

November 12, 2024

## MODULE 11 — Assignment

### Problem 1: Solve Ginsberg 9.28

The absolute velocity of a particle may be represented by the components  $v_x$ ,  $v_y$ , and  $v_z$  relative to the axes of a moving reference system  $xyz$ . Suppose that the angular velocity  $\bar{\omega}$  of  $xyz$  and the velocity  $\bar{v}_O$  of the origin of  $xyz$  are known as functions of time. Derive the Gibbs-Appell equations of motion relating the quasi-velocities  $\dot{\gamma}_1 = v_x$ ,  $\dot{\gamma}_2 = v_y$ , and  $\dot{\gamma}_3 = v_z$  to the resultant force acting on the particle.

Where:

$$\bar{\omega} = \left\langle \begin{array}{c} \omega_x \\ \omega_y \\ \omega_z \end{array} \right\rangle$$

Given that:

$$\bar{v} = \left\langle \begin{array}{c} v_x \\ v_y \\ v_z \end{array} \right\rangle = \left\langle \begin{array}{c} \dot{\gamma}_1 \\ \dot{\gamma}_2 \\ \dot{\gamma}_3 \end{array} \right\rangle$$

Solving for acceleration:

$$\begin{aligned} \bar{a} &= \frac{\partial \bar{v}}{\partial t} + \bar{\omega} \times \bar{v} \\ &= \frac{\partial \dot{\gamma}}{\partial t} + \bar{\omega} \times \dot{\gamma} \\ &= \left\langle \begin{array}{c} \ddot{\gamma}_1 - \dot{\gamma}_2 \omega_z + \dot{\gamma}_3 \omega_y \\ \ddot{\gamma}_2 + \dot{\gamma}_1 \omega_z - \dot{\gamma}_3 \omega_x \\ \ddot{\gamma}_3 - \dot{\gamma}_1 \omega_y + \dot{\gamma}_2 \omega_x \end{array} \right\rangle \end{aligned}$$

Given that the Gibbs-Appell function for a system of particles is:

$$S = \sum_p \frac{1}{2} m \bar{a}_p \cdot \bar{a}_p$$

For this single particle case:

$$\begin{aligned} S &= \frac{1}{2} m (\bar{a} \cdot \bar{a}) \\ &= \frac{1}{2} m \left[ (\ddot{\gamma}_3 - \dot{\gamma}_1 \omega_y + \dot{\gamma}_2 \omega_x)^2 + (\ddot{\gamma}_2 + \dot{\gamma}_1 \omega_z - \dot{\gamma}_3 \omega_x)^2 + (\ddot{\gamma}_1 - \dot{\gamma}_2 \omega_z + \dot{\gamma}_3 \omega_y)^2 \right] \end{aligned}$$

Where the equations of motion are calculated as:

$$\frac{\partial S}{\partial \ddot{\gamma}_j} = \Gamma_j = \Gamma_1$$

The virtual work associated with the forces applied to the particle is:

$$\delta W = \sum \bar{F} \cdot \delta \bar{x} = \sum_{j=1}^K \Gamma_j \delta \gamma_j = \sum \bar{F} \cdot \left\langle \begin{matrix} \delta \gamma_1 \\ \delta \gamma_2 \\ \delta \gamma_3 \end{matrix} \right\rangle$$

The equation of motion is solved for as:

$$\frac{\partial S}{\partial \ddot{\gamma}} = m \left\langle \begin{matrix} \ddot{\gamma}_1 - \dot{\gamma}_2 \omega_z + \dot{\gamma}_3 \omega_y \\ \ddot{\gamma}_2 + \dot{\gamma}_1 \omega_z - \dot{\gamma}_3 \omega_x \\ \ddot{\gamma}_3 - \dot{\gamma}_1 \omega_y + \dot{\gamma}_2 \omega_x \end{matrix} \right\rangle = \Gamma_1 = \left\langle \begin{matrix} \sum F_x \\ \sum F_y \\ \sum F_z \end{matrix} \right\rangle = \left\langle \begin{matrix} F_x \\ F_y \\ F_z \end{matrix} \right\rangle$$

