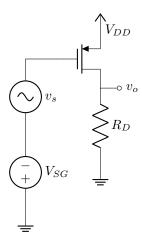
EE 105 HW 08

1

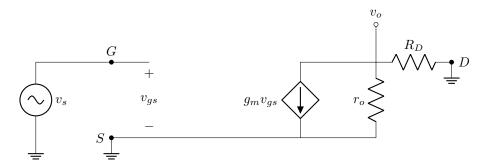


(a) We have that $V_{SG} - |V_{TP}| = V_0$ and that $\mu_0 C_{ox} \frac{W}{L} = k$. For the PMOS to be in saturation mode, we want

$$V_{SD} \leqslant V_0 = V_{DD} - I_D R_D \tag{1}$$

$$\implies R_D = \frac{V_{DD} - V_0}{I_D} = \frac{2(V_{DD} - V_0)}{kV_0^2} \tag{2}$$

(b) Converting to an NMOS common-source amplifier, the small-signal equivalent is



We then have

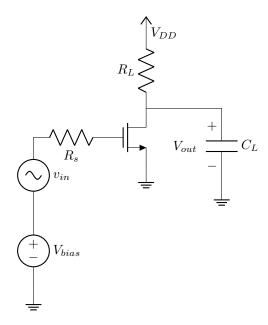
$$g_m v_s = \frac{-v_o}{r_o \parallel R_D} \tag{3}$$

$$g_m(r_0 \parallel R_D)v_s = -v_0 \tag{4}$$

$$g_m(r_0 \parallel R_D)v_s = -v_0 \tag{4}$$

$$\implies A = \frac{v_o}{v_s} = -g_m \frac{r_o R_D}{r_0 + R_D} \tag{5}$$

2



$$I_{DS} = k(V_{GS} - V_{TH})^2 (6)$$

$$V_{TH} = 0.65 \,\mathrm{V}$$
 (7)

$$k = 20 \,\mathrm{mA} \,\mathrm{V}^{-2}$$
 (8)

(a)

$$V_{DD} = 1.8 \,\mathrm{V} \tag{9}$$

$$R_s = 10 \,\mathrm{k}\Omega \tag{10}$$

$$R_L = 1 \,\mathrm{k}\Omega \tag{11}$$

$$C_L = 1 \,\mathrm{pF} \tag{12}$$

$$V_{bias} = 0.85 \,\mathrm{V} \tag{13}$$

At the DC operating point, we have $v_s = 0$, so we have

$$V_{GS} = V_{bias} = 0.85 \,\mathrm{V} \tag{14}$$

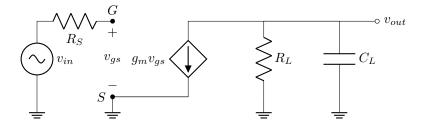
$$I_{DS} = k(V_{bias} - 0.65 \,\mathrm{V})^2 = 0.8 \,\mathrm{mA}$$
 (15)

$$V_{out} = V_{DD} - I_{DS}R_L = 1 \,\mathrm{V} \tag{16}$$

(b)

$$g_m = \frac{\partial I_{DS}}{\partial V_{GS}} = 2k(V_{GS} - V_{TH}) = 8 \,\text{mS}$$
(17)

(c) The small-signal model of the circuit is



The transfer function is

$$g_m v_{in} + \frac{v_{out}}{R_L} + sC_L v_{out} = 0 (18)$$

$$g_m v_{in} = -v_{out} \left(\frac{1}{R_L} + sC_L \right) \tag{19}$$

$$g_m v_{in} = -v_{out} \left(\frac{1}{R_L} + sC_L \right)$$

$$\implies \frac{v_{out}}{v_{in}} = -\frac{g_m R_L}{1 + sR_L C_L}$$
(20)

(d)

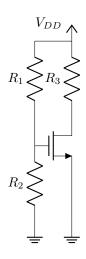
$$\lim_{\omega \to 0} |H(j\omega)| = g_m R_L = 8 \tag{21}$$

$$|H(j\omega)| = \frac{g_m R_L}{\sqrt{1 + (R_L C_L)^2}} \tag{22}$$

$$|H(j\omega)| = \frac{g_m R_L}{\sqrt{1 + (R_L C_L)^2}}$$

$$\implies \omega_c = \frac{g_m \mathcal{P}_L}{2\pi \mathcal{P}_L C_L} = 1.27 \,\text{GHz}$$
(22)

