Austin Barrilleaux Whiting School of Engineering Johns Hopkins University

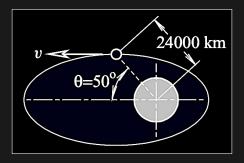
October 21, 2024

MODULE 8 — Midterm Exam

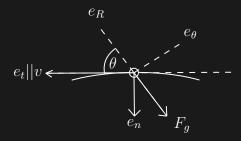
Problem 1

A satellite is in an orbit about the Earth. The magnitude of the acceleration of this body is $g(R_e/R)^2$, where R is the distance from the body to the center of the Earth, $R_e = 6370$ km is the radius of the Earth, and g = 9.807 m/s². At the position shown, the speed of the body is v = 27~000km/h.

- (a) Determine the rate of change of the speed and the radius of curvature of the orbit at this position.
- (b) Determine \dot{R} , \ddot{R} , $\dot{\theta}$, and $\ddot{\theta}$ at this position.



Sketching the following block diagram where, by inspection, the unit tangent vector e_t is parallel with the velocity vector, and the normal direction unit vector e_n extends toward the center of curvature (which is toward the center of the elliptical orbit.)



From this, we can define the unit tangent vector as:

$$\bar{e}_t = \begin{bmatrix} \cos(-\theta) & -\sin(-\theta) \\ \sin(-\theta) & \cos(-\theta) \end{bmatrix} \begin{bmatrix} 1 \\ 0 \end{bmatrix} = \begin{bmatrix} \cos(\theta) & \bar{e}_R \\ -\sin(\theta) & \bar{e}_\theta \end{bmatrix}$$

Because \dot{v} is the tangential component of acceleration, we find that:

$$\dot{v} = \bar{a} \cdot \bar{e}_t = g \left(\frac{R_e}{R}\right)^2 \begin{bmatrix} -1 \ \bar{e}_R \\ 0 \ \bar{e}_\theta \end{bmatrix} \cdot \begin{bmatrix} \cos\left(\theta\right) \ \bar{e}_R \\ -\sin\left(\theta\right) \ \bar{e}_\theta \end{bmatrix} = -9.807 \left(\frac{6370 \times 10^3}{24000 \times 10^3}\right)^2 \cos\left(\theta\right)$$

This evaluates to:

$$\dot{v} = -0.4441 \text{ m/s}^2$$

 $\longrightarrow \mathcal{A}$ nswer

Looking at the equation for acceleration:

$$\bar{a} = \dot{v}\bar{e}_t + \frac{v^2}{\rho}\bar{e}_n$$

To solve for the radius of curvature:

$$\frac{v^2}{\rho}\bar{e}_n = \bar{a} - \dot{v}\bar{e}_t \rightarrow \rho = \frac{v^2}{|\bar{a} - \dot{v}\bar{e}_t|}$$

The radius of curvature is:

$$\rho = \frac{v^2}{|\bar{a} - v\bar{e}_t|} = \frac{\left(27\ 000 \times 10^3/3600\right)^2}{\left[-9.807\left(\frac{6370 \times 10^3}{24000 \times 10^3}\right)^2 \left[\begin{array}{c} -1\ \bar{e}_R \\ 0\ \bar{e}_\theta \end{array}\right] - \left(-0.4441\right) \left[\begin{array}{c} \cos\left(\theta\right)\ \bar{e}_R \\ -\sin\left(\theta\right)\ \bar{e}_\theta \end{array}\right]\right|}$$

This evaluates to:

$$\rho = 1.0629 \times 10^8 \text{ m}$$

 $\longrightarrow \mathcal{A}$ nswer

Using the following velocity equation:

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$$\bar{v} = \dot{R} \; \bar{e}_R + R\dot{\theta} \; \bar{e}_{\theta}$$

Looking at the sketch:

$$\bar{v} = \left(\frac{27\ 000 \times 10^3}{3600}\right) \begin{bmatrix} \cos\left(\theta\right) \ \bar{e}_R \\ -\sin\left(\theta\right) \ \bar{e}_\theta \end{bmatrix}$$