Or:

$$\begin{aligned} m (\ddot{\gamma}_1 - \dot{\gamma}_2 \omega_z + \dot{\gamma}_3 \omega_y) &= F_x \\ m (\ddot{\gamma}_2 + \dot{\gamma}_1 \omega_z - \dot{\gamma}_3 \omega_x) &= F_y \\ m (\ddot{\gamma}_3 - \dot{\gamma}_1 \omega_y + \dot{\gamma}_2 \omega_x) &= F_z \end{aligned}$$

→ Answer

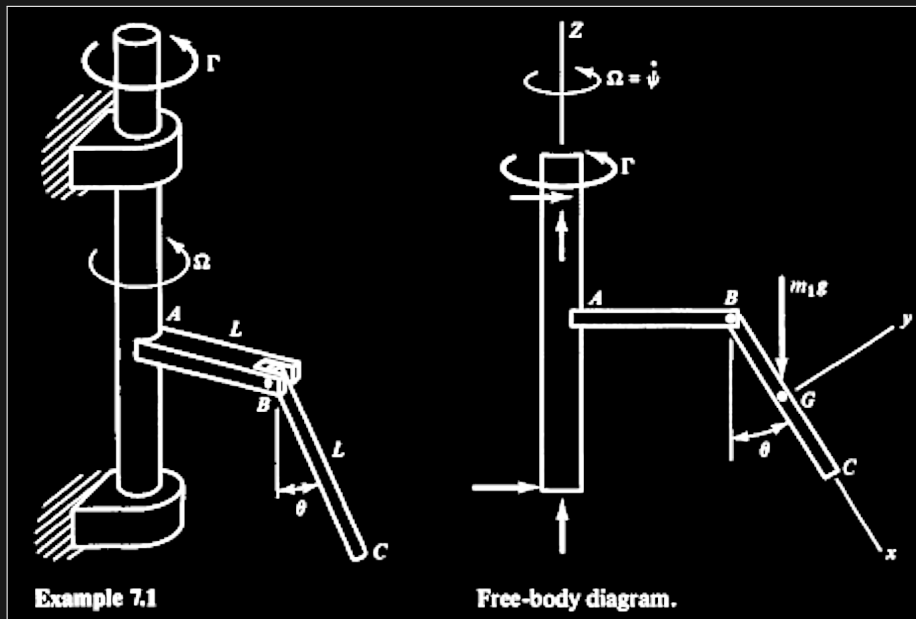
Where:

$$\dot{\gamma} = \left\langle \begin{matrix} \dot{\gamma}_1 \\ \dot{\gamma}_2 \\ \dot{\gamma}_3 \end{matrix} \right\rangle = v = \left\langle \begin{matrix} v_x \\ v_y \\ v_z \end{matrix} \right\rangle = v_0 + \bar{\omega} \times \bar{r} = \left\langle \begin{matrix} v_{0x} - \omega_z y + \omega_y z \\ v_{0y} + \omega_z x - \omega_x z \\ v_{0z} - \omega_y x + \omega_x y \end{matrix} \right\rangle$$

## Problem 2:

Use the Gibbs-Appell approach to find the equations of motion for this problem.

A torque  $\Gamma$  applied to the vertical shaft of the T-bar causes the rotation rate  $\Omega$  about the vertical axis to increase in proportion to the angle  $\theta$  by which bar BC swings outward, that is,  $\Omega = c\theta$ . The mass of bar BC is  $m_1$  and the moment of inertia of the T-bar about its axis of rotation is  $I_2$ . Determine the equations of motion for the system, and for the torque  $\Gamma$ .



For the purpose of this problem, as was recommended in the office hour, we will replace the  $y$ -axis of the body frame with the  $z$ -axis. This will simplify the inertial to body rotation we perform later in the solution.

