}), \tag{28}$$

$$\alpha_2^l = \frac{\Delta t}{\tau_{\sigma l}^{\lambda} \sum_{l=1}^{N} \frac{\tau_{\epsilon l}^{\lambda}}{\tau_{\lambda}^{\lambda}}},$$
(29)

$$\beta_1^l = \exp(-\frac{\Delta t}{\tau_{\sigma l}^{\mu}}), \tag{30}$$

$$\beta_2^l = \frac{\Delta t}{\tau_{\sigma l}^{\mu} \sum_{l=1}^{N} \frac{\tau_{el}^{\mu}}{\tau_{\sigma l}^{\mu}}}, \tag{31}$$

$$\eta_1^l = \exp(-\frac{\Delta t}{\tau_{\sigma l}^{\rho}}), \tag{32}$$

$$\eta_2^l = \frac{\Delta t}{\tau_{\sigma l}^{\rho} \sum_{l=1}^{N} \frac{\tau_{el}^{\rho}}{\tau_{\sigma l}^{\rho}}}$$

$$(33)$$

we get

$$\gamma_{\lambda}^{l}(t) = \alpha_{1}^{l} \gamma_{\lambda}^{l}(t - \Delta t) + \alpha_{2}^{l} \left(\dot{e}_{xx} + \dot{e}_{y}y + \dot{e}_{z}z\right), 
\gamma_{ij}^{l}(t) = \beta_{1}^{l} \gamma_{ij}^{l}(t - \Delta t) + \beta_{2}^{l} \dot{e}_{ij}. 
\theta_{kij}^{l}(t) = \eta_{1}^{l} \theta_{kij}^{l}(t - \Delta t) + \eta_{2}^{l} \partial_{k} \sigma_{ij}.$$
(34)

#### Discretization of the three dimensional case

We now consider a regular grid with positions x defined as

$$\boldsymbol{x} = (x, y, z), \tag{35}$$

$$x = p\Delta x, \tag{36}$$

$$y = q\Delta y, (37)$$

$$z = r\Delta z, \tag{38}$$

$$t = n\Delta t. (39)$$

where  $p = 0, 1, 2, ..., N_x$ ,  $q = 0, 1, 2, ..., N_y$  and  $r = 0, 1, 2, ..., N_z$  and  $N_x, N_y$  and  $N_z$  are the number of grid points in the x, y and z-directions.  $n = 0, 1, 2, ..., N_t$  where  $N_t$  is the number of time steps.

We will also need a regular grid which is displaced, or staggered, relative to the the regular grid. Sometimes we will refer to the regular grid as the reference grid.

The particle velocities  $v_x, v_y$  and  $v_z$  are defined on staggered grids as follows

$$v_x(x,t) = v_x(x + \Delta x/2, y, z, t), \tag{40}$$

$$v_y(\boldsymbol{x},t) = v_y(x, y + \Delta y/2, z, t), \tag{41}$$

$$v_z(\boldsymbol{x},t) = v_z(x,y,z+\Delta z/2,t). \tag{42}$$

The  $\theta_{kij}$  are defined on the same staggered grid as the particle velocities:

$$\theta_{xxx}(\boldsymbol{x},t) = \theta(x + \Delta x/2, y, z)_{xxx}, \tag{43}$$

$$\theta_{yxy}(\boldsymbol{x},t) = \theta(x, y + \Delta y/2, z)_{yxy}, \tag{44}$$

$$\theta_{zxz}(\boldsymbol{x},t) = \theta(x,y,z + \Delta z/2)_{zxz}, \tag{45}$$

$$\theta_{xyx}(\boldsymbol{x},t) = \theta(x + \Delta x/2, y, z)_{xyx}, \tag{46}$$

$$\theta_{yyy}(\boldsymbol{x},t) = \theta(x, y + \Delta y/2, z)_{yyy}, \tag{47}$$

$$\theta_{zuz}(\boldsymbol{x},t) = \theta(x,y,z + \Delta z/2)_{zuz}, \tag{48}$$

$$\theta_{xzx}(\boldsymbol{x},t) = \theta(x + \Delta x/2, y, z)_{xzx}, \tag{49}$$

$$\theta_{uzy}(\boldsymbol{x},t) = \theta(x, y + \Delta y/2, z)_{uzy} \tag{50}$$

$$\theta_{zzz}(x,t) = \theta(x,y,z + \Delta z/2)_{xxx}. \tag{51}$$

The diagonal stresses and the gamma functions are defined on a regular grid:

$$\sigma_{xx}(\boldsymbol{x},t) = \sigma_{xx}(x,y,z,t), \tag{52}$$

$$\sigma_{yy}(\boldsymbol{x},t) = \sigma_{yy}(x,y,z,t),$$
 (53)

$$\sigma_{zz}(\boldsymbol{x},t) = \sigma_{zz}(x,y,z,t), \tag{54}$$

$$\gamma_{\lambda}(\boldsymbol{x},t) = \gamma_{\lambda}(x,y,z,t), \tag{55}$$

$$\gamma_{\mu}(\boldsymbol{x},t) = \gamma_{\mu}(x,y,z,t), \tag{56}$$

$$\gamma_{xx}(\boldsymbol{x},t) = \gamma_{xx}(x,y,z,t), \tag{57}$$

$$\gamma_{yy}(\boldsymbol{x},t) = \gamma_{yy}(x,y,z,t), \tag{58}$$

$$\gamma_{zz}(\boldsymbol{x},t) = \gamma_{zz}(x,y,z,t). \tag{59}$$

The off-diagonal stresses and the off-diagonal gamma functions are defined on several staggered grids

$$\sigma_{xy}(\boldsymbol{x},t) = \sigma_{xy}(x + \Delta x/2, y + \Delta y/2, z, t), \tag{60}$$

$$\sigma_{xz}(x,t) = \sigma_{xz}(x + \Delta x/2, y, z + \Delta z/2, t), \tag{61}$$

$$\sigma_{yz}(\boldsymbol{x},t) = \sigma_{yz}(x,y + \Delta y/2, z + \Delta z/2, t), \tag{62}$$

$$\gamma_{xy}(\boldsymbol{x},t) = \gamma_{xy}(x + \Delta x/2, y + \Delta y/2, z, t), \tag{63}$$

$$\gamma_{xz}(\boldsymbol{x},t) = \gamma_{xz}(x + \Delta x/2, y, z + \Delta z/2, t), \tag{64}$$

$$\gamma_{yz}(\boldsymbol{x},t) = \gamma_{yz}(x,y+\Delta y/2,z+\Delta z/2,t), \tag{65}$$

(66)

The Lamé parameters are defined on a regular grid as follows: as follows:

$$\lambda_u(\mathbf{x}) = \lambda_u(x, y, z), \tag{67}$$

$$\mu_u(\mathbf{x}) = \mu_u(x, y, z). \tag{68}$$

The inverse density and  $\mu$  are defined on three different staggered grids as follows:

$$\rho_x^{-1}(\mathbf{x}) = \rho^{-1}(x + \Delta x/2, y, z), \tag{69}$$

$$\rho_y^{-1}(x) = \rho^{-1}(x, y + \Delta y/2, z), \tag{70}$$

$$\rho_z^{-1}(\mathbf{x}) = \rho^{-1}(x, y, z + \Delta z/2),$$
(71)

$$\mu_{uxy}(\mathbf{x}) = \mu_u(x + \Delta x/2, y + \Delta y/2, z), \tag{72}$$

$$\mu_{uyz}(\boldsymbol{x}) = \mu_u(x, y + \Delta y/2, z + \Delta z/2), \tag{73}$$

$$\mu_{uxz}(\boldsymbol{x}) = \mu_u(x + \Delta x/2, y, z + \Delta z), \tag{74}$$

The visco-elastic parameters  $\beta_1$ ,  $\beta_2$  and  $\eta_1$  and  $\eta_2$  are also defined on several staggered grids:

$$\beta_{1xy}x) = \beta_1(x + \Delta x, y + \Delta y, z), \tag{76}$$

$$\beta_{1uz}(\boldsymbol{x}) = \beta_1(x, y + \Delta y, z + \Delta z), \tag{77}$$

$$\beta_{1xz}(\boldsymbol{x}) = \beta_1(x + \Delta x, y, z + \Delta z), \tag{78}$$

$$\beta_{2xy}(\boldsymbol{x}) = \beta_2(x + \Delta x, y + \Delta y, z), \tag{79}$$

$$\beta_{2yz}(\mathbf{x}) = \beta_2(x, y + \Delta y, z + \Delta z), \tag{80}$$

$$\beta_{2xz}(\boldsymbol{x}) = \beta_2(x + \Delta x, y, z + \Delta z), \tag{81}$$

$$\eta_{1x}(\boldsymbol{x}) = \eta_1(x + \Delta x/2, y, z), \tag{82}$$

$$\eta_{2x}(\boldsymbol{x}) = \eta_2(x + \Delta x/2, y, z), \tag{83}$$

$$\eta_{1y}(x) = \eta_1(x, y + \Delta y/2, z),$$
(84)

$$\eta_{2y}(\boldsymbol{x}) = \eta_1(x, y + \Delta y/2, z), \tag{85}$$

$$\eta_{1z}(\boldsymbol{x}) = \eta_1(x, y, z + \Delta z/2), \tag{86}$$

$$\eta_{2z}(\boldsymbol{x}) = \eta_1(x, y, z + \Delta z/2). \tag{87}$$

Differentiation is now replaced by numerical approximations so that  $\partial_x, \partial_y$  and  $\partial_z$  are replaced with numerical operators  $d_x^+, d_x^-, d_y^+, d_y^-, d_z^+$  and  $d_z^-$ . These operators connects the staggered and reference grids, and we illustrate this with the differentiation in the x-direction. The derivative of a function a(x) is approximately given at  $a(x + \Delta x/2)$  and at  $a(x - \Delta x/2)$  by

$$a'(x + \Delta x/2) = d_x^+ a(x),$$
 (88)

$$a'(x - \Delta x/2) = d_x^- a(x).$$
 (89)

The differentiators  $d^+$  and  $d^-$  are given by (Holberg, 1987)

$$\partial^{+} = \frac{1}{\Delta x} \sum_{l=1}^{L} \alpha_{l} \left[ u(x + l\Delta x) - u(x - (l-1)\Delta x) \right]$$

$$\partial^{-} = \frac{1}{\Delta x} \sum_{l=1}^{L} \alpha_{l} \left[ u(x + (l-1)\Delta x) - u(x - l\Delta x) \right]$$
(90)

where the coefficients  $\alpha_l$  are found through an optimization procedure. Similar differentiators are defined for the y-direction and for the z-direction, with obvious names.

Using the numerical differentiators the equations of motion becomes:

$$\partial_t v_x = \rho_i^{-1} \left( d_x^+ \sigma_{xx} + d_y^+ \sigma_{xy} + d_z^+ \sigma_{xz} \right) + f_x$$
 (91)

$$+ \sum_{l=0}^{N} \theta_{xxx}^{l} + \sum_{l=0}^{N} \theta_{yxy}^{l} + \sum_{l=0}^{N} \theta_{zxz}^{l}, \tag{92}$$

$$\partial_t v_y = d_x^+ \sigma_{yx} + d_y^+ \sigma_{yy} + d_z^+ \sigma_{yz} + f_y, \tag{93}$$

$$+ \sum_{l=0}^{N} \theta_{xyx}^{l} + \sum_{l=0}^{N} \theta_{yyy}^{l} + \sum_{l=0}^{N} \theta_{zyz}^{l}, \tag{94}$$

$$\partial_t v_z = d_x^+ \sigma_{zx} + d_y^+ \sigma_{zy} + d_z^+ \sigma_{zz} + f_z, \tag{95}$$

$$+ \sum_{l=0}^{N} \theta_{xzx}^{l} + \sum_{l=0}^{N} \theta_{yzy}^{l} + \sum_{l=0}^{N} \theta_{zzz}^{l}.$$
 (96)

The computation of the strains becomes as follows:

$$\dot{e}_{xx} = d_x^- v_x, 
\dot{e}_{yy} = d_y^- v_y, 
\dot{e}_{zz} = d_z^- v_z, 
\dot{e}_{xy} = \frac{1}{2} (d_x^+ v_y + d_y^+ v_x), 
\dot{e}_{xz} = \frac{1}{2} (d_x^+ v_z + d_z^+ v_x), 
\dot{e}_{yz} = \frac{1}{2} (d_y^+ v_z + d_z^+ v_y).$$
(97)

The time derivatives is approximated by the central difference

$$\dot{a}(t) = \frac{a(t + \Delta t/2) - a(t - \Delta t/2)}{\Delta t} \tag{98}$$

# Solution algorithm for the three dimensional case

We are now in a position to formulate a complete numerical solution of the visco-elastic equations.

#### Computation of the particle velocity

We use the expression for the approximate time derivative given by equation (98) in equations (??) to obtain an expression for the components of the particle velocity

$$\begin{split} v_x(t + \Delta t/2) &= \Delta t \rho_x^{-1} \left[ d_x^+ \sigma_{xx}(t) + d_y^+ \sigma_{xy}(t) + d_z^+ \sigma_{xz}(t) \right] + \Delta t \rho_x^{-1} f_x(t) + \\ &+ \Delta t \sum_{l=0}^N \theta_{xxx}^l(t) + \Delta t \sum_{l=0}^N \theta_{yxy}^l(t) + \Delta t \sum_{l=0}^N \theta_{zxz}^l(t) + v_x(t - \Delta t/2), \end{split}$$

$$v_{y}(t + \Delta t/2) = \Delta t \rho_{y}^{-1} \left[ d_{x}^{+} \sigma_{yx}(t) + d_{y}^{+} \sigma_{yy}(t) + d_{z}^{+} \sigma_{yz}(t) \right] + \Delta t \rho_{y}^{-1} f_{y}(t)$$

$$+ \Delta t \sum_{l=0}^{N} \theta_{xyx}^{l}(t) + \Delta t \sum_{l=0}^{N} \theta_{yyy}^{l}(t) + \Delta t \sum_{l=0}^{N} \theta_{zyz}^{l}(t) + v_{y}(t - \Delta t/2),$$

$$v_{z}(t + \Delta t/2) = \Delta t \rho_{z}^{-1} \left[ d_{x}^{+} \sigma_{zx}(t) + d_{y}^{+} \sigma_{zy}(t) + d_{z}^{+} \sigma_{zz}(t) \right] + \Delta t \rho_{z}^{-1} f_{z}(t)$$

$$+ \Delta t \sum_{l=0}^{N} \theta_{xzx}^{l}(t) + \Delta t \sum_{l=0}^{N} \theta_{yzy}^{l}(t) + \Delta t \sum_{l=0}^{N} \theta_{zzz}^{l}(t). + v_{z}(t - \Delta t/2)$$

$$(99)$$

The strains can now be computed from equation (97)

$$\dot{e}_{xx}(t + \Delta t/2) = d_x^- v_x(t + \Delta t/2), 
\dot{e}_{yy}(t + \Delta t/2) = d_y^- v_y(t + \Delta t/2), 
\dot{e}_{zz}(t + \Delta t/2) = d_z^- v_z(t + \Delta t/2), 
\dot{e}_{xy}(t + \Delta t/2) = \frac{1}{2} \left[ d_x^+ v_y(t + \Delta t/2) + d_y^+ v_x(t + \Delta t/2) \right], 
\dot{e}_{xz}(t + \Delta t/2) = \frac{1}{2} \left[ d_x^+ v_z(t + \Delta t/2) + d_z^+ v_x(t + \Delta t/2) \right], 
\dot{e}_{yz}(t + \Delta t/2) = \frac{1}{2} \left[ d_y^+ v_z(t + \Delta t/2) + d_z^+ v_y(t + \Delta t/2) \right].$$
(100)

