

A multiport MR-compatible neuroendoscope: spanning the gap between rigid and flexible scopes

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OBJECTIVE Rigid endoscopes enable minimally invasive access to the ventricular system; however, the operative field is limited to the instrument tip, necessitating rotation of the entire instrument and causing consequent tissue compression while reaching around corners. Although flexible endoscopes offer tip steerability to address this limitation, they are more difficult to control and provide fewer and smaller working channels. A middle ground between these instruments—a rigid endoscope that possesses multiple instrument ports (for example, one at the tip and one on the side)—is proposed in this article, and a prototype device is evaluated in the context of a third ventricular colloid cyst resection combined with septostomy.

METHODS A prototype neuroendoscope was designed and fabricated to include 2 optical ports, one located at the instrument tip and one located laterally. Each optical port includes its own complementary metal-oxide semiconductor (CMOS) chip camera, light-emitting diode (LED) illumination, and working channels. The tip port incorporates a clear silicone optical window that provides 2 additional features. First, for enhanced safety during tool insertion, instruments can be initially seen inside the window before they extend from the scope tip. Second, the compliant tip can be pressed against tissue to enable visualization even in a blood-filled field. These capabilities were tested in fresh porcine brains. The image quality of the multiport endoscope was evaluated using test targets positioned at clinically relevant distances from each imaging port, comparing it with those of clinical rigid and flexible neuroendoscopes. Human cadaver testing was used to demonstrate third ventricular colloid cyst phantom resection through the tip port and a septostomy performed through the lateral port. To extend its utility in the treatment of periventricular tumors using MR-guided laser therapy, the device was designed to be MR compatible. Its functionality and compatibility inside a 3-T clinical scanner were also tested in a brain from a freshly euthanized female pig.

RESULTS Testing in porcine brains confirmed the multiport endoscope's ability to visualize tissue in a blood-filled field and to operate inside a 3-T MRI scanner. Cadaver testing confirmed the device's utility in operating through both of its ports and performing combined third ventricular colloid cyst resection and septostomy with an endoscope rotation of less than 5°.

CONCLUSIONS The proposed design provides freedom in selecting both the number and orientation of imaging and instrument ports, which can be customized for each ventricular pathological entity. The lightweight, easily manipulated device can provide added steerability while reducing the potential for the serious brain distortion that happens with rigid endoscope navigation. This capability would be particularly valuable in treating hydrocephalus, both primary and secondary (due to tumors, cysts, and so forth). Magnetic resonance compatibility can aid in endoscope-assisted ventricular aqueductal plasty and stenting, the management of multiloculated complex hydrocephalus, and postinflammatory hydrocephalus in which scarring obscures the ventricular anatomy.

<http://thejns.org/doi/abs/10.3171/2016.7.FOCUS16181>

KEY WORDS neuroendoscopy; optical window; silicone cap; chip-on-the-tip camera; side-firing camera; MR-compatible endoscope

ABBREVIATIONS CCD = charge-coupled device; CMOS = complementary metal-oxide semiconductor; CSF = cerebrospinal fluid; ETV = endoscopic third ventriculostomy; LED = light-emitting diode.

SUBMITTED May 2, 2016. **ACCEPTED** July 1, 2016.

INCLUDE WHEN CITING DOI: 10.3171/2016.7.FOCUS16181.

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THE primary clinical use for endoscopes in neurosurgery is the treatment of hydrocephalus, either primary or secondary.^{18,23} Secondary hydrocephalus can occur from tumors or cysts located within the ventricular system, rendering them suitable for endoscopic resection or fenestration to treat both the lesion and the resultant hydrocephalus.^{39,61,95} Rigid endoscopes are commonly used to perform endoscopic third ventriculostomy (ETV) in treating hydrocephalus, obviating the need for ventriculoperitoneal shunt placement, especially in obstructive hydrocephalus. In complex loculated hydrocephalus, ETV is also combined with septostomy. In lesions such as colloid cysts or in scarring of the unilateral foramen of Monro causing asymmetrical hydrocephalus, a septostomy forms the mainstay of endoscopic management. Sometimes loculated or encysted hydrocephalus is treated with extensive endoscopic adhesiolysis or wide fenestrations, followed by ventriculoperitoneal shunt placement if deemed necessary.^{1,76} The use of flexible neuroendoscopes is best illustrated by the combined procedure of ETV with choroid plexus coagulation.^{13,44,82} This steerable technique is also applicable in multiloculated hydrocephalus associated with ex vacuo atrophy or encystment of the periventricular brain parenchyma. To achieve optimum results, the use of a steerable endoscope is highly advisable to reach around corners during ETV combined with posterior third ventricular–pineal region tumor biopsy.^{6,14} Endoscopic intraventricular biopsy of a tumor in obstructive hydrocephalus helps to obtain a histological diagnosis along with emergency cerebrospinal fluid (CSF) diversion, contrary to a risky stereotactic transcranial biopsy in the setting of persistent intracranial tension. Intuitively, direct vision during a biopsy can reduce the chance of procedural hemorrhages and allows one to instantly and safely address them as and when they occur.¹⁶

Straight endoscopes provide imaging and working channels only at the instrument tip, leading to several limitations in their use. First, it is not possible to image or operate tools at an angle with respect to the endoscope axis, which makes it impossible to work around corners. Second, reorientation of the endoscope axis requires rotation of the entire instrument about a pivot point located at the bur hole. This motion can cause the instrument shaft to press against adjacent brain tissue, leading to potential deformational injury to vital periventricular brain structures such as the fornices.^{2,5} Flexible scopes address the orientation limitation of straight endoscopes by providing a steerable tip mounted on a compliant shaft; however, they typically have fewer and smaller instrument channels than the straight endoscopes. Furthermore, since the proximal length is passive, care must be taken to avoid brain tissue damage from pressure or abrasion caused by the shaft. These instruments are used by fewer surgeons and involve additional skills training to hold the tip position; to maneuver thinner, flexible instruments; and, above all, to avoid disorientation during zoomed-in views.^{14,58,98}

One method of gaining some of the benefits of steerable endoscopes while maintaining the operational simplicity of a straight endoscope is through the use of multiple imaging and/or tool ports within a single endoscope shaft offering an internal radius of curvature. With such a device,

imaging ports could be positioned at the instrument tip, as well as anywhere and at any angle along the endoscope body. If imaging and illumination are accomplished using chip cameras and light-emitting diodes (LEDs), many imaging ports can be supported in a given-diameter instrument because of the small wiring size, while also producing an instrument that is much lighter and easier to manipulate than a standard rigid endoscope. Although the endoscope cross-section does limit the total number and size of the independent tool channels, these channels can be distributed or shared between imaging ports based on procedural requirements.

For example, the novel multiport neuroendoscope in Fig. 1 was designed for performing a colloid cyst resection combined with septostomy.^{17,45} The tip port combines irrigation and aspiration channels with 1 tool channel for colloid cyst dissection. A second port located on the side of the endoscope includes a single tool channel. This port can be used to perform a septostomy with minimal pivoting of the instrument shaft about the center of the bur hole. This endoscope design could also be used in lieu of a steerable endoscope for treating multiloculated hydrocephalus. The lateral port would enable extensive multiplanar fenestration of the fibrous septae, which could not be easily accessed by the tip port. Many design variations are possible. Figure 2A illustrates how several cameras can be positioned in the same port to provide multiple viewing angles simultaneously. Figure 2B shows how instrument ports can be angled to achieve tool triangulation. Figure 2C illustrates a laterally oriented tip port with multiple tool channels. This multiport design could be safely employed in the tailored resection of posterior third ventricle tumors with minimal neurological morbidities.

