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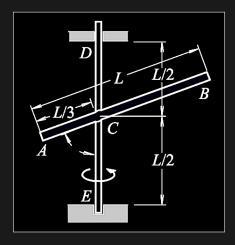
October 8, 2024

MODULE 6 — Assignment

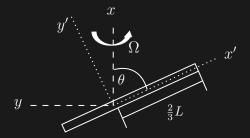
EXERCISE 5.26

Thin bar ACB is welded to a shaft that rotates at the constant angular speed Ω , so the angle θ between the bar and the shaft is constant.

- (a) Derive expressions for the angular momentum \bar{H}_C and the kinetic energy of the bar. Draw a sketch of \bar{H}_C .
- (b) Based on an analysis of the manner in which \bar{H}_C in Part (a) rotates, derive an expression for $\frac{\partial}{\partial t}\bar{H}_C$.
- (c) Use Eq. (5.3.4) to evaluate $\frac{\partial}{\partial t}\bar{H}_C$, and compare it with the result of Part (b).



The following sketch shows the two frames of the system:



The rotation matrix that converts the $\{xyz\}$ frame to the $\{x'y'z'\}$ frame is:

$$R = \begin{bmatrix} \cos(-\theta) & \sin(-\theta) & 0 \\ -\sin(-\theta) & \cos(-\theta) & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

Constructing the angular velocity vector:

$$\bar{\omega} = \Omega i$$

In the body frame is:

$$ar{\omega} = R \; \Omega \; i = \left[egin{array}{ccc} \Omega \; \cos \left(heta
ight) \; i' \ \Omega \; \sin \left(heta
ight) \; j' \ 0 \; k' \end{array}
ight]$$

From textbook Appendix, the centroidal inertia mass properties of the shaft are:

$$I_{xx} = 0$$

$$I_{yy} = \frac{1}{12}m L^2$$

$$I_{zz} = \frac{1}{12}m L^2$$

This expressed as the inertia tensor is:

$$I_{x'y'z'} = \left[egin{array}{ccc} 0 & 0 & 0 \ 0 & rac{1}{12}m\,L^2 & 0 \ 0 & 0 & rac{1}{12}m\,L^2 \end{array}
ight]$$

The distance from the body frame is:

$$d_{x'y'z'} = \left[\begin{array}{ccc} rac{1}{6} \, L & 0 & 0 \end{array}
ight]$$

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Using the parallel axis theorem to get the parallel axis transformation of inertia matrix relative to the center of the frame of reference in question:

$$I_{pat} = m \left[egin{array}{ccc} 0 & 0 & 0 \ 0 & rac{1}{36} L^2 & 0 \ 0 & 0 & rac{1}{36} L^2 \end{array}
ight]$$

This makes the inertia tensor at point C:

$$I_C = I_{x'y'z'} + I_{pat}m \left(egin{array}{ccc} 0 & 0 & 0 \ 0 & rac{1}{9}L^2 & 0 \ 0 & 0 & rac{1}{9}L^2 \end{array}
ight)$$

From this we can compute the angular momentum as:

$$ar{H}_C = I_C \; ar{\omega} = rac{1}{9} m \, L^2 \, \Omega, \sin \left(heta
ight) \; j'$$

 $\longrightarrow \mathcal{A}$ nswer

Since the bar rotates about the x axis, the rotation component in the terminal frame that is orthogonal to the j'-axis is $\Omega \cos(\theta)$ i', therefore:

$$\dot{ar{H}}_C = rac{1}{9} m L^2 \Omega^2 \cos{(heta)} \sin{(heta)} k'$$

 $\longrightarrow \mathcal{A}$ nswer

If we use Eq. (5.3.4) to evaluate this, we get the same answer:

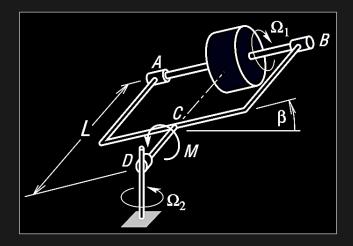
$$\dot{\bar{H}}_C = \frac{\partial}{\partial t} \tilde{H}_C + \bar{\omega} \times \bar{H}_C$$

$$egin{aligned} \dot{ar{H}}_C &= \left[egin{array}{ccc} 0 \ i' \ 0 \ j' \ rac{1}{9} m \ L^2 \ \Omega^2 \cos \left(heta
ight) \sin \left(heta
ight) \ k' \ \end{array}
ight] \ &= rac{1}{9} m \ L^2 \ \Omega^2 \cos \left(heta
ight) \sin \left(heta
ight) \ k' \end{aligned}$$

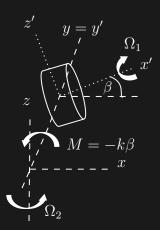
 $o \mathcal{A}$ nswer

EXERCISE 6.8

The torque M acting on the gimbal of the gyroscopic turn indicator is exerted by a torsional spring, so $M = -k\beta$. The precession rate Ω_2 is a specified function of time, and the spin rate Ω_1 is held constant by a servomotor. Let I_1 denote the moment of inertia of the flywheel about axis AB, and let I_2 be the centroidal moment of inertia perpendicular to axis AB. Derive the differential equation of motion for β .