Equations (108) can be solved for the stresses using the same approach as for the particle velocities:

$$\sigma_{xx}(t + \Delta t) = \Delta t \lambda_{u} \left[ \dot{e}_{xx}(t + \Delta t/2) + \dot{e}_{yy}(t + \Delta t/2) + \dot{e}_{zz}(t + \Delta t/2) \right] 
+ 2\mu_{u}\dot{e}_{xx}(t + \Delta t/2) + \Delta t \dot{q}_{xx} 
+ \Delta t \sum_{l=1}^{N} \gamma_{\lambda}^{l}(t + \Delta t/2) \Delta \lambda_{l} + 2\Delta t \sum_{l=1}^{N} \gamma_{xx}^{l}(t + \Delta t/2) \Delta \mu_{l}(t + \Delta t/2) 
+ \sigma_{xx}(t), (101) 
\sigma_{yy}(t + \Delta t) = \Delta t \lambda_{u} \left[ \dot{e}_{xx}(t + \Delta t/2) + \dot{e}_{yy}(t + \Delta t/2) + \dot{e}_{zz}(t + \Delta t/2) \right] 
+ 2\Delta t \mu_{u}\dot{e}_{yy}(t + \Delta t/2) + \Delta t \dot{q}_{yy}(t + \Delta t/2) 
+ \Delta t \sum_{l=1}^{N} \gamma_{\lambda}^{l}(t + \Delta t/2) \Delta \lambda_{l} + 2\Delta t \sum_{l=1}^{N} \gamma_{yy}^{l}(t + \Delta t/2) \Delta \mu_{l} (103) 
+ \sigma_{yy}(t) (104) 
\sigma_{zz}(t + \Delta t) = \Delta t \lambda_{u} \left[ \dot{e}_{xx}(t + \Delta t/2) + \dot{e}_{yy}(t + \Delta t/2) + \dot{e}_{zz}(t + \Delta t/2) \right] (105) 
+ 2\mu_{x}\dot{e}_{zz}(t + \Delta t/2) + \Delta t \dot{q}_{zz}(t + \Delta t/2)$$

$$+ \Delta t \sum_{l=1}^{N} \gamma_{\lambda}^{l}(t + \Delta t/2) \Delta \lambda_{l} + 2\Delta t \sum_{l=1}^{N} \gamma_{zz} \Delta \mu_{l}(t + \Delta t/2),$$

$$+ \sigma_{zz}. \qquad (106)$$

$$\sigma_{xy}(t + \Delta t) = 2\Delta t \mu \dot{e}_{xy}(t + \Delta t/2) + 2\Delta t \sum_{l=1}^{N} \gamma_{xy}^{l}(t + \Delta t/2) \Delta \mu_{l} + \Delta t \dot{q}_{xy}(t + \Delta t/2)$$

$$+ \sigma_{xy}(t),$$

$$\sigma_{xz}(t + \Delta t) = 2\Delta t \mu \dot{e}_{xz}(t + \Delta t/2) + 2\Delta t \sum_{l=1}^{N} \gamma_{xz}^{l}(t + \Delta t/2) \Delta \mu_{l} + \Delta t \dot{q}_{xz}(t + \Delta t/2)$$

$$+ \sigma_{xz}(t), \qquad (107)$$

$$\sigma_{yz}(t + \Delta t) = 2\Delta \mu \dot{e}_{yz}(t + \Delta t/2) + 2\Delta t \sum_{l=1}^{N} \gamma_{yz}^{l}(t + \Delta t/2) \Delta \mu_{l} + \dot{q}_{yz}(t + \Delta t/2)$$

$$+ \sigma_{yz}(t). \qquad (108)$$

The gamma functions are updated as follows

$$\gamma_{\lambda}^{l}(t+3/2\Delta t) = \alpha_{1}^{l}\gamma_{\lambda}^{l}(t+\Delta t/2) + \alpha_{2}^{l}\left[\dot{e}_{xx}(t+\Delta t/) + \dot{e}_{yy}(t+\Delta t/2) + \dot{e}_{zz}(t+\Delta t/2)\right], 
\gamma_{\mu}^{l}(t+3/2\Delta t) = \beta_{1}^{l}\gamma_{\mu}^{l}(t+\Delta t/2) + \beta_{2}^{l}\left[\dot{e}_{xx}(t+\Delta t/) + \dot{e}_{yy}(t+\Delta t/2) + \dot{e}_{zz}(t+\Delta t/2)\right], 
\gamma_{xy}^{l}(t+3/2\Delta t) = \beta_{1xy}^{l}\gamma_{xy}^{l}(t+\Delta t/2) + \beta_{2xy}^{l}\dot{e}_{xy}(t+\Delta t/2). 
\gamma_{xz}^{l}(t+3/2\Delta t) = \beta_{1xz}^{l}\gamma_{xz}^{l}(t+\Delta t/2) + \beta_{2xz}^{l}\dot{e}_{xz}(t+\Delta t/2). 
\gamma_{yz}^{l}(t+3/2\Delta t) = \beta_{1xz}^{l}\gamma_{yz}^{l}(t+\Delta t/2) + \beta_{2xz}^{l}\dot{e}_{yz}(t+\Delta t/2).$$
(109)

The  $\theta$  functions are updated as:

$$\begin{array}{lll} \theta_{xxx}(t+\Delta t) &=& \eta_1^l \theta_{xxx}^l(t+\Delta t/2) + \eta_2^l \partial_x \sigma_{xx}(t+\Delta t/2). \\ \theta_{yxy}(t+\Delta t) &=& \eta_1^l \theta_{yxy}^l(t+\Delta t/2) + \eta_2^l \partial_y \sigma_{xy}(t+\Delta t/2). \\ \theta_{zxz}(t+\Delta t) &=& \eta_1^l \theta_{zxz}^l(t+\Delta t/2) + \eta_2^l \partial_z \sigma_{xz}(t+\Delta t/2). \\ \theta_{xyx}(t+\Delta t) &=& \eta_1^l \theta_{xyx}^l(t+\Delta t/2) + \eta_2^l \partial_x \sigma_{yx}(t+\Delta t/2). \\ \theta_{yyy}(t+\Delta t) &=& \eta_1^l \theta_{yyy}^l(t+\Delta t/2) + \eta_2^l \partial_y \sigma_{yy}(t+\Delta t/2). \\ \theta_{zyz}(t+\Delta t) &=& \eta_1^l \theta_{zyz}^l(t+\Delta t/2) + \eta_2^l \partial_z \sigma_{yz}(t+\Delta t/2). \\ \theta_{xyx}(t+\Delta t) &=& \eta_1^l \theta_{xyx}^l(t+\Delta t/2) + \eta_2^l \partial_x \sigma_{yx}(t+\Delta t/2). \\ \theta_{xzx}(t+\Delta t) &=& \eta_1^l \theta_{xzx}^l(t+\Delta t/2) + \eta_2^l \partial_x \sigma_{zx}(t+\Delta t/2). \\ \theta_{yzy}(t+\Delta t) &=& \eta_1^l \theta_{yzy}^l(t+\Delta t/2) + \eta_2^l \partial_x \sigma_{zx}(t+\Delta t/2). \\ \theta_{yzy}(t+\Delta t) &=& \eta_1^l \theta_{yzy}^l(t+\Delta t/2) + \eta_2^l \partial_x \sigma_{zy}(t+\Delta t/2). \end{array}$$

$$\theta_{zzz}(t + \Delta t) = \eta_1^l \theta_{zzz}^l(t + \Delta t/2) + \eta_2^l \partial_z \sigma_{zz}(t + \Delta t/2).$$
(110)

