

## 习 题 答 案

### 第二章

2.1 解：相量是正弦波（电压、电流或电磁波）从时域到复数域（或频域）数字变换的结果，它只保留了正弦波的幅度和初相角信息。

2.2      (1)  $A = 5\sqrt{3} = 5\sqrt{3}e^{j0^\circ}$

(2)  $A = -1 + 5\sqrt{2} - j5\sqrt{2} = 9.3e^{-j49.3^\circ}$

(3)  $A = \sqrt{2}e^{-j15^\circ}$

2.3      (1)  $A(t) = \operatorname{Re}[Ae^{j6t}] = 2\sqrt{5} \cos(6t + 3.43^\circ)$

(2)  $B(t) = \operatorname{Re}[Be^{j8t}] = 13.99 \cos(8t - 30.4^\circ)$

(3)  $C(t) = \operatorname{Re}[Ce^{j2t}] = 7.6 \cos(2t + 48.9^\circ)$

2.4      (1)  $40 \cos(100t)$

(2)  $-4000 \sin(100t)$

(3)  $\frac{1}{1000} \sin(100t)$

2.5 电路的稳态电压为：  $32 \cos(\omega t)$

2.6      (1)  $\sqrt{10}$

(2)  $10^{2.5}$

(3)  $10^5$

(4)  $10^{7.5}$

2.7      (1)  $10^{-0.7}$

(2)  $10^{-1}$

(3)  $10^{-0.3}$

2.8      (1)  $\sqrt{12}$

(2)  $\frac{\sqrt{26}}{2}$

$$(3) \sqrt{82-20\sqrt{2}}$$

2.9

2.10 在微波频段电阻、电感和电容这类集总元件不再表现为纯电阻、电感和电容，而是有额外的阻抗和电抗（寄生效应）。在微波频段，同一元件在不同的频率下可能会表现出不同的容性、感性或阻性。

### 第三章

$$3.1 \quad Z_0 = 33.3\Omega$$

3.2 证明

3.3 解： 1200 欧姆，300 欧姆

3.4 解：电压驻波最大点位置为

$$d_{\max} = \frac{\lambda}{4\pi} \phi_L + n \frac{\lambda}{2} = \frac{\lambda}{4\pi} \pi + n \frac{\lambda}{2} = \frac{\lambda}{4} + n \frac{\lambda}{2} \quad n = 0, 1, 2, \dots$$

电压驻波最小点位置为

$$d_{\min} = \frac{\lambda}{4\pi} \phi_L + (2n+1) \frac{\lambda}{4} = \frac{\lambda}{4} + n \frac{\lambda}{2} + \frac{\lambda}{4} = n \frac{\lambda}{2} + \frac{\lambda}{2} \quad n = 0, 1, 2, \dots$$

3.5 证明

3.6 (1)

$$\begin{aligned} Z(z) &= Z_0 \frac{1+\Gamma(z)}{1-\Gamma(z)} = 50 \times \frac{1-0.5e^{-j2\beta z}}{1+0.5e^{-j2\beta z}} = 50 \times \frac{1-0.5^2 + j2 \times 0.5 \sin(180^\circ - 2\beta z)}{1+0.5^2 - 2 \times 0.5 \cos(180^\circ - 2\beta z)} \\ &= 50 \times \frac{3+j4\sin(2\beta z)}{5+4\cos(2\beta z)} \end{aligned}$$

(2)  $50/3 \Omega$

(3)  $50/3 \Omega$

3.7  $250 \Omega$  ,  $0.2W$

$$3.8 \quad (1) \quad \Gamma(z) = |\Gamma_L| e^{j(\phi_L - 2\beta z)} = \frac{\sqrt{2}}{2} e^{j\left(\frac{2\pi}{3} - 2\beta z\right)}$$