3



$$V_{DD} = 3.3 \,\mathrm{V} \tag{24}$$

$$R_1 = 2.3 \,\mathrm{k}\Omega \tag{25}$$

$$R_2 = 1.2 \,\mathrm{k}\Omega \tag{26}$$

$$R_3 = 1.2 \,\mathrm{k}\Omega \tag{27}$$

$$V_{TH} = 0.5 \,\mathrm{V}$$
 (28)

$$\lambda = 0 \, \mathrm{V}^{-1} \tag{29}$$

$$\mu_n C_{ox} = 2 \times 10^{-4} \,\mathrm{A} \,\mathrm{V}^2 \tag{30}$$

$$\frac{W}{L} = 20 \tag{31}$$

$$L = 0.5 \,\mu\text{m} \tag{32}$$

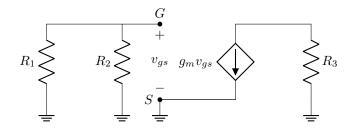
(a) The gate voltage forms a resistive divider, so we have $V_{GS} = 1.13 \,\text{V}$. Since $V_{GS} > V_{TH}$, the NMOS is either in the linear/triode or saturation region. We can test the saturation condition for an NMOS:

$$V_{DS} = V_{DD} - I_D R_D \geqslant V_{GS} - V_{TH} \tag{33}$$

$$\Rightarrow R_D \leqslant \frac{V_{DD} + V_{TH} - V_{GS}}{I_D} = \frac{2(V_{DD} + V_{TH} - V_{GS})}{\mu_n C_{ox} \frac{W}{L} (V_{GS} - V_{TH})^2} = 3.3 \,\text{k}\Omega > R_3$$
 (34)

Since the condition is satisfied, the NMOS is in saturation mode. Thus, $V_{DS} = V_{DD} - I_D R_D = 2.34 \,\text{V}$. This confirms the operating region.

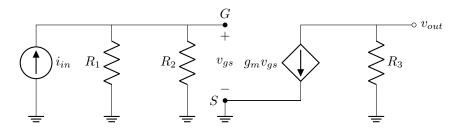
(b) Since $\lambda = 0 \,\mathrm{V}^{-1}$, there is no channel-length modulation, so $r_o = \infty$. The small-signal model is



We can find g_m as

$$g_m = \frac{\partial I_D}{\partial V_{DS}} = \mu_n C_{ox} \frac{W}{L} (V_{GS} - V_{TH}) = 2.52 \,\text{mS}$$
 (35)

(c) The small-signal model is now



We have the equation

$$-v_{out} = g_m i_{in}(R_1 \parallel R_2) R_3 \implies A = \frac{v_{out}}{i_{in}} = -g_m(R_1 \parallel R_2) R_3 = -2.39 \,\mathrm{k}\Omega \tag{36}$$

4

$$V_{GS} = 1 \text{ V}$$
 $V_{DS} = 1 \text{ V}$
 $V_{SB} = 0.2 \text{ V}$
 $V_{TN} = 0.5 \text{ V}$
 $W = 5 \text{ µm}$
 $L = 1 \text{ µm}$
 $t_{ox} = 10 \text{ nm}$
 $\epsilon_{ox} = 3.9\epsilon_0$
 $L_j = 2 \text{ µm}$
 $L_{ov} = 0.05 \text{ µm}$
 $C_{j0} = 1 \text{ mF m}^{-2}$
 $C_{j,sw0} = 4 \times 10^{-10} \text{ F m}^{-1}$
 $\phi_b = 1 \text{ V}$
 $C_{\text{fringe}} = 1 \text{ fF}$

$$C_{gs} = \frac{2}{3}WLC_{ox} + C_{ov} = \frac{2}{3}WL\frac{\epsilon_{ox}}{t_{ox}} + L_{ov}W\frac{\epsilon_{ox}}{t_{ox}} = 1.24 \times 10^{-14} \,\text{F}$$
(37)

$$C_{gd} = C_{ov} + C_{\text{fringe}} = L_{ov}WC_{ox} + C_{\text{fringe}} = 1.86 \times 10^{-15} \,\text{F}$$
 (38)

$$A_{d,j} = A_{s,j} = L_j W = 1 \times 10^{-11} \,\mathrm{m}^2$$
 (39)

$$P_{d,j} = P_{s,j} = 2L_j + W = 9 \,\mu\text{m} \tag{40}$$

$$C_{db} = \frac{C_{j0}}{\sqrt{1 + \frac{V_{DB}}{\phi_B}}} A_{d,j} + \frac{C_{j,sw0}}{\sqrt{1 + \frac{V_{DB}}{\phi_B}}} P_{d,j} = 1.01 \times 10^{-14} \,\text{F}$$
(41)

$$C_{sb} = \frac{C_{j0}}{\sqrt{1 + \frac{V_{SB}}{\phi_B}}} A_{s,j} + \frac{C_{j,sw0}}{\sqrt{1 + \frac{V_{SB}}{\phi_B}}} P_{s,j} = 1.24 \times 10^{-14} \,\text{F}$$
(42)