

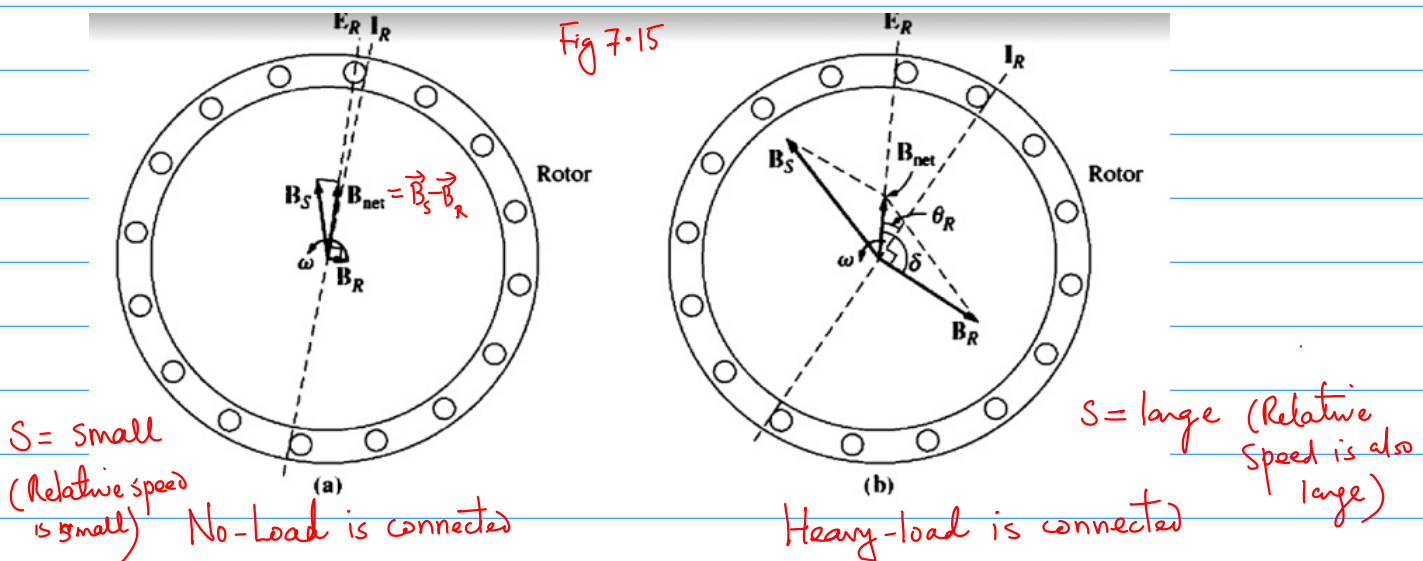
Torque-Speed Characteristics of the Induction Motor

(Reference : Section 7.5)

- Relationship among the torque ($T_{ind.}$); speed (n_m) and power.
- Primarily we would like to find the answers of the following questions :
 - ✓ (i) How does the induced torque depend on the variation in mechanical load?
 - (ii) What is the starting torque on the I.M.?
 - (iii) How the speed of I.M. drop as its shaft load increases?

Approach-I: We look at the Motor's Magnetic fields under the following conditions:

(i) No-load ; (ii) With-load .



