OpenCMISS-iron examples and tests used by OpenCMISS developers at University of Stuttgart, Germany

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CONTENTS

1	Introduction				
	1.1	Cmgu	ii files for cmgui-2.9	_	
	1.2		ions to consider	_	
	1.3	Folder	r structure	5	
2	Hov	v to wo	ork on this document		
3	Unt	il Frida	V		
4			tely after Friday		
5		g-term	•		
6	Diffusion equation				
	6.1				
	6.2 Example-0001 [VALIDATED]				
		6.2.1		8	
		6.2.2	Mathematical model - 3D	8	
		6.2.3		8	
		6.2.4	Result summary	g	
	· · · · · · · · · · · · · · · · · · ·		ple-ooo1-u [VALIDATED]	12	
		6.3.1	Mathematical model - 2D	12	
		6.3.2	Mathematical model - 3D	12	
		6.3.3	Computational model	12	
		6.3.4	Result summary	13	
	6.4	ple-0002 [VALIDATED]	16		
		6.4.1	Mathematical model - 2D	16	
		6.4.2	Mathematical model - 3D	16	

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		6.4.3	Computational model	16
		6.4.4	Result summary	17
	6.5	Exam	ple-ooo3 [COMPILES]	20
		6.5.1	Mathematical model - 2D	20
		6.5.2	Mathematical model - 3D	20
		6.5.3	Computational model	20
		6.5.4	Result summary	21
	6.6	Exam	ple-0004 [VALIDATED]	24
		6.6.1	Mathematical model - 2D	24
		6.6.2	Computational model	24
		6.6.3	Result summary	24
	6.7		ple-0011 [RUNS]	26
	- 7	6.7.1	Mathematical model - 2D	26
		6.7.2	Mathematical model - 3D	26
		6.7.3	Computational model	26
		6.7.4	Result summary	27
_	Lino	ar elas	·	
7			•	30
	7.1		ion in general form	30
	7.2	_	ple-0101 [PLAUSIBLE]	31
		7.2.1	Mathematical model	31
		7.2.2	Computational model	31
		7.2.3	Results	32
		7.2.4	Validation	32
	7.3	Exam	ple-o102 [PLAUSIBLE]	35
		7.3.1	Mathematical model	35
		7.3.2	Computational model	35
		7.3.3	Results	36
		7.3.4	Validation	36
8	Finit	te elasti	icity	39
9	Nav	ier-Stol	kes flow	40
	•		ion in general form	40
	9.2	-	ple-o302-u [COMPILES]	41
	<i>J</i>	9.2.1	Mathematical model - 2D	41
		9.2.2	Mathematical model - 3D	41
		9.2.3	Computational model	41
			Result summary	
10	Mon	9. 2.4 10doma		42
				43
11	Cell	ML mo	odel	44
LI	ST	OF FI	IGURES	
	-			
Fig	gure 1	Ĺ	2D results, iron reference w/ command line argu-	
	,		ments [2.0 1.0 0.0 8 4 0 1 0]	9
Fig	gure 2	,	2D results, current run w/ command line arguments	9
- 18	5 arc 2	_	[2.0 1.0 0.0 8 4 0 1 0]	10
Figure 3		,		10
		•	3D results, iron reference w/ command line arguments [2, 2, 1, 2, 1, 2, 2, 4, 4, 4, 4]	40
T/2	~		ments [2.0 1.0 1.0 8 4 4 1 0]	10
Г18	gure 2	}	3D results, current run w/ command line arguments	
г.		_	[2.0 1.0 1.0 8 4 4 1 0]	11
F18	gure 5	5	2D results, iron reference w/ command line argu-	
			ments [2.0 1.0 0.0 8 4 0 1 0]	14

36

36

LIST OF TABLES

Figure 6

Figure 7

Figure 8

Figure 9

Figure 10

Figure 11

Figure 12

Figure 13

Figure 14

Figure 15

Figure 16

Figure 17

Figure 18

Figure 19

Figure 20

Figure 21

Figure 22

Figure 23

Figure 24

Figure 25

Figure 26

Figure 27

Figure 28

Figure 29

Figure 30

Table 1	Initials of people working on examples, in alphabeti-	
	cal order (surnames)	5
Table 2	Quantiative error between Abaqus 2017 and iron sim-	
	ulations for linear elastic uniaxial extenions	33
Table 3	Quantiative error between Abaqus 2017 and iron sim-	
2	ulations for linear elastic shear	38

Results, Abaqus 2D fine mesh.

