

Experiment 4: Diodes, LEDs, Photodetectors

Pre-Lab Worksheet

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Lab group: Tuesday 8-11 / Tuesday 5-8 / [Thursday 8-11](#) / Thursday 5-8

Before adding Cadence plots to your report, please **change the background color to white**:
Edit->Properties-> Click the black rectangle near the "Background" -> change to white.

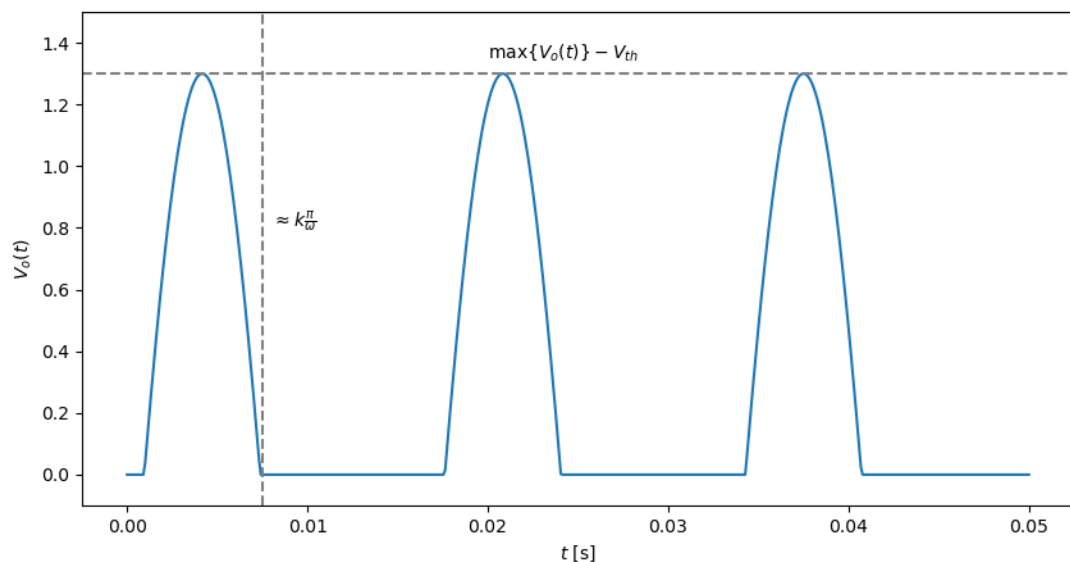
2. Pre-Lab

2.1. Intro to Diodes

Estimated threshold voltage for the 1N4148 diode from the datasheet [0.5 V](#)

2.2. Rectifiers

Attach a drawing/plot of the expected output of the half-bridge rectifier circuit for a sinusoidal input. Be sure to mark the amplitude and zero crossings on your axes (can be in terms of variables). Assume the sinusoid amplitude is larger than the threshold voltage.



2.3. LED transmitter

The supply voltage V_s for an LED current of 20mA: [3 V](#)