While most neuroendoscopes are not MR compatible (see Gütterl et al.³¹ for an exception), some procedures could benefit from combined endoscopic and MRI guidance.^{48,86} In the treatment of multiloculated hydrocephalus, for example, MRI can reveal the extent and direction of intraventricular septations and periventricular cavitations with respect to the nearest cisterns to enable fenestration of these optically occluded tissues, resulting in a functioning cystoventriculocisternostomy.⁸⁸ Another potential application leveraging multiple endoscopic ports and MR compatibility is transventricular biopsy, resection, or laser ablation of periventricular lesions. This transventricular approach could be particularly beneficial in treating these multiple lesions since standardized ventricular access is faster and relatively safe, compared with more time-consuming preoperative planning necessary for transparentchymal access. In addition, endoscopic imaging could enhance effectiveness by providing optical imaging of tumor margins and improve safety by enabling real-time visualization of intraprocedural hemorrhage and tool-based hemostasis.

Another feature of the novel neuroendoscope proposed here is the soft, distal, silicone optical window used to encase our imaging ports (Fig. 1B). When a surgeon inserts a tool through a standard neuroendoscope, it becomes visible only after it exits the endoscope, creating a risk of iatrogenic injury if the tool inadvertently contacts eloquent brain tissue as it moves into view. The optically clear sili-

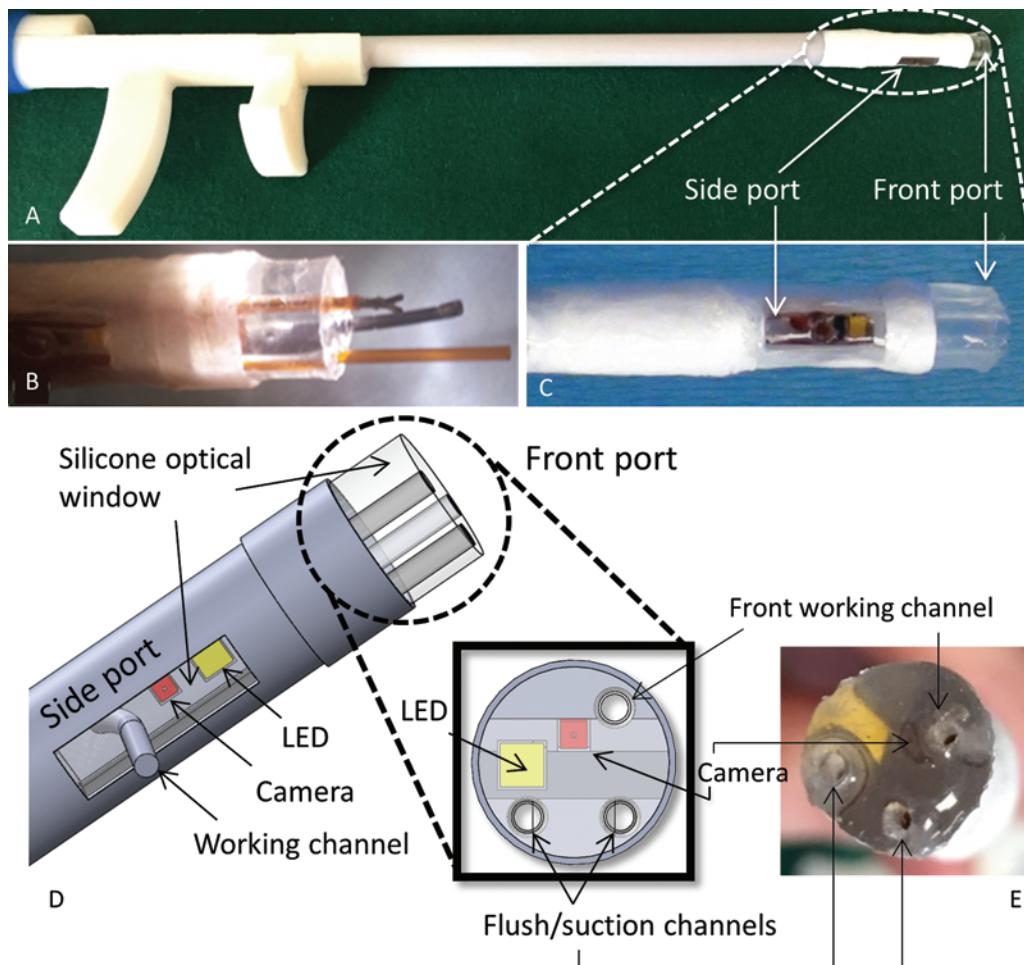


FIG. 1. Prototype of MR-compatible multiport neuroendoscope (A) with tip (B and E) and side (C) ports. A computer-aided design (CAD) drawing (D) of the device showing the ports.

cone window enables initial tool visualization while the tool is passing through the window (Fig. 3A) and before it can make contact with tissue (Fig. 3B). With the clinical endoscopes currently in use, you can only see the tool when it has already extended out of the working channel (Fig. 3C). The soft clear window also makes it possible to safely visualize tissue in a blood-filled field. When the window is pressed lightly against tissue, the blood between the window and tissue is displaced to provide a clear view of the contacted tissue. This technique has been successfully shown to provide endoscopic guidance inside the blood-filled beating heart.^{4,30,90} In neuroendoscopy, this technique might be used to locate a hemorrhaging vessel.

In this study we present the design and evaluation of the 2-port MR-compatible neuroendoscope shown in Fig. 1. After designing and fabricating the device, we first examined its image quality using test targets positioned at clinically relevant distances from each imaging port. These experiments demonstrated how our multiple ports using chip cameras provide resolution and image quality in between those of flexible and rigid endoscopes. To appraise the ability to image through contact in a blood-

filled field, ex vivo testing using porcine and human brains was performed. We next evaluated MR compatibility by testing the instrument inside a scanner and the ability to obtain MR images of tissue adjacent to the endoscope as well as to stream endoscope video inside the scanner. Finally, to determine the instrument's ability in the context of a multiport procedure, we performed a combined colloid cyst resection and septostomy in a cadaveric head.

Methods

Endoscope Design

The neuroendoscope (Fig. 1) was designed to provide 2 imaging ports enabling tissue resection at the tip port and electrocautery at the lateral port. The device has a total weight of less than 50 g. The instrument body (7-mm outer diameter) consists of a straight 150-mm-long plastic tube with a proximal ergonomic handle. The tip (Fig. 1D and E) and lateral (Fig. 1C and D) imaging ports each contain a 1 × 1 × 1-mm complementary metal-oxide semiconductor (CMOS) video camera (250 × 250 pixels, NanEye, Awaiba Inc.) and an LED for illumination (1.6 × 1.6 mm, Cree Inc.). The tip port contains three 1-mm

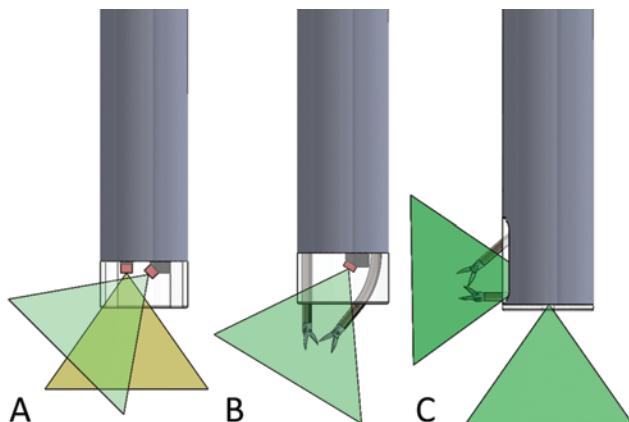


FIG. 2. Schematic of possible alternate locations for cameras and ports at any angle or site along the axis of the endoscope, with emerging tools to suit the nature and location of selected ventricular pathologies. Multiple cameras (0° and 45°) at the same port (A), curved tool ports for instrument triangulation (B), and bimanual instrument control through a lateral imaging port (C).

channels positioned close to the corners of the camera frame of view (Fig. 1E). These working channels can be respectively used for tools, irrigation, and aspiration. The lateral port contains a single 1-mm channel with a 7-mm radius of curvature, which is sized to deliver a Bugbee wire to perform monopolar cautery for fenestration of the septum pellucidum. All channels are lined by 1.2-mm-outer-diameter polyimide tubes.