From these two equations we get that:

$$\dot{R} = \left(\frac{27\ 000 \times 10^3}{3600}\right) \cos\left(\theta\right) = 4820.9 \text{ m/s}$$
 $\dot{\theta} = \left(\frac{27\ 000 \times 10^3}{3600}\right) \sin\left(\theta\right) / R = -0.0002394 \text{ rad/s}$

 $\longrightarrow \mathcal{A}$ nswer

Using the following acceleration equation:

$$\bar{a} = \left(\ddot{R} - R\dot{\theta}^2\right)\bar{e}_R + \left(R\ddot{\theta} + 2\dot{R}\dot{\theta}\right)\bar{e}_{\theta}$$

Where:

$$\bar{a} = -9.807 \left(\frac{6370 \times 10^3}{24000 \times 10^3} \right)^2 \begin{bmatrix} -1 \ \bar{e}_R \\ 0 \ \bar{e}_\theta \end{bmatrix}$$

We get that:

$$\ddot{R} = \bar{a} \cdot \bar{e}_R + R\dot{\theta}^2 = 0.6845 \text{ m/s}^2$$

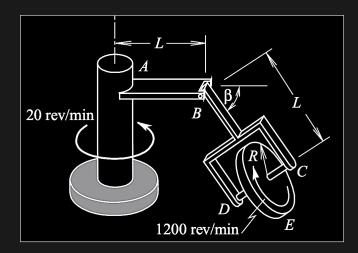
$$\ddot{\theta} = \left(\bar{a} \cdot \bar{e}_{\theta}^{-0} - 2\dot{R}\dot{\theta}\right)/R = 9.617 \times 10^8 \text{ rad/s}^2$$

 $\longrightarrow \mathcal{A}$ nswer

```
clc, clear
syms t
syms theta(t)
assume(t, {'real', 'positive'})
e_t = zRot(-theta) * [1;0;0];
e_n = zRot(-theta) * [0;1;0];
a_bar = -g*(Re/R)^2*[1;0;0];
v_dot = subs(transpose(a_bar)*e_t,theta(t),50*pi/180); % [ans]
v_bar = double((27000E3/3600)*subs(e_t,theta(t),50*pi/180));
subs(norm(a_bar - v_dot*e_t), theta(t), 50*pi/180); % m
R_dot = v_bar(1); % m/s^2 (2.3.11)
theta_dot = v_bar(2)/R; % rad/s^2 (2.3.11)
R_dot = a_bar(1) + R*theta_dot^2; % m/s^2 (2.3.13)
theta_ddot = (a_bar(2) - 2*R_dot*theta_dot)/R; % rad/s^2 (2.3.13)
function R = zRot(ang)
   R = [\cos(ang) - \sin(ang) 0;
          sin(ang) cos(ang) 0;
                          0 1];
```

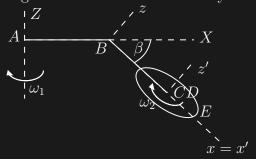
Problem 2

The disk spins about its axis CD at 1200 rev/min as the system rotates about the vertical axis at 20 rev/min. Both rates are constant. The angle of elevation of the arm supporting the disk is such that $\dot{\beta} = 10$ rad/s and $\ddot{\beta} = -500$ rad/s² when $\beta = 36.87^{\circ}$. Determine the velocity and acceleration of point E, which is the lowest point on the perimeter of the disk. Note: the solution for velocity in the text is for a clockwise rotation about the vertical axis



We will solve this problem consistent with the note in the prompt.

We will define the following coordinate frames for the system:



You will note that the $\{xyz\}$ frame and $\{x'y'z'\}$ frame are identical for this problem, so I will use $\{xyz\}$ to express the coordinate frame at both points from this point. Constructing the angular velocity vector $\bar{\omega}$ of $\{xyz\}$ by vectorially adding the simple rotation rates according to:

$$\bar{\omega} = \omega_1 \bar{e}_1 + \omega_2 \bar{e}_2 + \omega_3 \bar{e}_3$$

This gives us:

$$\bar{\omega} = -\omega_1 K + \dot{\beta} j - \omega_2 k$$

Using the following coordinate transformation:

$$R_{\text{rot}} = \begin{bmatrix} \cos(\beta) & 0 & -\sin(\beta) \\ 0 & 1 & 0 \\ \sin(\beta) & 0 & \cos(\beta) \end{bmatrix}$$
$$K = R_{\text{rot}} \begin{bmatrix} 0 & I \\ 0 & J \\ 1 & K \end{bmatrix} = \begin{bmatrix} -\sin(\beta) & i \\ 0 & j \\ \cos(\beta) & k \end{bmatrix} = -\sin(\beta) i + \cos(\beta) k$$

