

# Analysis of Common-Emitter Amplifier

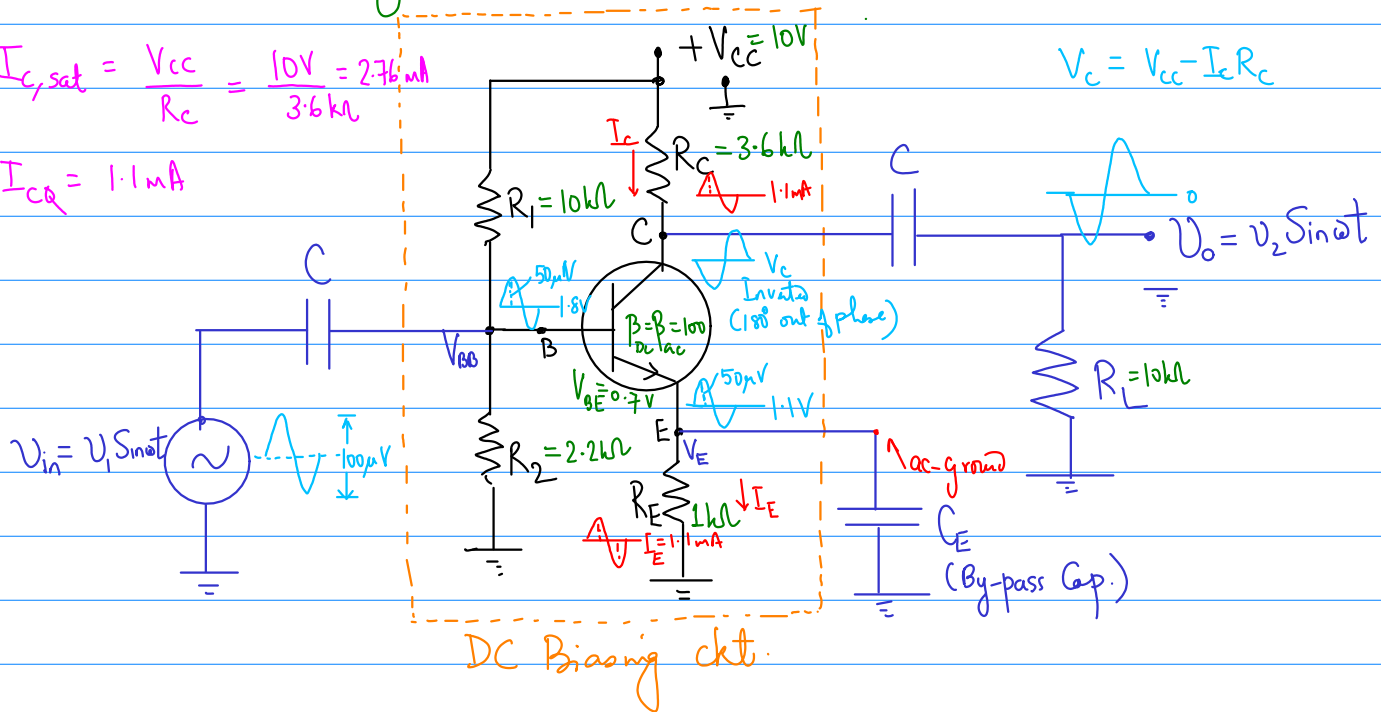
$$I_{C,sat} = \frac{V_{CC}}{R_C} = \frac{10V}{3.6k\Omega} = 2.76mA$$