(2)

$$Z(z_1) = Z_0 \frac{1+\Gamma(z_1)}{1-\Gamma(z_1)} = 50 \times \frac{1+\frac{\sqrt{2}}{2}}{1-\frac{\sqrt{2}}{2}} = 50(3+2\sqrt{2}) (\Omega)$$

$$\text{或 } Z(z_1) = Z_0 \rho = \frac{Z_0}{k} = \frac{50}{3-2\sqrt{2}} = 50(3+2\sqrt{2}) (\Omega)$$

$$3.10 \quad Z_L = 50 \frac{1-j1.336}{2-j0.668} = 39.57 e^{-j34.71^\circ}$$

3.11

$$Z_{in}(d) = Z_0 \frac{Z_L + jZ_0 \tan(\beta d)}{Z_0 + jZ_L \tan(\beta d)} = 38.24 + j3.14$$

3.12 (137.5-j237.5) 欧姆

$$3.13 \quad Z_{in} = 50\Omega$$

$$3.14 \quad |\Gamma_L| = 1, \rho = 0$$

3.15 证明

$$3.16 \quad \text{当有损时,} \quad Z_c = \sqrt{\frac{Z_0}{Y_0}} = \sqrt{\frac{5+100j}{0.01+0.15j}}$$

$$\gamma = \sqrt{Z_0 Y_0} = \sqrt{1.75j - 14.95}$$

$$\text{当无损时,} \quad Z_c = \sqrt{\frac{Z_0}{Y_0}} = \sqrt{\frac{100j}{0.15j}} = 25.82\Omega$$

$$\gamma = \sqrt{Z_0 Y_0} = \sqrt{-15} = 3.87j$$

$$3.17 \quad Z_0 = 66.7\Omega \quad \text{或} \quad Z_0 = 150\Omega$$

$$3.18 \quad (1) \quad V\left(\frac{\lambda}{8}\right)^- = V\left(\frac{\lambda}{8}\right)^+ \quad \Gamma_L = 5\sqrt{2}V$$

$$(2) \quad I(0) = \frac{3-j}{10} A \quad I\left(\frac{\lambda}{8}\right) = \frac{\sqrt{2}(2-j)}{10} A$$

$$(3) \quad P(0) = 2.5W \quad P\left(\frac{\lambda}{8}\right) = 2.5W$$

$$P(0) = P\left(\frac{\lambda}{8}\right)$$

$$(4) \quad Z_{in} = Z_0 \frac{Z_L + jZ_0 \tan 45^\circ}{Z_0 + jZ_L \tan 45^\circ} = (50-100j)\Omega$$

3.19

$$P^- = \frac{1}{2} \frac{|V_0^+|}{Z_0} \left| \frac{Z_{in} - Z_0}{Z_{in} + Z_0} \right|^2 = \frac{1}{5200} W$$

$$3.21 \quad (1) \quad Z_L = 116.7\Omega$$

$$(2) \quad \Gamma_{in} = \frac{Z_{in} - Z_0}{Z_{in} + Z_0} = \frac{20+21j}{29}$$

$$(3) \quad \rho = 1$$

$$3.22 \quad Z_0 = 100\Omega \quad \text{或} \quad Z_0 = 400\Omega$$

$$3.23 \quad |\Gamma_L| = 1 \quad \rho = \infty$$

## 第四章

4.1 (1)  $Z_{in} = 60 + j35$ ,  $Y_{in} = 0.0125 - j0.0075$

(2)  $Z_L = 30 - j18.5$

(3)  $\Gamma(0) = 0.27e^{-j26^\circ}$ ,  $\Gamma(0.35\lambda) = 0.27e^{j82^\circ}$ ,  $\rho = 1.9$

(4)  $l/\lambda = 0.454$

(5)  $l/\lambda = 0.12 + 0.5n, n = 1, 2, 3 \cdots b_{in} = 0.75$

(6)  $l/\lambda = 0.468$

4.2  $l_{\text{波节}} = 0.475\lambda$ ,  $l_{\text{波腹}} = 0.225\lambda$ ,  $\Gamma = 0.86e^{-j\beta l}$ ,  $\rho = 10$

