

November 13, 2024

MODULE 11 — Assignment

Problem 1: Solve Ginsberg 9.28

The absolute velocity of a particle may be represented by the components v_x , v_y , and v_z relative to the axes of a moving reference system xyz . Suppose that the angular velocity $\bar{\omega}$ of xyz and the velocity \bar{v}_O of the origin of xyz are known as functions of time. Derive the Gibbs-Appell equations of motion relating the quasi-velocities $\dot{\gamma}_1 = v_x$, $\dot{\gamma}_2 = v_y$, and $\dot{\gamma}_3 = v_z$ to the resultant force acting on the particle.

Where:

$$\bar{\omega} = \left\langle \begin{array}{c} \omega_x \\ \omega_y \\ \omega_z \end{array} \right\rangle$$

Given that:

$$\bar{v} = \left\langle \begin{array}{c} v_x \\ v_y \\ v_z \end{array} \right\rangle = \left\langle \begin{array}{c} \dot{\gamma}_1 \\ \dot{\gamma}_2 \\ \dot{\gamma}_3 \end{array} \right\rangle$$

Solving for acceleration:

$$\begin{aligned} \bar{a} &= \frac{\partial \bar{v}}{\partial t} + \bar{\omega} \times \bar{v} \\ &= \frac{\partial \dot{\gamma}}{\partial t} + \bar{\omega} \times \dot{\gamma} \\ &= \left\langle \begin{array}{c} \ddot{\gamma}_1 - \dot{\gamma}_2 \omega_z + \dot{\gamma}_3 \omega_y \\ \ddot{\gamma}_2 + \dot{\gamma}_1 \omega_z - \dot{\gamma}_3 \omega_x \\ \ddot{\gamma}_3 - \dot{\gamma}_1 \omega_y + \dot{\gamma}_2 \omega_x \end{array} \right\rangle \end{aligned}$$

Given that the Gibbs-Appell function for a system of particles is:

$$S = \sum_p \frac{1}{2} m \bar{a}_p \cdot \bar{a}_p$$

For this single particle case:

$$\begin{aligned} S &= \frac{1}{2} m (\bar{a} \cdot \bar{a}) \\ &= \frac{1}{2} m \left[(\ddot{\gamma}_3 - \dot{\gamma}_1 \omega_y + \dot{\gamma}_2 \omega_x)^2 + (\ddot{\gamma}_2 + \dot{\gamma}_1 \omega_z - \dot{\gamma}_3 \omega_x)^2 + (\ddot{\gamma}_1 - \dot{\gamma}_2 \omega_z + \dot{\gamma}_3 \omega_y)^2 \right] \end{aligned}$$

Where the equations of motion are calculated as:

$$\frac{\partial S}{\partial \ddot{\gamma}_j} = \Gamma_j = \Gamma_1$$

The virtual work associated with the forces applied to the particle is:

$$\delta W = \sum \bar{F} \cdot \delta \bar{x} = \sum_{j=1}^K \Gamma_j \delta \gamma_j = \sum \bar{F} \cdot \left\langle \begin{matrix} \delta \gamma_1 \\ \delta \gamma_2 \\ \delta \gamma_3 \end{matrix} \right\rangle$$

The equation of motion is solved for as:

$$\frac{\partial S}{\partial \ddot{\gamma}} = m \left\langle \begin{matrix} \ddot{\gamma}_1 - \dot{\gamma}_2 \omega_z + \dot{\gamma}_3 \omega_y \\ \ddot{\gamma}_2 + \dot{\gamma}_1 \omega_z - \dot{\gamma}_3 \omega_x \\ \ddot{\gamma}_3 - \dot{\gamma}_1 \omega_y + \dot{\gamma}_2 \omega_x \end{matrix} \right\rangle = \Gamma_1 = \left\langle \begin{matrix} \sum F_x \\ \sum F_y \\ \sum F_z \end{matrix} \right\rangle = \left\langle \begin{matrix} F_x \\ F_y \\ F_z \end{matrix} \right\rangle$$