$$I_{CQ} = 1.1mA$$

$$\beta_{DC} = \frac{I_C}{I_B}$$

$$\beta_{AC} = \frac{i_c}{i_b}$$

$$\beta_{DC} \approx \beta_{AC}$$



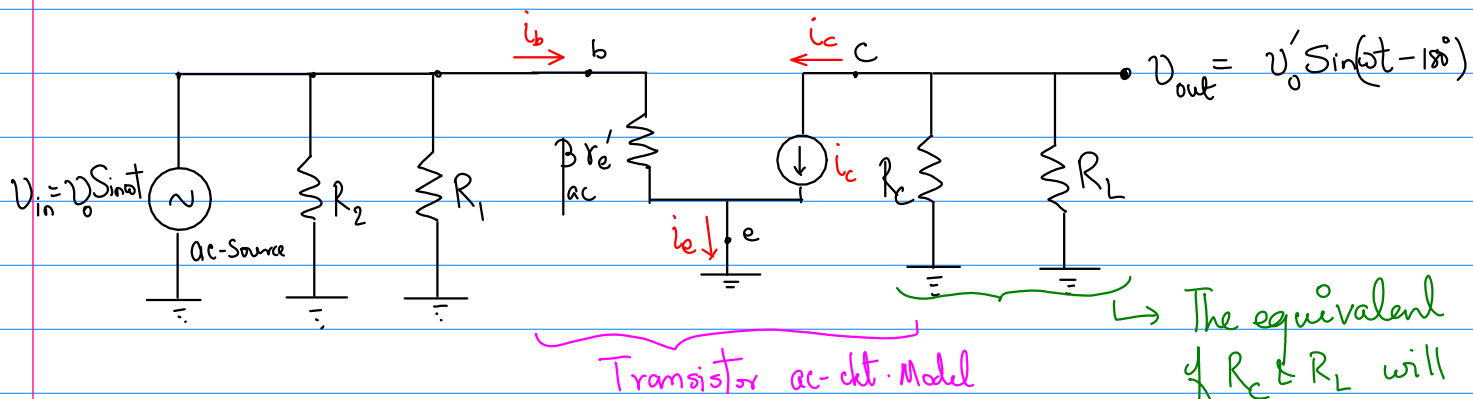
Recap: 1) For DC Analysis

- All capacitors are OPEN.
- Value of the resistors  $R_1$ ,  $R_2$ ,  $R_E$  &  $R_C$  are selected such that the operating point (Q-point) lies <sup>nearby</sup> at the middle of load line. ( $V_{CEQ} = 0.5 V_{CC}$ ).

2) For AC Analysis

- All capacitors are SHORT.
- All dc-sources are also SHORT.
- Use ac-equivalent model of the transistor. (either T-model or  $\pi$ -model)

ac-equivalent ckt. of the CE amplifier:



$$r_c = R_c \parallel R_L$$

$$A_v = \frac{r_c}{r'_e}$$

Estimation of voltage-gain:

$$r_c = 3.6 \text{ k}\Omega \parallel 10 \text{ k}\Omega = \left[ \frac{3.6 \times 10}{3.6 + 10} \right] \text{ k}\Omega$$

$$r_c = \frac{36}{13.6} \text{ k}\Omega = 2.65 \text{ k}\Omega$$

Also,  $r'_e = \frac{25 \text{ mV}}{1.1 \text{ mA}} = 22.7 \Omega$

Therefore,  $A_v = \frac{r_c}{r'_e} = \frac{2.65 \text{ k}\Omega}{22.7 \Omega} = \frac{2650}{22.7}$