We will define the following frames for the system:



Construct the angular velocity vector $\bar{\omega}$ of xyz by vectorially adding the simple rotation rates according to:

$$\bar{\omega} = \omega_1 \bar{e}_1 + \omega_2 \bar{e}_2 + \omega_3 \bar{e}_3$$

This gives us:

$$\bar{\omega} = \Omega_2 \ k + \dot{\beta}(-j') + \Omega_1(-i')$$

We can equate k, given the following rotation as:

$$R(-\beta) = \begin{bmatrix} \cos(\beta) & 0 & \sin(\beta) \\ 0 & 1 & 0 \\ -\sin(\beta) & 0 & \cos(\beta) \end{bmatrix}$$

$$k = R(-\beta) \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} = \begin{bmatrix} \sin(\beta) & i' \\ 0 & j \\ \cos(\beta) & k' \end{bmatrix}$$

This allows us to express the angular velocity vector as:

$$\bar{\omega} = \Omega_2 \left(\sin(\beta) \ i' + \cos(\beta) \ k' \right) - \dot{\beta} \ j' - \Omega_1 \ i'$$

Or:

$$\bar{\omega} = \begin{bmatrix} \left\{ \sin \left(\beta \right) \, \Omega_2 - \Omega_1 \right\} \, i' \\ \left\{ -\dot{\beta} \right\} \, j' \\ \left\{ \cos \left(\beta \right) \, \Omega_2 \right\} \, k' \end{bmatrix}$$

Next solve for angular acceleration:

$$\bar{\alpha} = \sum_{n} \left(\dot{\omega}_n \bar{e}_n + \bar{\Omega}_n \times \omega_n \bar{e}_n \right)$$

Where:

$$\begin{split} & \omega_{n=1} = -\Omega_1 \ i', & \dot{\omega}_{n=1} = 0, & \Omega_{n=1} = \Omega_2 R \ k - \dot{\beta} \ j' \\ & \omega_{n=2} = -\dot{\beta} \ j', & \dot{\omega}_{n=2} = -\ddot{\beta} \ j', & \Omega_{n=2} = \Omega_2 R \ k \\ & \omega_{n=3} = \Omega_2 R \ k, & \dot{\omega}_{n=3} = \dot{\Omega}_2 R \ k, & \Omega_{n=3} = 0 \end{split}$$

Substituting these into $\bar{\alpha}$:

$$\bar{\alpha} = \begin{bmatrix} \left\{ \dot{\Omega}_2 \sin(\beta) +, \Omega_2 \dot{\beta} \cos(\beta) \right\} i' \\ \left\{ -\ddot{\beta} - \Omega_1 \Omega_2 \cos(\beta) \right\} j' \\ \left\{ \dot{\Omega}_2 \cos(\beta) - \Omega_2 \dot{\beta} \sin(\beta) - \Omega_1 \dot{\beta} \right\} k' \end{bmatrix}$$

Since the torque M is acting in the j' direction, we can refer to equation 6.1.6 in the textbook:

$$\sum \bar{M}_{cg} \ j' = k\beta = I_{yy}\alpha_y + (I_{zz} - I_{xx}) \,\omega_x \omega_z$$

Where the rotation of the frame, which is not rigidly fixed to the flywheel, is:

$$\omega = \Omega_2 \ k + \dot{\beta}(-j') = \left[egin{array}{c} \Omega_2 \sin{(eta)} \ i' \\ -\dot{eta} \ j' \\ \Omega_2 \cos{(eta)} \ k' \end{array}
ight]$$

And:

$$I_{xx} = I_1$$
$$I_{yy} = I_{zz} = I_2$$

This evaluates to:

$$egin{aligned} keta &= \cos{(eta)} \, \sin{(eta)} \, \, \Omega_2^{\,2} \, \left(I_1 - I_2
ight) - I_2\ddot{eta} - I_2\Omega_1 \, \cos{(eta)} \, \, \Omega_2 \ &\longrightarrow \mathcal{A}$$
nswer

Attached

The MATLAB scripts used to solve both problems are included in the submission.

Submitted by Austin Barrilleaux on October 8, 2024.