#### 2D Acoustic case

For the acoustic 2D case we reduce the equations above by neglecting the y-axis terms and putting  $\mu = 0$ . We consider also the pseudo-stress  $\sigma$  defined by

$$\sigma = \frac{1}{2} \left( \sigma_{xx} + \sigma_{zz} \right)$$

We then get the acoustic 2D scheme as:

$$v_{x}(t + \Delta t/2) = \Delta t \left[ \rho_{ux}^{-1} d_{x}^{+} \sigma_{xx}(t) + \rho_{ux}^{-1} f_{x}(t) \right] +$$

$$+ \Delta t \sum_{l=0}^{N} \theta_{x}^{l}(t) \Delta \rho_{x}^{-1} + v_{x}(t - \Delta t/2),$$

$$v_{z}(t + \Delta t/2) = \Delta t \left[ \rho_{uz}^{-1} d_{z}^{+} \sigma_{zz}(t) + \Delta t \rho_{uz}^{-1} f_{z}(t) \right]$$

$$+ \Delta t \sum_{l=0}^{N} \theta_{z}^{l}(t) \Delta \rho_{z}^{-1} + v_{z}(t - \Delta t/2).$$

The strains can now be computed from:

$$\dot{e}_{xx}(t + \Delta t/2) = d_x^- v_x(t + \Delta t/2),$$
  
 $\dot{e}_{zz}(t + \Delta t/2) = d_z^- v_z(t + \Delta t/2).$ 

Equations (108) can be solved for the stresses using the same approach as for the particle velocities:

$$\sigma(t + \Delta t) = \Delta t \lambda_u \left[ \dot{e}_{xx}(t + \Delta t/2) + \dot{e}_{zz}(t + \Delta t/2) \right] + \Delta t \dot{q},$$

$$+ \Delta t \sum_{l=1}^{N} \gamma^l (t + \Delta t/2) \Delta \lambda_l + \sigma(t).$$

We now split the  $\gamma^l$  into two parts  $\gamma^l_x$  and  $\gamma^l_z$  as follows:

$$\begin{split} \sigma(t+\Delta t) &= \Delta t \lambda_u \left[ \dot{e}_{xx}(t+\Delta t/2) + \dot{e}_{zz}(t+\Delta t/2) \right] + \Delta t \dot{q} \\ &+ \Delta t \sum_{l=1}^{N} \left[ \gamma_x^l (t+\Delta t/2) \Delta \lambda_l + \gamma_z^l (t+\Delta t/2) \Delta \lambda_l \right] + \sigma(t). \end{split}$$

The  $\theta$  functions are updated as:

$$\theta_x(t + \Delta t) = \eta_{1x}^l \theta_x^l(t) + \eta_{2x}^l \partial_x \sigma(t),$$
  
$$\theta_z(t + \Delta t) = \eta_{1z}^l \theta_x^l(t) + \eta_{2z}^l \partial_y \sigma(t).$$

The  $\gamma$  functions are given by

$$\begin{array}{lcl} \gamma_{x}^{l}(t+3/2\Delta t) & = & \alpha_{1x}^{l}\gamma_{x}^{l}(t+\Delta t/2) + \alpha_{2x}^{l}\dot{e}_{xx}(t+\Delta t/2), \\ \gamma_{z}^{l}(t+3/2\Delta t) & = & \alpha_{1z}^{l}\gamma_{z}^{l}(t+\Delta t/2) + \alpha_{2z}^{l}\dot{e}_{zz}(t+\Delta t/2). \end{array}$$

#### Standard linear solid

The coefficients are

$$\begin{array}{rcl} \alpha_{1x}^{l} & = & \exp\left(-\frac{d_{x}(x)\Delta t}{\tau_{\sigma l}^{\lambda}}\right), \\ \alpha_{2x}^{l} & = & \frac{d_{x}(x)\Delta t}{(\tau_{\sigma l}^{\lambda}\sum_{l=1}^{N}\frac{\tau_{el}^{\lambda}}{\tau_{\sigma l}^{\lambda}})} \\ \alpha_{1z}^{l} & = & \exp\left(-\frac{d_{z}(z)\Delta t}{\tau_{\sigma l}^{\lambda}}\right), \\ \alpha_{2z}^{l} & = & \frac{d_{z}(z)\Delta t}{(\tau_{\sigma l}^{\lambda}\sum_{l=1}^{N}\frac{\tau_{el}^{\lambda}}{\tau_{\sigma l}^{\lambda}})} \\ \eta_{1x}^{l} & = & \exp\left(-\frac{d_{x}(x)\Delta t}{\tau_{\sigma l}^{\rho}}\right), \\ \eta_{2x}^{l} & = & \frac{d_{x}(x)\Delta t}{(\tau_{\sigma l}^{\rho}\sum_{l=1}^{N}\frac{\tau_{el}^{\rho}}{\tau_{\sigma l}^{\rho}})}, \\ \eta_{1z}^{l} & = & \exp\left(-\frac{d_{z}(z)\Delta t}{\tau_{\sigma l}^{\rho}}\right), \\ \eta_{2z}^{l} & = & \frac{d_{z}(z)\Delta t}{(\tau_{\sigma l}^{\rho}\sum_{l=1}^{N}\frac{\tau_{el}^{\rho}}{\tau_{\sigma l}^{\rho}})}. \end{array}$$

The profile functions  $d_x$  and  $d_z$  are

$$d_x(x) = (x/L)^2, d_z(y) = (z/L)^2,$$

where L is the length of the absorbing layer and and we also have

$$\Delta \lambda_l = \lambda_u \left( 1 - \frac{\tau_{\epsilon l}^{\lambda}}{\tau_{\sigma l}^{\lambda}} \right) \Delta \rho^{-1} = \rho_u^{-1} \left( 1 - \frac{\tau_{\epsilon l}^{\rho}}{\tau_{\sigma l}^{\rho}} \right)$$
 (111)

#### Maxwell solid

The coefficients are

$$\alpha_{1x} = -\frac{1}{\tau_0^{\lambda}} \exp\left(-\frac{d_x(x)\Delta t}{\tau_0^{\lambda}}\right),$$
(112)

$$\alpha_{2x} = \frac{d_x(x)\Delta t}{\tau_0^{\lambda}},\tag{113}$$

$$\alpha_{1z} = -\frac{1}{\tau_0^{\lambda}} \exp\left(-\frac{d_z(z)\Delta t}{\tau_0^{\lambda}}\right),$$
(114)

$$\alpha_{2z} = \frac{d_z(z)\Delta t}{\tau_0^{\lambda}}. (115)$$

$$\eta_{1x} = -\frac{1}{\tau_0^{\rho}} \exp\left(-\frac{d_x(x)\Delta t}{\tau_0^{\rho}}\right),$$
(116)

$$\eta_{2x} = \frac{d_x(x)\Delta t}{\tau_0^{\rho}},\tag{117}$$

$$\eta_{1z} = -\frac{1}{\tau_0^{\rho}} \exp\left(-\frac{d_z(z)\Delta t}{\tau_0^{\rho}}\right),$$
(118)

$$\eta_{2z} = \frac{d_z(z)\Delta t}{\tau_0^{\rho}}. (119)$$

We also have

$$\Delta \lambda = \lambda_{u}, \tag{120}$$

$$\Delta \lambda = \lambda_u, \qquad (120)$$

$$\Delta \rho^{-1} = \rho_u^{-1}. \qquad (121)$$

#### Plane Waves

The bulk modulus is considered to be visco-acoustic and is in the frequency domain given as

$$K(\omega) = K_0 G(\omega), \tag{122}$$

where  $K_0$  is a constant to be specified. The density is also taken to be frequency dependent and complex

$$\rho(\omega) = \rho_0 G^{-1}(\omega), \tag{123}$$

Consider a horizontally layered medium with bulk-modulus and density given by equations 122 and 123. According to Ursin (1983), a downgoing wave in a homogeneous layer with unit amplitude is given by

$$\exp(-ik_z|z|),\tag{124}$$

where z is the depth of the layer and the vertical wavenumber  $k_z$  is given as:

$$k_z = -\frac{\omega}{c}\cos(\theta). \tag{125}$$

Here  $\theta$  is the angle between the z-axis and the propagation direction of the wave. The wave velocity c is given by

$$c = \sqrt{\frac{K(\omega)}{\rho(\omega)}} = \sqrt{\frac{K_0}{\rho_0}} G(\omega). \tag{126}$$

