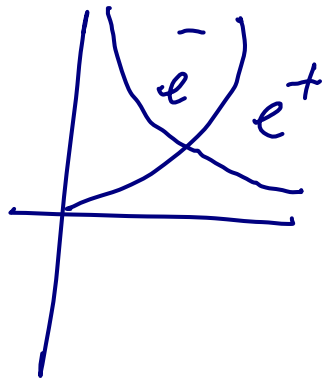


# BJT small-signal Analysis

การวิเคราะห์ของ Diode สามารถทำได้ใน 2 กรณี  
กรณี 1 Forward and Reverse bias region  
ทำได้



$$I_D = I_S (e^{k V_D / T_k} - 1)$$

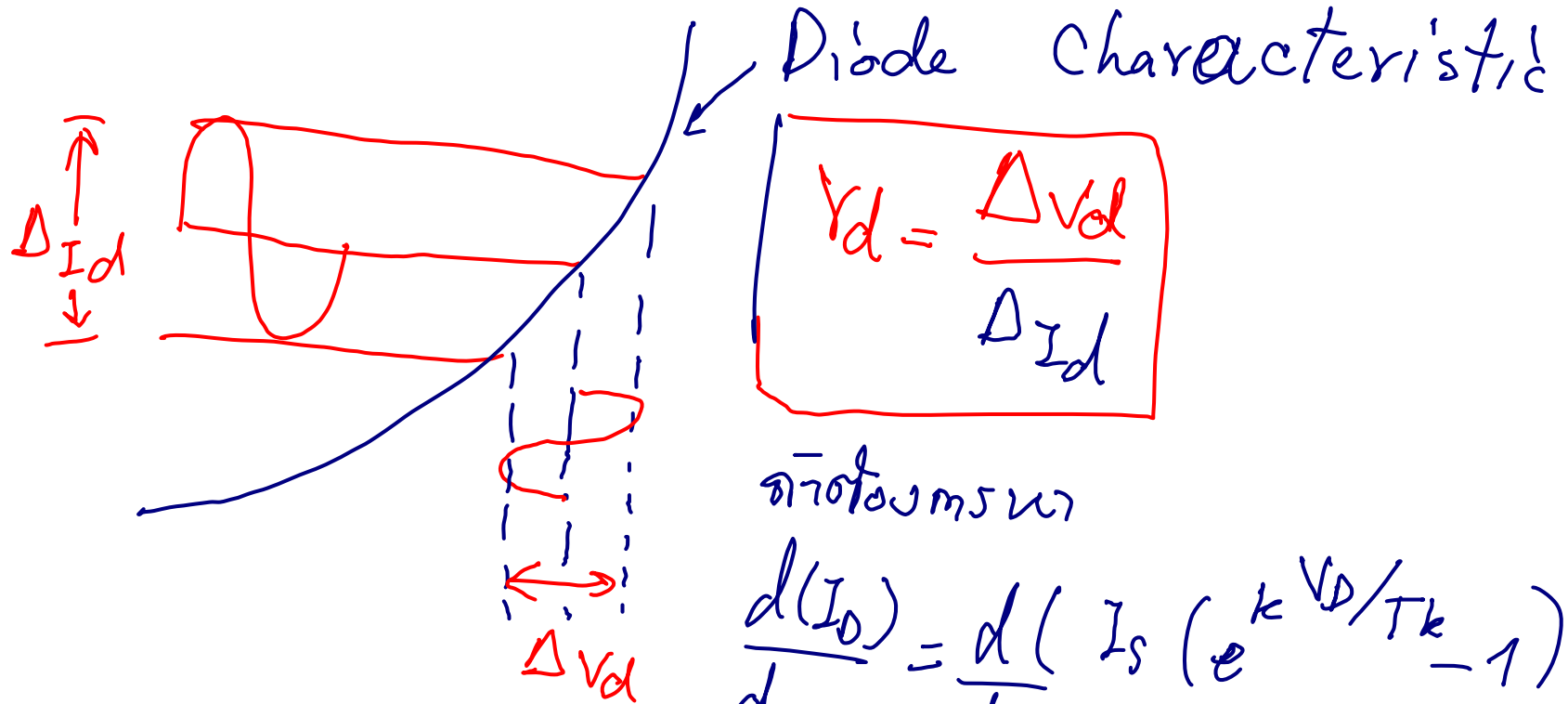
$I_S$  = reverse saturation current

$$k = 11,600 / n \rightarrow n = \begin{cases} 1 & \text{for Ge} \\ 2 & \text{for Si} \end{cases}$$

$$T_k = T_c + 273^\circ \text{ (kelvin)}$$

$$V_D = 115 \text{ mV สำหรับ Diode}$$

# AC and Dynamic Resistance



∴  $\frac{dI_D}{dV_D} = \frac{k}{T_k} (I_D + I_S)$  if  $I_D \gg I_S$

$$\frac{dI_D}{dV_D} = \frac{k}{T_k} I_D$$

สมมติให้ Diode เป็น Ge จงหา

$$k = \frac{11,600}{1} = \frac{11,600}{1} = 11,600$$

ที่อุณหภูมิห้อง 25°C จงหา

$$T_k = 25^\circ + 273^\circ = 298^\circ$$

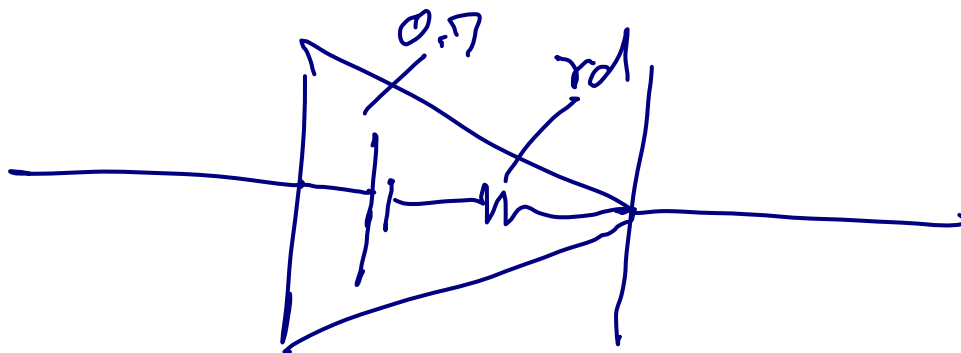
หา  $k/T_k$  จงหา

$$\frac{k}{T_k} = \frac{11,600}{298} = 38.93$$

$$\frac{dI_D}{dv_D} = 38.93 I_D$$

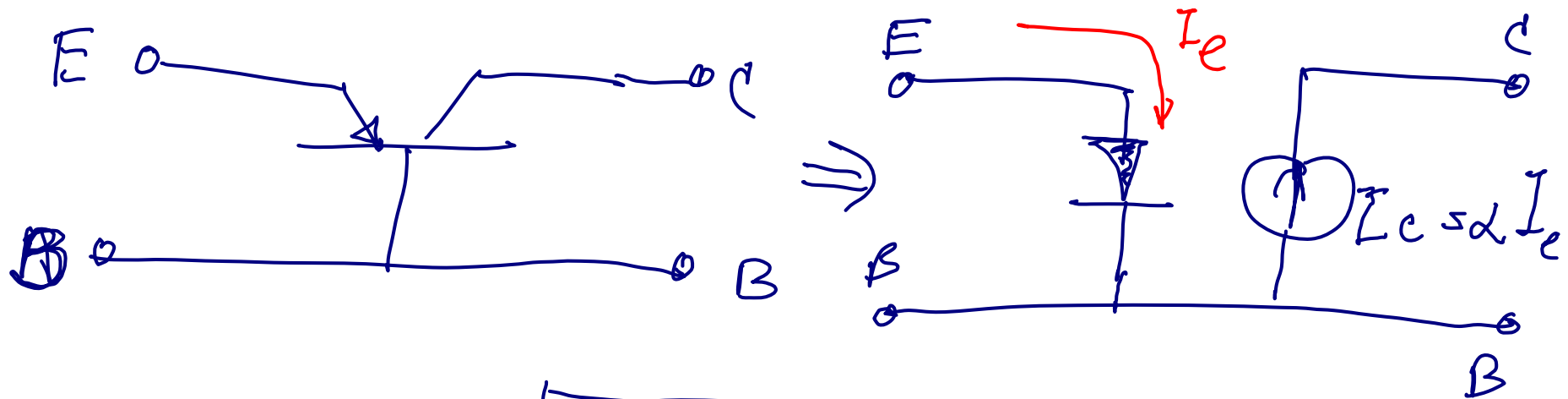
$$\frac{dv_D}{dI_D} = \frac{1}{38.93 I_D} = \frac{0.026V}{I_D}$$