Or:

$$\begin{aligned} m (\ddot{\gamma}_1 - \dot{\gamma}_2 \omega_z + \dot{\gamma}_3 \omega_y) &= F_x \\ m (\ddot{\gamma}_2 + \dot{\gamma}_1 \omega_z - \dot{\gamma}_3 \omega_x) &= F_y \\ m (\ddot{\gamma}_3 - \dot{\gamma}_1 \omega_y + \dot{\gamma}_2 \omega_x) &= F_z \end{aligned}$$

→ Answer

Where:

$$\dot{\gamma} = \left\langle \begin{matrix} \dot{\gamma}_1 \\ \dot{\gamma}_2 \\ \dot{\gamma}_3 \end{matrix} \right\rangle = v = \left\langle \begin{matrix} v_x \\ v_y \\ v_z \end{matrix} \right\rangle = v_0 + \bar{\omega} \times \bar{r} = \left\langle \begin{matrix} v_{0x} - \omega_z y + \omega_y z \\ v_{0y} + \omega_z x - \omega_x z \\ v_{0z} - \omega_y x + \omega_x y \end{matrix} \right\rangle$$

The following MATLAB script was used to solve this problem:

```
%[text] Problem 1: Solve Ginsberg 9\28
%[text]
syms t m
syms v_x(t) v_y(t) v_z(t)
syms v_x_o(t) v_y_o(t) v_z_o(t)
syms x(t) y(t) z(t)
syms omega_x(t) omega_y(t) omega_z(t)

omega_bar = [omega_x;omega_y;omega_z];
v_o = [v_x_o;v_y_o;v_z_o];
v_bar = [v_x;v_y;v_z];
r_p_o = [x;y;z];

v_p = v_o + cross(omega_bar,r_p_o) % gamma_dot %[output:3f34eeb3]

syms gamma_dot_1(t) ...
    gamma_dot_2(t) ...
    gamma_dot_3(t)

gamma_dot = [gamma_dot_1;
             gamma_dot_2;
             gamma_dot_3];

a_p = diff(gamma_dot,t) + cross(omega_bar,gamma_dot) %[output:6931f860]

S = simplify(0.5*m*(transpose(a_p)*a_p)) %[output:10e7d569]

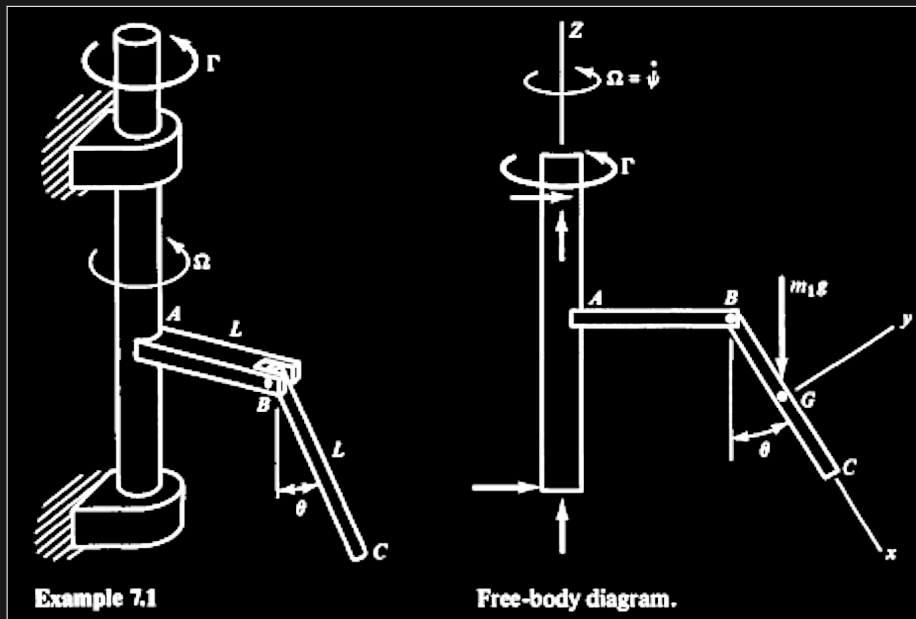
Gamma_lhs = simplify([ ... %[output:group:8b609d04] %[output:92d1caac]
    diff(S,diff(gamma_dot_1,t)); %[output:92d1caac]
    diff(S,diff(gamma_dot_2,t)); %[output:92d1caac]
    diff(S,diff(gamma_dot_3,t))]) %[output:group:8b609d04] %[output:92d1caac]
syms F_x F_y F_z
F =[F_x F_y F_z] %[output:89f6e948]
Gamma_rhs = [[F_x 0 0]*gamma_dot; %[output:group:02f1af22] %[output:7788bb0f]
             [0 F_y 0]*gamma_dot; %[output:7788bb0f]
             [0 0 F_z]*gamma_dot] %[output:group:02f1af22] %[output:7788bb0f]

collect(Gamma_lhs,m) == Gamma_rhs %[output:585416fa]
```