This gives us the angular velocity vector in the form:

$$\bar{\omega} = \begin{bmatrix} \omega_1 \sin(\beta) & i \\ \dot{\beta} & j \\ -\omega_2 - \omega_1 \cos(\beta) & k \end{bmatrix}$$

For the angular rotations, the angular velocity is:

$$\Omega_{1} = -\omega_{1}K = \begin{bmatrix} \omega_{1} \sin(\beta) & i \\ 0 & j \\ -\omega_{1} \cos(\beta) & k \end{bmatrix}$$

$$\Omega_{2} = -\omega_{1}K + \dot{\beta}j = \begin{bmatrix} \omega_{1} \sin(\beta) & i \\ \dot{\beta} & j \\ -\omega_{1} \cos(\beta) & k \end{bmatrix}$$

$$\Omega_{3} = \bar{\omega}$$

Using the following relative positions:

$$\bar{r}_{B/A} = L \begin{pmatrix} \cos(\beta) & i \\ 0 & j \\ \sin(\beta) & k \end{pmatrix}$$

$$\bar{r}_{CD/B} = L i$$

$$\bar{r}_{E/CD} = R i$$

Referencing the velocity equation:

$$\bar{v}_P = \bar{v}_O + \bar{\omega} \times \bar{r}_{P/O}$$

We solve for the velocities along the system from A to E:

$$\bar{v}_B = \Omega_1 \times \bar{r}_{B/A} = \begin{bmatrix} 0 \\ -2.0944 L \\ 0 \end{bmatrix}$$

$$\bar{v}_{CD} = \bar{v}_B + \Omega_2 \times \bar{r}_{CD/B} = \begin{bmatrix} 0 \\ -3.7699 L \\ -10 L \end{bmatrix}$$

$$\bar{v}_E = \bar{v}_{CD} + \Omega_3 \times \bar{r}_{E/CD} = \begin{bmatrix} 0 \\ -3.7699 L - 127.34 R \\ -10 L - 10 R \end{bmatrix}$$

Therefore:

$$ar{v}_E = -\left(3.7699\,L + 127.34\,R
ight)j - 10\left(L + R
ight)k$$

 $\longrightarrow \mathcal{A}$ nswer

We can solve for the angular rotation at the rotation points using the equation for angular acceleration:

$$\bar{\alpha} = \sum_{n} \left(\dot{\omega}_n \bar{e}_n + \bar{\Omega}_n \times \omega_n \bar{e}_n \right)$$

The relative angular accelerations across the system for points A to E are:

$$\begin{split} \bar{\alpha}_1 &= \Omega_1 \times \Omega_1 = 0 \\ \bar{\alpha}_2 &= \bar{\alpha}_1 + \ddot{\beta}j + \Omega_2 \times \dot{\beta}j \\ \bar{\alpha}_3 &= \bar{\alpha}_2 + \Omega_3 \times \omega_2(-k) = \bar{\alpha} \end{split}$$

Using the acceleration equation:

$$\bar{a}_P = \bar{a}_O + \bar{\alpha} \times \bar{r}_{P/O} + \bar{\omega} \times (\bar{\omega} \times \bar{r}_{P/O})$$