$$\boxed{\therefore r_d = \frac{26 \text{ mV}}{I_D}} \leftarrow \text{Diode}$$



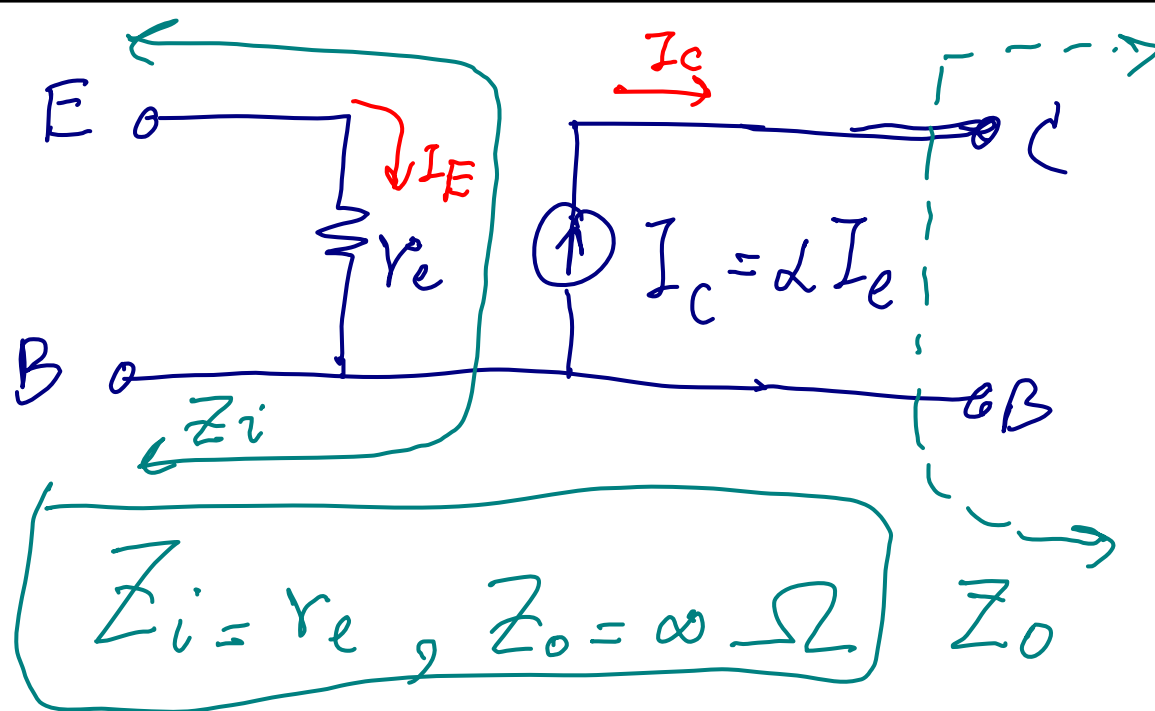
# The $r_e$ Transistor Model (Transistor)

= Common base



$$r_e = \frac{26\text{mV}}{I_E}$$

~~$I_E$~~



$$V_o = -I_o R_L = -(-I_c R_L) = \alpha I_e R_L$$

$$v_i = I_e Z_i = I_e r_e$$

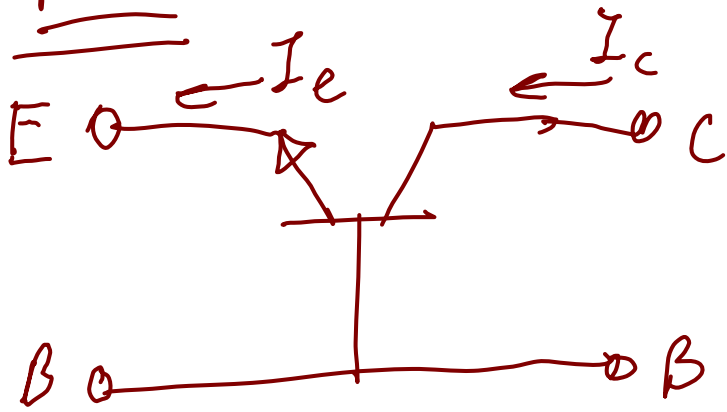
อัตราขยาย  
1150 ต่อ 1  $\rightarrow A_v = \frac{V_o}{V_i} = \frac{\cancel{\alpha} \cancel{I_e} R_L}{\cancel{I_e} r_e} = \alpha \frac{R_L}{r_e}$

ถ้า  $\alpha \approx 1$   
ดังนั้น  $A_v \approx \frac{R_L}{r_e}$  #

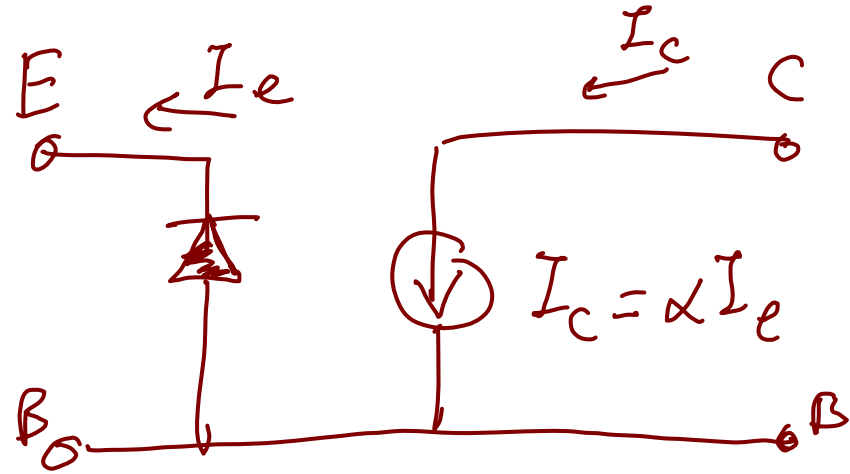
$A_i$  (อัตราขยายกระแส: 1150)  $= \frac{I_o}{I_i}$

$A_{i(cB)} = - \frac{I_c}{I_e} = - \frac{\cancel{\alpha} \cancel{I_e}}{\cancel{I_e}} = -\alpha \approx -1$

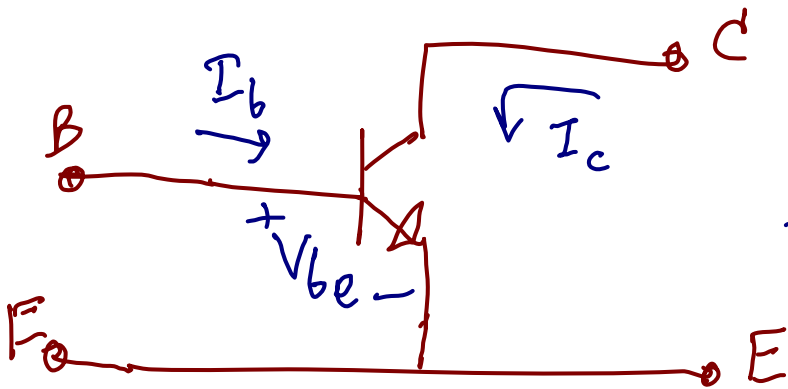
NPN



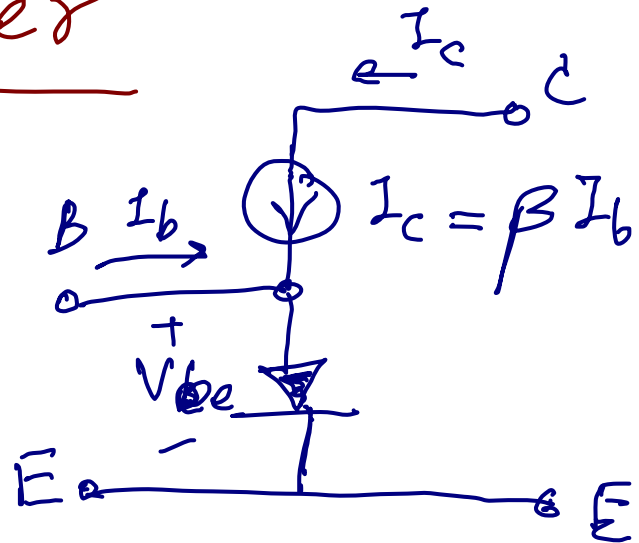
$\Rightarrow$



Common Emitter



$\Rightarrow$





$$I_c = \beta I_b$$

$$I_e = I_c + I_b = \beta I_b + I_b = (\beta + 1) I_b$$

$$I_e \approx \beta I_b$$

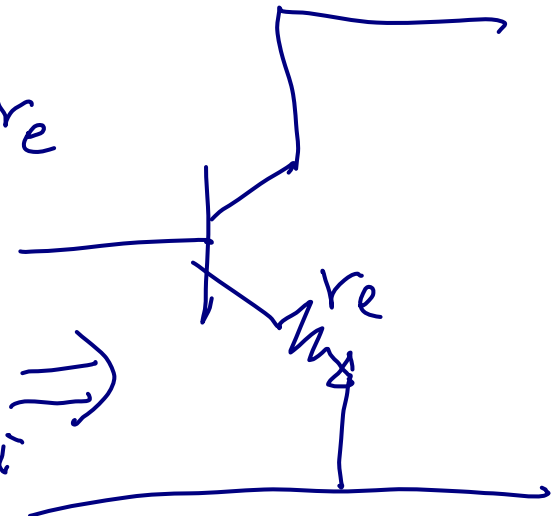
on  $Z_i$

$$Z_i = \frac{V_i}{I_i} = \frac{V_{be}}{I_b} \quad \#$$

$$\text{on } V_i = V_{be} = I_e r_e \approx \beta I_b r_e$$

$$Z_i = \frac{\beta I_b r_e}{I_b} = \beta r_e \quad \#$$

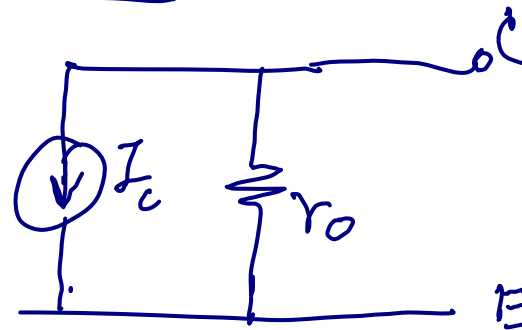
$\Rightarrow Z_i$



สำหรับ CE ทรานซิสเตอร์  $Z_i$  มีค่าประมาณ 100  $\Omega$  - 7k  $\Omega$

$Z_o$  (output impedance)