2.4. Receiver - DC

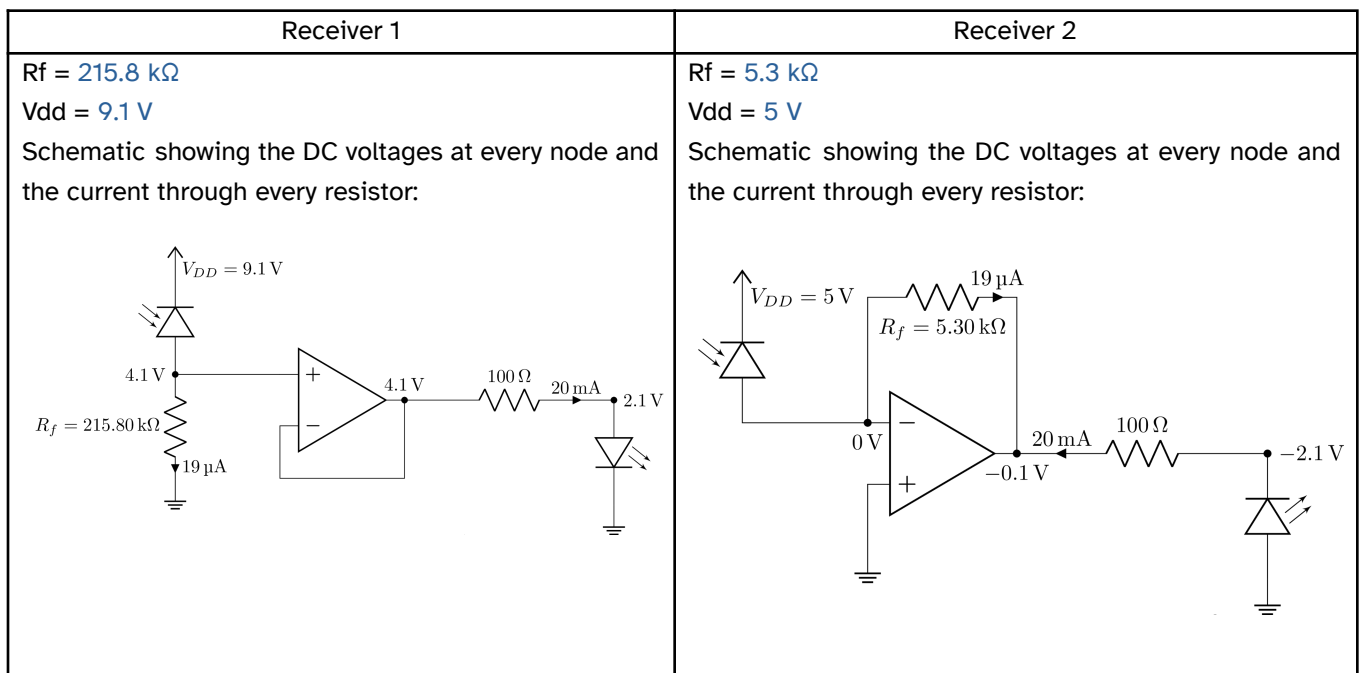
What is the expected reverse bias photo current for the TEFD4300 with an irradiance of $1000 \mu\text{W}/\text{cm}^2$? $19 \mu\text{A}$

Why do we need the amplifier in Receiver 1? Can we connect the photodiode directly to the indicator LED?

We need the amplifier in Receiver 1 since the LED will load the already small current from the photodiode. We cannot connect the photodiode directly for this reason.

Why is the indicator LED flipped in Receiver 2?

The indicator LED is flipped in Receiver 2 since the LED is now connected to the inverting input of the op amp.



From DC standpoint, can you see an advantage to one of the implementations?

Receiver 2 has the advantage of requiring half the supply voltage.

2.5. Receiver - AC, infinite speed opamp

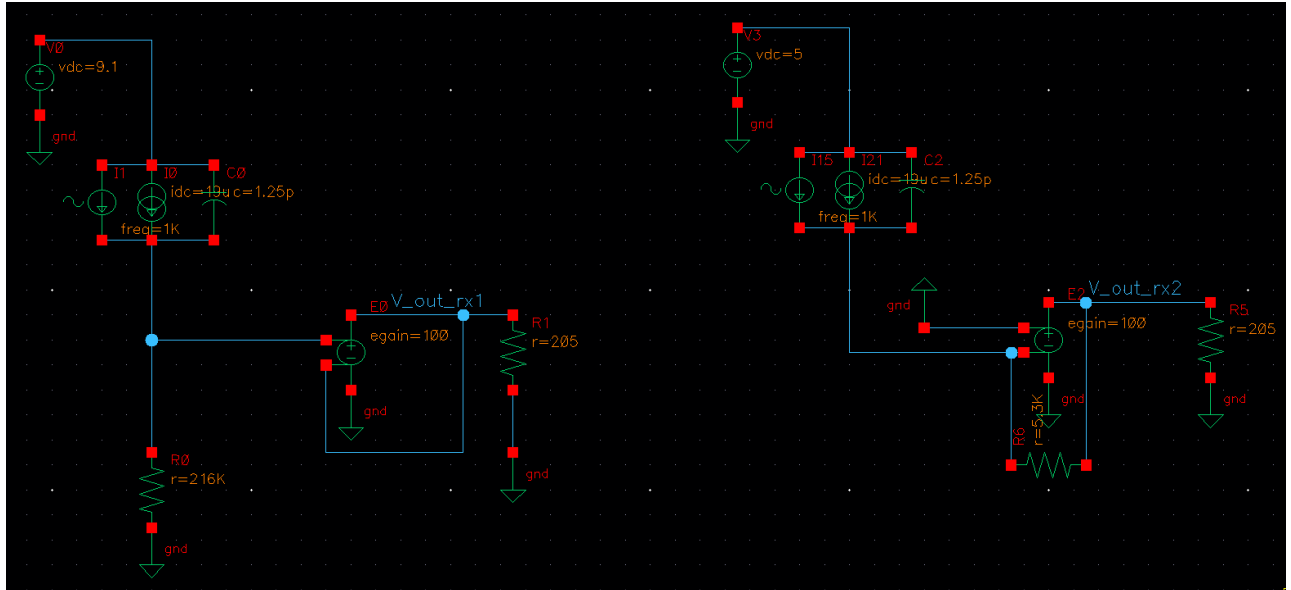
Parasitic Capacitance for the TEFD4300: 1.25 pF

The expected bandwidth (-3dB frequency) in each implementation?