INTRODUCTION 1

This document contains information about examples used for testing OpenCMISSiron. Read: How-to¹ and [1].

- Cmgui files for cmgui-2.9
- Variations to consider
 - Geometry and topology

1D, 2D, 3D

Length, width, height

Number of elements

Interpolation order

Generated or user meshes

quad/hex or tri/tet meshes

- Initial conditions
- Load cases

Dirichlet BC

Neumann BC

Volume force

Mix of previous items

- Sources, sinks
- Time dependence

Static

Quasi-static

Dynamic

Material laws

Linear

Nonlinear (Mooney-Rivlin, Neo-Hookean, Ogden, etc.)

Active (Stress, strain)

- Material parameters, anisotropy
- Solver

Direct

Iterative

Test cases

Numerical reference data

Analytical solution

• A mix of previous items

¹ https://bitbucket.org/hessenthaler/opencmiss-howto

1.3 Folder structure

TBD..

HOW TO WORK ON THIS DOCUMENT

In the Google Doc at https://docs.google.com/spreadsheets/d/1RGKj8vVPqQ-PH0UwMX_ e9TAzqaYavKi0z0D4pKY9RGI/edit#gid=0 please indicate what you are working on or if a given example was finished

• no mark: to be done

• x: currently working on it

xx: done

Initials	Full name	
СВ	Christian Bleiler	
AH	Andreas Hessenthaler	
TK	Thomas Klotz	
AK	Aaron Krämer	
BM	Benjamin Maier	
SM	Sergio Morales	
MM	Mylena Mordhorst	
HS	Harry Saini	

Table 1: Initials of people working on examples, in alphabetical order (surnames).

UNTIL FRIDAY 3

- Finish open examples
- Set a TAG for each example in document title:

DOCUMENTED: finish the documentation of the example (spatial domain, number of time steps, boundary conditions, etc.

COMPILES: example compiles (for default parameters)

RUNS: example runs (for default parameters)

CONVERGES: no convergence issues (for default parameters, results not plausible)

PLAUSIBLE: results look sensible (for default parameters)

VALIDATED: for all parameter sets it gives the correct results as compared to CHeart/Abaqus/analytical solution (includes visualisation scripts, run scripts, comparison scripts, documentation!, ...)

Move progress Google-document into PDF-document

Make from top directory - ensure all run_example.sh scripts are working as intended

IMMEDIATELY AFTER FRIDAY 4

- Move tags CONVERGE, PLAUSIBLE to VALIDATED
- Add GitHub issue for all tests/tags; VALIDATED means issue closed, else issue open
- Everybody runs everything!
- Meeting with Oliver
- Meeting with Auckland

5 LONG-TERM

- SMALL/BIG/PARALLEL targets
- Add more examples/those which were on the agenda but not started
- Jenkins

test SMALL/BIG/PARALLEL targets

integrate with GitHub (pull-requests triggers Jenkins, merge on success)

6 DIFFUSION EQUATION

6.1 Equation in general form

The governing equation is,

$$\partial_t \mathbf{u} + \nabla \cdot [\boldsymbol{\sigma} \nabla \mathbf{u}] = \mathbf{f}, \tag{1}$$

with conductivity tensor $\boldsymbol{\sigma}.$ The conductivity tensor is,

- defined in material coordinates (fibre direction),
- diagonal,
- defined per element.

Example uses generated regular meshes and solves a static problem, i.e., applies the boundary conditions in one step.

6.2.1 Mathematical model - 2D

We solve the following scalar equation,

$$\nabla \cdot \nabla u = 0 \qquad \qquad \Omega = [0, 2] \times [0, 1], \tag{2}$$

with boundary conditions

$$u = 0 x = y = 0, (3)$$

$$u = 1$$
 $x = 2, y = 1.$ (4)

No material parameters to specify.

6.2.2 Mathematical model - 3D

We solve the following scalar equation,

$$\nabla \cdot \nabla \mathbf{u} = 0 \qquad \qquad \Omega = [0, 2] \times [0, 1] \times [0, 1], \tag{5}$$

with boundary conditions

$$u = 0 \qquad \qquad x = y = z = 0, \tag{6}$$

$$u = 1$$
 $x = 2, y = z = 1.$ (7)

No material parameters to specify.