The reflection coefficient across an interface between two layers (Ursin, 1983) is given by

$$R = \frac{Z_{-} - Z_{+}}{Z_{-} + Z_{+}},\tag{127}$$

where the impedances  $Z_{-}$  and  $Z_{+}$  above and below the interface, respectively, are given by

$$Z = \frac{\rho\omega}{k_z} = Z_0,\tag{128}$$

where  $Z_0 = \rho_0 c_0 \cos(\theta)$ . Consider the special case where the medium above the interface is purely acoustic, i.e G = H = 1, and the medium below the interface is visco-acoustic, and in addition choose  $Z_0$  above the interface equal to  $Z_0$  below the interface. Then R is exactly zero for all incidence angles.

#### Maxwell solid

A particular choice is the classical Maxwell visco-acoustic medium with G given by (Casula et al., 1992)

$$G(\omega) = \left(1 - \frac{i}{\omega \tau}\right)^{-1},\tag{129}$$

We then get for the velocity c

$$c = \left(1 - \frac{i}{\omega \tau}\right)^{-1} \sqrt{\frac{K_0}{\rho_0}},\tag{130}$$

and the vertical wavenumber  $k_z$  becomes

$$k_z = \frac{\omega}{c_0} - \frac{i}{c_0 \tau}. (131)$$

The wave are then described by

$$\exp\left(\frac{-i\omega z}{c_0}\right)\exp\left(\frac{-z}{c_0\tau}\right),\tag{132}$$

which is a dispersion-free wave with frequency independent attenuation.

#### Standard linear solid

A particular choice is the standard linear solid visco-acoustic medium with G given by (Casula et al., 1992)

$$G(\omega) = \frac{1 + i\omega\tau_{\epsilon}}{1 + i\omega\tau_{\sigma}} \tag{133}$$

We then get for the velocity c

$$c = \frac{1 + i\omega\tau_{\epsilon}}{1 + i\omega\tau_{\sigma}} \sqrt{\frac{K_0}{\rho_0}},\tag{134}$$

and the vertical wavenumber  $k_z$  becomes

$$k_z = \frac{\omega}{c_0} \frac{1 + i\omega \tau_{\epsilon}}{1 + i\omega \tau_{\sigma}} \tag{135}$$

The wave are then described by

$$\exp\left[iz\left(\frac{\omega}{c_0}\right)\frac{1+i\omega\tau_{\epsilon}}{1+i\omega\tau_{\sigma}}\right]. \tag{136}$$

which is

$$\exp\left[iz\left(\frac{\omega}{c_0}\right)\frac{1+\omega^2\tau_{\epsilon}\tau_{\sigma}}{1+\omega^2\tau_{\sigma}^2}\right]\exp\left[\left(\frac{-z}{c_0}\right)\frac{\omega^2(\tau_{\epsilon}-\tau_{\sigma})}{1+\omega^2\tau_{\sigma}^2}\right]$$
(137)

# Time dependent density

Williams (2001) gives an expression for dynamic density used for acoustic waves in porous media:

$$\rho_{eff}(\omega) = \rho_f \left( \frac{\alpha (1 - \beta)\rho_s + \beta (\alpha - 1)\rho_f + \frac{i\beta \rho F\eta}{\rho_f \omega \kappa}}{\beta (1 - \beta)\rho_s + (\alpha - 2\beta + \beta^2)\rho_f + \frac{i\beta F\eta}{\omega \kappa}} \right)$$
(138)

The parameters are

$$\beta$$
 porosity

 $\rho_s$  Mass density of grains

 $\eta$  Viscosity

 $\kappa$  Permeability

 $\alpha$  Tortuosity

 $F$  Frequency correction function

Multiply by  $i\omega$  to get:

$$\rho_{eff}(\omega) = \rho_f \left( \frac{[\alpha(1-\beta)\rho_s + \beta(\alpha-1)\rho_f]i\omega - \frac{\beta\rho F\eta}{\rho_f \kappa}}{[\beta(1-\beta)\rho_s + (\alpha-2\beta+\beta^2)\rho_f]i\omega - \frac{\beta F\eta}{\kappa}} \right)$$
(139)

$$\rho_{eff}(\omega) = \frac{\beta \rho F \eta / \rho_f \kappa}{\beta F \eta / \kappa} \rho_f \left( \frac{\frac{[\alpha(1-\beta)\rho_s + \beta(\alpha-1)\rho_f]}{\beta \rho F \eta / \rho_f \kappa} i\omega - 1}{\frac{[\beta(1-\beta)\rho_s + (\alpha-2\beta + \beta^2)\rho_f]}{\beta F \eta / \kappa} i\omega - 1} \right)$$
(140)

$$\rho_{eff}(\omega) = \rho \left( \frac{1 - \frac{[\alpha(1-\beta)\rho_s + \beta(\alpha-1)\rho_f]}{\beta\rho F \eta/\rho_f \kappa} i\omega}{1 - \frac{[\beta(1-\beta)\rho_s + (\alpha-2\beta+\beta^2)\rho_f]}{\beta F \eta/\kappa} i\omega} \right)$$
(141)

$$\rho_{eff}^{-1}(\omega) = \rho^{-1} \left( \frac{1 - \frac{\left[\alpha(1-\beta)\rho_s + \beta(\alpha-1)\rho_f\right]}{\beta\rho F\eta/\rho_f \kappa} i\omega}{1 - \frac{\left[\beta(1-\beta)\rho_s + (\alpha-2\beta+\beta^2)\rho_f\right]}{\beta F\eta/\kappa} i\omega} \right)^{-1}$$
(142)

$$\rho_{eff}^{-1}(\omega) = \rho^{-1} \left( \frac{1 - \tau_{\epsilon} i\omega}{1 - \tau_{\sigma} i\omega} \right)^{-1} \tag{143}$$

where

$$\tau_{\sigma} = \frac{\left[\alpha(1-\beta)\rho_{s} + \beta(\alpha-1)\rho_{f}\right]}{\beta\rho F\eta/\rho_{f}\kappa},$$

$$\tau_{\epsilon} = \frac{\left[\beta(1-\beta)\rho_{s} + (\alpha-2\beta+\beta^{2})\rho_{f}\right]}{\beta F\eta/\kappa}.$$
(144)

#### References

Casula, G., J. Carcione, et al., 1992, Generalized mechanical model analogies of linear viscoelastic behaviour: Bollettino di geofisica teorica ed applicata, **34**, 235–256.

Holberg, O., 1987, Computational aspects of the choice of operator and sampling interval for numerical differentiation in large-scale simulation of wave phenomena: Geophysical P, **35**, 629–655.

Hudson, J., 1985, The excitation and propagation of elastic waves: Cambridge University Press. Cambridge Monographs on Mechanics Series.