$$Z_o = r_o$$



✓  
ถ้าสมมติให้  $Z_o = \infty \Omega$  ปรากฏว่า  
Voltage gain ใกล้เคียง 1



$$V_o = I_c R_L = \beta I_b R_L$$

$$\text{In: } V_i, I_i Z_i = I_b \beta r_e$$

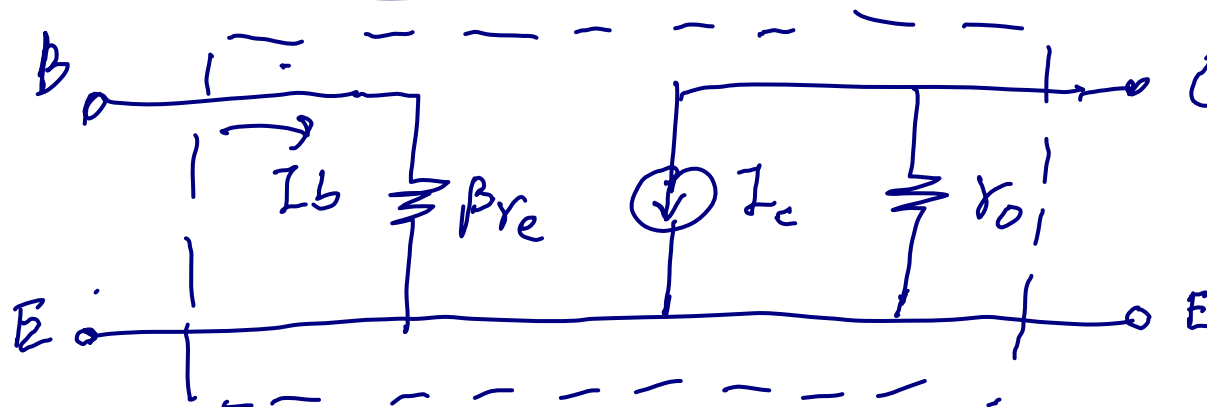
$$\therefore A_v = \frac{V_o}{V_i} = \frac{\beta I_b R_L}{\beta I_b r_e} = \frac{R_L}{r_e}$$

$$\downarrow \text{No } r_o = \infty \Omega$$

อัตราส่วนกระแส (A<sub>i</sub>)

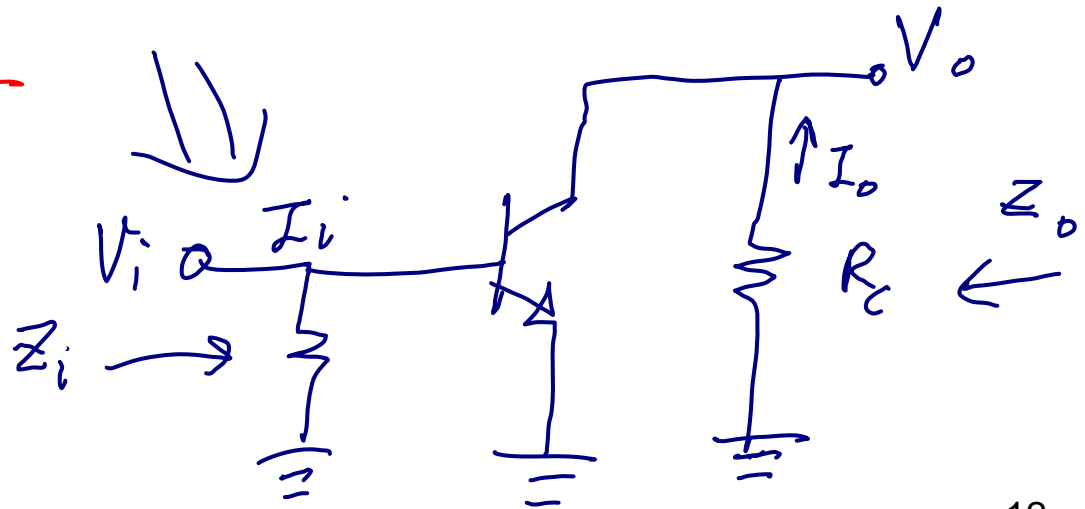
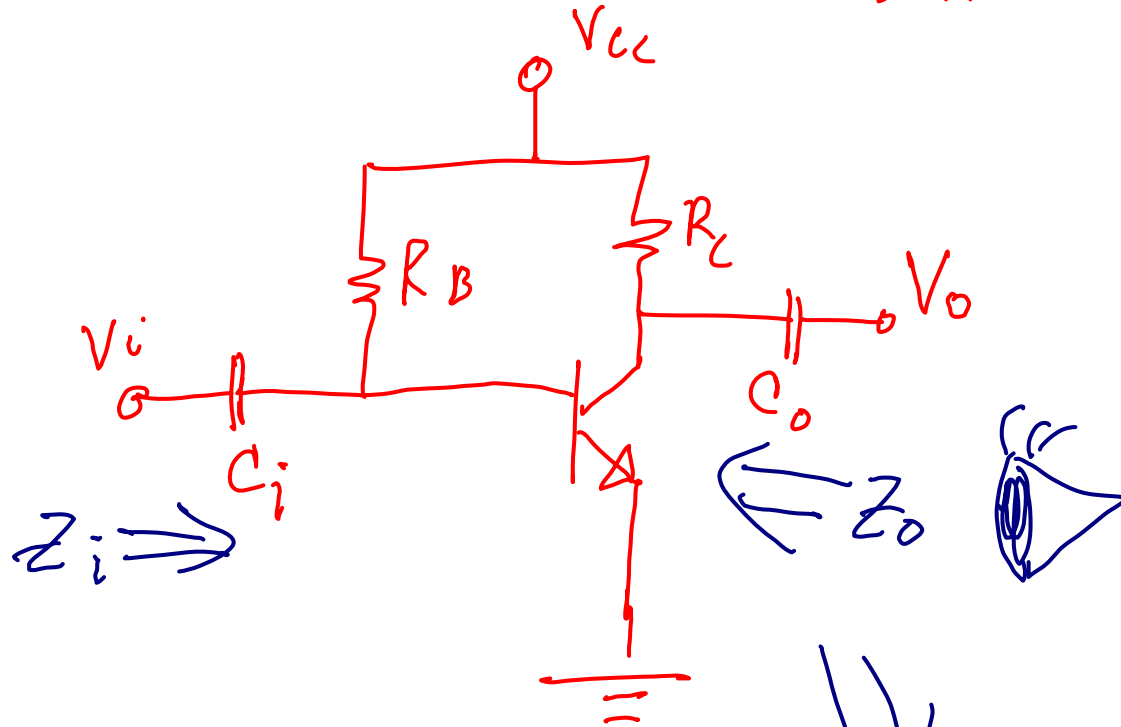
$$A_i = \frac{I_o}{I_i} = \frac{I_c}{I_b} = \frac{\beta I_b}{I_b} = \beta$$