Each imaging port is molded from optically clear silicone (QSil 218, Quantum Silicones LLC), which encapsulates the camera and LED while creating an optical window with a refractive index of 1.4⁵⁷ (close to that of CSF at 1.33⁹ to minimize distortion). While the optical window of the lateral port is approximately 2 mm thick and molded to be flush with the instrument's cylindrical surface, the window of the tip port has been designed with a thickness of approximately 6 mm. While a much thinner window can be substituted, this thickness was used to enable both visualization of inserted tools before they extend from the tip of the endoscope and safe tissue contact with concurrent imaging.

Evaluation of Imaging

Imaging of test targets was performed at multiple clinically relevant standoff distances (on contact and 5, 10, 15, and 20 mm) at both the tip and lateral ports in saline. These distances were also examined using clinical straight rod-lens and flexible neuroendoscopes. The USAF-1951 3-Bar Resolving Power Test Chart was used as a standard reference in all of our testing (Fig. 4). The target was printed on white paper using a 1200-dpi printer. (Since the smallest features are not printed clearly, a microscope view is also included in the figure.)

MR Compatibility

MR compatibility testing comprised 3 components: 1) testing for dangerous magnetic forces or torques as the device was introduced into and manipulated inside the scanner bore, 2) determining the size of any MRI artifacts produced by the device in surrounding tissue, and 3) ensuring normal operation of the cameras inside the scanner. Figure 5A shows a schematic of the MRI testing. The cables ran from the camera and LED of the multiport endoscope to a laptop computer located in the MRI control room. The endoscope was first carefully manually inserted inside the scanner bore and then moved throughout the interior of the bore. Next, cephalic MRI was performed in a freshly euthanized adult female Yorkshire pig (*Sus scrofa domesticus*). After evaluating the brain anatomy, we transcranially advanced the endoscope through a prepositioned bur hole into a lateral ventricle inside the scanner bore (Skyra 3T, Siemens). Magnetic resonance images were acquired using standard T2-weighted FLAIR sequences. Separately, endoscope video sequences were acquired with and without simultaneous MR pulse sequence execution using the test targets to more easily detect any changes in image quality during scanning (Fig. 5B–D).

Cadaver-Based Instrument Evaluation

The Boston Children's Hospital Post Mortem Research Committee approved the use of human tissue for this study. After creating a frontal bur hole and cruciate durotomy on a human cadaver skull, we introduced an obturator through the underlying cortex into the brain parenchyma. This cavity was widened with suction and filled with

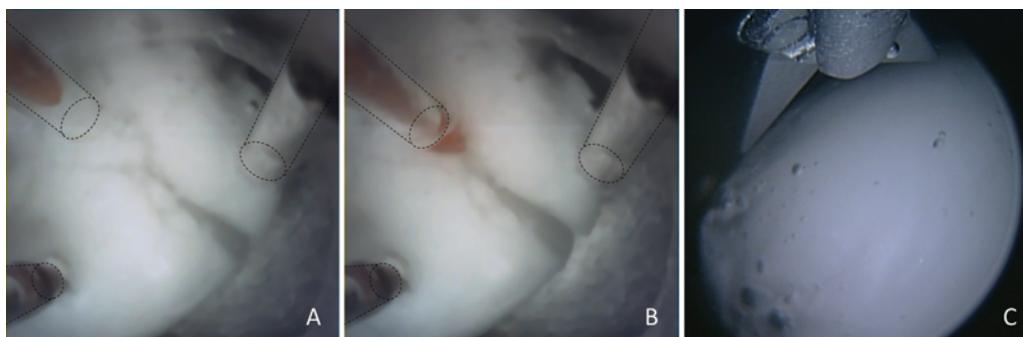


FIG. 3. Suction instrument emerging through the transparent working channel (left upper port) within the silicone optical window of the multiport endoscope. The instrument is inside the window (A) and then has emerged (B). In comparison, when endoscopic scissors become visible in a current clinical endoscope, they have already emerged from the working channel (C). Dashed lines indicate working channels.

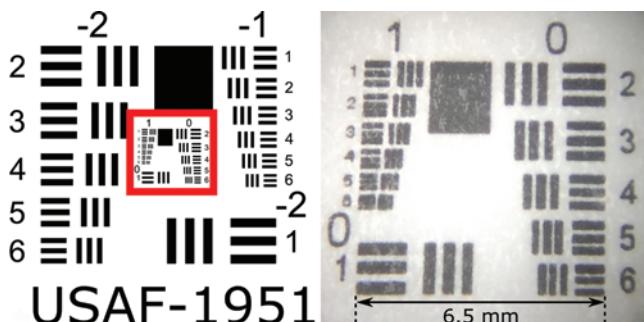


FIG. 4. USAF-1951 test target (left) showing the area of imaging interest outlined in red, and conventional microscopic imaging of the laminated test chart used during our experiments (right). Note that the diminished quality of the right image with a target size of 6.5 mm is attributable to our printer limitations.

blood, and the endoscope was introduced. To determine if the optical window would enable visualization during contact, we slowly advanced the scope until contact was made with the tissue. Given the fixed, shrunken, cadaveric ventricular anatomy, a 4-bur-hole craniotomy was made to implant an artificial colloid cyst transcallosally at the left foramen of Monro. To make the colloid cyst phantom, we dissolved 0.05% ultrapure agarose (Life Technolo-

gies) in 1× phosphate-buffered saline (PBS) by boiling the mixture in a microwave oven and cooling it down to 45°C before adding cream cheese to produce the whitish color of the cyst contents. Immediately, the whole mixture was poured into stretched Parafilm (Bemis Co.) to simulate a colloid cyst with whitish viscous contents that could be readily aspirated. Septostomy was performed inside the cadaveric head using a Bugbee wire inserted through the lateral port of the new endoscope under direct vision. The scattered cadaver debris in the ventricles obscured the views for both a standard endoscope and the new multiport scope. Consequently, a phantom test bed was made in a clear, saline-filled container to perform cutting, suction, and irrigation on the colloid cyst phantom.

To measure the scope rotation needed to perform the combined procedure, we used an electromagnetic tracking system (3D Guidance trakSTAR, Ascension Technology Corp.). A tracking sensor was attached to the endoscope, allowing continuous recording of the instrument position and orientation (Fig. 6A). The pivoting angle with respect to the bur hole was measured for a case in which both procedures were performed via the tip port of the standard scope (Fig. 6B and C). The angle was also measured for the multiport scope when the tip port was used for cyst resection and the lateral port was used for septostomy (Fig. 6D).