4.3 (a)  $SWR = 1.6$

(b)  $|\Gamma| = 0.22$

(c)  $Y_L = 0.013 + j0.004$

(d)  $Z_{in} = 42.5 - j19$

(e)  $0.201\lambda$

(f)  $0.451\lambda$

4.4 如果  $Z_L = (20 - j100)\Omega$ , 重做习题 4.3。

略, 同 4.3

4.5 如果传输线长度为  $1.5\lambda$ , 重做习题 4.3

略, 同 4.3

### 4.6 短路线

(1)  $l = 0$

(2)  $l = \frac{\lambda}{4}$

(3)  $l = \frac{3\lambda}{8}$

(4)  $l = \frac{\lambda}{60}$

(5)  $l = \frac{3\lambda}{50}$

开路线

(1)  $l = \frac{\lambda}{4}$

(2)  $l = 0$

(3)  $l = \frac{\lambda}{8}$

$$(4) \quad l = \frac{4\lambda}{15}$$

$$(5) \quad l = \frac{31\lambda}{100}$$

$$4.7 \quad Z_L = (0.7 - j0.15) \times 75 = (52.5 - j11.25)\Omega$$

$$4.8 \quad \Gamma_{in} = \frac{z_{in} - 1}{z_{in} + 1} = \frac{11 - 9j}{16 - 9j}$$

$$(1) \quad \rho = r = 7.33$$

$$(2) \quad Z_{in} = (5.4 - j3.68) \times 100 = (540 - j368)\Omega$$

$$(3) \quad l = \frac{10}{360} \lambda = \frac{\lambda}{36}$$

$$4.9 \quad Z_L = (\Omega 252 - j105)$$

$$4.11 \quad (1) \quad \Gamma_L = 0.291e^{-j30^\circ}$$

$$(2) \quad \rho = 2.6$$

$$(3) \quad Z_{in} = 25 - j17.5$$

$$(4) \quad Y_l = 0.01 - j0.02$$

$$(5) \quad Y_{in} = 0.003 - j0.032$$

$$(6) \quad Z_l = 27.5 + j12$$

$$(7) \quad Z_l = 9.4 + j22.4$$

$$4.12 \quad d = 0.125\lambda \text{ 和 } l = 0.127\lambda$$

$$4.13 \quad \text{解 1: } d_1 = 0.456\lambda \text{ 和 } l_1 = 0.432\lambda$$

$$\text{解 2: } d_2 = 0.091\lambda \text{ 和 } l_2 = 0.067\lambda$$

$$4.14 \quad (1) \quad \text{解 1: } l_1 = 0.39\lambda \text{ 和 } l_2 = 0.33\lambda$$

$$\text{解 2: } l_1 = 0.44\lambda \text{ 和 } l_2 = 0.40\lambda$$

$$(2) \quad \text{解 1: } l_1 = 0.14\lambda \text{ 和 } l_2 = 0.07\lambda$$

解 2:  $l_1 = 0.25\lambda$  和  $l_2 = 0.43\lambda$

(3) 解 1:  $l_1 = 0.36\lambda$  和  $l_2 = 0.41\lambda$

解 2:  $l_1 = 0.14\lambda$  和  $l_2 = 0.33\lambda$

(4)  $l_1 = 0.22\lambda$  和  $l_2 = 0.09\lambda$

(5) 解 1:  $l_1 = 0.125\lambda$  和  $l_2 = 0.44\lambda$

解 2:  $l_1 = 0.07\lambda$  和  $l_2 = 0.04\lambda$

(6) 解 1:  $l_1 = 0.198\lambda$  和  $l_2 = 0.14\lambda$

解 2:  $l_1 = 0.125\lambda$  和  $l_2 = 0.36\lambda$

$$4.18 \quad |\Gamma(\theta)| = \frac{\pi^2}{2} \left| \ln \frac{Z_0}{Z_L} \right| \left| \frac{\cos \beta L}{\pi^2 - (2\beta L)^2} \right|$$