Problem 2:

Use the Gibbs-Appell approach to find the equations of motion for this problem.

A torque Γ applied to the vertical shaft of the T-bar causes the rotation rate Ω about the vertical axis to increase in proportion to the angle θ by which bar BC swings outward, that is, $\Omega = c\theta$. The mass of bar BC is m_1 and the moment of inertia of the T-bar about its axis of rotation is I_2 . Determine the equations of motion for the system, and for the torque Γ .



For the purpose of this problem, as was recommended in the office hour, we will replace the y -axis of the body frame with the z -axis. This will simplify the inertial to body rotation we perform later in the solution.

First we will determine location of point G in the inertial frame. By inspection this is:

$$\bar{r}_G = \begin{pmatrix} \cos(\psi) \left(L + \frac{1}{2}L \sin(\theta) \right) \\ \sin(\psi) \left(L + \frac{1}{2}L \sin(\theta) \right) \\ -\frac{1}{2}L \cos(\theta) \end{pmatrix}$$

From this we can compute the velocity at point G :

$$\bar{v}_G = \left\langle \begin{array}{l} \frac{1}{2}L \cos(\psi) \cos(\theta) \frac{\partial \theta}{\partial t} - \sin(\psi) \left(L + \frac{1}{2}L \sin(\theta)\right) \frac{\partial \psi}{\partial t} \\ \frac{1}{2}L \cos(\theta) \sin(\psi) \frac{\partial \theta}{\partial t} + \cos(\psi) \left(L + \frac{1}{2}L \sin(\theta)\right) \frac{\partial \psi}{\partial t} \\ \frac{1}{2}L \sin(\theta) \frac{\partial \theta}{\partial t} \end{array} \right\rangle$$

Which we can then use to compute acceleration at point G :

$$\bar{a}_G = \left\langle \begin{array}{l} \frac{L \cos(\psi) \cos(\theta) \frac{\partial^2 \theta}{\partial t^2}}{2} - \frac{L \cos(\psi) \sin(\theta) \left(\frac{\partial \theta}{\partial t}\right)^2}{2} - \frac{L \cos(\psi) (\sin(\theta)+2) \left(\frac{\partial \psi}{\partial t}\right)^2}{2} - \frac{L \sin(\psi) (\sin(\theta)+2) \frac{\partial^2 \psi}{\partial t^2}}{2} - L \cos(\theta) \sin(\psi) \frac{\partial \theta}{\partial t} \frac{\partial \psi}{\partial t} \\ \frac{L \cos(\theta) \sin(\psi) \frac{\partial^2 \theta}{\partial t^2}}{2} - \frac{L \sin(\psi) \sin(\theta) \left(\frac{\partial \theta}{\partial t}\right)^2}{2} - \frac{L \sin(\psi) (\sin(\theta)+2) \left(\frac{\partial \psi}{\partial t}\right)^2}{2} + \frac{L \cos(\psi) (\sin(\theta)+2) \frac{\partial^2 \psi}{\partial t^2}}{2} + L \cos(\psi) \cos(\theta) \frac{\partial \theta}{\partial t} \frac{\partial \psi}{\partial t} \\ \frac{L \sin(\theta) \frac{\partial^2 \theta}{\partial t^2}}{2} + \frac{L \cos(\theta) \left(\frac{\partial \theta}{\partial t}\right)^2}{2} \end{array} \right\rangle$$