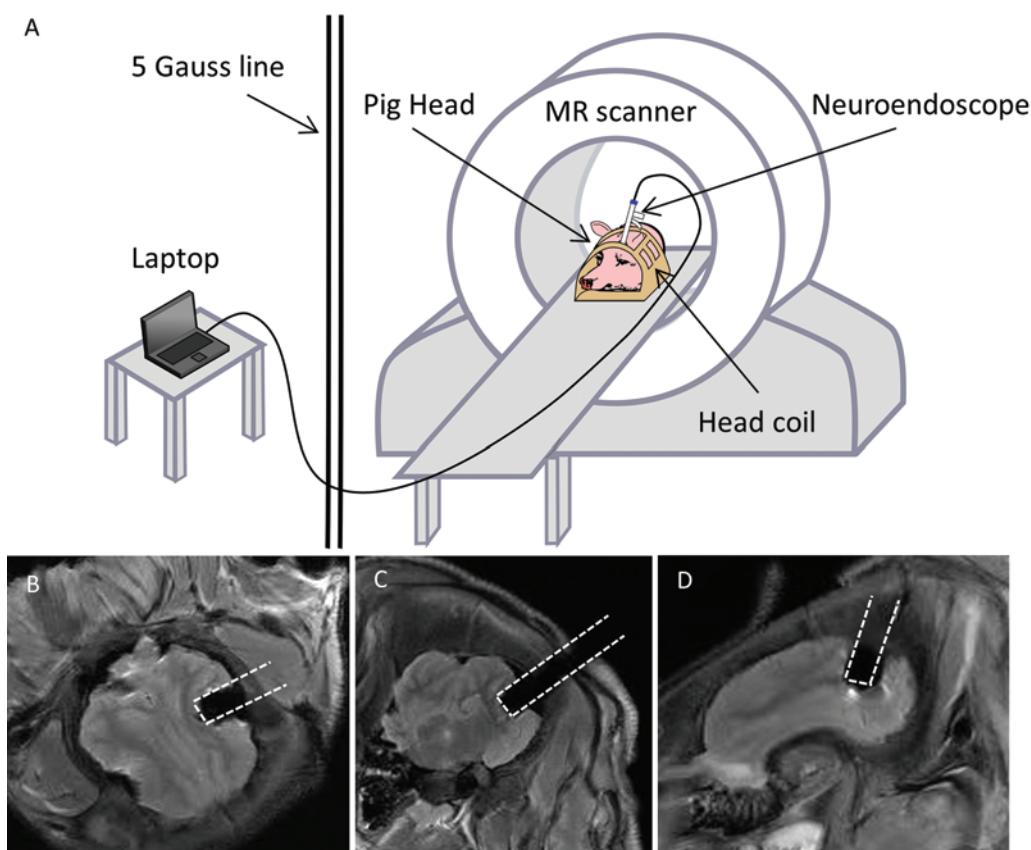


FIG. 5. A: Schematic of MRI testing, with the pig head positioned in the head coil while the neuroendoscope was inserted via a preplanned bur hole. B–D: Demonstration of the MR compatibility of the novel multiport endoscope without any significant artifacts using a fresh porcine brain.

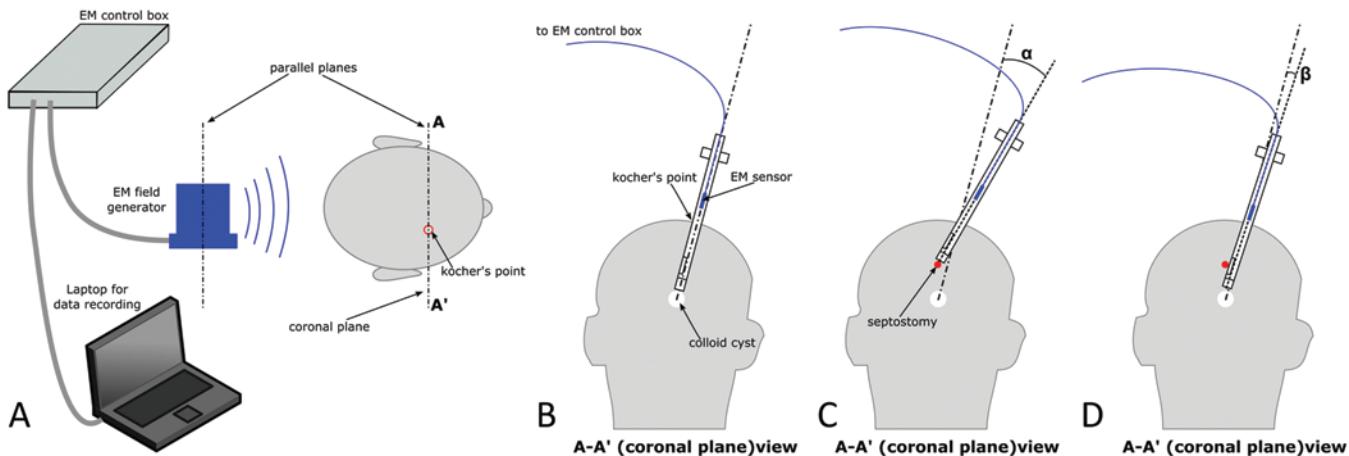


FIG. 6. Measurement of brain deformation during ventricular neuroendoscopy. Setup of the electromagnetic (EM) tracker (A), insertion path for the colloid cyst resection (B), instrument pivoting (measured by angle α) required for septostomy using a standard rigid scope (C), and pivoting (measured by angle β) required using a multiport endoscope (D).

Results

Image Quality

Image quality for the multiport scope was compared with that for the clinical rigid and flexible scopes (Fig. 7). Since fiber-based scopes are often used slightly defocused to avoid visualization of the boundaries of individual fibers, Fig. 7 provides both focused and defocused images for comparison. On contact, only the multiport scope provided a clear focused view. For all noncontact distances, the image quality of the multiport endoscope appeared to lie between those of the rigid scope and the flexible scope. Note that both clinical scopes have been optimized and refined during product development, whereas the multiport scope is a research lab prototype, which can probably be significantly improved.

MR Compatibility in the Porcine Brain

When the new neuroendoscope was inserted into the scanner and moved manually inside the bore, no magnetic forces were perceived. Furthermore, video streaming was unaffected by device placement inside the bore. Subsequently, pulse sequences were obtained during video streaming. We found that the radiofrequency (RF) portion of the pulses would sometimes interfere with video streaming. Since the camera cabling was not RF shielded, this interference is not surprising. Finally, images of the endoscope inside a porcine brain were recorded (Fig. 5B–D). The endoscope appears as a void in these images. Strikingly, while artifacts of instruments are often larger than the instruments themselves, the size of the new endoscope artifact corresponds exactly to its actual size.

Cadaver-Based Instrument Evaluation

The multiport endoscope's ability to visualize tissue through contact is illustrated in Fig. 8. As with a standard scope, nothing can be seen in a blood-filled cavity (Fig. 8A). Once soft contact with the tissue is made, however, the silicone optical window displaces the blood in front of the camera making clear visualization possible (Fig.

8B). Fenestration and/or aspiration of a colloid cyst phantom were first attempted in a cadaver brain. Owing to the shrunken ventricles and tissue debris, our attempts were not feasible with either the multiport or rigid scopes. Consequently, cyst removal was demonstrated in a phantom test bed. Endoscopic tip views of the classic skills of cutting, suction, and irrigation on the colloid cyst phantom are shown in Fig. 9. The lateral port was then used to perform septostomy, but inside the cadaver head, while maintaining a stable view of the anterior field near the colloid cyst phantom at the foramen of Monro as in Fig. 10A. Figure 10 elucidates the sequential steps of positioning the side port close to the septum (Fig. 10B), passing the Bugbee wire through the side port (Fig. 10C), firing the coagulation probe (Fig. 10D), and finally a view of the septostomy hole (Fig. 10E).

Using the electromagnetic tracking sensor, the scope tip was moved between the positions needed for cyst resection and septostomy by pivoting about the bur hole in the skull. The angle of rotation (α in Fig. 6) was 23° , and significant compression of the tissue was observed in performing this rotation. Subsequently, the scope was rotated between the configurations appropriate for cyst resection using the tip port and for septostomy using the lateral port. The rotation angle (β in Fig. 6) was 4.3° .