Komatitsch, D., and R. Martin, 2007, An unsplit convolutional perfectly matched layer improved at grazing incidence for the seismic wave equation: Geophysics, 72, SM155–SM167.

Williams, K. L., 2001, An effective density fluid model for acoustic propagation in sediments derived from biot theory: The Journal of the Acoustical Society of America, **110**, 2276–2281.

#### APPENDIX A: The viscoelastic standard linear solid

Bolzman's generalization of Hook's law to the visco-elastic case is (Hudson, 1985):

$$\sigma_{ij} = \psi_{ijkl} * \dot{e}_{kl}, \tag{A-1}$$

where  $\psi_{ijkl}$  is known as the relaxation tensor. The \* denotes convolution defined by

$$a(t) * b(t) = \int_0^t a(t-\tau)b(\tau). \tag{A-2}$$

Integrating (A-1) by parts

$$\sigma_{ij}(t) = |_0^t \psi_{ijkl}(t-\tau)e_{kl}(\tau) + \int_0^t \dot{\psi}_{ijkl}(t-\tau)e_{kl}(\tau), \tag{A-3}$$

and using e(t=0) = 0 I get

$$\sigma_{ij}(t) = \psi(0)_{ijkl} e_{kl}(t) + \int_{0+}^{t} \dot{\psi}_{ijkl}(t-\tau) e_{kl}(\tau)$$
 (A-4)

For the Zener model the components of the  $\psi_{ijkl}$  tensor have the form

$$\psi(t) = K \left[ 1 - \frac{1}{N} \sum_{l=1}^{N} (1 - \frac{\tau_{el}}{\tau_{\sigma l}}) \exp(-t/\tau_{\sigma l}) \right] H(t).$$
 (A-5)

where  $K_r$  is a relaxed modulus, N is the number of Zener mechanisms,  $\tau_{\sigma l}$  and  $\tau_{\epsilon l}$  are relaxation times. H(t) is the Heavy side function. The time derivative of  $\psi$  is equal to:

$$\dot{\psi} = \phi(t),\tag{A-6}$$

where  $\phi$  is equal to:

$$\phi(t) = \frac{1}{N} \sum_{l=1}^{N} \left[ \left( \frac{K_r}{\tau_{\sigma l}} \right) \left( 1 - \frac{\tau_{\epsilon l}}{\tau_{\sigma l}} \right) \exp(-t/\tau_{\sigma l}) \right] H(t). \tag{A-7}$$

Using the above we have for the stress:

$$\sigma_{ij}(t) = c_{ijkl}e_{kl} + \int_{0+}^{t} \phi_{ijkl}(t-\tau)e_{kl}(\tau)$$
(A-8)

This is most conveniently written as

$$\sigma_{ij}(t) = c_{ijkl}(t) * e_{kl}(t), \tag{A-9}$$

where

$$c_{ijkl}(t) = \psi(0)_{ijkl}\delta(t) + \phi_{ijkl}(t), \tag{A-10}$$

By definition  $\psi(t=0)$  corresponds to the unrelaxed modulus so that we have

$$K_u = \frac{1}{N} \sum_{l=1}^{N} \frac{\tau_{el}}{\tau_{\sigma l}} K_r \tag{A-11}$$

or

$$K_r = \frac{K_u}{\frac{1}{N} \sum_{l=1}^{N} \frac{\tau_{\epsilon l}}{\tau_{\sigma l}}}$$
 (A-12)

The  $\phi$  function can then be expressed in terms of the unrelaxed moduli:

$$\phi(t) = \sum_{l=1}^{N} \left[ \left( \frac{\exp(-t/\tau_{\sigma l})}{\tau_{\sigma l} \sum_{l=1}^{N} \frac{\tau_{\epsilon l}}{\tau_{\sigma l}}} \right) K_u \left( 1 - \frac{\tau_{\epsilon l}}{\tau_{\sigma l}} \right) \right]$$
(A-13)

Finally, we express  $\phi$  as:

$$\phi(t) = \sum_{l=1}^{N} \phi^l(t) \tag{A-14}$$

where

$$\phi^{l}(t) = \left(\frac{\exp(-t/\tau_{\sigma l})}{\tau_{\sigma l} \sum_{l=1}^{N} \frac{\tau_{e l}}{\tau_{\sigma l}}}\right) \Delta K_{l}$$
(A-15)

and  $\Delta K_l$  is

$$\Delta K_l = K_u \left( 1 - \frac{\tau_{\epsilon l}}{\tau_{\sigma l}} \right) \tag{A-16}$$

It is most practical to write the time-dependent visco-elastic constants as

$$\lambda(t) = \lambda_u \delta(t) + \phi_{\lambda}(t), \tag{A-17}$$

$$\mu(t) = \mu_u \delta(t) + \phi_\mu(t), \tag{A-18}$$

where  $\phi_{\lambda}$  is given as:

$$\phi_{\lambda}(t) = \sum_{l=1}^{N} \left( \frac{\exp(-t/\tau_{\sigma l}^{\lambda})}{\tau_{\sigma l}^{\lambda} \sum_{l=1}^{N} \frac{\tau_{\sigma l}^{\lambda}}{\tau_{\sigma l}^{\lambda}}} \right) \Delta \lambda_{l}$$
(A-19)

and  $\phi_{\mu}$  is given as:

$$\phi_{\mu}(t) = \sum_{l=1}^{N} \left( \frac{\exp(-t/\tau_{\sigma l}^{\mu})}{\tau_{\sigma l}^{\mu} \sum_{l=1}^{N} \frac{\tau_{el}^{\mu}}{\tau_{rl}^{\mu}}} \right) \Delta \mu_{l}$$
(A-20)

#### **Q**-factors

See Casula et al. (1992) for further relations between Q and relaxation times. The Q values are related to the Fourier transform of the  $\lambda$  modulus as

$$Q_{\lambda}^{-1}(\omega) = \frac{Im\lambda(\omega)}{Re\lambda(\omega)}$$
 (A-21)

Assuming  $\lambda$  is given as

$$\lambda(t) = \lambda_u \delta(t) + \phi_{\lambda}(t). \tag{A-22}$$

The fourier transform of  $\lambda$  is given by

$$\lambda(\omega) = \lambda_u + \int_{-\infty}^{\infty} \phi_{\lambda}(t) \exp(-i\omega t). \tag{A-23}$$

The Fourier transform of  $\phi_{\lambda}$  is:

$$\phi_{\lambda}(\omega) = \frac{1}{N} \sum_{l=1}^{N} \left( \frac{\lambda_r}{\tau_{\sigma l}^{\lambda}} \right) \left( 1 - \frac{\tau_{\epsilon l}^{\lambda}}{\tau_{\sigma l}^{\lambda}} \right) \int_{0}^{+\infty} dt \exp(-i\omega) \exp(-t/\tau_{\sigma l}^{\lambda}). \quad (A-24)$$

The results is:

$$\phi_{\lambda}(\omega) = \frac{1}{N} \sum_{l=1}^{N} \left( \frac{\lambda_r}{\tau_{\sigma l}^{\lambda}} \right) \left( 1 - \frac{\tau_{\epsilon l}^{\lambda}}{\tau_{\sigma l}^{\lambda}} \right) \frac{1}{1 + i\omega\tau_{\sigma l}^{\lambda}}.$$
 (A-25)

The fourier transform of  $\lambda$  is then

$$\lambda(\omega) = \lambda_u + \frac{1}{N} \sum_{l=1}^{N} \left(\frac{\lambda_r}{\tau_{\sigma l}^{\lambda}}\right) \left(1 - \frac{\tau_{el}^{\lambda}}{\tau_{\sigma l}^{\lambda}}\right) \frac{1}{1 + i\omega\tau_{\sigma l}^{\lambda}}.$$
 (A-26)