Replacing $\dot{\theta}$ and $\dot{\psi}$ with the quasi-velocity terms gives us:

$$\bar{a}_G = \left\langle \begin{array}{l} \frac{L \cos(\psi) \cos(\theta) \ddot{\gamma}_1}{2} - \frac{L \cos(\psi) \sin(\theta) (\dot{\gamma}_1)^2}{2} - \frac{L \cos(\psi) (\dot{\gamma}_2)^2 (\sin(\theta)+2)}{2} - \frac{L \sin(\psi) (\sin(\theta)+2) \ddot{\gamma}_2}{2} - L \cos(\theta) \sin(\psi) \dot{\gamma}_2 \dot{\gamma}_1 \\ \frac{L \cos(\theta) \sin(\psi) \ddot{\gamma}_1}{2} - \frac{L \sin(\psi) \sin(\theta) (\dot{\gamma}_1)^2}{2} - \frac{L \sin(\psi) (\dot{\gamma}_2)^2 (\sin(\theta)+2)}{2} + \frac{L \cos(\psi) (\sin(\theta)+2) \ddot{\gamma}_2}{2} + L \cos(\psi) \cos(\theta) \dot{\gamma}_2 \dot{\gamma}_1 \\ \frac{L \sin(\theta) \ddot{\gamma}_1}{2} + \frac{L \cos(\theta) (\dot{\gamma}_1)^2}{2} \end{array} \right\rangle$$

To convert this acceleration into the body frame, we will define the following inertial to body rotation:

$$R_{xyz}^{XYZ} = R_z(\psi)R_y(\theta) = \begin{bmatrix} \cos(\psi) & -\sin(\psi) & 0 \\ \sin(\psi) & \cos(\psi) & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} \cos(\theta) & 0 & \sin(\theta) \\ 0 & 1 & 0 \\ -\sin(\theta) & 0 & \cos(\theta) \end{bmatrix}$$

Which simplifies to:

$$R_{xyz}^{XYZ} = \begin{bmatrix} \cos(\psi) \cos(\theta) & -\sin(\psi) \cos(\theta) & \sin(\theta) \\ \cos(\psi) \sin(\theta) & \cos(\psi) & \sin(\psi) \sin(\theta) \\ -\sin(\theta) & 0 & \cos(\theta) \end{bmatrix}$$

The transpose of this gives us the inertial to body transform:

$$R_{XYZ}^{xyz} = \begin{bmatrix} \cos(\psi) \cos(\theta) & \cos(\theta) \sin(\psi) & -\sin(\theta) \\ -\sin(\psi) & \cos(\psi) & 0 \\ \cos(\psi) \sin(\theta) & \sin(\psi) \sin(\theta) & \cos(\theta) \end{bmatrix}$$

We can compute the acceleration term as:

$$\bar{a}_G = R_{XYZ}^{xyz} \bar{a}_G = \left\langle \begin{array}{c} \frac{L \cos(2\theta) \ddot{\gamma}_1}{2} - \frac{L \sin(2\theta) (\dot{\gamma}_1)^2}{2} - \frac{L \sin(2\theta) (\dot{\gamma}_2)^2}{4} - L \cos(\theta) (\dot{\gamma}_2)^2 \\ L \ddot{\gamma}_2 + \frac{L \sin(\theta) \ddot{\gamma}_2}{2} + L \cos(\theta) \dot{\gamma}_2 \dot{\gamma}_1 \\ \frac{L (2 \cos(\theta)^2 - 1) (\dot{\gamma}_1)^2}{2} - L \sin(\theta) (\dot{\gamma}_2)^2 - \frac{L (\dot{\gamma}_2)^2}{4} + \frac{L (2 \cos(\theta)^2 - 1) (\dot{\gamma}_2)^2}{4} + L \cos(\theta) \sin(\theta) \ddot{\gamma}_1 \end{array} \right\rangle$$

The Gibbs-Appell function for the system is given by:

$$S = \frac{1}{2} m (\bar{a}_G \cdot \bar{a}_G) + \frac{1}{2} \bar{\alpha} \cdot \frac{\partial \bar{H}_G}{\partial t} + \bar{\alpha} \cdot (\bar{\omega} \times \bar{H}_G) + \frac{1}{2} I_2 \dot{\psi}^2$$