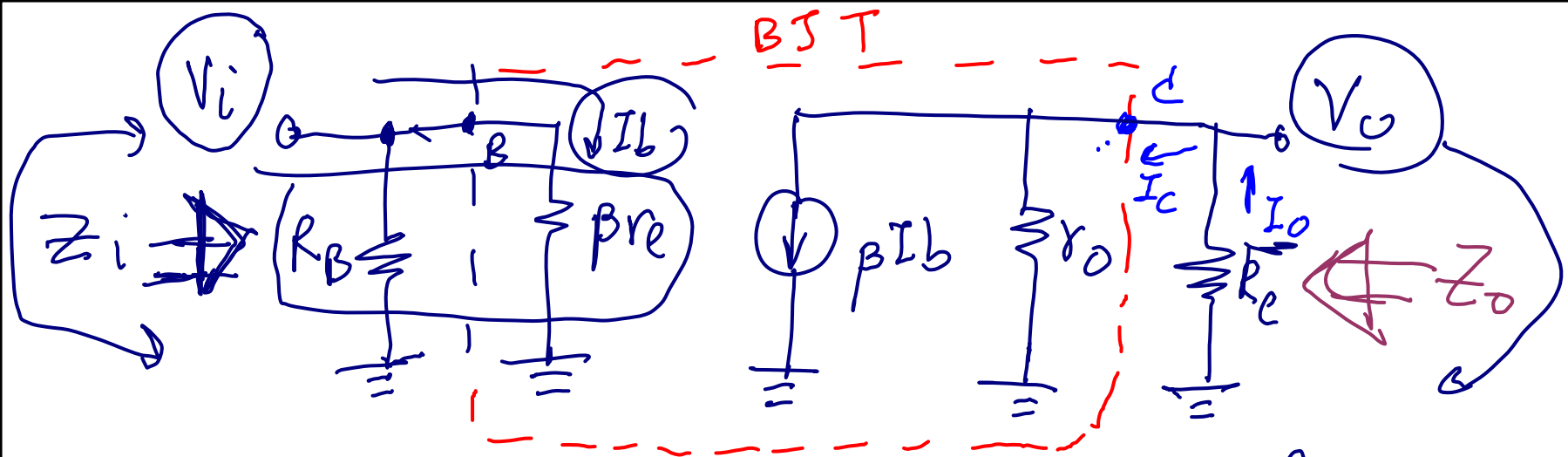
$$\downarrow \text{No } r_o = \infty \Omega$$



# COMMON EMITTER FIXED-BIAS

out send





u1 Zi

$$Z_{i(tot)} = R_B \parallel \beta r_e$$

nsn  $R_B \gg 10 \beta r_e$   $\alpha = \frac{V_{out}}{V_{in}}$

$Z_i = \beta r_e$

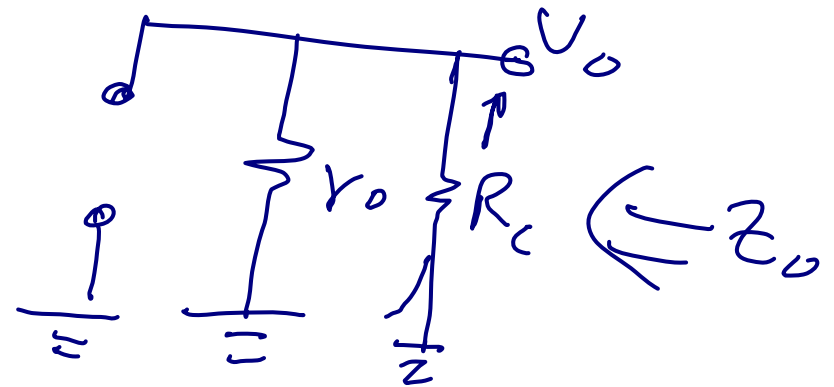
u1 Zo

$Z_o = R_C \parallel r_o$

$$\frac{R_B \times \beta r_e}{R_B + \beta r_e}$$

જો  $r_o \gg 10 R_c$  તો:

$$Z_o = R_c$$



ક,  $A_v$

$$V_o = -\beta \overbrace{I_b}^{I_c} (R_c \parallel r_o)$$

તેથી  $I_b = \frac{V_i}{\beta r_e}$

અથવા  $I_b$  થી

$$V_o = -\beta \left( \frac{V_i}{\beta r_e} \right) (R_c \parallel r_o) =$$

$$A_v = \frac{V_o}{V_i} = - \frac{(R_c \parallel r_o)}{r_e}$$

12/0  $r_o \gg 10 R_c$   $\approx 70\%$

$$A_v = -\frac{R_c}{r_e} \quad \#$$

หา  $A_v$  หา  $I_o$  ก่อน

$$I_o = \frac{r_o \beta I_b}{r_o + R_c}$$

$$\text{หรือ } \frac{I_o}{I_b} = \frac{r_o \beta}{r_o + R_c}$$

หา  $I_b$  ก่อน

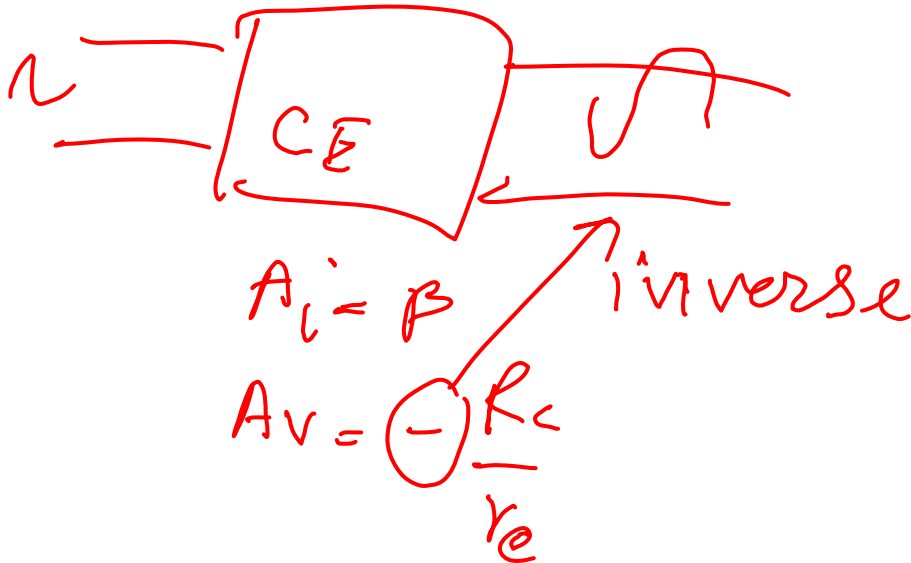
$$I_b = \frac{R_B I_i}{\beta r_e + R_B}$$

$$\text{หา  $I_i$  } I_i = \frac{(\beta r_e + R_B) I_b}{R_B}$$

$$\text{ดังนั้น } A_v = \frac{I_o}{I_i} = \frac{r_o \beta \cancel{I_b}}{r_o + R_c} \cdot \frac{R_B}{(\beta r_e + R_B) \cancel{I_b}} = \frac{R_B r_o \beta}{(r_o + R_c)(\beta r_e + R_B)}$$

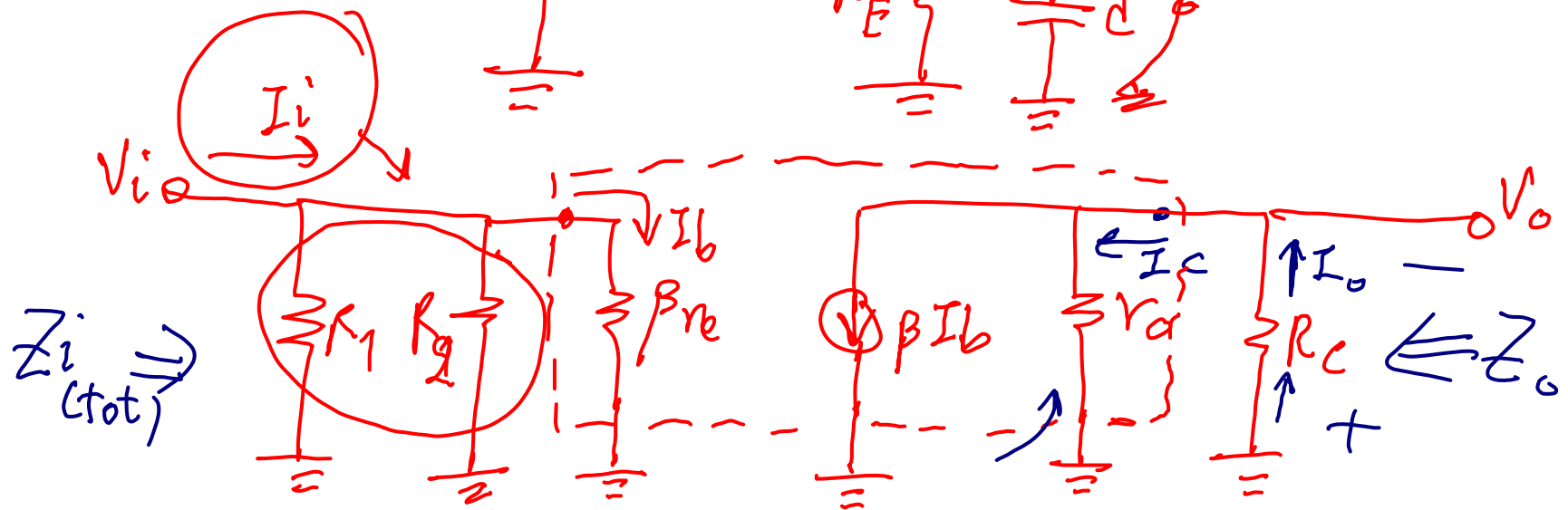
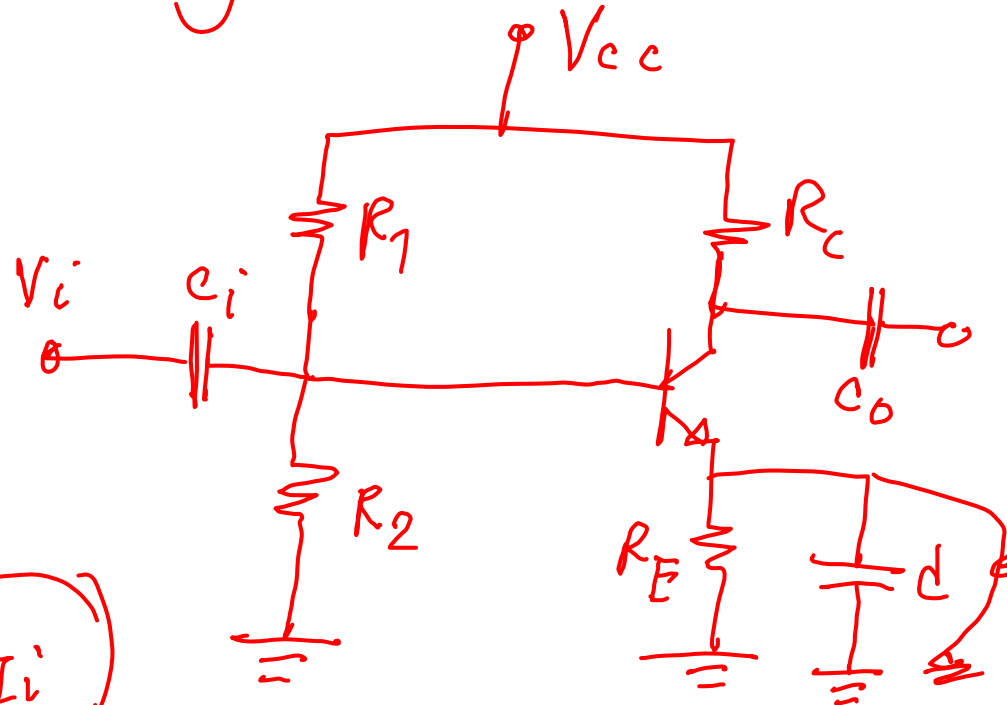
$$\beta r_o \gg 10 R_L \quad \text{and} \quad R_B \gg 10 \beta r_e \quad \Rightarrow \quad \gamma = 100\%$$