$$4.19 \quad (1) \quad L = \frac{11\lambda_0}{2\pi} = 1.75\lambda_0$$

$$(2) \quad N = 3$$

## 第五章

5.1 答: 将微波元件作为微波网络来研究, 能够避开微波元件内部不均匀性区域场分布的复杂计算, 使微波问题的处理大大简化, 因此微波网络方法在微波工程技术中得到了广泛的应用。微波网络方法的一个优点是, 微波网络的外特性参量可以通过网络参量转化得到, 而网络参量可以用实验的方法来测量或者通过捡的计算得到。

5.2 答: 传输线均匀。阻抗的不确定性会使得等效双线的模式电压和模式电流不能唯一确定, 为了消除阻抗的不确定性, 引入了归一化阻抗。

5.3 证明

5.4 分别计算题图 5.4 所示的二端口网络的阻抗矩阵及导纳矩阵。

解:

(a)

阻抗矩阵:

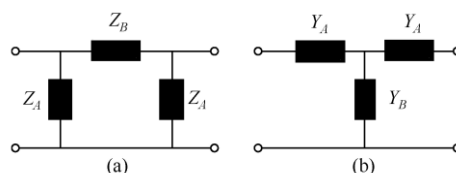


图 5.4

$$[Z] = \begin{bmatrix} \frac{Z_A(Z_B + Z_A)}{2Z_A + Z_B} & \frac{Z_A^2}{2Z_A + Z_B} \\ \frac{Z_A^2}{2Z_A + Z_B} & \frac{Z_A(Z_B + Z_A)}{2Z_A + Z_B} \end{bmatrix} = \frac{1}{2Z_A + Z_B} \begin{bmatrix} Z_A(Z_B + Z_A) & Z_A^2 \\ Z_A^2 & Z_A(Z_B + Z_A) \end{bmatrix}$$

导纳矩阵为阻抗矩阵的逆矩阵

(b)

导纳矩阵：

$$[Y] = \begin{bmatrix} \frac{Y_A(Y_A + Y_B)}{2Y_A + Y_B} & \frac{Y_A^2}{2Y_A + Y_B} \\ \frac{Y_A^2}{2Y_A + Y_B} & \frac{Y_A(Y_A + Y_B)}{2Y_A + Y_B} \end{bmatrix} = \frac{1}{2Y_A + Y_B} \begin{bmatrix} Y_A(Y_A + Y_B) & Y_A^2 \\ Y_A^2 & Y_A(Y_A + Y_B) \end{bmatrix}$$

5.5 (1) 证明。

(2)

$$[S] = \frac{1}{(1 + \frac{Z_{11}}{Z_0})(1 + \frac{Z_{22}}{Z_0}) - \frac{Z_{12}Z_{21}}{Z_0^2}} \begin{pmatrix} (1 + \frac{Z_{22}}{Z_0})(\frac{Z_{11}}{Z_0} - 1) - \frac{Z_{12}Z_{21}}{Z_0^2} & \frac{2Z_{12}}{Z_0} \\ \frac{2Z_{12}}{Z_0} & (1 + \frac{Z_{11}}{Z_0})(\frac{Z_{22}}{Z_0} - 1) - \frac{Z_{12}Z_{21}}{Z_0^2} \end{pmatrix}$$