$$\approx 116$$

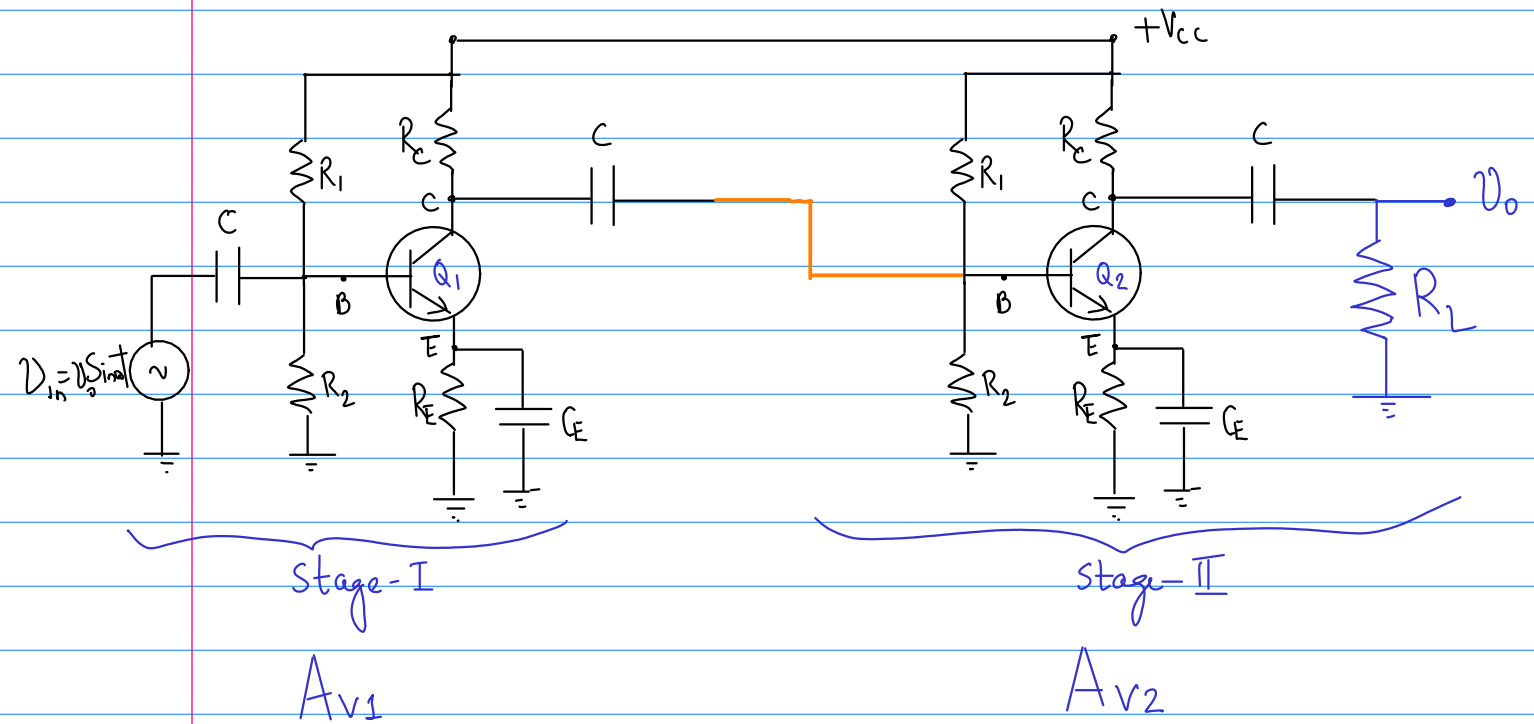
$$A_v = 116$$

input ac-signal of amplitude  
Let's consider,  $V_o(p-p) = 100\mu V$

then,  $V_o'(p-p) = A_v \cdot 100\mu V = 116 \times 100\mu V$

$$V_o'(p-p) = 11.6 \text{ mV}$$

Multi-stage (eg. two-stage) direct coupled CE Amplifier:



Overall voltage gain  $A_v = A_{v1} \cdot A_{v2}$

Similarly, if there 'n' no. of stages, we have

$$A_v = A_{v1} \cdot A_{v2} \cdot A_{v3} \cdots A_{vn}$$

For a given input signal of amp. =  $100\mu\text{V}$  (p-p)

Output of the two-stage amp =  $A_v \cdot 100\mu\text{V}$  (p-p)