Solving for the acceleration across the system for points A to E:

$$\bar{a}_{B} = 0 + \bar{\alpha}_{1} \times \bar{r}_{B/A} + \Omega_{1} \times \left(\Omega_{1} \times \bar{r}_{B/A}\right) = \begin{bmatrix} -3.5092 \, L \\ 0 \\ -2.6319 \, L \end{bmatrix}$$

$$\bar{a}_{CD} = \bar{a}_{B} + \bar{\alpha}_{2} \times \bar{r}_{CD/B} + \Omega_{2} \times \left(\Omega_{2} \times \bar{r}_{CD/B}\right) = \begin{bmatrix} -106.32 \, L \\ 25.133 \, L \\ 495.26 \, L \end{bmatrix}$$

$$\bar{a}_{E} = \bar{a}_{CD} + \bar{\alpha}_{3} \times \bar{r}_{E/CD} + \Omega_{3} \times \left(\Omega_{3} \times \bar{r}_{E/CD}\right) = \begin{bmatrix} -106.32 \, L - 16315 \, R \\ 25.133 \, L + 25.133 \, R \\ 495.26 \, L + 182.07 \, R \end{bmatrix}$$

Therefore:

$$a_E = -(106.32\,L + 16315\,R)\;i + 25.133(L+R)\;j + (495.26\,L + 182.07\,R)\;k \ \longrightarrow \mathcal{A}$$
nswer

These solutions match the text.

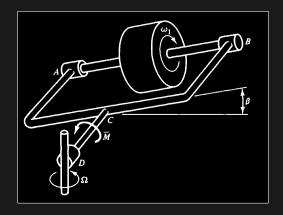
If I solve this for the solution where the vertical axis rotation is counter-clockwise, we get that:

$$egin{aligned} v_E &= (0.4189L - 127.3392R)\,j - 10\,(L+R)\,k \ a_E &= -(106.32\,L + 16315\,R)\,\,i + 25.133(L+R)\,\,j + (495.26\,L + 182.07\,R)\,k \ &\longrightarrow \mathcal{A}$$
nswer

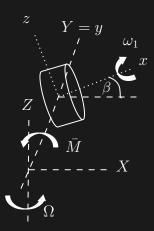
```
syms L R
omega_1 = 20*2*pi/60; % rad/s
omega_2 = 1200 * 2 * pi/60; % rad/s
beta = 36.87*pi/180; % rad
beta_dot = 10; % rad/s
beta_ddot = -500; % rad/s^2
R_{rot} = yRot(beta);
Z = R_rot*z;
Omega_1 = -omega_1 * Z;
Omega_2 = -\text{omega}_1 \times Z + \text{beta}_dot \times y;
Omega_3 = -omega_1*Z+beta_dot*y-omega_2*z; % omega_bar
r_B_A = L*[cos(beta);0;sin(beta)];
r_CD_B = L*x;
r_E_CD = R*x;
v_B = 0 + cross(Omega_1, r_B_A);
v_CD = v_B + cross(Omega_2, r_CD_B);
v_E = v_{CD} + cross(Omega_3, r_E_CD);
alpha_1 = cross(Omega_1,Omega_1);
alpha_3 = alpha_2 + cross(Omega_3,-omega_2*z); % alpha_bar
a_B = 0 + cross(alpha_1, r_B_A) + ...
   cross(Omega_1,cross(Omega_1,r_B_A));
a_CD = a_B + cross(alpha_2, r_CD_B) + ...
   cross(Omega_2,cross(Omega_2,r_CD_B));
a_E = a_{CD} + cross(alpha_3, r_E_{CD}) + ...
   cross(Omega_3,cross(Omega_3,r_E_CD));
function R = yRot(ang)
R = [\cos(ang) \ 0 \sin(ang);
     -sin(ang) 0 cos(ang)]';
```

Problem 3

The gyroscopic turn indicator consists of a 1-kg flywheel whose principal radii of gyration are $k_x=50$ mm and $k_y=k_z=40$ mm. The center of mass of the flywheel coincides with the intersection of axes AB and CD. The flywheel spins relative to the gimbal at the constant rate $\omega_1=10,000$ rev/min. A couple \bar{M} acts about shaft CD, which supports the gimbal, in order to control the angle β between the gimbal and the horizontal. Determine \bar{M} when the rotation rate about the vertical axis is $\Omega=0.8$ rad/s.



We will define the following frames for the system:



For this problem the prompt seems to imply that the rotation rate about the vertical axis is constant.