We know that the magnitude of the induced torque in the IM is given as

$$\tau_{ind.} = k \cdot |\vec{B}_R| \cdot |\vec{B}_{net}| \cdot \sin \delta$$

Where, $\vec{B}_{net} = \vec{B}_s - \vec{B}_R$

k = machine constant

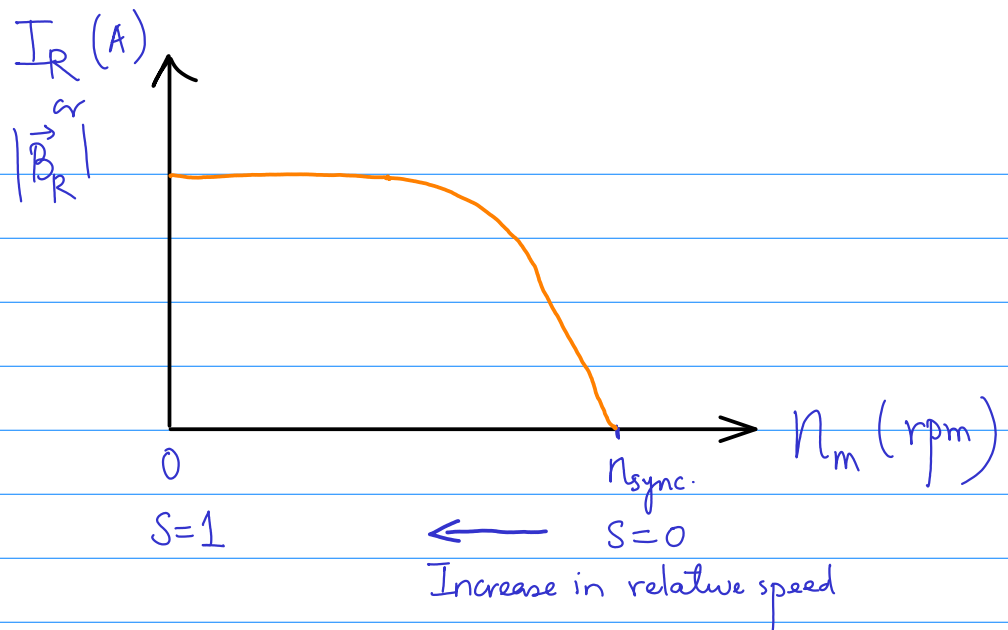
δ = torque angle (ie, angle b/w \vec{B}_R and \vec{B}_{net}).

Therefore, to develop τ -speed characteristics, we should have to develop dependency of \vec{B}_R , \vec{B}_{net} , δ to the speed.

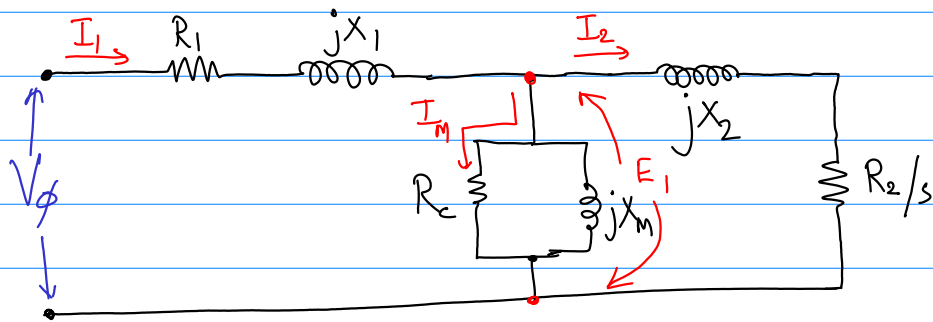
(i) Let look at the dependency of $|\vec{B}_R|$ on the slip (s)

- the magnitude of \vec{B}_R is directly dependent on the current I_R .
- Now, I_R increases with increasing slip (ie decreasing speed n_m)

$$I_R \uparrow = \frac{E_{R0}}{R_R/s + jX_{R0}}$$



- How $|\vec{B}_{net}|$ depends upon the speed?



