



# BME 790

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Spring 2017  
Weekly Summary

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Week: 01/30/17-02/05/17

Relevant Topics: Articulated Systems, Holonomic Constraints, Fixed Base Systems, Intro to Mobile Systems

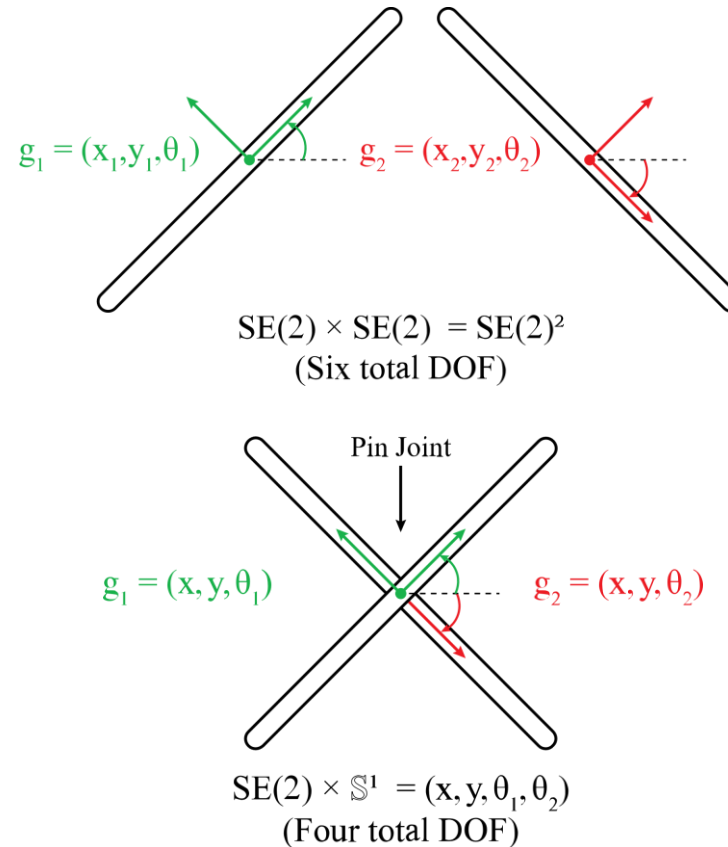
# Articulated Systems and Holonomic Constraints



The **full configuration space** of a set of  $n$  **planar** rigid bodies is the **direct product** of their **individual configuration spaces**.

**Holonomic constraints** – like pin joints – are (possibly time-varying) constraint functions,  $f$ , on the configuration space that **reduces the dimension of the system by 1** for each constraint applied.

The **zero set** forms the **accessible manifold** (i.e., the set of all configurations that satisfy these constraints).



$$\text{Zero Set} = \{ q \in Q \mid f(q, t) = 0 \}$$

**Multiple constraints act in concert**, with the overall accessible manifold being the intersection of individual accessible manifolds.

Although these constraints reduce the dimensionality of the system, they **do not remove the dependence** of the **system dynamics** on the actual **physical positions** of the rigid bodies – inertial and collision effects cannot be ignored!

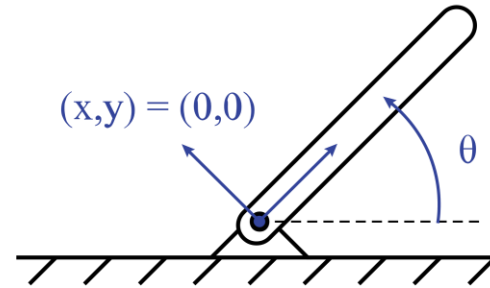
It is therefore important to map between these configuration space positions and the ambient forces that are acting on the rigid bodies.