Constructing the angular velocity vector $\bar{\omega}$ of $\{xyz\}$ by vectorially adding the simple rotation rates according to:

$$\bar{\omega} = \omega_1 \bar{e}_1 + \omega_2 \bar{e}_2$$

This gives us:

$$\bar{\omega} = \Omega K + \omega_1(-i)$$

Using the following coordinate transformation:

$$R_{\text{rot}} = \begin{bmatrix} \cos(-\beta) & 0 & -\sin(-\beta) \\ 0 & 1 & 0 \\ \sin(-\beta) & 0 & \cos(-\beta) \end{bmatrix}$$

$$K = R_{\text{rot}} \begin{bmatrix} 0 & I \\ 0 & J \\ 1 & K \end{bmatrix} = \begin{bmatrix} \sin(\beta) \\ 0 \\ \cos(\beta) \end{bmatrix} = \sin(\beta) i + \cos(\beta) k$$

This gives us the angular velocity vector in the form:

$$\bar{\omega} = \begin{bmatrix} \left(\Omega \sin (\beta) - \omega_1\right) & i \\ 0 & j \\ \Omega \cos (\beta) & k \end{bmatrix} = \left(\Omega \sin (\beta) - \omega_1\right) i + \Omega \cos (\beta) k$$

Using the equation for angular acceleration:

$$\bar{\alpha} = \sum_{n} \left(\dot{\omega}_n \bar{e}_n + \bar{\Omega}_n \times \omega_n \bar{e}_n \right)$$

We see compute that the angular acceleration is:

$$\bar{\alpha} = \bar{\omega} \times \omega_1(-i) = -\Omega \,\omega_1 \,\cos(\beta) \,j$$

Since the torque \bar{M} is acting in the j direction, we can refer to equation 6.1.6 in the textbook:

$$\sum \bar{M} \ j = I_{yy}\alpha_y + (I_{zz} - I_{xx}) \,\omega_x \omega_z$$

Solving for the principal axis inertia quantities:

$$I_{xx} = mk_1^2 = (1 \text{ kg}) \left(\frac{50}{1000} \text{ m}\right)^2 = 0.0025 \text{ kg-m}^2$$
$$I_{yy} = I_{zz} = mk_2^2 = (1 \text{ kg}) \left(\frac{40}{1000} \text{ m}\right)^2 = 0.0016 \text{ kg-m}^2$$

We can solve for M as:

$$\bar{M} = 0.0016 \left(-\Omega \,\omega_1 \,\cos(\beta) \right) + \left(0.0016 - 0.0025 \right) \left(\Omega \,\sin(\beta) - \omega_1 \right) \left(\Omega \,\cos(\beta) \right)
= 0.0016 \left(-0.8 \left(\frac{10000(2\pi)}{60} \right) \,\cos(\beta) \right) +
\left(0.0016 - 0.0025 \right) \left(0.8 \,\sin(\beta) - \left(\frac{10000(2\pi)}{60} \right) \right) \left(0.8 \,\cos(\beta) \right)
= 0.000576 \cos(\beta) \sin(\beta) - 2.0944 \cos(\beta) \text{ N-m}$$

The couple \bar{M} when the rotation rate about the vertical axis is $\Omega = 0.8$ rad/s is:

$$\bar{M} = 0.000576\cos(\beta)\sin(\beta) - 2.0944\cos(\beta) \text{ N-m}$$

 $\longrightarrow \mathcal{A}$ nswer

```
clc,clear
syms k t beta
syms omega_1 Omega M
sympref('FloatingPointOutput',true);

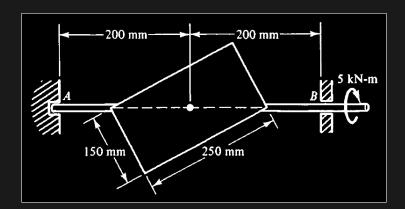
R = yRot(-beta);
omega_bar = Omega*R*[0;0;1] + omega_1*[-1;0;0];
alpha_bar = cross(omega_bar,omega_1*[-1;0;0]);

m = 1; % kg
k_1 = 50/1000; % m
k_2 = 40/1000; % m
I_1 = m*k_1^2;
I_2 = m*k_2^2;

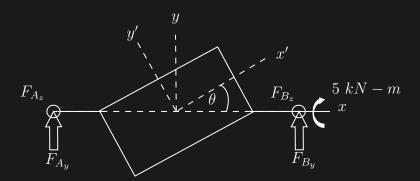
M = I_2*alpha_bar-(I_2-I_1)*omega_bar(1)*omega_bar(3);
```