First we will determine location of point  $G$  in the inertial frame. By inspection this is:

$$\bar{r}_G = \begin{pmatrix} \cos(\psi) \left( L + \frac{1}{2}L \sin(\theta) \right) \\ \sin(\psi) \left( L + \frac{1}{2}L \sin(\theta) \right) \\ -\frac{1}{2}L \cos(\theta) \end{pmatrix}$$

From this we can compute the velocity at point  $G$ :

$$\bar{v}_G = \left\langle \begin{array}{l} \frac{1}{2}L \cos(\psi) \cos(\theta) \frac{\partial \theta}{\partial t} - \sin(\psi) \left(L + \frac{1}{2}L \sin(\theta)\right) \frac{\partial \psi}{\partial t} \\ \frac{1}{2}L \cos(\theta) \sin(\psi) \frac{\partial \theta}{\partial t} + \cos(\psi) \left(L + \frac{1}{2}L \sin(\theta)\right) \frac{\partial \psi}{\partial t} \\ \frac{1}{2}L \sin(\theta) \frac{\partial \theta}{\partial t} \end{array} \right\rangle$$

Which we can then use to compute acceleration at point  $G$ :

$$\bar{a}_G = \left\langle \begin{array}{l} \frac{L \cos(\psi) \cos(\theta) \frac{\partial^2 \theta}{\partial t^2}}{2} - \frac{L \cos(\psi) \sin(\theta) \left(\frac{\partial \theta}{\partial t}\right)^2}{2} - \frac{L \cos(\psi) (\sin(\theta)+2) \left(\frac{\partial \psi}{\partial t}\right)^2}{2} - \frac{L \sin(\psi) (\sin(\theta)+2) \frac{\partial^2 \psi}{\partial t^2}}{2} - L \cos(\theta) \sin(\psi) \frac{\partial^2 \theta}{\partial t^2} \\ \frac{L \cos(\theta) \sin(\psi) \frac{\partial^2 \theta}{\partial t^2}}{2} - \frac{L \sin(\psi) \sin(\theta) \left(\frac{\partial \theta}{\partial t}\right)^2}{2} - \frac{L \sin(\psi) (\sin(\theta)+2) \left(\frac{\partial \psi}{\partial t}\right)^2}{2} + \frac{L \cos(\psi) (\sin(\theta)+2) \frac{\partial^2 \psi}{\partial t^2}}{2} + L \cos(\psi) \cos(\theta) \frac{\partial^2 \theta}{\partial t^2} \\ \frac{L \sin(\theta) \frac{\partial^2 \theta}{\partial t^2}}{2} + \frac{L \cos(\theta) \left(\frac{\partial \theta}{\partial t}\right)^2}{2} \end{array} \right\rangle$$

Replacing  $\dot{\theta}$  and  $\dot{\psi}$  with the quasi-velocity terms gives us:

$$\bar{a}_G = \left\langle \begin{array}{l} \frac{L \cos(\psi) \cos(\theta) \dot{\gamma}_1}{2} - \frac{L \cos(\psi) \sin(\theta) (\dot{\gamma}_1)^2}{2} - \frac{L \cos(\psi) (\dot{\gamma}_2)^2 (\sin(\theta)+2)}{2} - \frac{L \sin(\psi) (\sin(\theta)+2) \ddot{\gamma}_2}{2} - L \cos(\theta) \sin(\psi) \dot{\gamma}_2 \dot{\gamma}_1 \\ \frac{L \cos(\theta) \sin(\psi) \dot{\gamma}_1}{2} - \frac{L \sin(\psi) \sin(\theta) (\dot{\gamma}_1)^2}{2} - \frac{L \sin(\psi) (\dot{\gamma}_2)^2 (\sin(\theta)+2)}{2} + \frac{L \cos(\psi) (\sin(\theta)+2) \ddot{\gamma}_2}{2} + L \cos(\psi) \cos(\theta) \dot{\gamma}_2 \dot{\gamma}_1 \\ \frac{L \sin(\theta) \dot{\gamma}_1}{2} + \frac{L \cos(\theta) (\dot{\gamma}_1)^2}{2} \end{array} \right\rangle$$

To convert this acceleration into the body frame, we will define the following inertial to body rotation:

$$R_{xyz}^{XYZ} = R_z(\psi)R_y(\theta) = \begin{bmatrix} \cos(\psi) & -\sin(\psi) & 0 \\ \sin(\psi) & \cos(\psi) & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} \cos(\theta) & 0 & \sin(\theta) \\ 0 & 1 & 0 \\ -\sin(\theta) & 0 & \cos(\theta) \end{bmatrix}$$