将 (1) 式所得的阻抗矩阵  $Z$  导入即可。

(3)

$$[S] = \frac{1}{(1 + \frac{Z_{11}}{Z_0})(1 + \frac{Z_{22}}{Z_0}) - \frac{Z_{12}Z_{21}}{Z_0^2}} \begin{pmatrix} [(1 + \frac{Z_{22}}{Z_0})(\frac{Z_{11}}{Z_0} - 1) - \frac{Z_{12}Z_{21}}{Z_0^2}]e^{-j2\theta} & \frac{2Z_{12}}{Z_0}e^{-j2\theta} \\ \frac{2Z_{12}}{Z_0}e^{-j2\theta} & [(1 + \frac{Z_{11}}{Z_0})(\frac{Z_{22}}{Z_0} - 1) - \frac{Z_{12}Z_{21}}{Z_0^2}]e^{-j2\theta} \end{pmatrix}$$

$$5.6 (1) [Z] = \begin{bmatrix} Z_{11} & Z_{12} \\ Z_{21} & Z_{22} \end{bmatrix} = \begin{bmatrix} -50j & 0 \\ 0 & -50j \end{bmatrix}$$

$Z_{11}$  即为从 1 端口看进去的输入阻抗,  $Z_{22}$  即为从 2 端口看进去的输入阻抗。

$$(2) \begin{matrix} V_1^+ = 20(1-j) & V_2^+ = -4(1+j) \\ V_1^- = 20(1+j) & V_2^- = 4(1-j) \end{matrix}$$

5.7

(1)

$$\alpha = \begin{bmatrix} -1 & 0 \\ j & -1 \end{bmatrix} \begin{bmatrix} \cos \theta & j \sin \theta \\ j \sin \theta & \cos \theta \end{bmatrix} \begin{bmatrix} -1 & 0 \\ j & -1 \end{bmatrix} = \begin{bmatrix} \cos \theta + \sin \theta & j \sin \theta \\ -2j \cos \theta & \cos \theta + \sin \theta \end{bmatrix}$$

(2)

$$S_{11} = \frac{j(\sin \theta + 2 \cos \theta)}{2(\cos \theta + \sin \theta) + j(\sin \theta - 2 \cos \theta)}$$

$$S_{22} = \frac{j(\sin \theta + 2 \cos \theta)}{2(\cos \theta + \sin \theta) + j(\sin \theta - 2 \cos \theta)}$$

$$S_{12} = \frac{2}{2(\cos \theta + \sin \theta) + j(\sin \theta - 2 \cos \theta)}$$

$$S_{21} = \frac{2}{2(\cos \theta + \sin \theta) + j(\sin \theta - 2 \cos \theta)}$$

5.8

- (1) 显然，矩阵对称，为互易网络。  
而各矩阵元素并非为纯虚数，该网络非无耗。

$$RL = -20 \log(|S_{11}|) = -20 \log(0.1) = 20 \text{ dB}$$

$$IL = -20 \log(|S_{42}|) = -20 \log(0.2) = 14 \text{ dB}$$

相位延迟为 45 度。

(2)

$$\Gamma_{in} = \frac{b_1}{a_1} S_{11} + \frac{S_{31} S_{13} \Gamma_{L3}}{1 - S_{33} \Gamma_{L3}} = 0.1j + \left(0.3e^{j-45^\circ}\right)^2 (-1) = 0.19j$$

5.9 插入损耗  $IL = -20 \log\left(\frac{56}{121}\right) = 6.7 \text{ dB}$

相位延迟为  $\frac{7}{12} \pi$

5.10

$$S_{21} = \frac{V_2^- / \sqrt{Z_{02}}}{V_1^+ / \sqrt{Z_{01}}} \bigg|_{V_2^+ = 0} = \sqrt{\frac{Z_{01}}{Z_{02}}} \frac{V_2}{V_1 / (1 + S_{11})} = \sqrt{\frac{Z_{01}}{Z_{02}}} (1 + S_{11})$$

$$\Rightarrow S_{21} = \sqrt{\frac{Z_{01}}{Z_{02}}} \left(1 + \frac{Z_{02} - Z_{01}}{Z_{02} + Z_{01}}\right) = \frac{2\sqrt{Z_{01}Z_{02}}}{Z_{02} + Z_{01}}$$

$$S_{12} = S_{21} = \frac{2\sqrt{Z_{01}Z_{02}}}{Z_{02} + Z_{01}}, \quad S_{22} = \frac{Z_{01} - Z_{02}}{Z_{02} + Z_{01}}$$