The first term of S is computed as:

$$\begin{aligned} \frac{1}{2} m (\bar{a}_G \cdot \bar{a}_G) &= \frac{1}{2} m \left(L \ddot{\gamma}_2 + \frac{L \sin(\theta) \ddot{\gamma}_2}{2} + L \cos(\theta) \dot{\gamma}_2 \dot{\gamma}_1 \right)^2 \\ &+ \frac{1}{2} m \left(L \cos(\theta) (\dot{\gamma}_2)^2 + \frac{L \sin(2\theta) (\dot{\gamma}_1)^2}{2} + \frac{L \sin(2\theta) (\dot{\gamma}_2)^2}{4} - \frac{L \cos(2\theta) \ddot{\gamma}_1}{2} \right)^2 \\ &+ \frac{1}{2} m \left(\frac{L (2 \cos(\theta)^2 - 1) (\dot{\gamma}_1)^2}{2} - L \sin(\theta) (\dot{\gamma}_2)^2 - \frac{L (\dot{\gamma}_2)^2}{4} \right. \\ &\quad \left. + \frac{L (2 \cos(\theta)^2 - 1) (\dot{\gamma}_2)^2}{4} + L \cos(\theta) \sin(\theta) \ddot{\gamma}_1 \right)^2 \end{aligned}$$

The angular velocity vector of the system in the body frame is, by inspection:

$$\bar{\omega} = \left\langle \begin{array}{c} -\cos(\gamma_1) \dot{\gamma}_2 \\ -\dot{\gamma}_1 \\ \sin(\gamma_1) \dot{\gamma}_2 \end{array} \right\rangle$$

The angular acceleration vector is therefore:

$$\bar{\alpha} = \frac{\partial \bar{\omega}}{\partial t} + (\bar{\omega} \times \bar{\omega}) = \left\langle \begin{array}{c} \sin(\gamma_1) \dot{\gamma}_2 \dot{\gamma}_1 - \cos(\gamma_1) \ddot{\gamma}_2 \\ -\ddot{\gamma}_1 \\ \sin(\gamma_1) \ddot{\gamma}_2 + \cos(\gamma_1) \dot{\gamma}_2 \dot{\gamma}_1 \end{array} \right\rangle$$

The inertia tensor of the bar centered at G is:

$$I = \frac{1}{12}mL^2 \begin{bmatrix} 0 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

From this we can compute the angular momentum as:

$$\bar{H}_G = I\bar{\omega} = \left\langle \begin{array}{c} 0 \\ -\frac{L^2 m \dot{\gamma}_1}{12} \\ \frac{L^2 m \sin(\gamma_1) \dot{\gamma}_2}{12} \end{array} \right\rangle$$

The second term in the Gibbs-Appell function is computed as:

$$\frac{1}{2}\bar{\alpha} \cdot \frac{\partial \bar{H}_G}{\partial t} = \left(\frac{\sin(\gamma_1)}{2} \ddot{\gamma}_2 + \frac{\cos(\gamma_1)}{2} \dot{\gamma}_2 \dot{\gamma}_1 \right) \left(\frac{L^2 m \sin(\gamma_1)}{12} \ddot{\gamma}_2 + \frac{L^2 m \cos(\gamma_1)}{12} \dot{\gamma}_2 \dot{\gamma}_1 \right) + \frac{L^2 m (\ddot{\gamma}_1)^2}{24}$$

The third term is:

$$\bar{\alpha} \cdot (\bar{\omega} \times \bar{H}_G) = \frac{L^2 m \cos(\gamma_1) (\sin(\gamma_1) \ddot{\gamma}_2 + \cos(\gamma_1) \dot{\gamma}_2 \dot{\gamma}_1)}{12} - \frac{L^2 m \cos(\gamma_1) \sin(\gamma_1) (\dot{\gamma}_2)^2 \dot{\gamma}_1}{12}$$

