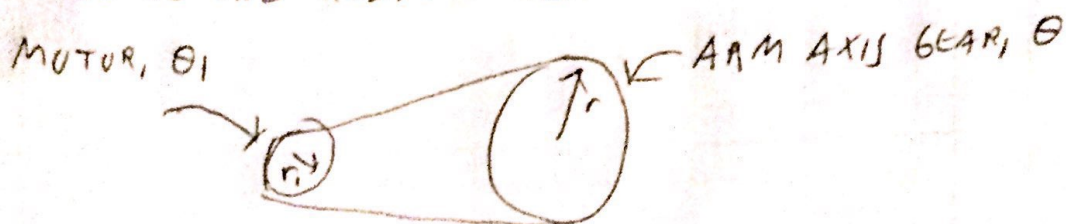


- 1.) OUR PEN PLOTTER MAKES USE OF POLAR COORDINATES. HOWEVER, THE POLAR COORDINATES ARE CONTROLLED BY THE ROTATION OF TWO MOTORS, EACH CONTROLLING A DEGREE OF FREEDOM. THUS, WE NEED TO CONVERT OUR POLAR COORDINATES INTO MOTOR ANGLES.

$\theta \rightarrow$ MOTOR 1 ANGLE:

SINCE WE HAVE A GEAR REDUCTION BETWEEN THE MOTOR AND ARM AXIS, $\theta \neq \theta_1$. WE DERIVE THE RELATION BELOW:



SINCE ALL PARTS OF THE PULLEY HAVE THE SAME VELOCITY, $v_1 = v$

$$r_1 \dot{\theta}_1 = r \dot{\theta}$$

$$\dot{\theta}_1 = (r/r_1) \dot{\theta} \quad (\text{INTEGRATE})$$

$$\theta_1 = (r/r_1) \theta$$

$$\underline{\theta_1 = g \theta} \quad (\text{OR } \theta = \frac{1}{g} \theta_1)$$

WHERE g IS THE GEAR RATIO

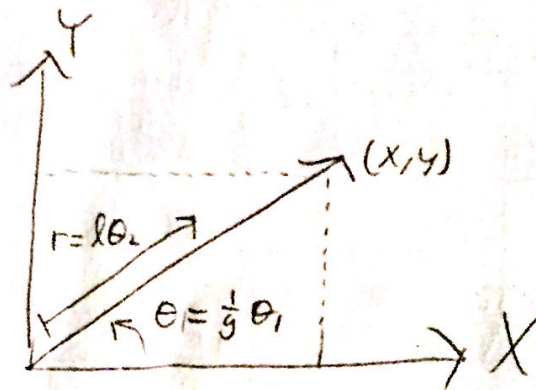
$r \rightarrow$ MOTOR 2 ANGLE:

A LEADSCREW IS ATTACHED TO MOTOR 2 SUCH THAT ROTATING THE SCREW ADVANCES THE PEN. ONE FULL ROTATION OF THE MOTOR ADVANCES THE PEN BY THE SCREW'S PITCH IN THE r DIRECTION. THUS,

$$\underline{r = l \theta_2}$$

WHERE l IS THE PITCH OF THE SCREW IN UNITS OF mm/rad.

A DIAGRAM OF THE SYSTEM IS SHOWN BELOW:



2. TO DEFINE THE FORWARD KINEMATICS, WE CAN WRITE

$$\underline{x} = \underline{f}(\underline{\theta})$$

$$\begin{bmatrix} x \\ y \end{bmatrix} = \begin{bmatrix} r \cos \theta \\ r \sin \theta \end{bmatrix}$$

$$\boxed{\begin{bmatrix} x \\ y \end{bmatrix} = \begin{bmatrix} l_1 \cos(\frac{1}{3} \theta_1) \\ l_1 \sin(\frac{1}{3} \theta_1) \end{bmatrix}}$$