$$A_i = \frac{\beta \cancel{R_B} \cancel{r_o}}{\cancel{r_o} \cancel{R_B}} = \beta$$





# Voltage-Divider bias



$$Z_i = R_1 \parallel R_2 \parallel \beta r_e \quad \#$$

$$Z_o = r_o \parallel R_c$$

if  $r_o \gg R_c$  then  $Z_o = R_c$

$$V_o = -(R_c \parallel r_o) \beta I_b$$

$$I_b = \frac{V_i}{\beta r_e}$$

$$V_o = -(R_c \parallel r_o) \beta \left( \frac{V_i}{\beta r_e} \right) = \frac{(R_c \parallel r_o) \cdot V_i}{r_e}$$

$$A_v = \frac{V_o}{V_i} = - \frac{R_c \parallel r_o}{r_e} \quad \text{if } r_o \gg R_c \Rightarrow A_v = - \frac{R_c}{r_e} \quad \#$$

$$A_i \approx \frac{I_o}{I_i}$$

$$I_o = \frac{r_o \beta I_b}{r_o + R_c}$$

$$I_b = \frac{(R_1 \parallel R_2) I_i}{(R_1 \parallel R_2) + \beta r_e}$$

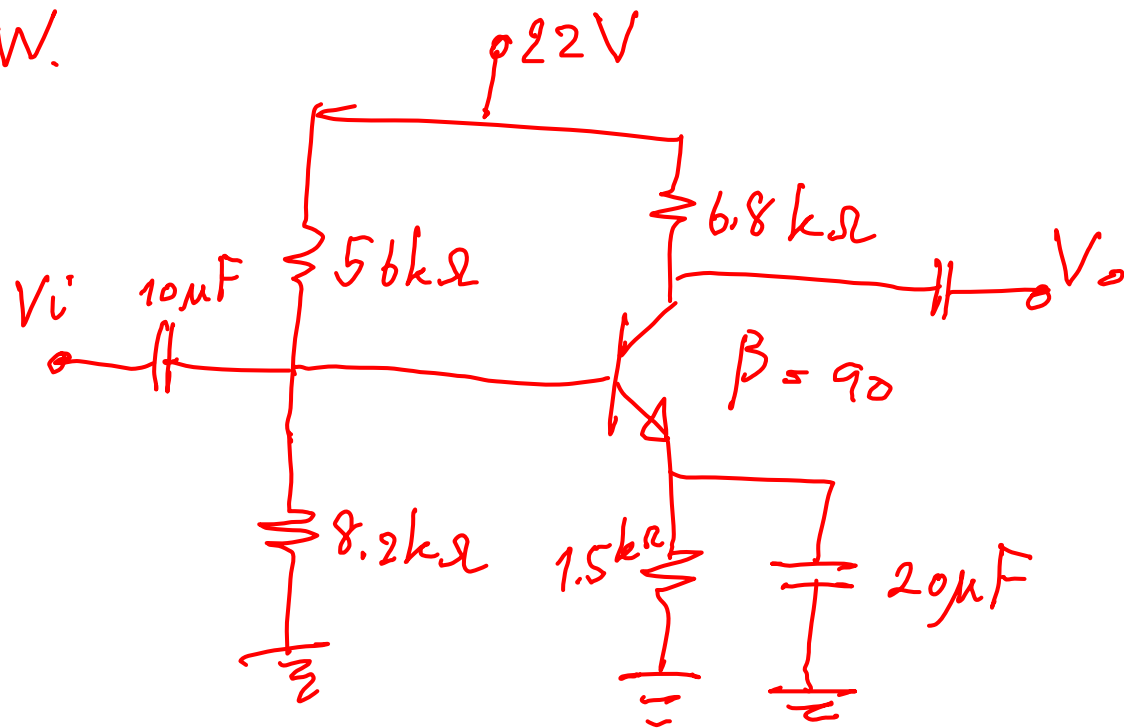
$$I_i = \frac{[(R_1 \parallel R_2) + \beta r_e] I_b}{(R_1 \parallel R_2)}$$

$$\beta r_o \gg r_o R_c \Rightarrow \beta r_o \approx r_o$$

$$A_i = \frac{\beta (R_1 \parallel R_2)}{(R_1 \parallel R_2) + \beta r_e}$$

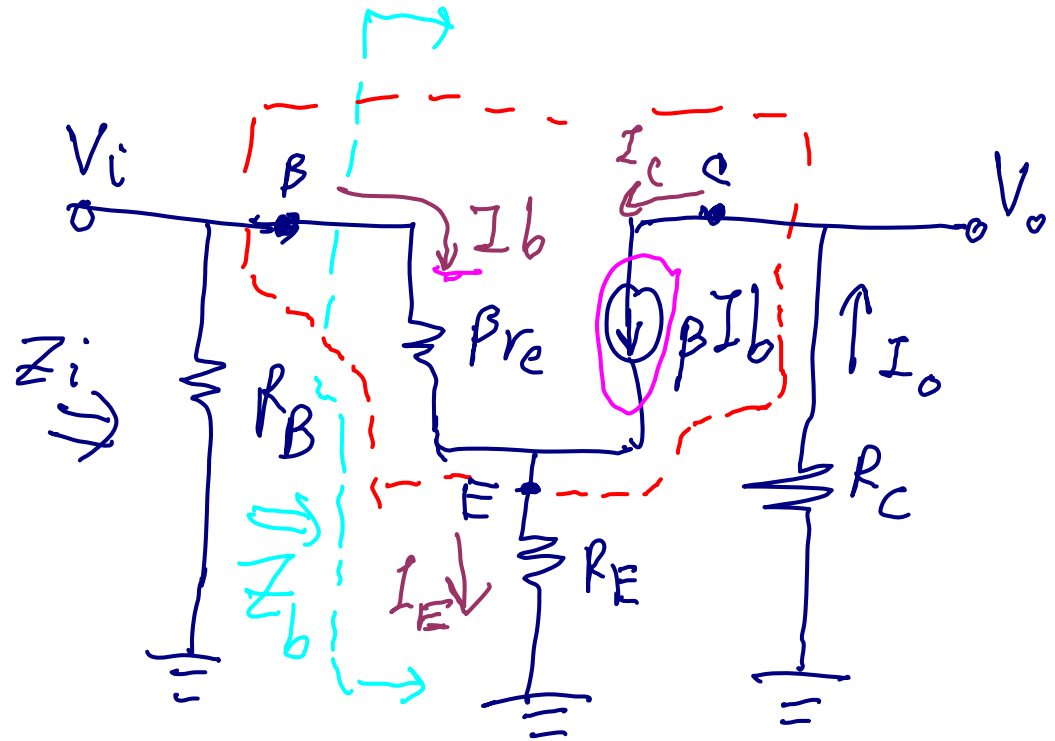
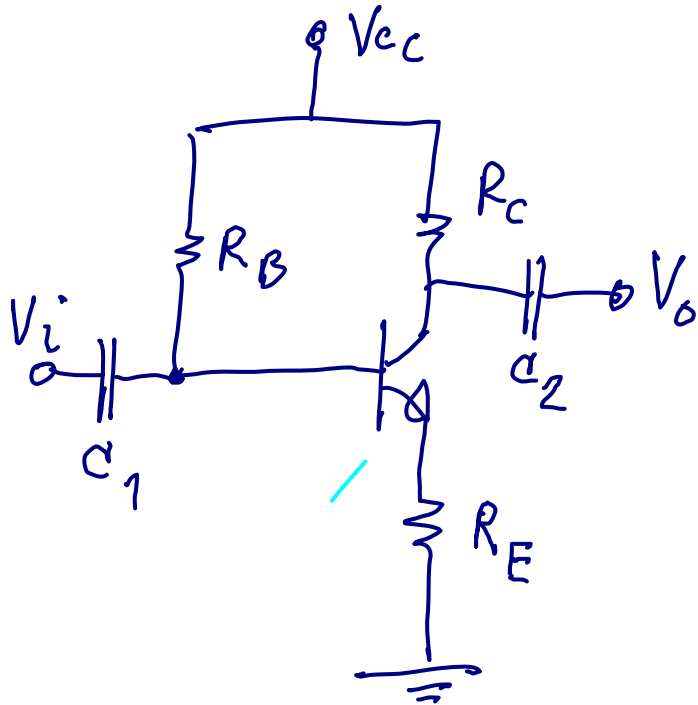
$$\therefore A_i = \frac{r_o \beta I_b}{r_o + R_c} \cdot \frac{(R_1 \parallel R_2)}{[(R_1 \parallel R_2) + \beta r_e] I_b} = \frac{r_o \beta (R_1 \parallel R_2)}{(r_o + R_c) [(R_1 \parallel R_2) + \beta r_e]}$$