# Fixed Base Systems

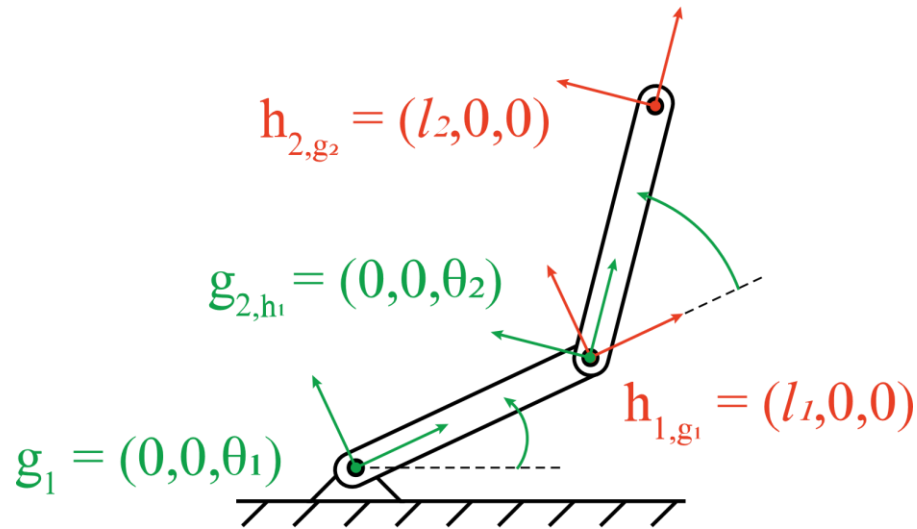


Note on Notation:  $g_{1,h}$  is the first frame of  $g$  defined with respect to base frame  $h$

The fixed frame provides holonomic constraints on the system, forcing both  $x$  and  $y$  to zero. Therefore the accessible manifold subset of  $SE(2)$  will be isomorphic to  $\theta \in \mathbb{S}^1$ .



$$g = \begin{matrix} SE(2) & & SO(2) & & \mathbb{S}^1 \\ \downarrow & & \downarrow & & \downarrow \\ \begin{bmatrix} \cos\theta & -\sin\theta & 0 \\ \sin\theta & \cos\theta & 0 \\ 0 & 0 & 1 \end{bmatrix} & = & \begin{bmatrix} \cos\theta & -\sin\theta \\ \sin\theta & \cos\theta \end{bmatrix} & = & \theta \end{matrix}$$



Adding additional links provides additional constraints.

- The distal and proximal ends of any link will share orientation.
- The joint constrains the position at the joint for the proximal end of one segment and the distal end of the previous segment.

Note that each frame is defined with respect to the previous frame. In terms of left/right actions, this notation reveals:

$$g_{1,h} = h^{-1} \circ g_1$$

# Fixed Base Systems (Cont.)

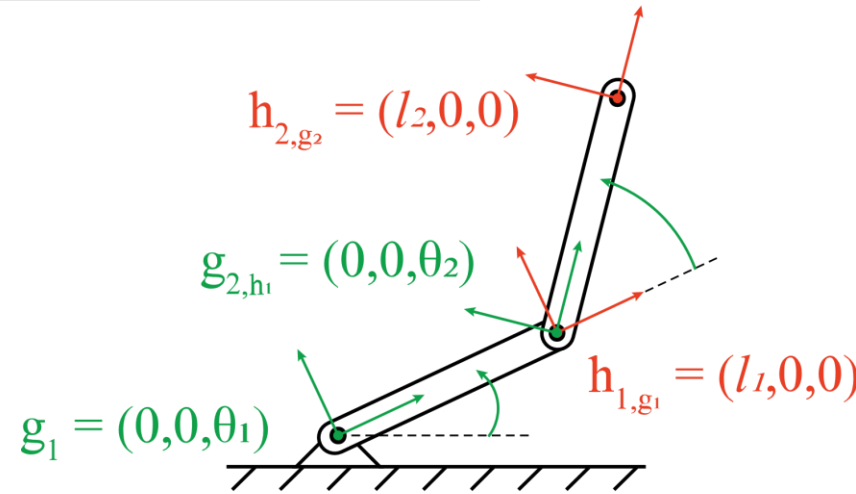


As a result of this notation, it can be seen that:

$$gh_g = g(g^{-1}h) = (gg^{-1})h = h.$$

- As a **left action**, this implies that the frame  $h$  (defined with respect to base frame  $g$ ) will be moved by  $g$ .
- As a **right action**, this implies that  $h_g$  is being placed into  $g$  (i.e., frames  $g$  and  $h$  are held by the relationship  $h_g$ ).

This will become particularly useful when discussing **mobile articulating systems** as this **right action** interpretation aids in determining the velocity kinematics of a system.



## Position of the Endpoint $h_2$

$$h_2 = g_2 h_{2,g_2} = (g_1 h_{1,g_1}) g_{2,h_1} h_{2,g_2}$$

$$h_2 = \begin{pmatrix} l_1 \cos \theta_1 + l_2 \cos(\theta_1 + \theta_2) \\ l_1 \sin \theta_1 + l_2 \sin(\theta_1 + \theta_2) \\ \theta_1 + \theta_2 \end{pmatrix}$$

$$h_1 = g_1 h_{1,g_1} = \begin{bmatrix} \cos \theta_1 & -\sin \theta_1 & 0 \\ \sin \theta_1 & \cos \theta_1 & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 & l_1 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

$$= \begin{bmatrix} \cos \theta_1 & -\sin \theta_1 & l_1 \cos \theta_1 \\ \sin \theta_1 & \cos \theta_1 & l_1 \sin \theta_1 \\ 0 & 0 & 1 \end{bmatrix}$$

$$g_2 = h_1 g_{2,h_1} = \begin{bmatrix} \cos \theta_1 & -\sin \theta_1 & l_1 \cos \theta_1 \\ \sin \theta_1 & \cos \theta_1 & l_1 \sin \theta_1 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} \cos \theta_2 & -\sin \theta_2 & 0 \\ \sin \theta_2 & \cos \theta_2 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

$$= \begin{bmatrix} \cos(\theta_1 + \theta_2) & -\sin(\theta_1 + \theta_2) & l_1 \cos \theta_1 \\ \sin(\theta_1 + \theta_2) & \cos(\theta_1 + \theta_2) & l_1 \sin \theta_1 \\ 0 & 0 & 1 \end{bmatrix}$$

$$h_2 = g_2 h_{2,g_2}$$

$$= \begin{bmatrix} \cos(\theta_1 + \theta_2) & -\sin(\theta_1 + \theta_2) & l_1 \cos \theta_1 \\ \sin(\theta_1 + \theta_2) & \cos(\theta_1 + \theta_2) & l_1 \sin \theta_1 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 & l_2 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

$$= \begin{bmatrix} \cos(\theta_1 + \theta_2) & -\sin(\theta_1 + \theta_2) & l_1 \cos \theta_1 + l_2 \cos(\theta_1 + \theta_2) \\ \sin(\theta_1 + \theta_2) & \cos(\theta_1 + \theta_2) & l_1 \sin \theta_1 + l_2 \sin(\theta_1 + \theta_2) \\ 0 & 0 & 1 \end{bmatrix}$$

# Conclusions/Impressions

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**Forward kinematics** provides a way to understand the interaction between configuration spaces that produce endpoint configurations in articulated systems – with **group actions being not only useful for these transformations in position space, but also in velocity space** (to be discussed in Section 2.5 next week).

**Holonomic constraints** allow for a **reduction in the dimensionality** of the configuration space, BUT **do not remove the considerations** that must be made with respect to the physical world (**inertial and/or collision interactions**).

**Matrix multiplication operators** on the frames (and their positions/orientations) allows for a useful way to **determine the position and relationship between rigidly attached frames** – which will become more useful when these frames are in motion.