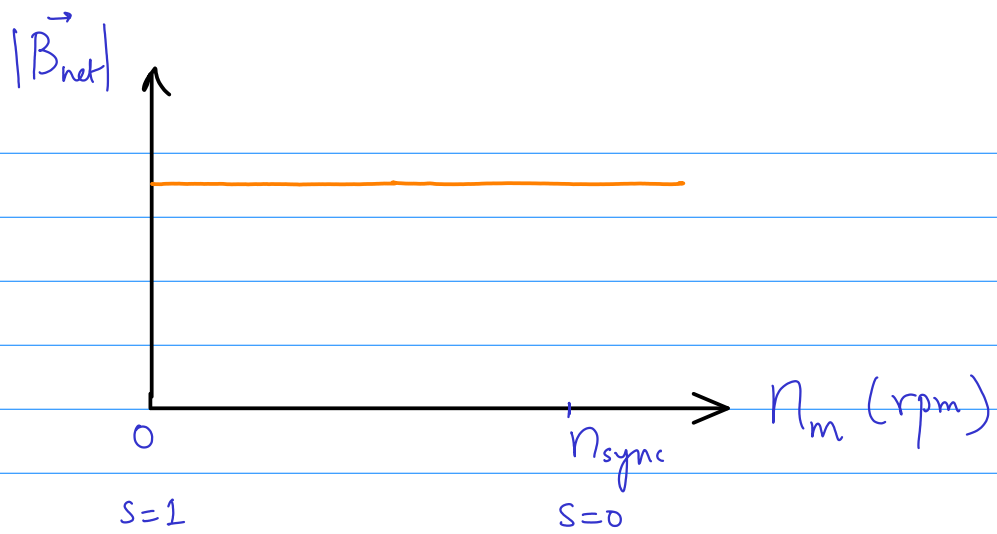
$$I_1 = \text{stator current} \longrightarrow \vec{B}_s$$

$$I_2 = \text{Rotor current} \longrightarrow \vec{B}_R$$

$$I_1 - I_2 = I_m \longrightarrow \vec{B}_{net} \quad (\vec{B}_s - \vec{B}_R)$$

here, the value of I_m depends upon E_1 ; however, the value of E_1 remains (approximately) the same at all the value of I_2

Therefore, I_m remains approx. constant, hence for practical purpose, \vec{B}_{net} remains constant with speed



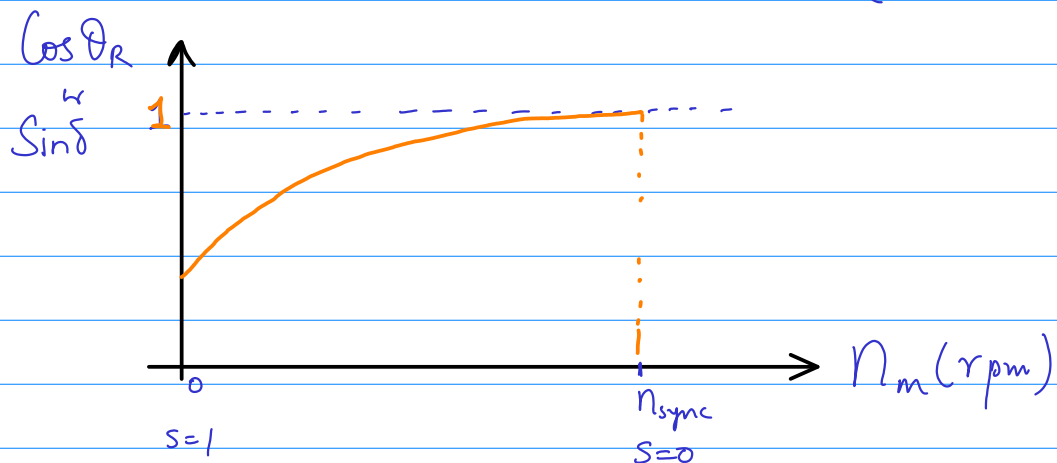
- How ' $\sin \delta$ ' varies with the speed?