H.W.



- W. a)  $r_e$  ( $7.15\text{ k}\Omega$ )  
 b)  $Z_i$  ( $1.35\text{ k}\Omega$ )  
 c)  $Z_o$  ( $r_o = \infty\text{ }\Omega$ ) ( $6.8\text{ k}\Omega$ )  
 d)  $A_v$  ( $r_o = \infty\text{ }\Omega$ ) ( $-367.97$ )  
 e)  $A_i$  ( $r_o = \infty\text{ }\Omega$ ) ( $73.04$ )

## CE EMITTER-BIAS



u z<sub>6</sub>

2507

$$V_{i5} = I_b \beta r_e + I_E R_E \rightarrow (\beta + 1) I_b$$

$$V_i = I_b \beta r_e + (\beta + 1) I_b R_E$$

$$V_i = \cancel{I_b} [\beta r_e + (\beta + 1) R_E]$$

$$Z_b = \frac{V_i}{I_b} = \frac{\cancel{I_b} [\beta r_e + (\beta + 1) R_E]}{\cancel{I_b}}$$

$$Z_b = \beta r_e + (\beta + 1) R_E$$

$$\text{if } (\beta + 1) \approx \beta$$

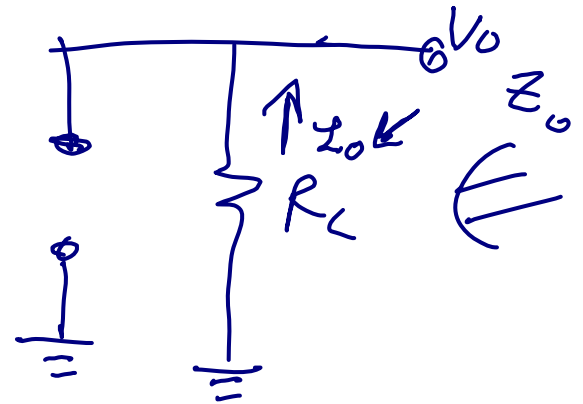
$$\therefore Z_b = \beta (r_e + R_E)$$

$$\text{if } R_E \gg r_e$$

$$\therefore \boxed{Z_b = \beta R_E}$$

$$\boxed{Z_i = Z_b \parallel R_B = \beta R_E \parallel R_B} \quad \#$$

$$\therefore Z_o = R_c \quad | \quad \text{open } \beta I_b$$



u1  $A_v$

$$V_o = -\beta I_b R_c$$

$$I_b = \frac{V_i}{Z_b} = \frac{V_i}{\beta R_E}$$

$$V_i = \beta R_E I_b$$

$$\therefore A_v = \frac{V_o}{V_i} = \frac{-\cancel{\beta I_b R_c}}{\cancel{\beta R_E I_b}} = -\frac{R_c}{R_E} \quad \#$$

$$A_i = \frac{I_o}{I_i}$$

$$I_o = \frac{-V_o}{R_c} = -\beta \frac{I_b R_c}{R_c} = -\beta I_b = -I_c$$

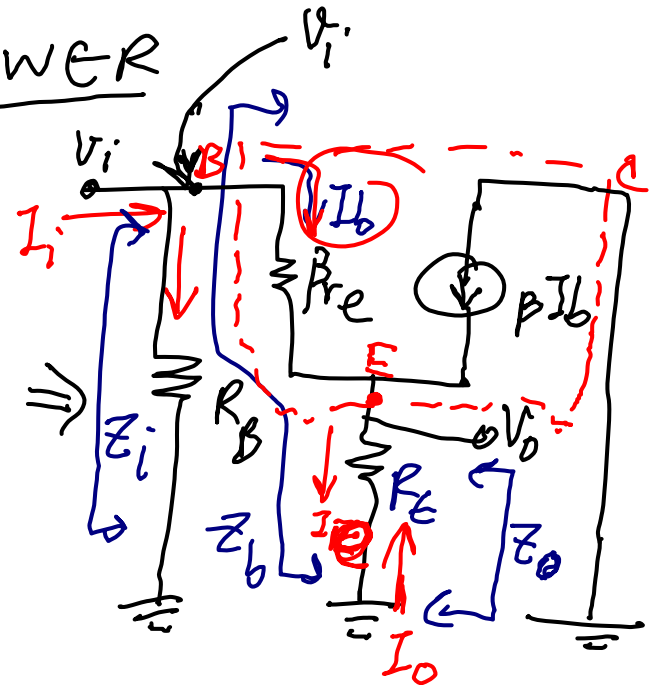
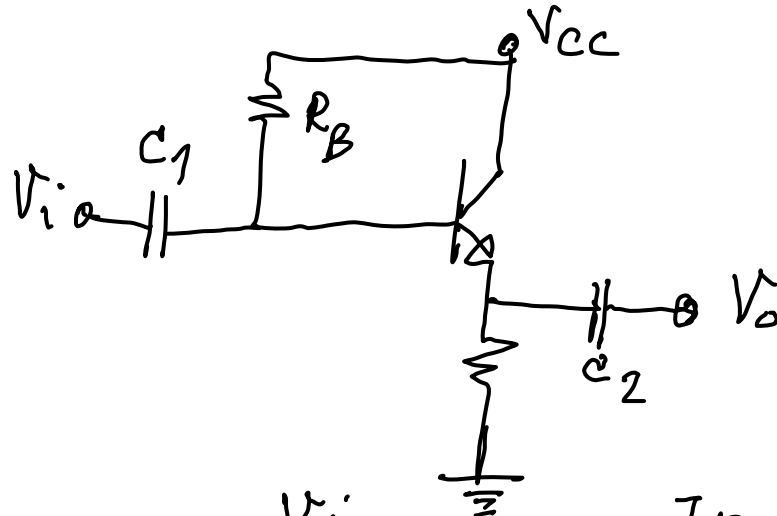
Then  $I_b = \frac{R_B I_i}{R_B + Z_b}$  (Current divider)

$$I_i = \frac{(R_B + Z_b) I_b}{R_B}$$

$$\therefore A_i = \frac{I_o}{I_i} = \frac{-\beta I_b}{(R_B + Z_b) I_b} \cdot R_B = \frac{-\beta R_B}{R_B + Z_b}$$