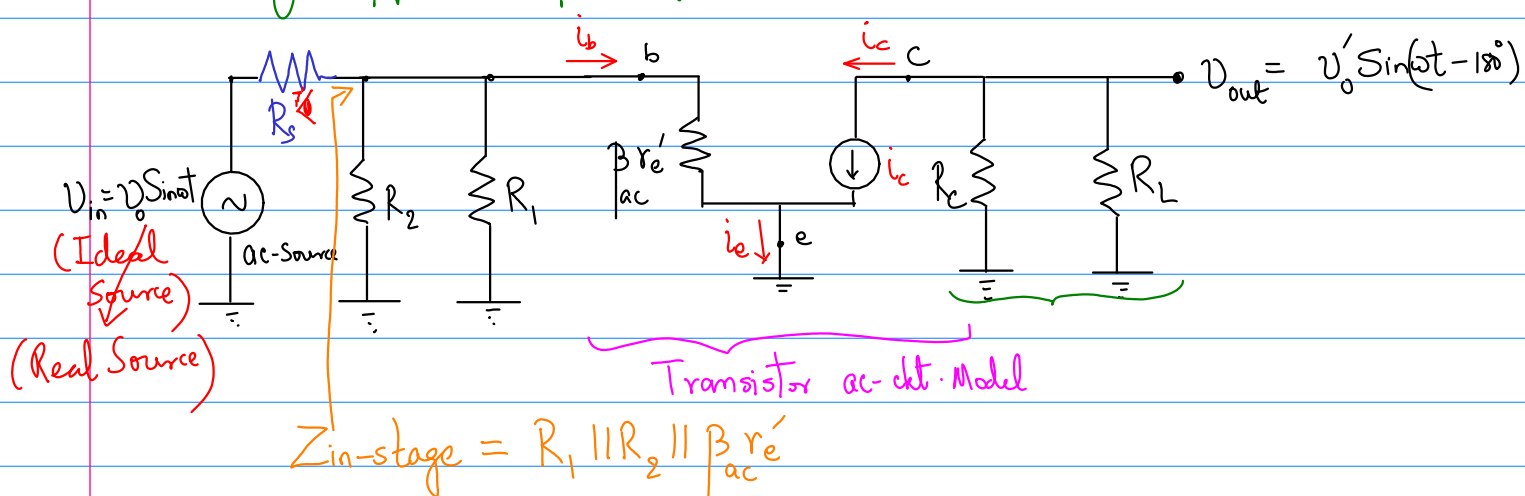
$$= A_{v_1} \cdot A_{v_2} \cdot 100\mu\text{V} \text{ (p-p)}$$

$$= \underbrace{(116)}_{\text{Calculated value}} \cdot \underbrace{(100)}_{\text{Assuming}} \cdot 100\mu\text{V} \text{ (p-p)}$$

$$= 1.16 \text{ V (p-p)}$$

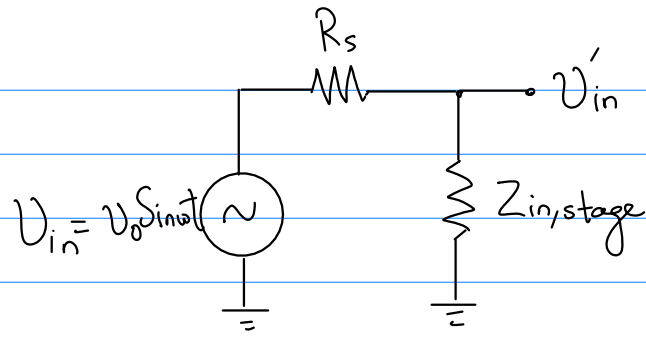
$\Rightarrow$  there is an enhancement (amplification) of 4-orders of magnitude.

Loading effect of Input ac-source :



if  $Z_{in-stage} \geq 100 R_s$  then the input ac-source is stiff.

But in case  $Z_{in-stage} \sim R_s$  or lower



If the stiff cond<sup>n</sup> is meeting then  $V'_{in} = V_{in} = V_0 \sin \omega t$

In case the stiff cond<sup>n</sup> is not meeting then,

$$V'_{in} = \left[ \frac{Z_{in,stage}}{Z_{in,stage} + R_s} \right] \cdot V_{in}$$