Which simplifies to:

$$R_{xyz}^{XYZ} = \begin{bmatrix} \cos(\psi) \cos(\theta) & -\sin(\psi) \cos(\theta) & \sin(\theta) \\ \cos(\theta) \sin(\psi) & \cos(\psi) \cos(\theta) & \sin(\psi) \sin(\theta) \\ -\sin(\theta) & 0 & \cos(\theta) \end{bmatrix}$$

The transpose of this gives us the inertial to body transform:

$$R_{XYZ}^{xyz} = \begin{bmatrix} \cos(\psi) \cos(\theta) & \cos(\theta) \sin(\psi) & -\sin(\theta) \\ -\sin(\psi) & \cos(\psi) & 0 \\ \cos(\psi) \sin(\theta) & \sin(\psi) \sin(\theta) & \cos(\theta) \end{bmatrix}$$

We can compute the acceleration term as:

$$\bar{a}_G = R_{XYZ}^{xyz} \bar{a}_G = \left\langle \begin{array}{c} \frac{L \cos(2\theta) \dot{\gamma}_1}{2} - \frac{L \sin(2\theta) (\dot{\gamma}_1)^2}{2} - \frac{L \sin(2\theta) (\dot{\gamma}_2)^2}{4} - L \cos(\theta) (\dot{\gamma}_2)^2 \\ L \ddot{\gamma}_2 + \frac{L \sin(\theta) \ddot{\gamma}_2}{2} + L \cos(\theta) \dot{\gamma}_2 \dot{\gamma}_1 \\ \frac{L (2 \cos(\theta)^2 - 1) (\dot{\gamma}_1)^2}{2} - L \sin(\theta) (\dot{\gamma}_2)^2 - \frac{L (\dot{\gamma}_2)^2}{4} + \frac{L (2 \cos(\theta)^2 - 1) (\dot{\gamma}_2)^2}{4} + L \cos(\theta) \sin(\theta) \ddot{\gamma}_1 \end{array} \right\rangle$$

The Gibbs-Appell function for the system is given by:

$$S = \frac{1}{2} m (\bar{a}_G \cdot \bar{a}_G) + \frac{1}{2} \bar{\alpha} \cdot \frac{\partial \bar{H}_G}{\partial t} + \bar{\alpha} \cdot (\bar{\omega} \times \bar{H}_G) + \frac{1}{2} I_2 \ddot{\psi}^2$$

The first term of  $S$  is computed as:

$$\frac{1}{2} m (\bar{a}_G \cdot \bar{a}_G) = \frac{1}{2} m \left[ \left( L \ddot{\gamma}_2 + \frac{L \sin(\theta) \ddot{\gamma}_2}{2} + L \cos(\theta) \dot{\gamma}_2 \dot{\gamma}_1 \right)^2 + \left( L \cos(\theta) (\dot{\gamma}_2)^2 + \frac{L \sin(2\theta) (\dot{\gamma}_1)^2}{2} + \frac{L \sin(2\theta) (\dot{\gamma}_2)^2}{4} \right)^2 \right]$$

The angular velocity vector of the system in the body frame is, by inspection:

$$\bar{\omega} = \left\langle \begin{array}{c} -\cos(\gamma_1) \dot{\gamma}_2 \\ -\dot{\gamma}_1 \\ \sin(\gamma_1) \dot{\gamma}_2 \end{array} \right\rangle$$

The angular acceleration vector is therefore:

$$\bar{\alpha} = \frac{\partial \bar{\omega}}{\partial t} + (\bar{\omega} \times \bar{\omega}) = \left\langle \begin{array}{c} \sin(\gamma_1) \dot{\gamma}_2 \dot{\gamma}_1 - \cos(\gamma_1) \ddot{\gamma}_2 \\ -\ddot{\gamma}_1 \\ \sin(\gamma_1) \ddot{\gamma}_2 + \cos(\gamma_1) \dot{\gamma}_2 \dot{\gamma}_1 \end{array} \right\rangle$$

The inertia tensor of the bar centered at  $G$  is:

$$I = \frac{1}{12} m L^2 \begin{bmatrix} 0 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

