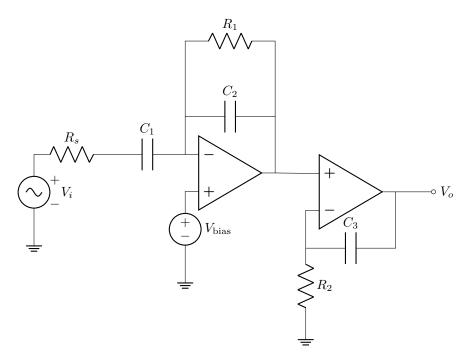
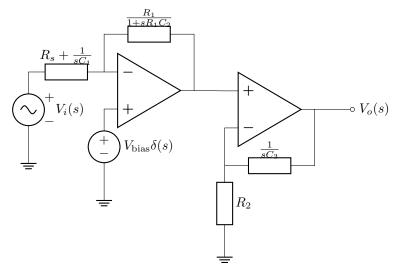
## EE 105 HW 05

1



In the s-domain,



Using superposition, we can derive the output of the first op-amp as

$$V_{x}(s) = -V_{i}(s) \frac{\frac{R_{1}}{1+sR_{1}C_{2}}}{\frac{1+sR_{s}C_{1}}{sC_{1}}} + V_{\text{bias}}\delta(s) \left(1 + \frac{\frac{R_{1}}{1+sR_{1}C_{2}}}{\frac{1+sR_{s}C_{1}}{sC_{1}}}\right)$$

$$= -V_{i}(s) \frac{sR_{1}C_{1}}{(1+sR_{1}C_{2})(1+sR_{s}C_{1})} + V_{\text{bias}}\delta(s) \left(1 + \frac{sR_{1}C_{1}}{(1+sR_{1}C_{2})(1+sR_{s}C_{1})}\right)$$
(2)

$$= -V_i(s) \frac{sR_1C_1}{(1 + sR_1C_2)(1 + sR_sC_1)} + V_{\text{bias}}\delta(s) \left(1 + \frac{sR_1C_1}{(1 + sR_1C_2)(1 + sR_sC_1)}\right)$$
(2)

We can then multiply by the second op-amp's transfer function to get

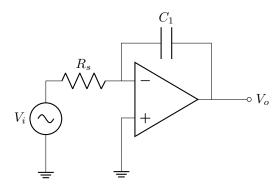
$$V_{o}(s) = V_{x} \left( 1 + \frac{1}{sR_{2}C_{3}} \right)$$

$$= \left( -V_{i}(s) \frac{sR_{1}C_{1}}{(1 + sR_{1}C_{2})(1 + sR_{s}C_{1})} + V_{\text{bias}} \delta(s) \left( 1 + \frac{sR_{1}C_{1}}{(1 + sR_{1}C_{2})(1 + sR_{s}C_{1})} \right) \right) \left( 1 + \frac{1}{sR_{2}C_{3}} \right)$$

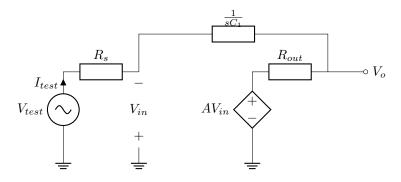
$$\Longrightarrow \frac{V_{o}(s)}{V_{i}(s)} = -\frac{sR_{1}C_{1}}{(1 + sR_{1}C_{2})(1 + sR_{s}C_{1})} \left( 1 + \frac{1}{sR_{2}C_{3}} \right)$$

$$(5)$$

 $\mathbf{2}$ 



- (a) Applying a test voltage at the input, the current through  $R_s$  is  $I_{test} = \frac{V_{test} V}{R_s}$ , where we use the ideality of the op amp to cancel out  $V^-$ . This means that  $Z_{test} = \frac{V_{test}}{I_{test}} = R_s$ . Applying a test voltage at the output, since we are applying a DC source, the voltage difference at the capacitor is 0 due to the virtual short, therefore we have  $Z_{out} = 0$ .
- (b) The circuit in the s-domain is now



We can create the loop equation

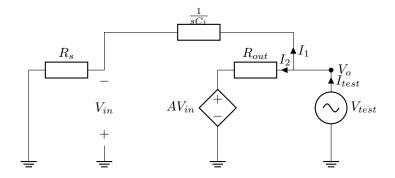
$$V_{test} - I_{test}R_s - I_{test}\frac{1}{sC_1} - I_{test}R_{out} + A(V_{test} - I_{test}R_s) = 0$$

$$\tag{6}$$

$$V_{test}(1+A) - I_{test}\left(R_s + \frac{1}{sC_1} - R_{out} - AR_s\right) = 0$$
 (7)

$$Z_{in} = \frac{V_{test}}{I_{test}} = \frac{R_s + \frac{1}{sC_1} - R_{out} - AR_s}{1 + A}$$
 (8)

For the output impedance, we can apply a test voltage at  $V_o$  and null  $V_i$  to get