From the fig 7.15, it is evident

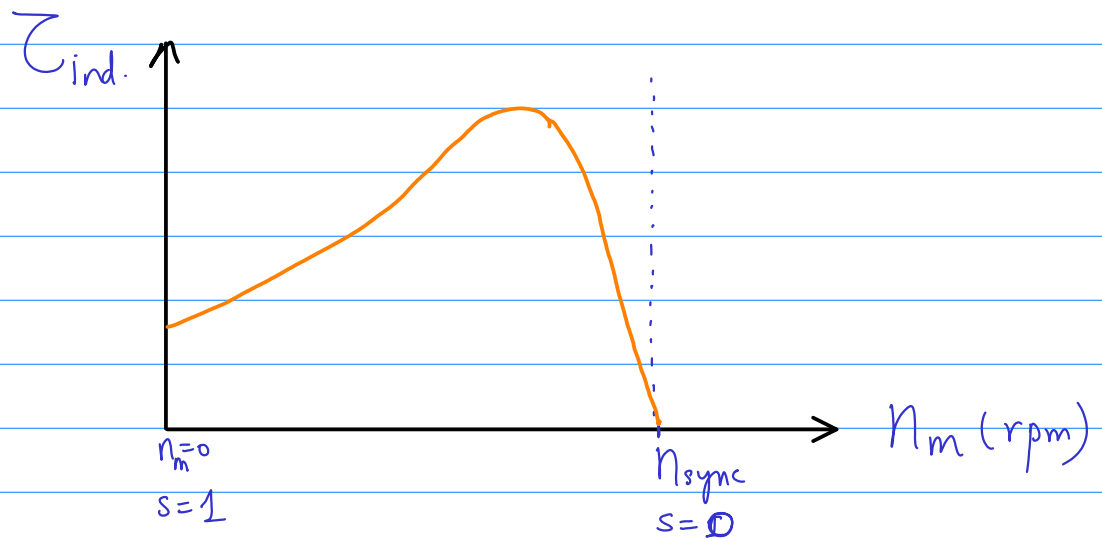
$$\delta = \theta_R + 90^\circ \quad \text{where } \theta_R \text{ is the angle b/w } E_R \text{ \& } I_R \text{ r,}$$

$$\sin \delta = \sin (\theta_R + 90^\circ) = \cos \theta_R$$

Also, $\theta_R = \tan^{-1} \left(\frac{X_R}{R_R} \right) = \tan^{-1} \left(\frac{s X_{R0}}{R_R} \right)$



$$\tau_{ind} = k \underbrace{|\vec{B}_R|} \underbrace{|\vec{B}_{net}|} \underbrace{\sin \delta}$$



Torque-Speed Characteristics of the I.M.

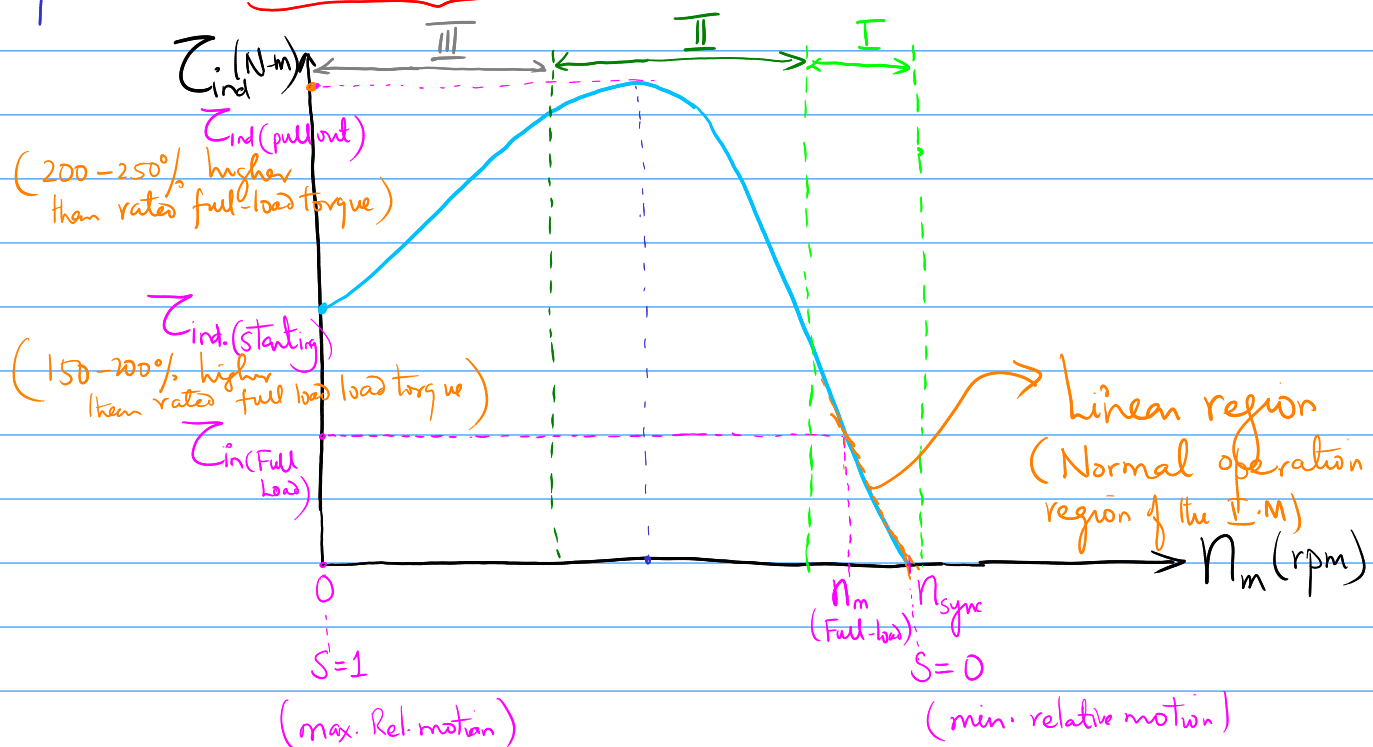
$$T_{ind} = k |\vec{B}_R| |\vec{B}_{net}| \cdot \sin \delta$$