The third term can be rewritten as:

$$\frac{1}{2}I_2 \ddot{\psi}^2 = \frac{I_2 (\ddot{\gamma}_2)^2}{2}$$

All together, we can compute the following derivatives that form the Gibbs-Appell equations as:

$$\begin{aligned} \frac{\partial S}{\partial \ddot{\gamma}_1} &= \frac{L^2 m \dot{\gamma}_1}{3} - \frac{L^2 m \sin(2\gamma_1) (\dot{\gamma}_2)^2}{24} - \frac{L^2 m \sin(2\theta) (\dot{\gamma}_2)^2}{8} - \frac{L^2 m \cos(\theta) (\dot{\gamma}_2)^2}{2} \\ \frac{\partial S}{\partial \ddot{\gamma}_2} &= I_2 \ddot{\gamma}_2 + \frac{4 L^2 m \dot{\gamma}_2}{3} - \frac{L^2 m \cos(\gamma_1)^2 \ddot{\gamma}_2}{12} - \frac{L^2 m \cos(\theta)^2 \ddot{\gamma}_2}{4} + L^2 m \sin(\theta) \ddot{\gamma}_2 + L^2 m \cos(\theta) \dot{\gamma}_2 \dot{\gamma}_1 \\ &\quad + \frac{L^2 m \sin(2\gamma_1) \dot{\gamma}_2 \dot{\gamma}_1}{12} + \frac{L^2 m \cos(\theta) \sin(\theta) \dot{\gamma}_2 \dot{\gamma}_1}{2} \end{aligned}$$

Imposing the constraint that $\dot{\gamma}_2 = c \dot{\theta}$ and $\ddot{\gamma}_2 = c \ddot{\theta} = c \dot{\gamma}_1$:

$$\begin{aligned}\frac{\partial S}{\partial \ddot{\gamma}_1} &= \frac{1}{3}L^2 m \ddot{\gamma}_1 - \frac{1}{3}L^2 c^2 m \sin(\theta) \cos(\theta) \gamma_1^2 - \frac{1}{2}L^2 c^2 m \cos(\theta) \gamma_1^2 \\ \frac{\partial S}{\partial \ddot{\gamma}_2} &= I_2 c \dot{\gamma}_1 + \frac{4}{3}L^2 c m \dot{\gamma}_1 - \frac{1}{3}L^2 c m \cos(\theta)^2 \dot{\gamma}_1 + L^2 c m \sin(\theta) \dot{\gamma}_1 \\ &\quad + \frac{2}{3}L^2 c m \sin(\theta) \cos(\theta) \gamma_1 \dot{\gamma}_1 + L^2 c m \cos(\theta) \gamma_1 \dot{\gamma}_1\end{aligned}$$

Further simplifying:

$$\begin{aligned}\frac{\partial S}{\partial \ddot{\gamma}_1} &= \frac{1}{3}L^2 m \ddot{\gamma}_1 - L^2 c^2 m \cos(\theta) \gamma_1^2 \left(\frac{1}{2} + \frac{1}{3} \sin(\theta) \right) = \Gamma_1 \\ \frac{\partial S}{\partial \ddot{\gamma}_2} &= I_2 c \dot{\gamma}_1 + L^2 c m \left(1 + \sin(\theta) + \frac{1}{3} \sin(\theta)^2 \right) \dot{\gamma}_1 + L^2 c m \cos(\theta) \left(1 + \frac{2}{3} \cos(\theta) \right) \gamma_1 \dot{\gamma}_1 = \Gamma_2\end{aligned}$$

Solving for Γ_j based on the generalized forces:

$$\delta W = \bar{\Gamma} \cdot \delta \bar{\gamma} = \begin{bmatrix} -m g \frac{L}{2} \sin(\theta) \delta \gamma_1 \\ \Gamma \delta \gamma_2 \end{bmatrix}$$

Therefore, the equations of motion for the system are:

$$\begin{aligned}\frac{1}{3}L^2 m \ddot{\gamma}_1 - L^2 c^2 m \cos(\theta) \gamma_1^2 \left(\frac{1}{2} + \frac{1}{3} \sin(\theta) \right) &= -m g \frac{L}{2} \sin(\theta) \\ I_2 c \dot{\gamma}_1 + L^2 c m \left(1 + \sin(\theta) + \frac{1}{3} \sin(\theta)^2 \right) \dot{\gamma}_1 &+ L^2 c m \cos(\theta) \left(1 + \frac{2}{3} \cos(\theta) \right) \gamma_1 \dot{\gamma}_1 = \Gamma\end{aligned}$$