# EMITTER-FOLLOWER



$$Z_b = \frac{V_i}{I_b} = \frac{I_b r_e + I_b (\beta + 1) R_E}{I_b} = \boxed{\beta r_e + (\beta + 1) R_E} \approx \beta (r_e + R_E)$$

$$Z_i = R_B \parallel Z_b = R_B \parallel \beta (r_e + R_E)$$

$$Z_o = ?$$

$$\text{then } I_b = V_i / z_b \quad \text{---} (*)$$

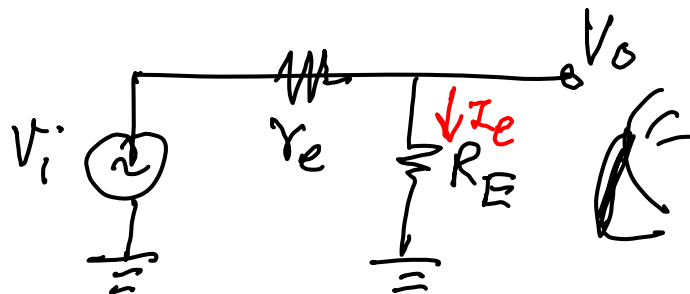
ถ้า  $(\beta+1)$  อนุพัทธ์  $(*)$  แล้ว  $V_o$

$$(\beta+1) I_b = (\beta+1) V_i / z_b$$

$$I_e = \frac{(\beta+1) V_i}{r_e + (\beta+1) R_E}$$

$$Q_{w}(\beta+1) \approx \beta$$

$$\text{so } I_e = \frac{V_i}{r_e + R_E}$$



ถ้า  $R_E \gg r_e$  หรือ

$$Z_o = r_e$$

$$Z_o = R_E \parallel r_e \quad V_i = 0$$

u)  $A_v$

$$V_o = \frac{R_E V_i}{R_E + r_e}$$

$$A_v = \frac{V_o}{V_i} = \frac{R_E}{R_E + r_e}$$

if  $R_E \gg r_e$  then  $A_v \approx 1$

$$A_v = \frac{R_E}{R_E} = 1$$

u)  $A_i$   $A_i = I_o / I_i$

$$I_b = \frac{R_B I_i}{R_B + Z_b}$$

$$I_i = \frac{I_b (R_B + Z_b)}{R_B}$$

$$I_o = -I_e = -(\beta + 1)I_b$$

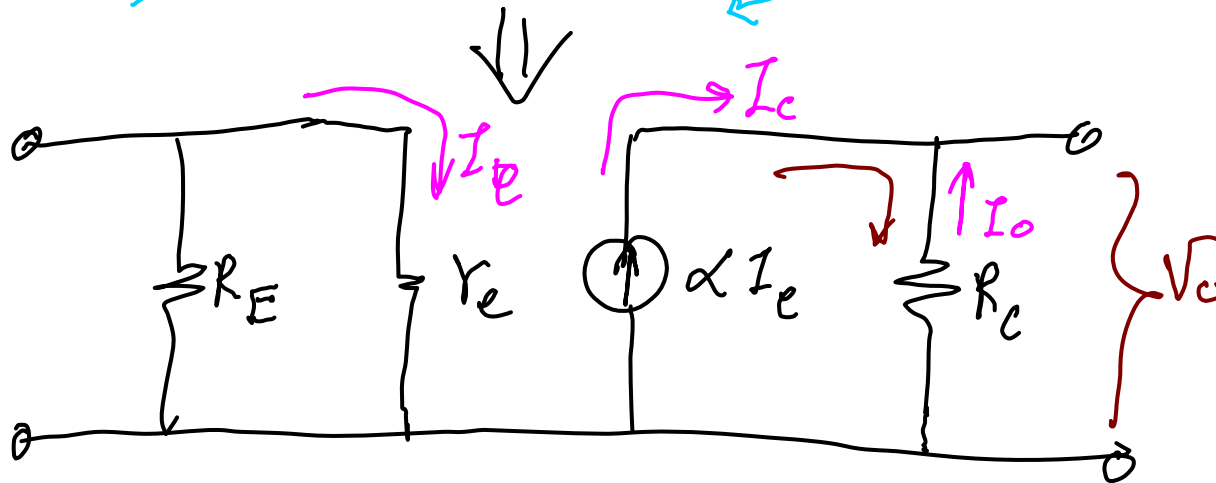
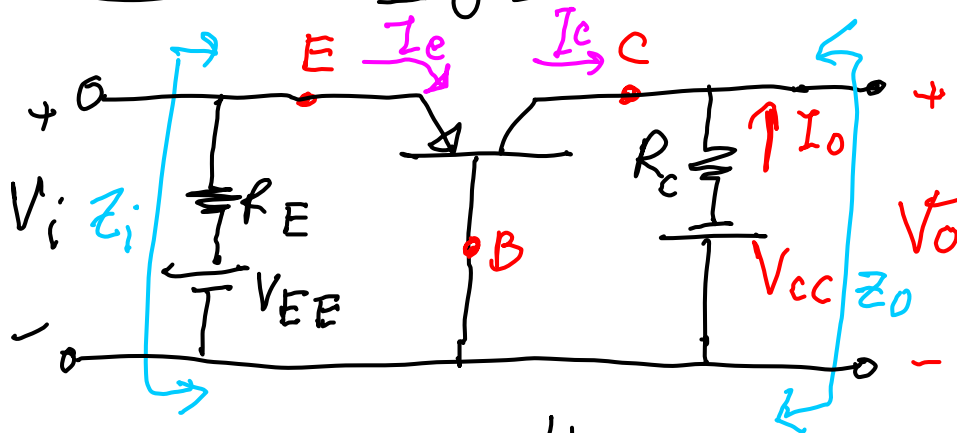
$$\therefore A_i = \frac{I_o}{I_i} = \frac{-(\beta + 1)I_b \cdot R_B}{(R_B + Z_b)I_b}$$

$$= \frac{-(\beta + 1)R_B}{R_B + Z_b}$$

$$\text{if } \beta \gg 1 \approx \beta$$

$$\therefore A_i = \frac{-\beta R_B}{R_B + Z_b}$$

# C-B configuration



$$Z_i = R_E \parallel r_e$$

$$Z_o = R_C$$

$$V_o = -I_o R_C = -(-I_c) R_C = \alpha I_e R_C$$

$$V_i = I_e r_e \rightarrow I_i$$

$$I_e = V_i / r_e$$

$$\text{Then } V_o = \alpha I_e R_c = \alpha \left( \frac{V_i}{r_e} \right) R_c$$

$$A_v = \frac{V_o}{V_i} = \alpha R_c / r_e$$

$\alpha \approx 1$

$$\therefore A_v = R_c / r_e \mid \alpha \approx 1$$

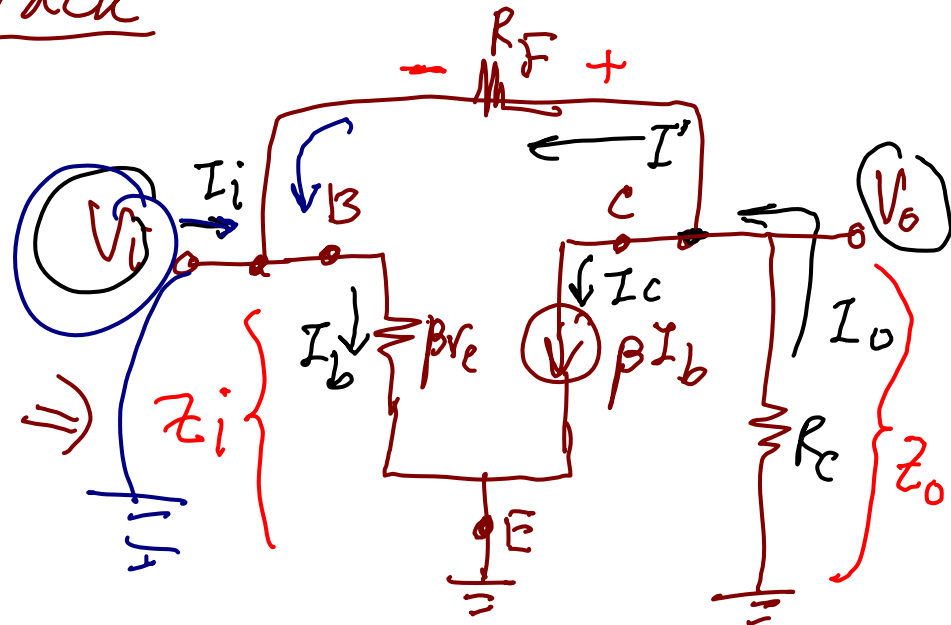
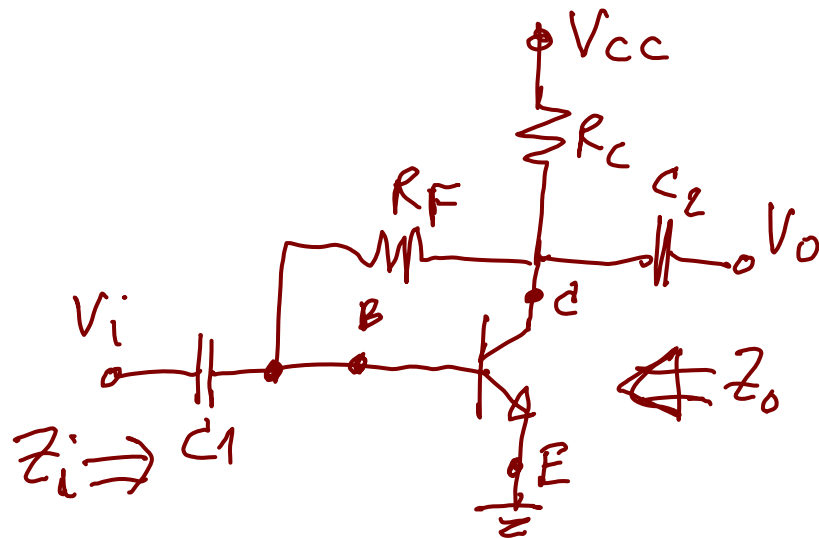
$$\text{Wt } A_i = \frac{I_o}{I_i}$$

$$\text{Then } I_o = -\alpha I_e = -\alpha I_i$$

$$A_i = \frac{I_o}{I_i} = -\alpha$$

$$A_i \approx -1$$

# Collector Feedback



$$I' = \frac{V_o - V_i}{R_F} \quad (1)$$

also  $V_o = -I_o R_c$

$$I_o = I' + \beta I_b$$

Since  $\beta I_b$  is much larger than  $I'$

$$I_o \approx \beta I_b$$

$$V_o = -\beta I_b R_c \quad \text{--- (2)}$$

$I_b = \frac{V_i'}{\beta r_e}$

Substituting (2)

$$V_o = -\beta \frac{V_i'}{\beta r_e} R_c \quad \text{--- (3)}$$

$$A_v = \frac{V_o}{V_i} = -\cancel{\beta} R_c / \cancel{\beta} r_e = -R_c / r_e$$