Problem 4

A 50-kg rectangular plate is mounted diagonally on a shaft whose mass is negligible. The system was initially at rest when a constant torque of 5 kN-m is applied to the shaft. Determine the reactions at bearings A and B four seconds after the application of the torque.



The following sketch details the body fixed frames $\{xyz\}$ and $\{x'y'z'\}$ and the reaction forces F_A and F_B .



The forces both consist of x and z components. The x-components are in the positive x direction which is up in the sketch, and the z-components are in the positive z direction which is out of the page in the sketch. The z-components are denoted by the circles in the sketch.

There is one rotation about the x-axis that I will denote as Ω . The angular velocity and angular rotation for the system is:

$$\bar{\omega} = \omega_1 \bar{e}_1 = -\Omega i$$

$$\bar{\alpha} = \dot{\omega}_1 \bar{e}_1 + \underline{\bar{\Omega}}_1 \times \omega_1 \bar{e}_1 = -\dot{\Omega} i$$

Using the centriodal inertia properties of a rectangular parallelepiped from the back of the textbook:

$$I_{x'x'} = \frac{1}{12}m (0.15)^2 = 0.09375 \text{ kg-m}^2$$

$$I_{y'y'} = \frac{1}{12}m (0.25)^2 = 0.26042 \text{ kg-m}^2$$

$$I_{z'z'} = \frac{1}{12}m (0.15^2 + 0.25^2) = 0.35417 \text{ kg-m}^2$$

This expressed as an inertia tensor is:

$$I_{\text{pa}} = \begin{bmatrix} 0.0938 & 0 & 0\\ 0 & 0.2604 & 0\\ 0 & 0 & 0.3542 \end{bmatrix}$$

Solving for θ , and the rotation matrix that expresses $\{x'y'z'\}$ in terms of $\{xyz\}$:

$$\theta = \tan^{-1} \left(\frac{75}{125} \right) = 0.5404 \text{ rads}$$

$$R = \begin{bmatrix} \cos(\theta) & -\sin(\theta) & 0\\ \sin(\theta) & \cos(\theta) & 0\\ 0 & 0 & 1 \end{bmatrix} = \begin{bmatrix} 0.8575 & -0.5145 & 0\\ 0.5145 & 0.8575 & 0\\ 0 & 0 & 1 \end{bmatrix}$$

With this we can solve for the inertia tensor in the $\{xyz\}$ frame:

$$I = I_{\{xyz\}} = RI_{pa}R^T = \begin{bmatrix} 0.1379 & -0.0735 & 0 \\ -0.0735 & 0.2163 & 0 \\ 0 & 0 & 0.3542 \end{bmatrix}$$

The equation for the resultant moment is:

$$\sum \bar{M}_A = \frac{\partial \bar{H}_A}{\partial t} + \bar{\omega} \times \bar{H}_A$$

Computing \bar{H}_A and $\frac{\partial \bar{H}_A}{\partial t}$ by:

$$\bar{H}_{A} = (I_{xx}\omega_{x} - I_{xy}\omega_{y} - I_{xz}\omega_{z}) i + (I_{yy}\omega_{y} - I_{yx}\omega_{x} - I_{yz}\omega_{z}) j + (I_{zz}\omega_{z} - I_{zx}\omega_{x} - I_{zy}\omega_{y}) k$$

$$= \begin{bmatrix} -0.1379 \Omega \\ -0.0735 \Omega \\ 0 \end{bmatrix}$$

$$\frac{\partial \bar{H}_{A}}{\partial t} = (I_{xx}\alpha_{x} - I_{xy}\alpha_{y} - I_{xz}\alpha_{z}) i + (I_{yy}\alpha_{y} - I_{yx}\alpha_{x} - I_{yz}\alpha_{z}) j + (I_{zz}\alpha_{z} - I_{zx}\alpha_{x} - I_{zy}\alpha_{y}) k$$

$$= \begin{bmatrix} -0.1379 \dot{\Omega} \\ -0.0735 \dot{\Omega} \\ 0 \end{bmatrix}$$