The equations of motion after simplification are:

$$\begin{aligned}\frac{1}{3}\ddot{\gamma}_1 - c^2 \cos(\theta) \gamma_1^2 \left(\frac{1}{2} + \frac{1}{3} \sin(\theta) \right) &= -\frac{g}{2L} \sin(\theta) \\ \frac{1}{L^2 m} I_2 \dot{\gamma}_1 + \left(1 + \sin(\theta) + \frac{1}{3} \sin(\theta)^2 \right) \dot{\gamma}_1 &+ \cos(\theta) \left(1 + \frac{2}{3} \cos(\theta) \right) \gamma_1 \dot{\gamma}_1 = \frac{1}{L^2 c m} \Gamma \\ &\longrightarrow \text{Answer}\end{aligned}$$

The following MATLAB script was used to solve this problem:


```

clc,clear
syms t psi(t) theta(t) L c m
syms gamma_1(t) gamma_2(t)

r_G = [(L+sin(theta)*L/2)*cos(psi); %[output:group:7db8fe06] %[output:1a1aebde]
        (L+sin(theta)*L/2)*sin(psi); %[output:1a1aebde]
        -cos(theta)*L/2] %[output:group:7db8fe06] %[output:1a1aebde]
v_G = diff(r_G,t) %[output:30bffc96]
a_G = simplify(diff(v_G,t)) %[output:42414e71]

a_G = subs(a_G,... %[output:group:8507d802] %[output:456fd1b3]
            [diff(theta,t) diff(psi,t)], [diff(gamma_1,t), diff(gamma_2,t)]) %[output:group:8507d802]

R = transpose(zRot(psi)*yRot(theta)) % transpose ? %[output:6d81fc71]
a_G = simplify(R*a_G) %[output:39ba844a]

S1 = (1/2)*m*simplify(transpose(a_G)*a_G) %[output:6860e3fb]

omega_bar = [-diff(gamma_2,t)*cos(gamma_1); %[output:group:4c308172] %[output:927f17bf]
              -diff(gamma_1,t); %[output:927f17bf]
              diff(gamma_2,t)*sin(gamma_1)] %[output:group:4c308172] %[output:927f17bf]

alpha_bar = diff(omega_bar,t)+cross(omega_bar,omega_bar) %[output:1d7cb1ea]

I = (m*L^2/12)*diag([0,1,1]) %[output:743b6c5e]

H_bar_G = I*omega_bar %[output:04de197a]

S2 = (1/2)*transpose(alpha_bar)*... %[output:group:2b48c35b] %[output:0a548ac1]
      (diff(H_bar_G,t))+cross(omega_bar,H_bar_G) %[output:group:2b48c35b] %[output:0a548ac1]

syms I_2 c

S3 = transpose(alpha_bar)*cross(omega_bar,H_bar_G) %[output:7e3a6cfa]

ST = (1/2)*I_2*diff(gamma_2,t,t)^2 %[output:0af23cf5]

S = S1 + S2 + S3 + ST %[output:73d236de]

EOM_1 = simplify(diff(S,diff(gamma_1,t,t)),1000) %[output:5ddf0e27]
EOM_2 = simplify(diff(S,diff(gamma_2,t,t)),1000) %[output:5ae9317d]

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EOM_1 = simplify(subs(EOM_1,diff(gamma_2,t),c*gamma_1) %[output:7378a275]
EOM_2 = subs(EOM_2,diff(gamma_2,t),c*gamma_1) %[output:2c497ac6]

function R = yRot(ang)
    R = [ cos(ang) 0 sin(ang);
          0 1 0;
          -sin(ang) 0 cos(ang)];
end

function R = zRot(ang)
    R = [ cos(ang) -sin(ang) 0;
          sin(ang) cos(ang) 0;
          0 0 1];
end

```

Submitted by Austin Barrilleaux on November 13, 2024.