Substituting (3) into (1)

$$I' = \left( -\frac{V_i R_c}{r_e} - V_i \right) / R_F = \frac{-V_i}{R_F} \left( \frac{R_c}{r_e} + 1 \right)$$

$$\text{on } V_i = I_b \beta r_e$$

$$\text{Ans } I_b = I_i + I'$$

$$\therefore V_i = (I_i + I') \beta r_e = \left[ I_i + \overbrace{\left[ -\frac{V_i'}{R_F} \left( \frac{R_c}{r_e} + 1 \right) \right]}^{I'} \right] \beta r_e$$

$$(V_i) = I_i \beta r_e - \frac{V_i' \beta r_e (R_c + 1)}{R_F}$$

$$I_i \beta r_e = V_i + \frac{V_i' \beta r_e (R_c + 1)}{R_F}$$

$$I_i \beta r_e = V_i \left[ 1 + \frac{\beta r_e (R_c + 1)}{R_F} \right] = V_i \left[ \frac{R_F + \beta r_e (R_c + 1)}{R_F} \right]$$

$$Z_i = \frac{V_i}{I_i} = \frac{\beta r_e}{\left[ 1 + \left( \frac{\beta r_e}{R_F} \right) \left( \frac{R_c}{r_e} + 1 \right) \right]}$$



$$Z_i = \frac{V_i}{I_i} = \frac{\beta r_e R_F}{R_F + \beta(R_C + r_e)}$$

$$\text{if } R_C \gg r_e$$

$$\therefore Z_i = \frac{\beta r_e R_F}{R_F + \beta R_C}$$

u)  $Z_o$

$$Z_o = R_c \parallel R_F \big|_{V_i=0}$$

u)  $A_i$  9u<sup>2</sup> 95 kVL 9u Loop σπν2601ν0052]

$$V_i + V_{R_F} - V_o = 0$$

$$\text{αν } V_i = I_b \beta r_e$$

$$V_{R_F} = I' R_F = (I_b - I_i) R_F$$

$$V_o = -I_o R_c \approx -\beta I_b R_c$$

11m4  $V_i, V_{R_F}, V_o$  δι' οτ

$$I_b \beta r_e + (I_b - I_i) R_F + \beta I_b R_c = 0$$
$$I_b (\beta r_e + R_F + \beta R_c) = I_i R_F$$

thn  $I_0 = \beta I_b$  do đó  $I_b = \frac{I_0}{\beta}$

$$\frac{I_0}{\beta} (\beta r_e + R_F + \beta R_C) = I_i R_F$$

thn  $\beta \otimes$  tho 2 tho

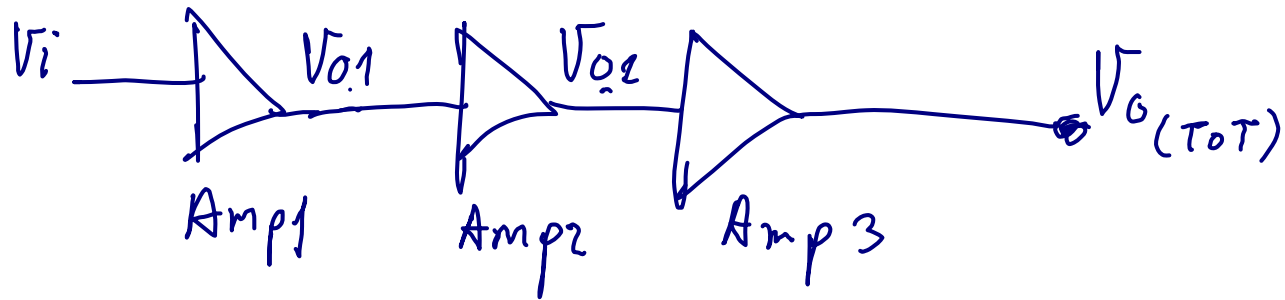
$$I_0 (\beta r_e + R_F + \beta R_C) = I_i \beta R_F$$

$$A_i = \frac{I_0}{I_i} = \frac{\beta R_F}{\beta r_e + R_F + \beta R_C}$$

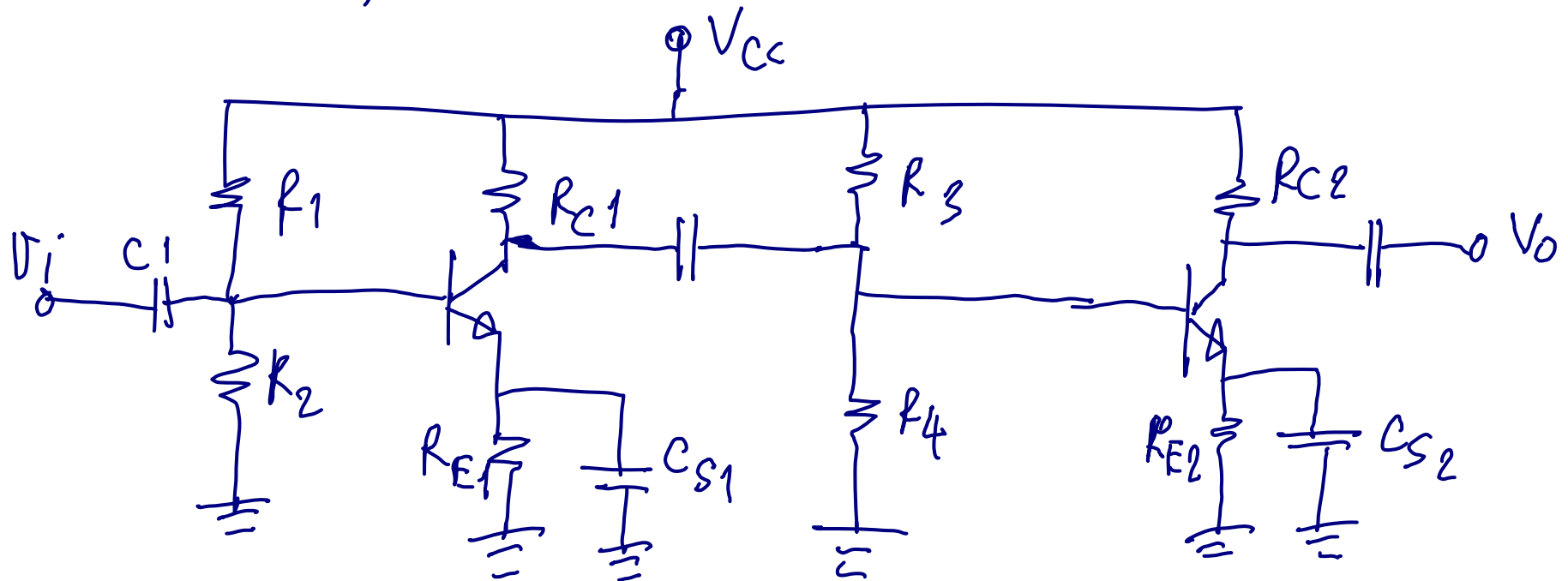
thn  $\beta r_e \leq R_F \leq \beta R_C$

$$A_i = \frac{\beta R_F}{\beta R_C} = R_F / R_C$$

# BJT cascade Amplifier



$$A_{V(tot)} = A_{V1} \times A_{V2} \times A_{V3}$$



$$Z_i = R_1 \parallel R_2 \parallel \beta r_e$$

$$Z_o = r_{o2} \parallel R_c$$

$$A_{v1} = \frac{R_{c1} \parallel R_3 \parallel R_4 \parallel \beta r_{e2}}{r_{e1}}$$

$$A_{v2} = \frac{R_{c2}}{r_{e2}}$$

$$\therefore A_v = A_{v1} \times A_{v2}$$

~~$$A_i \quad V_o = A_v \times V_i \quad \#$$~~