Discussion

The MR-compatible multiport endoscope technology proposed here combines several novel features. First, it introduces the concept of multiple imaging and instrument ports within the endoscope shaft. Second, it demonstrates how a transparent optical window can be used to view emerging tools and to image tissue clearly during soft contact. Third, it provides these features in an MR-compatible device. Since chip cameras are used instead of the heavier, bulkier charge-coupled device (CCD) cameras and rod lenses of standard rigid neuroendoscopes, the total weight of the multiport neuroendoscope is substantially reduced (45 vs 150 g). Furthermore, the weight of the proposed de-

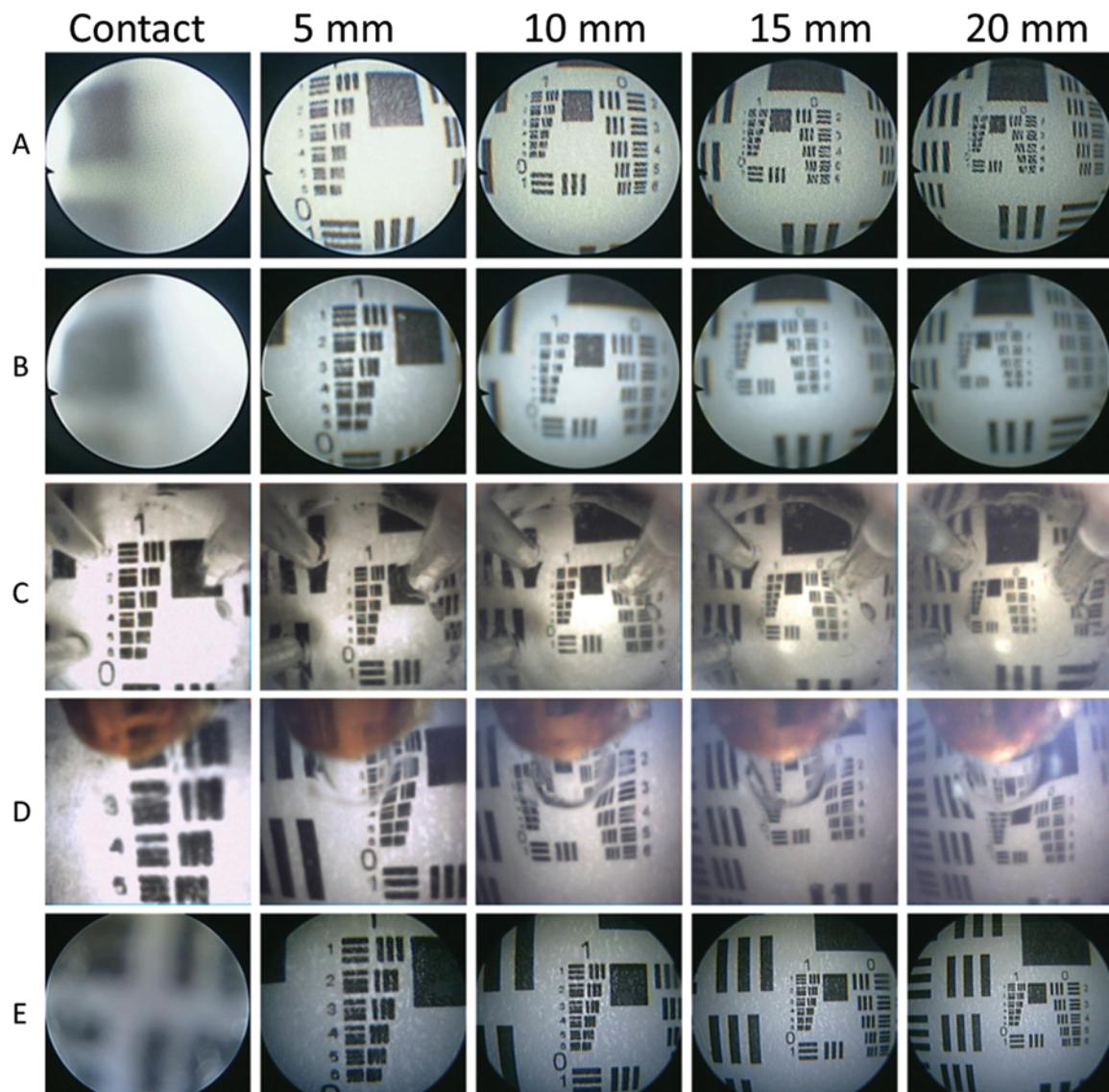


FIG. 7. Imaging results for the multiport neuroendoscope compared with those for the rigid and flexible neuroendoscopes in current clinical practice. **A:** Flexible neuroendoscope at contact and 5, 10, 15, and 20 mm (crisp). **B:** Flexible neuroendoscope at contact and 5, 10, 15, and 20 mm (blurred). **C:** Tip port images at contact and 5, 10, 15, and 20 mm. **D:** Side port images at contact and 5, 10, 15, and 20 mm. **E:** Rigid-lens straight endoscope images at contact and 5, 10, 15, and 20 mm.

vice is evenly distributed along its length (Fig. 11 upper) in contrast to a rigid endoscope, which behaves as an inverted pendulum because of the weight of the proximally attached camera (approximately 250 g) and the light cable (approximately 200 g; Fig. 11 lower). Thus, the multiport endoscope is much easier to manipulate and stabilize during surgery than existing models of rigid and flexible neuroendoscopes. In addition, the incorporation of multiple ports provides multidirectional imaging and tool deployment without the complexity of a flexible endoscope or wider parenchymal channels employed in port surgery or tubular retractors.^{25,27,51,59} Both front and side port imaging can be simultaneously performed, offering added safety for concurrent procedures, whereas the flexible scope tip can lead to disorientation after steering the tip 3 or 4 times

in different directions, getting the operator lost in terms of the global field view. Thus, the disorientation experienced by the operator is much less using our endoscope compared with the steerable tip vision-induced disorientation from a flexible scope. An endoscope-positioning device for stabilization during surgery can prevent inadvertent movement of the shaft while instruments are extending through one or both ports. The low cost of the multiport endoscope avoids the need for a large capital investment and offers the potential for disposable use.

Utility of Multiple Ports

We have demonstrated the utility of 2 ports in performing a combined colloid cyst resection and septostomy. When the combined procedure is routinely performed

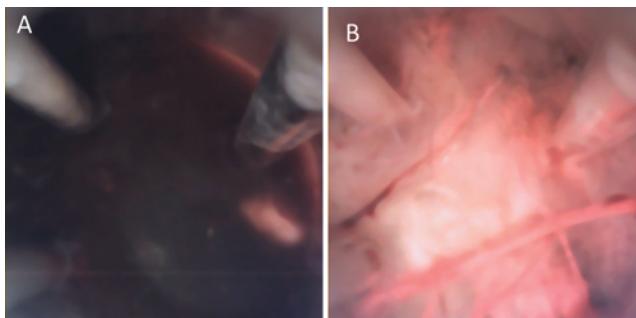


FIG. 8. Imaging in blood using the multiport neuroendoscope demonstrating the “diver’s mask effect” of a soft silicone optical window. **A:** Noncontact view in the human cadaver brain cavity field filled with citrated porcine blood. **B:** View through the tip port after advancing the neuroendoscope to contact the tissue in a blood-filled cavity.

with a rigid endoscope, the endoscope’s proximal inserted length compresses adjacent brain structures as the tip is redirected from the direction of the third ventricle at the foramen of Monro to the septal area devoid of veins. We have shown that the multiport endoscope’s second port can substantially reduce this rotation (23° vs 4.3°). Furthermore, since the septum contains a highly variable network of veins, the amount of endoscope rotation can be greater than the reported value since the septum must be explored to locate a vein-free location for perforation, especially during prophylactic septostomy in mild to moderate ventriculomegaly.⁹²