$|\vec{B}_R|$ varies with the N_m —(i)

$|\vec{B}_{net}|$ varies with the N_m —(ii)

$\sin \delta$ or $\cos \theta_R$ varies with N_m —(iii)

Combining these variations w.r.t speed N_m , we plotted T_{ind} versus N_m



Region-I : Low-slip region (Low relative speed)

- Normal steady-state operating range of the I.M.
- Within this region, the value of slip (s) increases linearly (approximately) with increase in load.
- Since $n_m \downarrow = (1 - s \uparrow) n_{sync}$; therefore, n_m decrease linearly with increase in load.

Region-II : Moderate-slip (s) region.

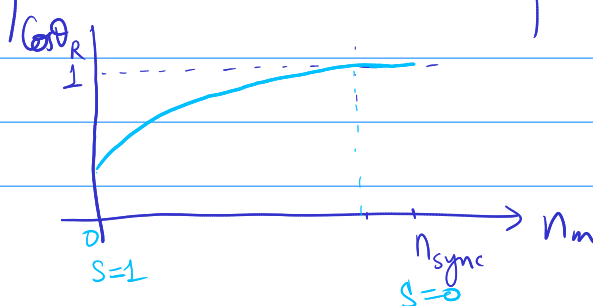
- Here, the rotor frequency (electrical) is higher.

$$\text{Since, } f_R = s f_e$$

- Since the frequency of the rotor current is having moderate value, therefore, within this region,

$$X_{\text{Rotor}} (= \omega_R L) \sim R_{\text{rotor}}$$

- The rotor current (I_R) is no longer increases as rapidly as in the linear region.
- Power factor starts to drop



- There is peak in the T_{ind} appearing called "Pullout Torque".

Region-III : High-slip(s) region

- Here, the $T_{ind} \downarrow$ with increase in load.
- Any increase in rotor current (ie, increase in $|\vec{B}_R|$) is completely overshadowed by the decrease in the rotor power factor (ie, $\cos \theta_R \sim \sin \delta$)

Important points :

(i) when $N_m = N_{sync}$; $T_{ind} = 0$

(ii) In normal operation of the I.M. (ie, operation b/w No-load to Full-load condition);

the T_{ind} vs N_m is nearly linear.

In this condⁿ; $R_R \gg X_R$ (since f_R is low)

So, I_R (or B_R or T_{ind}) increases linearly with 's'.

(iii) There is a maximum possible induced torque that cannot be exceeded.

"Pull-out torque" or "Breakdown torque"

(iv) The starting torque on the motor is higher than the $T_n(\text{Full-load})$.

So the motor will start carrying any load that it can supply at pull power.