

October 18, 2024

MODULE 6 — Assignment

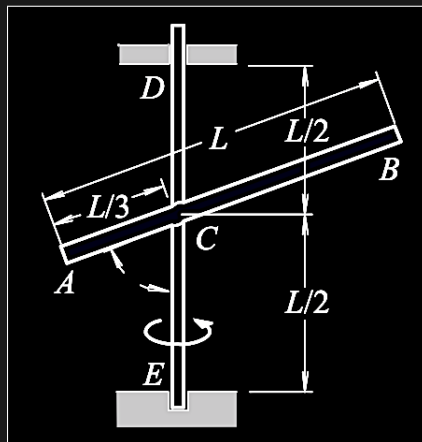
EXERCISE 5.26

Thin bar ACB is welded to a shaft that rotates at the constant angular speed Ω , so the angle θ between the bar and the shaft is constant.

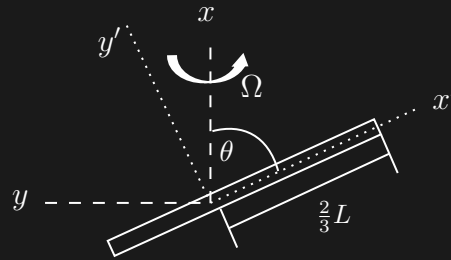
(a) Derive expressions for the angular momentum \bar{H}_C and the kinetic energy of the bar. Draw a sketch of \bar{H}_C .

(b) Based on an analysis of the manner in which \bar{H}_C in Part (a) rotates, derive an expression for $\frac{\partial}{\partial t} \bar{H}_C$.

(c) Use Eq. (5.3.4) to evaluate $\frac{\partial}{\partial t} \bar{H}_C$, and compare it with the result of Part (b).



The following sketch shows the two frames of the system:



The rotation matrix that converts the $\{xyz\}$ frame to the $\{x'y'z'\}$ frame is:

$$R = \begin{bmatrix} \cos(-\theta) & \sin(-\theta) & 0 \\ -\sin(-\theta) & \cos(-\theta) & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

Constructing the angular velocity vector:

$$\bar{\omega} = \Omega \, i$$

In the body frame is:

$$\bar{\omega} = R \, \Omega \, i = \begin{bmatrix} \Omega \cos(\theta) \, i' \\ \Omega \sin(\theta) \, j' \\ 0 \, k' \end{bmatrix}$$

From textbook Appendix, the centroidal inertia mass properties of the shaft are:

$$\begin{aligned} I_{xx} &= 0 \\ I_{yy} &= \frac{1}{12} m L^2 \\ I_{zz} &= \frac{1}{12} m L^2 \end{aligned}$$

This expressed as the inertia tensor is:

$$I_{x'y'z'} = \begin{bmatrix} 0 & 0 & 0 \\ 0 & \frac{1}{12} m L^2 & 0 \\ 0 & 0 & \frac{1}{12} m L^2 \end{bmatrix}$$

The distance from the body frame is:

$$d_{x'y'z'} = \begin{bmatrix} \frac{1}{6} L & 0 & 0 \end{bmatrix}$$

Using the parallel axis theorem to get the parallel axis transformation of inertia matrix relative to the center of the frame of reference in question:

$$I_{pat} = m \begin{bmatrix} 0 & 0 & 0 \\ 0 & \frac{1}{36} L^2 & 0 \\ 0 & 0 & \frac{1}{36} L^2 \end{bmatrix}$$

This makes the inertia tensor at point C:

$$I_C = I_{x'y'z'} + I_{pat} = m \begin{bmatrix} 0 & 0 & 0 \\ 0 & \frac{1}{9} L^2 & 0 \\ 0 & 0 & \frac{1}{9} L^2 \end{bmatrix}$$

From this we can compute the angular momentum as:

$$\bar{H}_C = I_C \bar{\omega} = \frac{1}{9} m L^2 \Omega, \sin(\theta) \ j'$$

→ Answer

Since the bar rotates about the x axis, the rotation component in the terminal frame that is orthogonal to the j' -axis is $\Omega \cos(\theta) \ i'$, therefore:

$$\dot{\bar{H}}_C = \frac{1}{9} m L^2 \Omega^2 \cos(\theta) \sin(\theta) \ k'$$

→ Answer

If we use Eq. (5.3.4) to evaluate this, we get the same answer:

$$\dot{\bar{H}}_C = \frac{\partial}{\partial t} \bar{H}_C + \bar{\omega} \times \bar{H}_C$$

$$\begin{aligned} \dot{\bar{H}}_C &= \begin{bmatrix} 0 \ i' \\ 0 \ j' \\ \frac{1}{9} m L^2 \Omega^2 \cos(\theta) \sin(\theta) \ k' \end{bmatrix} \\ &= \frac{1}{9} m L^2 \Omega^2 \cos(\theta) \sin(\theta) \ k' \end{aligned}$$