The brain shift during ETV has been studied extensively.^{10,43,100} However, fenestration of the septum pellucidum has not been studied for quantitative brain deformation

while using a standard precoronal bur hole for ETV or an adjusted bur hole for colloid cyst resection. The conventional scope is inserted in a trajectory for ETV or colloid cyst removal, then the endoscope itself distorts the brain medially when the scope is directed or forced toward the midline septum pellucidum, especially in cases with mild to moderate ventriculomegaly.^{25,32,87} We have used the septostomy as a prototypical procedure to show the utility of the side port for instruments and imaging, as the side port would allow direct access to the septum without significant brain deformation. Using this new multiport endoscope will facilitate safe resection of a lesion at the foramen of Monro while allowing one to identify a bleeding source in the lateral ventricle, and thus providing information on the focal field of surgery in real-time and augmenting the global view offered by intraoperative MRI.^{40,41}

The combined use of flexible and rigid endoscopes as well as dual bur hole endoscopic procedures has been demonstrated in various ventricular pathologies, often in small-sized ventricles.^{7,22,32,36,37,54,55,67,71,74,91,96,99} Two classic indications for using our novel endoscope instead of existing rigid and flexible scopes are loculated, or postinflammatory, hydrocephalus and posterior third ventricular lesions. The multidirectional septations and adhesions in the ventricular system can be fenestrated or lysed easily and effectively by multiplanar multichannel instrumentation using this new endoscope. The multiport scope can offer better image delineation than the fiber bundles of flexible endoscopes with less potential for disorientation, the same compatibility with navigational devices, and no additional skill training for surgeons. As an extension of this application, our new scope can provide a better bird’s eye view of the subependymal spread of disseminated ventricular tu-

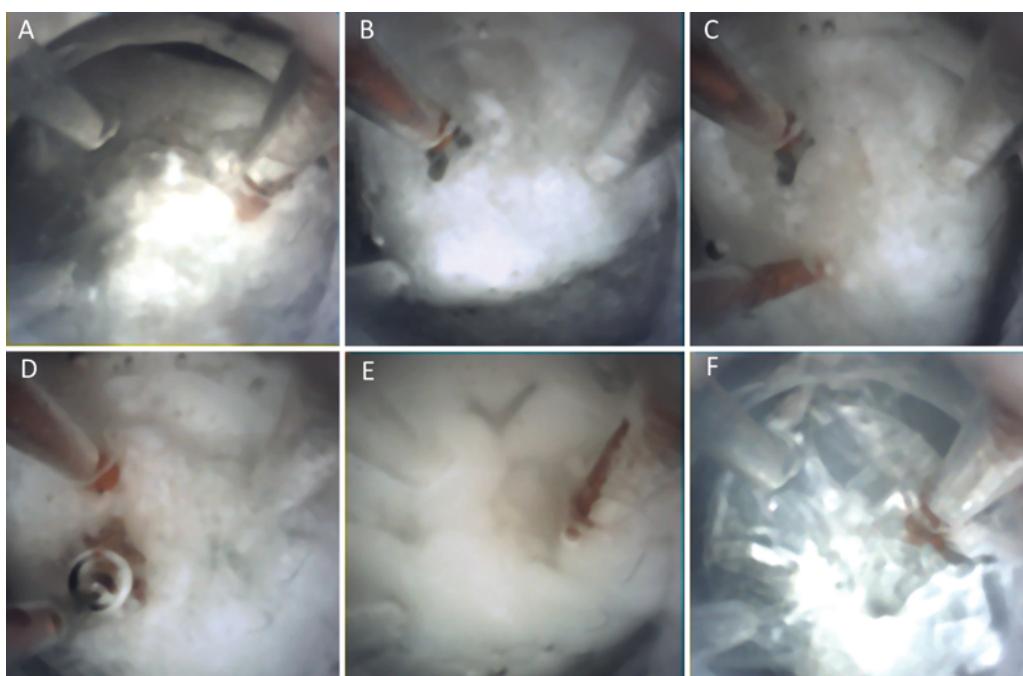


FIG. 9. Strategies resecting a colloid cyst phantom using a multiport silicone-tipped neuroendoscope with transparent channels within a distal silicone optical window (**A**). Endoscopic graspers for holding the capsule (**B** and **C**). Suction and irrigation (**D** and **E**) used to empty cyst contents from the capsule (**F**).

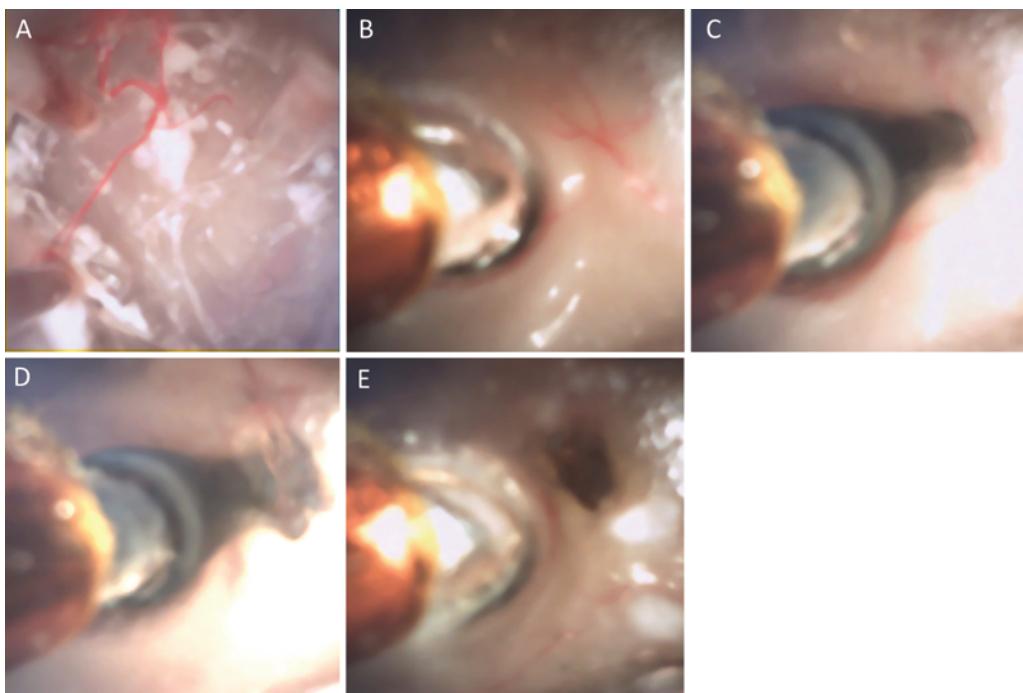


FIG. 10. Close-up tip port view (A) of the membranous capsule of the colloid cyst phantom. Side port septostomy steps using the novel neuroendoscope: advancing the endoscope toward the septum (B), emerging Bugbee probe (C), coagulation of the septum (D), and the site of fenestration (E).

mors and even offer transtumoral stent placement for CSF diversion, for example, third ventricular and aqueductal stents in craniopharyngiomas and tectal tumors, respectively.⁶⁶

Posterior third ventricular lesions are more amenable to ventricular access when there is triventricular hydrocephalus resulting from aqueductal obstruction and widening of one or both foramina of Monro.^{15,53} An optimal trajectory between the hairline and Kocher's point is often used for biopsy of the lesion combined with an ETV. Morota and Ogiwara have proposed another trajectory using a flexible endoscope over the interthalamic adhesions in the third ventricle.⁵⁵ Our current endoscope prototype has multiple channels at the tip; similarly, a modified design with a multichannel side port located very close to the tip of the endoscope would enable the surgical management of concurrent lesions in lateral and third ventricles, offering minimal traction at the foramen of Monro.^{19,20,73}