From this we can compute the angular momentum as:

$$\bar{H}_G = I \bar{\omega} = \left\langle \begin{array}{c} 0 \\ -\frac{L^2 m \dot{\gamma}_1}{12} \\ \frac{L^2 m \sin(\gamma_1) \dot{\gamma}_2}{12} \end{array} \right\rangle$$

The second term in the Gibbs-Appell function is computed as:

$$\frac{1}{2}\bar{\alpha}\cdot\frac{\partial\bar{H}_G}{\partial t} = \left(\frac{\sin(\gamma_1)}{2}\ddot{\gamma}_2 + \frac{\cos(\gamma_1)}{2}\dot{\gamma}_2\dot{\gamma}_1\right) \left(\frac{L^2 m \sin(\gamma_1)}{12}\ddot{\gamma}_2 + \frac{L^2 m \cos(\gamma_1)}{12}\dot{\gamma}_2\dot{\gamma}_1\right) + \frac{L^2 m (\ddot{\gamma}_1)^2}{24}$$

The third term is:

$$\bar{\alpha}\cdot(\bar{\omega} \times \bar{H}_G) = \frac{L^2 m \cos(\gamma_1)}{12} (\sin(\gamma_1)\ddot{\gamma}_2 + \cos(\gamma_1)\dot{\gamma}_2\dot{\gamma}_1) - \frac{L^2 m \cos(\gamma_1) \sin(\gamma_1) (\dot{\gamma}_2)^2 \ddot{\gamma}_1}{12}$$

The third term can be rewritten as:

$$\frac{1}{2}I_2\ddot{\psi}^2 = \frac{I_2 (\ddot{\gamma}_2)^2}{2}$$

All together, we can compute the following derivatives that form the Gibbs-Appell equations as:

$$\begin{aligned} \frac{\partial S}{\partial \ddot{\gamma}_1} &= \frac{L^2 m \ddot{\gamma}_1}{3} - \frac{L^2 m \sin(2\gamma_1) (\dot{\gamma}_2)^2}{24} - \frac{L^2 m \sin(2\theta) (\dot{\gamma}_2)^2}{8} - \frac{L^2 m \cos(\theta) (\dot{\gamma}_2)^2}{2} \\ \frac{\partial S}{\partial \ddot{\gamma}_2} &= I_2 \ddot{\gamma}_2 + \frac{4 L^2 m \ddot{\gamma}_2}{3} - \frac{L^2 m \cos(\gamma_1)^2 \ddot{\gamma}_2}{12} - \frac{L^2 m \cos(\theta)^2 \ddot{\gamma}_2}{4} + L^2 m \sin(\theta) \ddot{\gamma}_2 + L^2 m \cos(\theta) \dot{\gamma}_2 \dot{\gamma}_1 \\ &\quad + \frac{L^2 m \sin(2\gamma_1) \dot{\gamma}_2 \dot{\gamma}_1}{12} + \frac{L^2 m \cos(\theta) \sin(\theta) \dot{\gamma}_2 \dot{\gamma}_1}{2} \end{aligned}$$

Imposing the constraint that  $\dot{\gamma}_2 = c \dot{\theta}$  and  $\ddot{\gamma}_2 = c \ddot{\theta} = c\dot{\gamma}_1$ :

$$\begin{aligned} \frac{\partial S}{\partial \ddot{\gamma}_1} &= \frac{L^2 m \ddot{\gamma}_1}{3} - \frac{L^2 c^2 m \sin(\theta) \cos(\theta) \gamma_1^2}{3} - \frac{L^2 c^2 m \cos(\theta) \gamma_1^2}{2} \\ \frac{\partial S}{\partial \ddot{\gamma}_2} &= I_2 c \dot{\gamma}_1 + \frac{4 L^2 c m \dot{\gamma}_1}{3} - \frac{L^2 c m \cos(\theta)^2 \dot{\gamma}_1}{3} + L^2 c m \sin(\theta) \dot{\gamma}_1 \\ &\quad + \frac{2 L^2 c m \sin(\theta) \cos(\theta) \gamma_1 \dot{\gamma}_1}{3} + L^2 c m \cos(\theta) \gamma_1 \dot{\gamma}_1 \end{aligned}$$

*Submitted by Austin Barrilleaux on November 12, 2024.*