→ Answer

Matlab Code Used

The following MATLAB code was used to solve this problem:

```
%% EXERCISE 5.26
% Thin bar ACB is welded to a shaft that rotates at the constant
% angular speed, so the angle theta between the bar and the
% shaft is constant.
% (a) Derive expressions for the angular momentum H-C and the
%      kinetic energy of the bar. Draw a sketch of H-C.
% (b) Based on an analysis of the manner in which H-C in Part (a)
%      rotates, derive an expression for dH-C/dt.
% (c) Use Eq. (5.3.4) to evaluate dH-C/dt, and compare it
%      with the result of Part (b).

syms m L t
syms theta real
syms Omega real

R = Dynamics.Inertial2Body.zRot(-theta);

omega_bar = R*Omega*[1;0;0];

I = diag([0, (1/12)*m*L^2, (1/12)*m*L^2]);

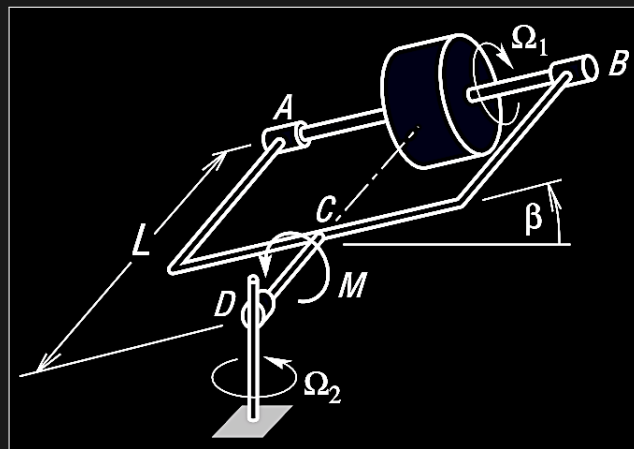
I_pa = Dynamics.Inertia.parallelAxisTransform(m, [(2*L/3-L/2), 0, 0]);

H_C = (I+I_pa)*omega_bar;

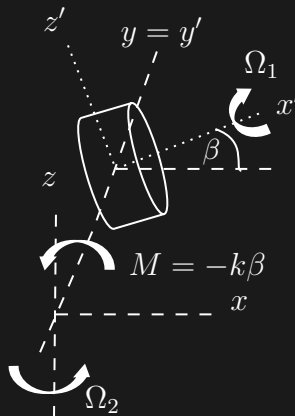
H_C_dot = diff(H_C,t) + cross(omega_bar,H_C);
```

EXERCISE 6.8

The torque M acting on the gimbal of the gyroscopic turn indicator is exerted by a torsional spring, so $M = -k\beta$. The precession rate Ω_2 is a specified function of time, and the spin rate Ω_1 is held constant by a servomotor. Let I_1 denote the moment of inertia of the flywheel about axis AB , and let I_2 be the centroidal moment of inertia perpendicular to axis AB . Derive the differential equation of motion for β .



We will define the following frames for the system:



Construct the angular velocity vector $\bar{\omega}$ of $xy'z$ by vectorially adding the simple rotation rates according to:

$$\bar{\omega} = \omega_1 \bar{e}_1 + \omega_2 \bar{e}_2 + \omega_3 \bar{e}_3$$

This gives us:

$$\bar{\omega} = \Omega_2 k + \dot{\beta}(-j') + \Omega_1(-i')$$

We can equate k , given the following rotation as:

$$R(-\beta) = \begin{bmatrix} \cos(\beta) & 0 & \sin(\beta) \\ 0 & 1 & 0 \\ -\sin(\beta) & 0 & \cos(\beta) \end{bmatrix}$$

$$k = R(-\beta) \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} = \begin{bmatrix} \sin(\beta) & i' \\ 0 & j \\ \cos(\beta) & k' \end{bmatrix}$$

This allows us to express the angular velocity vector as:

$$\bar{\omega} = \Omega_2 (\sin(\beta) i' + \cos(\beta) k') - \dot{\beta} j' - \Omega_1 i'$$