Beyond hydrocephalus, our neuroendoscope can also be used in endoscope-assisted microsurgical cisternal procedures such as corpus callosotomy in a minimally invasive manner with limited brain retraction. Furthermore, for neurosurgeons in remote underprivileged communities without access to stereotaxy, this device can be used in a disposable manner to perform an endoscope-assisted microsurgical procedure.^{94,95}

MR Compatibility

We have shown that the size of the MRI artifact corresponds to the size of the endoscope itself, providing the ability to image tissue adjacent to each imaging port. Since most endoscopes are not MR compatible, endo-

copy and MRI guidance are typically viewed as mutually exclusive.^{77,78} Intraoperative removal and reinsertion of the endoscope to perform MRI is deemed too risky in terms of iatrogenic hemorrhages. However, the combined use of MRI and endoscopy can provide the benefits of stereotaxy as well as real-time optical imaging.^{70,81,84,85} Currently, it is common practice to co-register the endoscope with preoperative MRI used for trajectory planning. In contrast, MRI with our new endoscope within the ventricular system can provide real-time continuous imaging and compensate for brain shift that occurs with CSF egress during ventriculostomy. This is especially critical in treating ventricles scarred from prior infection or inflammation or periventricular tumors with a diffuse or ill-defined brain-tumor interface, as in gliomas or central neurocytomas.^{34,38}

The MR compatibility of our new endoscope renders it suitable to treat complex or multiloculated hydrocephalus associated with multiplanar septations or cystic malformations of periventricular brain.⁶⁴ Solely depending on endoscopic luminal anatomy can cause inadvertent neurovascular injuries especially in an atrophic brain with deformed ventricular anatomy.³⁴ Magnetic resonance imaging guidance can offer safe, optimal, and tailored endoscopic fenestration in these cases (ventriculocystostomy, cystocystostomy, cystoventriculostomy, or cystoventriculocisternostomy as mandated) and precise insertion of a ventriculoperitoneal shunt in selected cases, avoiding catheter misplacement in a cul-de-sac. The same technology can be effectively used for intraventricular stent procedures (aqueductoplasty and stenting), as well as intratumoral stenting (in craniopharyngiomas sealing off the prior ETV

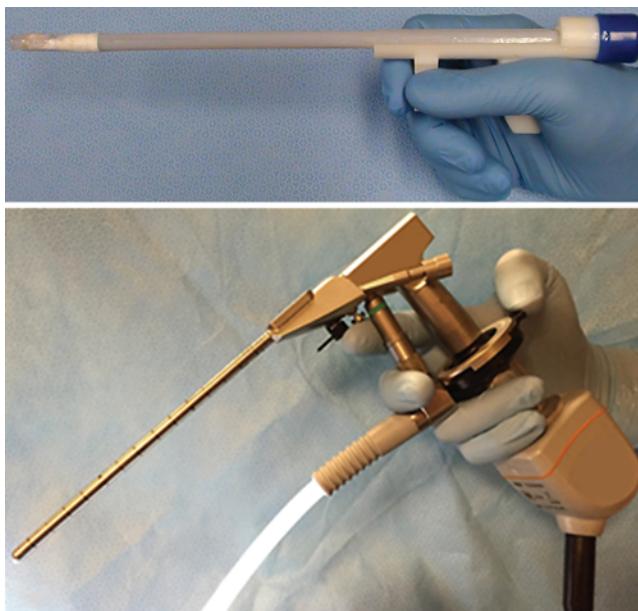


FIG. 11. Upper: New light-weight (< 50 g) multiport neuroendoscope. **Lower:** Currently used clinical neuroendoscope with an “inverted pendulum effect” due to the heavy proximal camera and light-cable attachments, weighing over 500 g in total.

or in a posterior third ventricular region tumor occluding the aqueduct.^{3,9,21,29,33,49,66,69,83} Magnetic resonance compatibility can be helpful in treating intraventricular neurocysticercosis as well as juxtaventricular parenchymal cystic changes such as tumefactive enlargement of thalamoperioduncular Virchow-Robin spaces.^{3,24}

Intraoperative MRI technology has revolutionized neurosurgery in the past 2 decades, especially with the advent of MR-compatible probe drivers (ClearPoint) and transventricular laser ablation of periventricular lesions via NeuroBlate and Visualase.^{52,62,65} The indications for real-time MR-guided laser treatment have extended from focal metastatic and glial neoplasms to refractory cerebral edema, radiation necrosis, lesional epilepsy, and even cavernous malformations in the brain.^{11,12,26,50,52,65,68,97} The paraventricular tumors, especially those in the thalamic region as well as those in which maximal safe resection is not feasible, have become amenable to MR-guided laser treatment.^{75,89,93,97} These technologies, however, provide real-time yet noncontinuous MRI during the procedure.⁷⁹ In a majority of these MR-guided laser therapies, surgeons use a skull bolt to deliver the laser probe via a single bur hole in the skull. However, for multiple lesions that are not accessible, a second trajectory is employed via a second skull entry point. A new 4.5-mm on-trajectory twist drill hole is typically made for additional trajectories. Surgeons generally try to avoid a trajectory through the cerebral ventricles for treating parenchymal lesions, but violation of a ventricular wall often does happen inadvertently with stereotactic errors. While using our device for ventriculostomy, the surgeon uses a familiar preplanned bur hole as an entry point and takes advantage of the appropriate side ports for both visualization and penetration of the periventricular lesion that needs laser ablation. The ability to use

the front and side ports interchangeably and concurrently, as well as multiple degrees of freedom in the ventricular cavity (translation, rotation), can enhance the safety and feasibility of targeting juxtaventricular lesions for laser therapy.

Magnetic resonance–guided neuroendoscopy using our device offers the combined advantages of stereotactic biopsy (whereby sampling the most representative or contrast-enhancing area of a heterogeneous MRI target can be achieved) and direct vision of the target.^{16,35,63,80} In addition, biopsy or resection of a lesion under endoscopic imaging could be improved by optical imaging of live tumor margins and could further enhance safety by enabling real-time visualization of intraprocedural hemorrhage and tool-based hemostasis, as in cases of vascular tumors or postinflammatory hydrocephalus with vascularized membranes.

Optical Window

With our design, we investigated the utility of an optically clear silicone window on the tip imaging port and demonstrated 2 potential advantages. First, the optical window enables visualization of inserted tools before they emerge from the endoscope tip. In addition, the optical window can be used to gently press against tissue and thus displace any fluid, including blood, between the window and this tissue. During near contact the suction and irrigation channels can still function, whereas during full contact there is clear vision and soft pressure at the bleeding site offering contact hemostasis. This transparent window is a built-in feature of our neuroendoscope, unlike a separate transparent sheath or trocar.^{56,60}

Intraventricular hemorrhage can be a fatal complication from endoscopic neurosurgical procedures.⁴⁷ Bleeding inside a ventricle during surgery is now typically managed through local warm saline irrigation, by promoting vasoconstriction and thus hemostasis. We designed the new endoscope with a soft silicone tip, which can exert even soft contact at the bleeding site, akin to the application of Gelfoam and cottonoid over bleeding veins and dural venous sinuses. Since the majority of intraventricular hemostasis during neurosurgical operations is performed without tissue contact, warm saline irrigation is the primary method of controlling minor hemorrhages, while bipolar coagulation is used for larger bleeding sites. Our new endoscope can offer focal soft contact pressure at the bleeding sites, especially venous hemorrhage.