After some (tedious) algebra one obtains

$$\lambda(\omega) = \lambda_r \frac{1}{N} \sum_{l=1}^{N} \frac{1 + i\omega \tau_{\epsilon l}^{\lambda}}{1 + i\omega \tau_{\sigma l}^{\lambda}}$$
 (A-27)

Separating into real and imaginary parts, I get

$$\lambda(\omega) = \lambda_r \frac{1}{N} \sum_{l=1}^{N} \frac{1 + \omega^2 \tau_{\sigma l}^{\lambda} \tau_{\epsilon l}^{\lambda}}{1 + (\omega \tau_{\sigma l}^{\lambda})^2}$$
 (A-28)

$$+ i\lambda_r \frac{1}{N} \sum_{l=1}^{N} \frac{\omega \tau_{\sigma l}^{\lambda} (\tau_{\epsilon}^{\lambda} / \tau_{\sigma l}^{\lambda} - 1)}{1 + (\omega \tau_{\sigma l}^{\lambda})^2}$$
(A-29)

We then have

$$Q_{\lambda}^{-1} = \frac{\sum_{l=1}^{N} \omega \tau_{\sigma l}^{\lambda} \left( \tau_{\epsilon l}^{\lambda} / \tau_{\sigma l}^{\lambda} - 1 \right) / \left[ 1 + (\omega \tau_{\sigma l}^{\lambda})^{2} \right]}{\sum_{l=1}^{N} (1 + \omega^{2} \tau_{\sigma l}^{\lambda} \tau_{\epsilon l}^{\lambda}) / \left[ 1 + (\omega \tau_{\sigma l}^{\lambda})^{2} \right]}$$
(A-30)

The results for the frequency dependence of  $\mu$  is obtained in exactly the same manner as above:

$$\mu(\omega) = \mu_r \frac{1}{N} \sum_{l=1}^{N} \frac{1 + i\omega \tau_{\epsilon l}^{\mu}}{1 + i\omega \tau_{\sigma l}^{\mu}}$$
(A-31)

and the Q-factor for  $\mu$  is

$$Q_{\mu}^{-1} = \frac{\sum_{l=1}^{N} \omega \tau_{\sigma l}^{\lambda} \left( \tau_{\epsilon l}^{\mu} / \tau_{\sigma l}^{\lambda} - 1 \right) / \left[ 1 + (\omega \tau_{\sigma l}^{\mu})^{2} \right]}{\sum_{l=1}^{N} (1 + \omega^{2} \tau_{\sigma l}^{\mu} \tau_{\epsilon l}^{\mu}) / \left[ 1 + (\omega \tau_{\sigma l}^{\mu})^{2} \right]}$$
(A-32)

In practice we need to relate  $Q_l$  and  $Q_\mu$  to  $Q_\kappa$ . We use the relation

$$\kappa(\omega) = \lambda(\omega) + \frac{2}{3}\mu(\omega). \tag{A-33}$$

Splitting into real and imaginary parts

$$\kappa_r(\omega) = \lambda_r(\omega) + \frac{2}{3}\mu_r(\omega).\kappa_i(\omega) = \lambda_i(\omega) + \frac{2}{3}\mu_i(\omega).$$
(A-34)

$$\frac{1}{Q_{\kappa}} = \frac{\kappa_i}{\kappa_r} = \frac{\lambda_i + (2/3)\mu_i}{\lambda_r + (2/3)\mu_r} \tag{A-35}$$

$$\frac{1}{Q_{\kappa}} = \frac{\kappa_i}{\kappa_r} = \frac{\left(\frac{\lambda_i}{\lambda_r}\right) \lambda_r + (2/3) \left(\frac{\mu_i}{\mu_r}\right) \mu_r}{\lambda_r + (2/3)\mu_r} \tag{A-36}$$

$$Q_{\kappa}^{-1} = \frac{Q_{\lambda}^{-1} \lambda_r + (2/3) Q_{\mu}^{-1}}{\lambda_r + (2/3) \mu_r}$$
(A-37)

We can use the P-wave and S-wave velocities

$$\lambda = \rho V_p^2 - (2/3)\rho V_s^2$$

$$\mu = \rho V_s^2 \tag{A-38}$$

$$Q_{\kappa}^{-1} = Q_{\lambda}^{-1} \left[ 1 - \left( \frac{2}{3} \right) \left( \frac{V_s}{V_p} \right)^2 \right] + Q_{\mu}^{-1} \left( \frac{2}{3} \right) \left( \frac{V_s}{V_p} \right)^2 \tag{A-39}$$

#### Q-model parametrization

Q-models can be described by the two relaxation times,  $\tau_{\sigma}$  and  $\tau_{\epsilon}$ . However it is simpler to use the two parameters  $\tau_0$  and  $Q_0$  to describe a model. According to Casula et al. (1992), Appendix B, we have

$$Q(\omega) = Q_0 \frac{1 + \omega^2 \tau_0^2}{2\omega \tau_0}$$

where

$$Q_0 = \frac{2\tau_0}{\tau_{\epsilon} - \tau_{\sigma}},$$
$$\tau_0^2 = \tau_{\epsilon} \tau_{\sigma}.$$

 $\omega=1/\tau_0$  is the minimum value for  $Q(\omega)$ , i.e. the absorption top. We can now find  $\tau_{\sigma}$  and  $\tau_{\epsilon}$  in terms of  $\tau_0$  and  $Q_0$  as:

$$\begin{split} \tau_\epsilon &= \frac{\tau_0}{Q_0} \left[ \sqrt{Q_0^2 + 1} + 1 \right], \\ \tau_\sigma &= \frac{\tau_0}{Q_0} \left[ \sqrt{Q_0^2 + 1} - 1 \right]. \end{split}$$

#### Effective density

We now assume that the effective density has the following form

$$\rho_{eff}^{-1}(t) = s(t). \tag{A-40}$$

We also assume that

$$s(t) = s(0)\delta(t) + \chi(t) \tag{A-41}$$

So that the inverse of the effective density reads

$$\rho_{eff}^{-1}(t) = s_u \delta(t) + \chi(t). \tag{A-42}$$

where  $s_u = s(0) = \rho_u^{-1}$ .

## APPENDIX C: The Maxwell visco-elastic solid

According to Casula et al. (1992) the Maxwell visco-elastic solid has a modulus given by

$$\lambda(t) = \lambda_u \exp(-t/\tau_0)H(t) \tag{A-1}$$

In the frequency domain one gets

$$\lambda(\omega) = \frac{\tau_0 \omega}{\omega \tau_0 - i}.$$
 (A-2)

or,

$$\lambda(\omega) = \frac{\tau_0 i \omega}{i \omega \tau_0 + 1}.$$
 (A-3)