Or:

$$\bar{\omega} = \begin{bmatrix} \{\sin(\beta) \Omega_2 - \Omega_1\} & i' \\ \{-\dot{\beta}\} & j' \\ \{\cos(\beta) \Omega_2\} & k' \end{bmatrix}$$

Next solve for angular acceleration:

$$\bar{\alpha} = \sum_n (\dot{\omega}_n \bar{e}_n + \bar{\Omega}_n \times \omega_n \bar{e}_n)$$

Where:

$$\begin{aligned} \omega_{n=1} &= -\Omega_1 i', & \dot{\omega}_{n=1} &= 0, & \Omega_{n=1} &= \Omega_2 R k - \dot{\beta} j' \\ \omega_{n=2} &= -\dot{\beta} j', & \dot{\omega}_{n=2} &= -\ddot{\beta} j', & \Omega_{n=2} &= \Omega_2 R k \\ \omega_{n=3} &= \Omega_2 R k, & \dot{\omega}_{n=3} &= \dot{\Omega}_2 R k, & \Omega_{n=3} &= 0 \end{aligned}$$

Substituting these into $\bar{\alpha}$:

$$\bar{\alpha} = \begin{bmatrix} \left\{ \dot{\Omega}_2 \sin(\beta) + \Omega_2 \dot{\beta} \cos(\beta) \right\} i' \\ \left\{ -\ddot{\beta} - \Omega_1 \Omega_2 \cos(\beta) \right\} j' \\ \left\{ \dot{\Omega}_2 \cos(\beta) - \Omega_2 \dot{\beta} \sin(\beta) - \Omega_1 \dot{\beta} \right\} k' \end{bmatrix}$$

Since the torque M is acting in the j' direction, we can refer to equation 6.1.6 in the textbook:

$$\sum \bar{M}_{cg} j' = k\beta = I_{yy}\alpha_y + (I_{zz} - I_{xx})\omega_x\omega_z$$

Where the rotation of the frame, which is not rigidly fixed to the flywheel, is:

$$\omega = \Omega_2 k + \dot{\beta}(-j') = \begin{bmatrix} \Omega_2 \sin(\beta) i' \\ -\dot{\beta} j' \\ \Omega_2 \cos(\beta) k' \end{bmatrix}$$

And:

$$\begin{aligned} I_{xx} &= I_1 \\ I_{yy} &= I_{zz} = I_2 \end{aligned}$$

This evaluates to:

$$k\beta = \cos(\beta) \sin(\beta) \Omega_2^2 (I_1 - I_2) - I_2 \ddot{\beta} - I_2 \Omega_1 \cos(\beta) \Omega_2$$

→ Answer

Matlab Code Used

The following MATLAB code was used to solve this problem:

```
%% EXERCISE 6.8
% The torque M acting on the gimbal of the gyroscopic turn indicator is
% exerted by a torsional spring, so M = -k beta. The precession rate
% Omega 2 is a specified function of time, and the spin rate Omega 1 is
% held constant by a servomotor. Let I1 denote the moment of inertia of
% the flywheel about axis AB, and let I2 be the centroidal moment of
% inertia perpendicular to axis AB. Derive the differential equation
```

```

% of motion for beta.

clc,clear
syms k t beta(t)

syms Omega_1 Omega_2(t)

syms I_1 I_2

R = yRot(-beta);

omega_bar = Omega_2*R*[0;0;1] + diff(beta,t)*[0;-1;0]...
            + Omega_1*[-1;0;0];

Omega_N = Omega_2(t)*R(t)*[0;0;1];

alpha_bar = cross(omega_bar,Omega_1*[-1;0;0]) +...
            diff(Omega_2,t)*R*[0;0;1] +...
            simplify(cross(Omega_N,Omega_2*R*[0;0;1])) +...
            diff(diff(beta,t),t)*[0;-1;0] +...
            cross(Omega_N,diff(beta,t)*[0;-1;0]);

system = ([0;1;0]*k*beta(t) == I_2*alpha_bar(t)-...
          (I_2-I_1)*Omega_N(1)*Omega_N(3));

system(2)

function R = yRot(ang)
R = [ cos(ang) 0 -sin(ang) ; %% Neg body 2 in
    0 1 0 ;
    sin(ang) 0 cos(ang) ];
end

```

Submitted by Austin Barrilleaux on October 18, 2024.