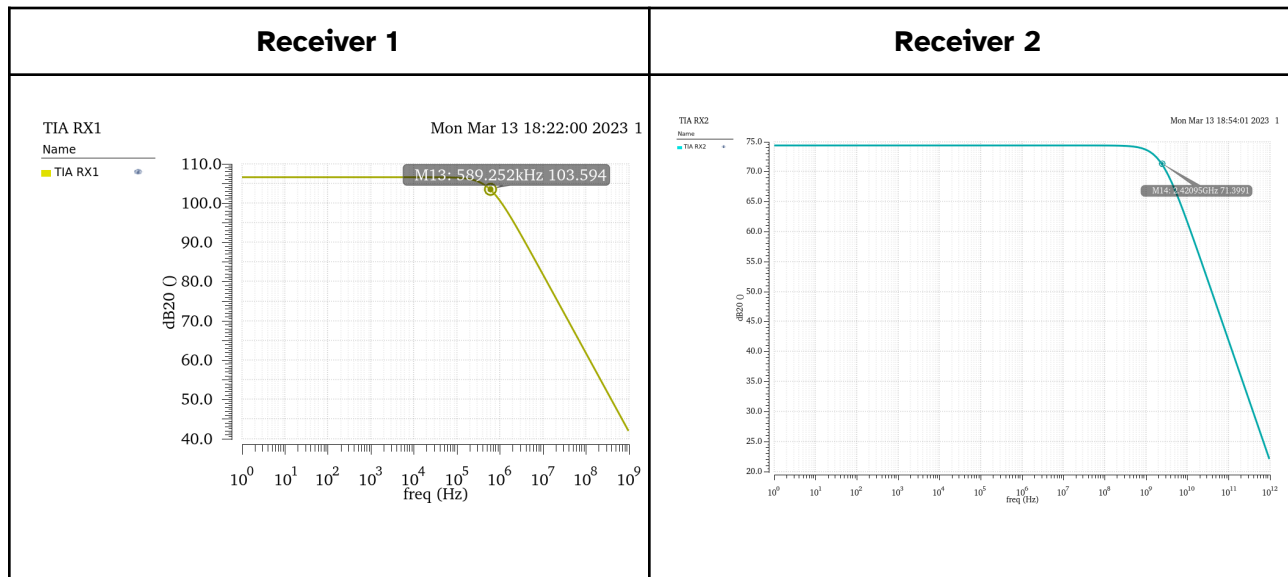
Receiver 1: 590 kHz

Receiver 2: 2.44 GHz

Cadence schematics:



Plots of the gain vs frequency:



Simulated bandwidth in each implementation: 589.252 kHz, 2.42 GHz

2.6. Receiver - AC, real opamp

Cadence simulation - open-loop opamp

Opamp low-frequency gain: 165 973

Opamp 3dB frequency: 5.18 Hz = 32.55 rad/s

Hand calculations

Receiver 1 transfer function:

$$\frac{V_{out}}{I_{in}} = \frac{A_0 R_f}{A_0 + 1} \frac{1}{1 + j \frac{\omega}{\omega_c (A_0 + 1)}} \frac{1}{1 + j \omega R_f C}$$