The function  $\phi$  is now:

$$\phi(t) = -\Delta \lambda \frac{1}{\tau_0} \exp(-t/\tau_0), \tag{A-4}$$

where  $\Delta \lambda = \lambda_u$ . The Q-value are related to  $\tau_0$  by:

$$\tau_0 = Q(\omega)/\omega. \tag{A-5}$$

A plane wave

## APPENDIX D: Recursive computation of $\gamma$ and s.

#### Standard Linear Solid

The  $\gamma$ 's involve a convolution, which is difficult to compute directly. However, a recursive relation can be found by considering

$$\gamma_x^{\lambda}(t + \Delta t) = \int_0^{t + \Delta t} d\tau \, \frac{1}{\tau_{\sigma l}^{\lambda} \sum_{l=1}^{N} \frac{\tau_{\sigma l}^{\lambda}}{\tau_{\sigma l}^{\lambda}}} \exp(-\frac{t + \Delta t - \tau}{\tau_{\sigma}^{\lambda}}) \dot{e}_{xx}(\tau).$$

$$\gamma_x^{\lambda}(t+\Delta t) = \frac{1}{\tau_{\sigma l}^{\lambda} \sum_{l=1}^{N} \frac{\tau_{\sigma l}^{\lambda}}{\tau_{\sigma l}^{\lambda}}} \exp(-\frac{\Delta t}{\tau_{\sigma}^{\lambda}}) \int_{0}^{t+\Delta t} d\tau \, \exp(-\frac{t-\tau}{\tau_{\sigma}^{\lambda}}) \dot{e}_{xx}(\tau).$$

$$\begin{split} \gamma_x^{\lambda}(t+\Delta t) &= \frac{1}{\tau_{\sigma l}^{\lambda} \sum_{l=1}^{N} \frac{\tau_{\sigma l}^{\rho}}{\tau_{\sigma l}^{\rho}}} \exp(-\frac{\Delta t}{\tau_{\sigma}^{\lambda}}) \int_{0}^{t} d\tau \, \exp(-\frac{t-\tau}{\tau_{\sigma}^{\lambda}}) \dot{e}_{xx}(\tau) \\ &+ \frac{1}{\tau_{\sigma l}^{\lambda} \sum_{l=1}^{N} \frac{\tau_{\sigma l}^{\rho}}{\tau_{\sigma l}^{\rho}}} \exp(-\frac{\Delta t}{\tau_{\sigma}^{\lambda}}) \int_{t}^{t+\Delta t} d\tau \, \exp(-\frac{t-\tau}{\tau_{\sigma}^{\lambda}}) \dot{e}_{xx}(\tau). \end{split}$$

The second integral is approximated by assuming that  $\dot{e}_{xx}(t)$  is constant in the interval t to  $t + \Delta t$ 

$$\gamma_x^{\lambda}(t + \Delta t) = \frac{1}{\tau_{\sigma l}^{\lambda} \sum_{l=1}^{N} \frac{\tau_{\epsilon l}^{\rho}}{\tau_{\sigma l}^{\rho}}} \exp(-\frac{\Delta t}{\tau_{\sigma}^{\lambda}}) \int_{0}^{t} d\tau \exp(-\frac{t - \tau}{\tau_{\sigma}^{\lambda}}) \dot{e}_{xx}(\tau) + \frac{1}{\tau_{\epsilon}} \exp(-\frac{\Delta t}{\tau_{\sigma}^{\lambda}}) \dot{e}_{xx}(t) \int_{t}^{t + \Delta t} d\tau \exp(-\frac{t - \tau}{\tau_{\sigma}^{\lambda}})$$

Performing the integral we then get

$$\gamma_x^{\lambda}(t + \Delta t) = \gamma_x^{\lambda}(t) \exp(-\frac{\Delta t}{\tau_{\sigma}^{\lambda}}) + \frac{\tau_{\sigma}}{\tau_{\epsilon}} \left[ 1 - \exp(-\frac{\Delta t}{\tau_{\sigma}^{\lambda}}) \right] \dot{e}_{xx}(t).$$

For small  $\Delta t \ll 1$  the last equation is also

$$\gamma_x^{\lambda}(t + \Delta t) = \gamma_x^{\lambda}(t) \exp(-\frac{\Delta t}{\tau_{\sigma}^{\lambda}}) + \frac{\Delta t}{\tau_{\epsilon}} \dot{e}_{xx}(t).$$

#### Maxwell solid

The  $\gamma$ 's involve a convolution, which is difficult to compute directly. However, a recursive relation can be found by considering

$$\gamma_x^{\lambda}(t+\Delta t) = -\int_0^{t+\Delta t} d\tau \, \frac{1}{\tau_0^{\lambda}} \exp(-\frac{t+\Delta t - \tau}{\tau_0^{\lambda}}) \dot{e}_{xx}(\tau).$$

$$\gamma_x^{\lambda}(t+\Delta t) = -\frac{1}{\tau_0^{\lambda}} \exp(-\frac{\Delta t}{\tau_0^{\lambda}}) \int_0^{t+\Delta t} d\tau \, \exp(-\frac{t-\tau}{\tau_0^{\lambda}}) \dot{e}_{xx}(\tau).$$

$$\gamma_x^{\lambda}(t+\Delta t) = -\frac{1}{\tau_0^{\lambda}} \exp(-\frac{\Delta t}{\tau_0^{\lambda}}) \int_0^t d\tau \, \exp(-\frac{t-\tau}{\tau_0^{\lambda}}) \dot{e}_{xx}(\tau).$$

$$-\frac{1}{\tau_0^{\lambda}} \exp(-\frac{\Delta t}{\tau_0^{\lambda}}) \int_t^{t+\Delta t} d\tau \, \exp(-\frac{t-\tau}{\tau_0^{\lambda}}) \dot{e}_{xx}(\tau).$$

The second integral is approximated by assuming that  $\dot{e}_{xx}(t)$  is constant in the interval t to  $t + \Delta t$ 

$$\gamma_x^{\lambda}(t + \Delta t) = -\frac{1}{\tau_0^{\lambda}} \exp(-\frac{\Delta t}{\tau_0^{\lambda}}) \int_0^t d\tau \exp(-\frac{t - \tau}{\tau_0^{\lambda}}) \dot{e}_{xx}(\tau)$$
$$- \frac{1}{\tau_0^{\lambda}} \exp(-\frac{\Delta t}{\tau_0^{\lambda}}) \dot{e}_{xx}(t) \int_t^{t + \Delta t} d\tau \exp(-\frac{t - \tau}{\tau_0^{\lambda}})$$

Performing the integral we then get

$$\gamma_x^{\lambda}(t + \Delta t) = \gamma_x^{\lambda}(t) \exp(-\frac{\Delta t}{\tau_{\sigma}^{\lambda}}) + \left[1 - \exp(-\frac{\Delta t}{\tau_{0}^{\lambda}})\right] \dot{e}_{xx}(t).$$

For small  $\Delta t \ll 1$  the last equation is also

$$\gamma_x^{\lambda}(t + \Delta t) = \gamma_x^{\lambda}(t) \exp(-\frac{\Delta t}{\tau_{\sigma}^{\lambda}}) + \frac{\Delta t}{\tau_0} \dot{e}_{xx}(t).$$

## APPENDIX E: Comparison with CPML

Komatitsch and Martin (2007) show that the implementation of the CPML method can be performed by replacing each spatial derivative with (Their's equation (16) and (18)):

$$s_x = \delta(t) - d_x H(t) \exp\left[-(d_x + \alpha_x)t\right]. \tag{A-1}$$

We compare this with our equation

$$\lambda(t)/\lambda_u = \delta(t) + \frac{1}{\tau_{\epsilon}} \exp(-t/\tau_{\sigma}) H(t) \left(1 - \frac{\tau_{\epsilon}}{\tau_{\sigma}}\right)$$
 (A-2)

Comparing equation (A-1) with equation (A-2) one gets:

$$-d_x = \frac{1}{\tau_{\epsilon}} \left( 1 - \frac{\tau_{\epsilon}}{\tau_{\sigma}} \right), \tag{A-3}$$

$$d_x + \alpha = \frac{1}{\tau_\sigma} \tag{A-4}$$

Solving for  $\tau_{\epsilon}$  and  $\tau_{\sigma}$  one gets

$$\tau_{\sigma} = \frac{1}{(d_x + \alpha)}, \tag{A-5}$$

$$\tau_{\epsilon} = \frac{1}{\alpha}. \tag{A-6}$$

. Here

$$d_x(x) = d_0 \left(\frac{x}{L}\right)^2, \tag{A-7}$$

where  $d_0$  is a constant and L is the length of the PML zone and x is the distance from the start (outer border) of the PML zone.