Endoscopic Imaging

Endoscopic imaging systems are comprised of a lens system, a camera, and the associated electronics. The major difference between current rigid and flexible endoscopes is the optical components used to transmit the image from the objective lenses at the tip to the camera at the base.⁴² Rigid endoscopes employ a set of relay lenses, typically rod lenses, whereas flexible endoscopes employ an optical fiber bundle. Since each fiber transmits one pixel of the image, resolution is limited by fiber size and by the number of fibers in the bundle. Since the fibers have a finite size and are round, they produce an image with reduced resolution and clarity in comparison with the optics

of a rigid endoscope. In our endoscope design, CMOS chip cameras are positioned directly at the port, and the image is transmitted electronically as a digital signal through the endoscope body to the frame grabber electronics and image display computer. Consequently, our designs do not employ either relay lenses or fiber bundles.

Current endoscopes rely on 2 camera technologies: CCDs and CMOSs. We have used a CMOS sensor, each pixel has its own charge-to-voltage conversion, and the sensor often also includes amplifiers, noise correction, and digitization circuits so that the chip outputs digital bits. This lowers camera cost while providing faster readout, lower power consumption, higher noise immunity, and a smaller system size. The CMOS camera used in our prototype, at 1 mm on a side, is among the smallest currently available and provides an image size of $250 \times 250 = 62,500$ pixels. For comparison, a fiber bundle of comparable cross-section contains only 20,000 fibers/pixels.²⁸ Thus, the image quality of our endoscope lies between that of existing rigid and flexible neuroendoscopes (Fig. 7).

While image resolution is limited by the size of the photodiodes that can be manufactured, image quality also depends on the camera lens(es) and on the image processing software. Both can be optimized on an application-specific basis, and chip-on-tip endoscopes have been clinically introduced in other fields such as general surgery, urology, and gynecology.^{28,42,46} Similar to our design and in contrast to existing neuroendoscopes, these devices are “focus-free” designs wherein their lens systems have been optimized to provide a sharp image over a large depth of field.

Device Limitations

The current design is intended as a proof-of-concept prototype, fabricated using materials and techniques available in our laboratory, and so has not benefited from the extensive product development cycle of an actual clinical device. Limitations of the current prototype relate to image quality and working channel size, as described below.

While the use of chip cameras enables multiple imaging ports, image quality is less than what is offered by the single imaging port of a standard scope. Specifically, image quality is reduced in air and at viewing distances greater than 2 cm. Just as smart phone cameras have had continued improvements, it is likely that the stated limitations of our prototype can be mitigated through the use of improved lenses, the addition of antireflective coatings to the optical window, optimization of the relative configuration of the camera, LED, and window surface to minimize internal reflections, and tuning of the image processing software for neurosurgical visualization.

The size of the working channels in the current prototype is small and must be enlarged. In any scope, including the proposed design, the number and diameter of the channels are constrained by the scope diameter. For example, Fig. 12 depicts the cross-section of a standard scope as shared by the optical channel and the working channels (Aesculap MINOP system FF399R). Note that while a traditional rod lens runs the entire length of the scope, the camera and LED pair (shown superimposed on the optical channel in Fig. 12) only consume a few millimeters of

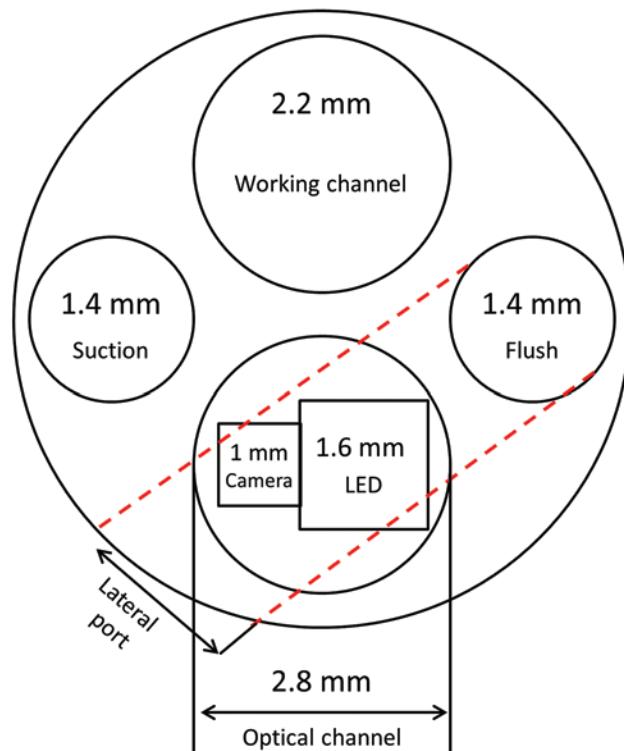


FIG. 12. Comparison of hardware arrangement within cross-sections of a 6-mm rigid endoscope with a multiport neuroendoscope. A conventional rod lens endoscope with a 2.8-mm scope channel can easily accommodate a 2.6-mm construct (1.6-mm LED and 1-mm chip-on-tip camera) of the multiport endoscope. The addition of a side port working channel with concurrent imaging tends to use up more of the cross-sectional area.

scope length. Thus, this portion of the cross-section is free to be used as a working channel terminating at a proximal imaging port. The constraint is that the working channel leading to a proximal port located on a lateral surface must curve inside the cross-section. For example, the dashed lines indicate how one of the 1.4-mm working channels can be connected to a lateral port. Such a design, while requiring sufficiently flexible tools for the lateral port, would include the same number and size of working channels as in a current rigid scope.

We have not performed sterilization testing of the multiport scope; however, its components are compatible with gas sterilization. Furthermore, existing endoscopes using chip cameras can be sterilized by autoclave, ethylene oxide (EtO), or STERRAD.⁷²

Conclusions

A multiport MR-compatible neuroendoscope can be a versatile tool in treating a wide spectrum of intraventricular and periventricular pathologies in the brain. This peel-packed plug-and-play device does not cause the typical torque-related “inverted pendulum effect” or heavily compromise on the visual quality (Fig. 13). Magnetic resonance compatibility allows for periventricular tumor resection and management of complex hydrocephalus, ex-

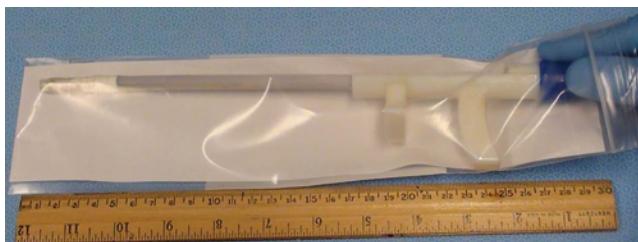


FIG. 13. Disposable “plug-and-play” MR-compatible multiport neuroendoscope: original prototype.

tending the spectrum of ventriculoscopic approaches in the brain. Additional clinical advantages of this landmark endoscope design stem from the utilization of a “diver’s mask” silicone window, which allows soft contact hemostasis and visualization of instruments coming through its transparent channels. More experiments are required to validate its use in treating cisternal brain pathologies and intraparenchymal lesions (tumors and hematomas) and in skull base surgeries.

Acknowledgments

This work was partially supported by the NIH Grant No. R01HL124020.

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- ### Disclosures
- Drs. Manjila, Mancattelli, Rosa, and Dupont are listed as co-inventors on a patent application that includes material in this article.
- ### Author Contributions
- Conception and design: Dupont, Manjila, Mencattelli, Rosa, Price. Acquisition of data: all authors. Analysis and interpretation of data: all authors. Drafting the article: Dupont, Manjila, Mencattelli, Rosa. Critically revising the article: Dupont, Manjila, Mencattelli. Reviewed submitted version of manuscript: Manjila, Mencattelli. Administrative/technical/material support: Mencattelli.
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