3. TO PREPARE FOR INVERSE KINEMATICS, WE COMPUTE THE JACOBIAN.

$$\frac{\partial \underline{f}}{\partial \underline{\theta}} = \begin{bmatrix} \frac{\partial f_1}{\partial \theta_1} & \frac{\partial f_1}{\partial \theta_2} \\ \frac{\partial f_2}{\partial \theta_1} & \frac{\partial f_2}{\partial \theta_2} \end{bmatrix}$$

$$\boxed{\frac{\partial \underline{f}}{\partial \underline{\theta}} = \begin{bmatrix} -\frac{l_1}{3} \theta_2 \sin(\frac{1}{3} \theta_1) & l_1 \cos(\frac{1}{3} \theta_1) \\ \frac{l_1}{3} \theta_2 \cos(\frac{1}{3} \theta_1) & l_1 \sin(\frac{1}{3} \theta_1) \end{bmatrix}}$$

4. WE NOW WANT THE VELOCITY OF THE END-EFFECTOR.

$$\dot{\underline{x}} = \frac{d}{dt} \underline{f}(\underline{\theta})$$

$$\dot{\underline{x}} = \frac{\partial \underline{f}}{\partial \underline{\theta}} \dot{\underline{\theta}}$$

$$\dot{\underline{x}} = \begin{bmatrix} -\frac{l_1}{3} \theta_2 \sin(\frac{1}{3} \theta_1) & l_1 \cos(\frac{1}{3} \theta_1) \\ \frac{l_1}{3} \theta_2 \cos(\frac{1}{3} \theta_1) & l_1 \sin(\frac{1}{3} \theta_1) \end{bmatrix} \begin{bmatrix} \dot{\theta}_1 \\ \dot{\theta}_2 \end{bmatrix}$$

$$\boxed{\dot{\underline{x}} = \begin{bmatrix} -\frac{l_1}{3} \dot{\theta}_1 \theta_2 \sin(\frac{1}{3} \theta_1) + l_1 \dot{\theta}_2 \cos(\frac{1}{3} \theta_1) \\ \frac{l_1}{3} \dot{\theta}_1 \theta_2 \cos(\frac{1}{3} \theta_1) + l_1 \dot{\theta}_2 \sin(\frac{1}{3} \theta_1) \end{bmatrix}}$$

5. WE NOW WRITE THE MATRIX EQUATION RESPONSIBLE FOR CARRYING OUT THE NEWTON-RAPHSON ALGORITHM.

FIRST, DEFINE

$$g(\theta) = X - f(\theta)$$

$$g(\theta) = \begin{bmatrix} x - l\theta_2 \cos(\frac{1}{3}\theta_1) \\ y - l\theta_2 \sin(\frac{1}{3}\theta_1) \end{bmatrix}$$

WE WILL ALSO WANT $dg/d\theta$. SINCE THE POINT OF THE ALGORITHM IS TO FIND THE θ_1 & θ_2 THAT GIVE X , THEN X MUST BE CONSTANT FOR A RUN OF THE ALGORITHM. THUS,

$$\frac{dg}{d\theta} = -\frac{df}{d\theta}$$

$$\frac{dg}{d\theta} = \begin{bmatrix} -\frac{1}{3}l\theta_2 \sin(\frac{1}{3}\theta_1) & -l\cos(\frac{1}{3}\theta_1) \\ \frac{1}{3}l\theta_2 \cos(\frac{1}{3}\theta_1) & -l\sin(\frac{1}{3}\theta_1) \end{bmatrix}$$

THE ALGORITHM WORKS AS FOLLOWS:

$$\theta_{n+1} = \theta_n - \left(\frac{dg(\theta_n)}{d\theta} \right)^{-1} g(\theta_n)$$

$$\begin{bmatrix} \theta_{1,n+1} \\ \theta_{2,n+1} \end{bmatrix} = \begin{bmatrix} \theta_{1,n} \\ \theta_{2,n} \end{bmatrix} - \left(\frac{dg(\theta_n)}{d\theta} \right)^{-1} \begin{bmatrix} x - l\theta_{2,n} \cos(\frac{1}{3}\theta_{1,n}) \\ y - l\theta_{2,n} \sin(\frac{1}{3}\theta_{1,n}) \end{bmatrix}$$