Receiver 1 3dB frequency: 590 kHz

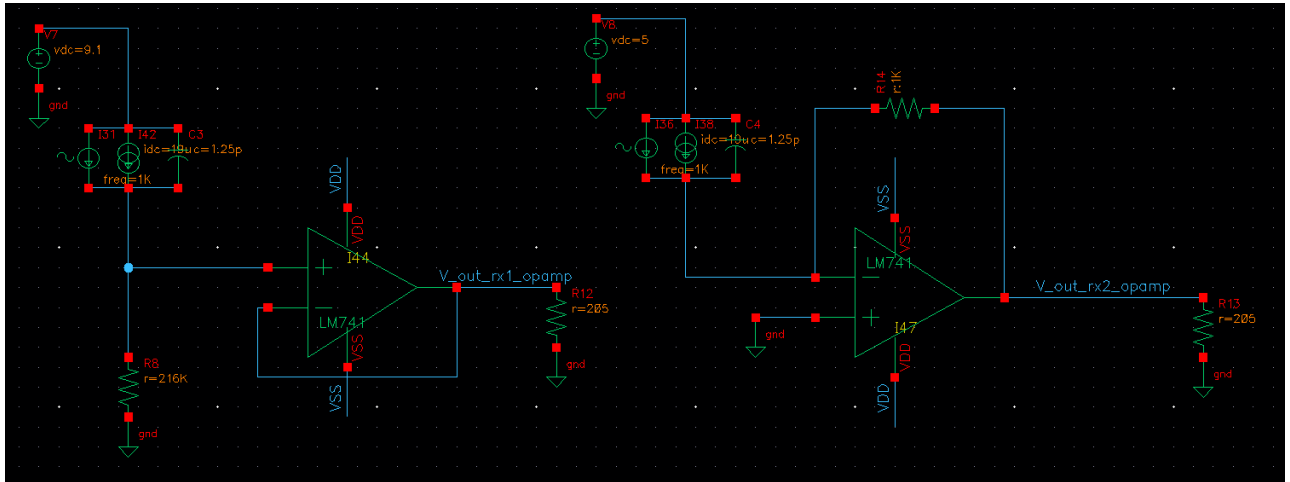
Receiver 2 transfer function:

$$\frac{V_{out}}{I_{in}} = \frac{-A_0 R_f}{A_0 + 1 + j\omega \left(\frac{1}{\omega_c} + R_f C \right) + (j\omega)^2 \frac{R_f C}{\omega_c}}$$

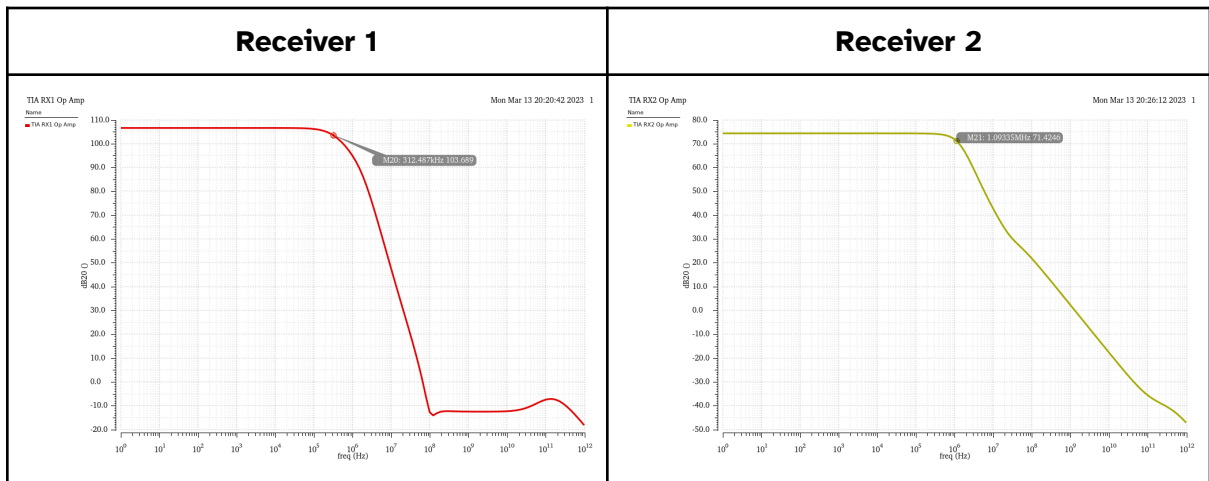
Receiver 2 3dB frequency: 0.894 MHz

Cadence simulation - receivers

Cadence schematics:



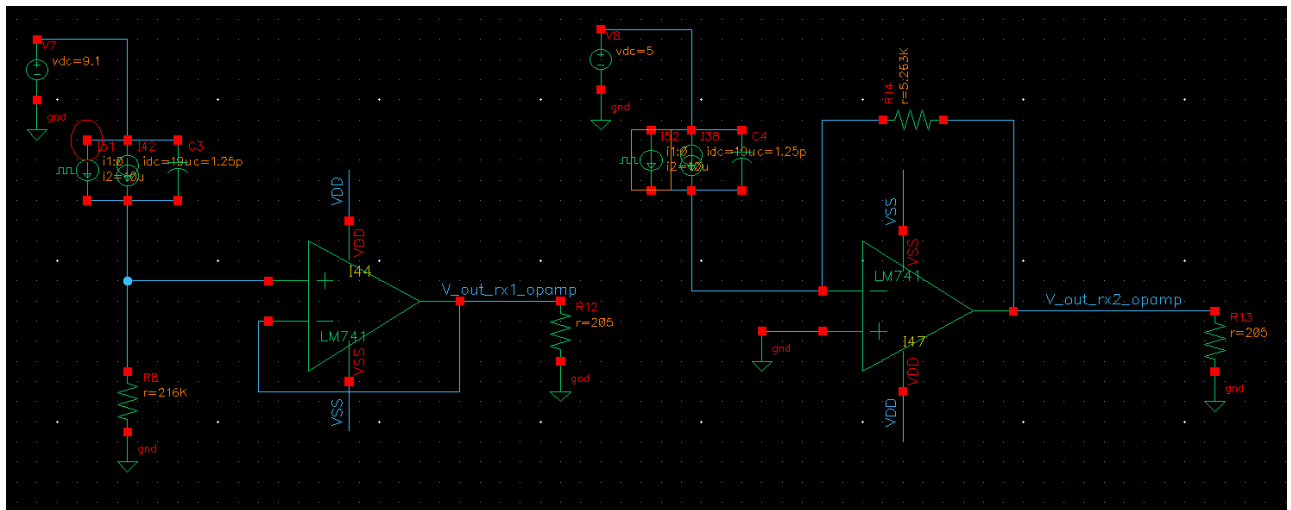
Plots of the gain vs frequency:



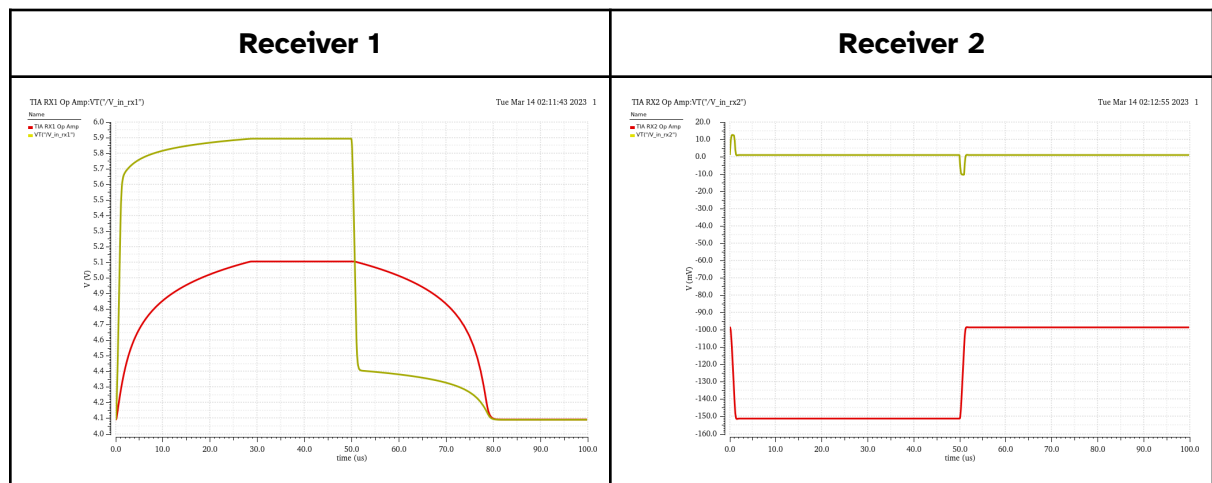
Simulated bandwidth in each implementation: 312.5 kHz, 1.09 MHz

2.7. Receiver - transient

Cadence schematics:



Plots of the transient voltage vs time at the photodiode output and at the amplifier output:



Explain the result. What is limiting the speed of the receiver in each implementation?

The first receiver roughly resembles a square wave, however there is a very large time constant with respect to the voltage output, resulting in a hump. It also does not reach unity, probably due to the filtering effect of the op amp.

In the second receiver, we have the output being reflected correctly, probably due to the higher cutoff frequency of the second receiver design. There is a slight slewing.

The speed of the receiver is limited by the frequency dependence of the op-amp, the internal capacitance of the photodiode, and the overall slewing effect of the op amp..