5.11 某二端口网络的散射参量为  $S_{11} = 0.4 + j0.6$ ,  $S_{12} = S_{21} = j0.8$ ,  $S_{22} = 0.5 - j0.9$ , 计算该网络的

等效阻抗矩阵（端口连接传输线特征阻抗为  $50\Omega$ ）。

解：



$$Z_{11}=Z_0 \frac{(1+S_{11})(1-S_{22})+S_{12}S_{21}}{(1-S_{11})(1-S_{22})-S_{12}S_{21}} = -7.4733 + j53.9146$$

$$Z_{22}=Z_0 \frac{(1-S_{11})(1+S_{22})+S_{12}S_{21}}{(1-S_{11})(1-S_{22})-S_{12}S_{21}} = -16.9039 - j45.9075$$

$$Z_{12}=Z_{21}=Z_0 \frac{2S_{21}}{(1-S_{11})(1-S_{22})-S_{12}S_{21}} = 8.5409 + j52.6690$$

5.12 某二端口网络的散射参量对端口传输线的特征阻抗  $Z_0$  归一化后为  $S_{ij}$ 。当端口 1 和端口 2 的特征阻抗分别变为  $Z_{01}$  和  $Z_{02}$  时，求其广义散射参量  $S'_{ij}$ 。

解：

$$S_{11} = \frac{Z_{02} - Z_{01}}{Z_{02} + Z_{01}}, \quad S_{12} = S_{21} = \frac{2\sqrt{Z_{01}Z_{02}}}{Z_{02} + Z_{01}}, \quad S_{22} = \frac{Z_{01} - Z_{02}}{Z_{02} + Z_{01}}$$

$$5.13 \quad Z_{11} = Z_{in}(l) = Z_0 \frac{Z_L + jZ_0 \tan(\beta l)}{Z_0 + jZ_L \tan(\beta l)} = \frac{Z_0}{j \tan(\beta l)}, \quad Z_{22} = Z_{11}$$

$$Z_{21} = \frac{V_2}{I_1} = \frac{V_1}{I_1} \frac{V_2}{V_1} = \frac{Z_0}{j \tan(\beta l)} \frac{V_2^+ + V_2^+ \Gamma}{V_2^+ (e^{j\beta l} + \Gamma e^{-j\beta l})} = \frac{Z_0}{j \tan(\beta l)} \frac{2}{e^{j\beta l} + e^{-j\beta l}} = \frac{Z_0}{j \sin(\beta l)}$$

由于对称性，有  $Z_{22} = Z_{11}, Z_{12} = Z_{21}$

$$5.14 \quad V_L = -j$$

$$5.15 \quad Y = Y_1 + Y_2 = \begin{bmatrix} \frac{Z_1 + Z_2}{Z_1^2 + 2Z_1Z_2} + \frac{1}{Z_3} & \frac{-Z_1}{Z_1^2 + 2Z_1Z_2} - \frac{1}{Z_3} \\ \frac{-Z_1}{Z_1^2 + 2Z_1Z_2} - \frac{1}{Z_3} & \frac{Z_1 + Z_2}{Z_1^2 + 2Z_1Z_2} + \frac{1}{Z_3} \end{bmatrix}$$

5.16 证明。

5.17

$$(1) \quad \text{证明 } \Gamma_1 = S_{11} + \frac{S_{12}^2 \Gamma_L}{1 - S_{22} \Gamma_L}。$$

$$(2) \quad S_{11} = \Gamma_{1C}, \quad S_{22} = \frac{\Gamma_{10} + \Gamma_{1S} - 2\Gamma_{1C}}{\Gamma_{10} - \Gamma_{1S}}, \quad S_{12} = \frac{2(\Gamma_{1C} - \Gamma_{1S})(\Gamma_{10} - \Gamma_{1C})}{\Gamma_{10} - \Gamma_{1S}}$$