The equation for the resultant moment becomes:

$$ar{M} = rac{\partial ar{H}_A}{\partial t} + ar{\omega} imes ar{H}_A = \left[egin{array}{c} -0.1379 \, \dot{\Omega} \\ -0.0735 \, \dot{\Omega} \\ 0.0735 \, \Omega^2 \end{array}
ight]$$

Equating this to the moments acting on the system:

$$\begin{bmatrix} 5000 \text{ N-m} \\ 0.2F_{A_z} - 0.2F_{B_z} \\ 0.2F_{B_y} - 0.2F_{A_y} \end{bmatrix} = \begin{bmatrix} -0.1379 \,\dot{\Omega} \\ -0.0735 \,\dot{\Omega} \\ 0.0735 \,\Omega^2 \end{bmatrix}$$

Since we can see by inspection that $\sum F_y = F_{A_y} + F_{B_y} = 0$ and $\sum F_z = F_{A_z} + F_{B_z} = 0$, we can rewrite the equation as:

$$\begin{bmatrix} 5000 \\ 0.4F_{A_z} \\ -0.4F_{A_y} \end{bmatrix} = \begin{bmatrix} -0.1379 \,\dot{\Omega} \\ -0.0735 \,\dot{\Omega} \\ 0.0735 \,\Omega^2 \end{bmatrix}$$

Given that $\Omega = \dot{\Omega}t$ we have four equations and four unknowns. Solving this system of equations, we get that:

$$\Omega = 145066.7 \text{ rad/s}$$
 $\dot{\Omega} = 36266.67 \text{ rad/s}^2$
 $F_{A_y} = -3.8684 \times 10^9 \text{ N}$
 $F_{A_z} = -6666.7 \text{ N}$
 $F_{B_y} = 3.8684 \times 10^9 \text{ N}$
 $F_{B_z} = 6666.7 \text{ N}$

 $\longrightarrow \mathcal{A}$ nswer

```
clc,clear
syms omega Omega_dot
% syms theta real
sympref('FloatingPointOutput',true);
theta = atan(75/125);

R = zRot(theta);
omega_bar = Omega*[-1;0;0];
alpha_bar = Omega_dot*[-1;0;0];
```

```
m = 50;
I_pa_x = (1/12) *m*(0.15)^2;
I_pa_yy = (1/12) *m*(0.25)^2;
I_pa_zz = (1/12) *m* (0.15^2+0.25^2);
I_pa = diag([I_pa_xx,I_pa_yy,I_pa_zz]);
I = R*I_pa*transpose(R);
[M_A, H_A, d_H_A] = computeResultantMoment(I, omega_bar, alpha_bar);
syms Fy Fz
soln = solve([-5000; 0.4*Fz; -0.4*Fy; Omega] == [M_A; Omega_dot*4]);
    R = [\cos(ang) - \sin(ang) 0;
           sin(ang) cos(ang) 0;
                             0 1];
function [M_A, H_A, d_H_A] = computeResultantMoment(I, omega, alpha)
     arguments
         omega (3,1)
     H_A = [I(1,1) * omega(1) - I(1,2) * omega(2) - I(1,3) * omega(3);
              I(2,2)*omega(2) - I(2,1)*omega(1) - I(2,3)*omega(3);
             I(3,3)*omega(3) - I(3,2)*omega(1) - I(3,2)*omega(2)];
     d_H_A = [I(1,1)*alpha(1) - I(1,2)*alpha(2) - I(1,3)*alpha(3);
                I(2,2)*alpha(2) - I(2,1)*alpha(1) - I(2,3)*alpha(3);
I(3,3)*alpha(3) - I(3,2)*alpha(1) - I(3,2)*alpha(2)];
    M_A = d_H_A + cross(omega, H_A);
```

Submitted by Austin Barrilleaux on October 21, 2024.