We can obtain the node equations

$$I_{test} = \frac{V_{test} - AV_{in}}{R_{out}} + sC_1(V_{test} + V_{in})$$

$$\tag{9}$$

$$V_{in} = V_{test} - sR_sC_1(V_{test} + V_{in}) \tag{10}$$

$$\implies V_{in} = V_{test} \frac{1 - sR_sC_1}{1 + sR_sC_1} \tag{11}$$

$$I_{test} = V_{test} \left( \frac{1}{R_{out}} - \frac{A}{R_{out}} \frac{1 - sR_sC_1}{1 + sR_sC_1} + sC_1 \left( 1 + \frac{1 - sR_sC_1}{1 + sR_sC_1} \right) \right)$$
(12)

$$V_{in} = V_{test} - sR_sC_1(V_{test} + V_{in})$$

$$\Rightarrow V_{in} = V_{test} \frac{1 - sR_sC_1}{1 + sR_sC_1}$$

$$I_{test} = V_{test} \left(\frac{1}{R_{out}} - \frac{A}{R_{out}} \frac{1 - sR_sC_1}{1 + sR_sC_1} + sC_1\left(1 + \frac{1 - sR_sC_1}{1 + sR_sC_1}\right)\right)$$

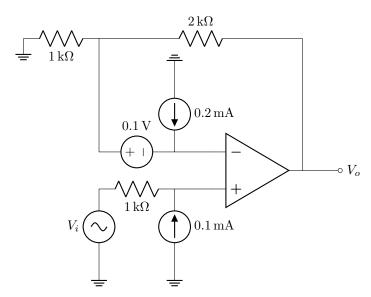
$$\Rightarrow \frac{1}{Z_{out}} = \left(\frac{1}{R_{out}} - \frac{A}{R_{out}} \frac{1 - sR_sC_1}{1 + sR_sC_1} + sC_1\left(1 + \frac{1 - sR_sC_1}{1 + sR_sC_1}\right)\right)$$

$$(13)$$

When  $A \to \infty$ , we have  $G_{out} = \infty \implies Z_{out} = 0$  and  $Z_{in} = R_s$ .

(c) The answer can be obtained similarly by substituting the constant gain A with the gain  $\frac{A}{1+j\frac{\omega}{\omega_0}}$ .

3



Slew rate:  $2 \,\mathrm{V} \,\mathrm{\mu s}^{-1}$ Signal:

$$x(t) = \begin{cases} 1 \text{ V} & 0 \le t \le 4 \text{ µs} \\ 0 & \text{elsewhere} \end{cases}$$
 (14)

We can define the node equations

$$0.2 \,\mathrm{mA} = \frac{V^{-} + 0.1 \,\mathrm{V} - V_{o}}{2 \,\mathrm{k}\Omega} + \frac{V^{-} + 0.1 \,\mathrm{k}\Omega}{1 \,\mathrm{k}\Omega} \tag{15}$$

$$V_i + (0.1 \,\mathrm{mA})(1 \,\mathrm{k}\Omega) = V^+$$
 (16)

$$V^+ = V^- \tag{17}$$

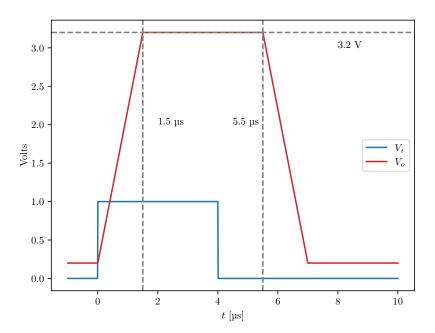
$$\implies 0.2 \,\mathrm{mA} = \frac{V_i + 0.1 \,\mathrm{V} + 0.1 \,\mathrm{V} - V_o}{2 \,\mathrm{k}\Omega} + \frac{V_i + 0.1 \,\mathrm{V} + 0.1 \,\mathrm{V}}{1 \,\mathrm{k}\Omega}$$

$$0.4 \,\mathrm{V} = V_i + 0.2 \,\mathrm{V} - V_o + 2V_i + 0.4 \,\mathrm{V}$$

$$(18)$$

$$0.4 V = V_i + 0.2 V - V_o + 2V_i + 0.4 V$$
(19)

$$\implies V_o = 3V_i + 0.2 \,\mathrm{V} \tag{20}$$



4

$$V_{cm} = \frac{V_1 + V_2}{2} \tag{21}$$

$$V_d = V_2 - V_1 (22)$$

$$V_{out} = A_{cm}V_{cm} + A_dV_d (23)$$

We can solve for  $V_1$  and  $V_2$  in terms of  $V_{cm}$  and  $V_d$  as

$$V_1 = V_{cm} - \frac{V_d}{2} \tag{24}$$

$$V_2 = V_{cm} + \frac{V_d}{2} \tag{25}$$

Then, we can find  $V_{out}$  as

$$V_{out} = -\frac{R_{0}^{10}}{R_{1}}V_{1} + \left(1 + \frac{R_{0}^{10}}{R_{1}}\right)^{10} \left(\frac{R_{4}}{R_{2} + R_{4}}\right)V_{2}$$
(26)

$$= -10V_1 + 11\left(1 + \frac{R_2}{R_4}\right)^{\frac{10}{11}} V_2 = -10V_1 + 10V_2$$

$$= -10\left(V_{em} - \frac{V_d}{2}\right) + 10\left(V_{em} + \frac{V_d}{2}\right) = 10V_d$$
(27)

$$= -10\left(V_{cm} - \frac{V_d}{2}\right) + 10\left(V_{cm} + \frac{V_d}{2}\right) = 10V_d \tag{28}$$

So  $A_{cm} = 0$  and  $A_d = 10$ .