6.2.3 Computational model

• Commandline arguments are:

float: length along x-direction float: length along y-direction

float: length along z-direction (set to zero for 2D)

integer: number of elements in x-direction integer: number of elements in y-direction

integer: number of elements in z-direction (set to zero for 2D)

interger: interpolation order (1: linear; 2: quadratic)

integer: solver type (o: direct; 1: iterative)

• Commandline arguments for tests are:

2.0 1.0 0.0 2 1 0 1 0

2.0 1.0 0.0 4 2 0 1 0

2.0 1.0 0.0 8 4 0 1 0

2.0 1.0 0.0 2 1 0 2 0

2.0 1.0 0.0 4 2 0 2 0

2.0 1.0 0.0 8 4 0 2 0

2.0 1.0 0.0 2 1 0 1 1

2.0 1.0 0.0 4 2 0 1 1

6.2.4 Result summary

We use CHeart rev. 6292 to produce numerical reference solutions.

Passed tests: 24 / 24

No failed tests.

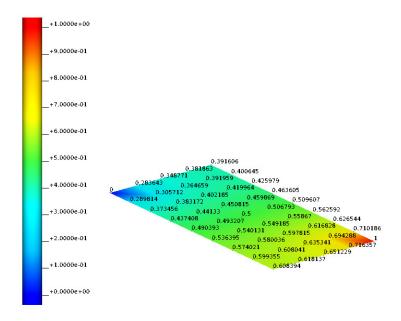


Figure 1: 2D results, iron reference w/ command line arguments [2.0 1.0 0.0 8 4 0 1 0].

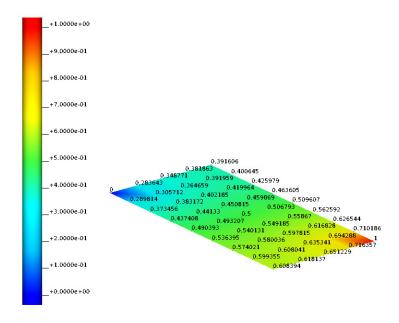


Figure 2: 2D results, current run w/ command line arguments [2.0 1.0 0.0 8 4 0 1 0].

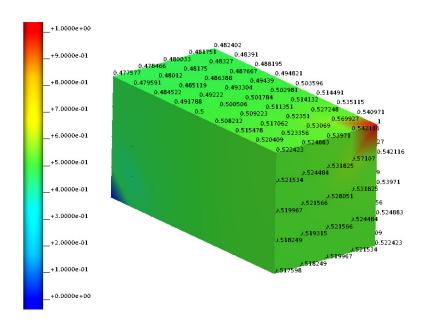


Figure 3: 3D results, iron reference w/ command line arguments [2.0 1.0 1.0 8 4 4 1 o].

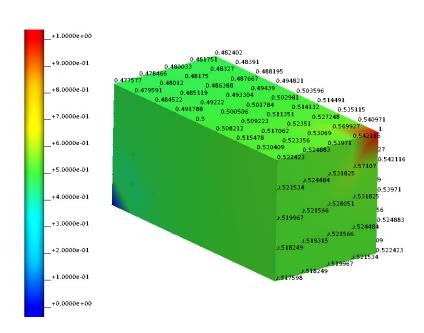


Figure 4: 3D results, current run w/ command line arguments [2.0 1.0 1.0 8 4 4 1 0].

6.3 Example-0001-u [VALIDATED]

Example uses user-defined regular meshes in CHeart mesh format and solves a static problem, i.e., applies the boundary conditions in one step.

6.3.1 Mathematical model - 2D

We solve the following scalar equation,

$$\nabla \cdot \nabla \mathbf{u} = 0 \qquad \qquad \Omega = [0, 2] \times [0, 1], \tag{8}$$

with boundary conditions

$$u = 0 x = y = 0, (9)$$

$$u = 1$$
 $x = 2, y = 1.$ (10)

No material parameters to specify.

6.3.2 Mathematical model - 3D

We solve the following scalar equation,

$$\nabla \cdot \nabla u = 0 \qquad \qquad \Omega = [0, 2] \times [0, 1] \times [0, 1], \tag{11}$$

with boundary conditions

$$u = 0 \qquad \qquad x = y = z = 0, \tag{12}$$

$$u = 1$$
 $x = 2, y = z = 1.$ (13)

No material parameters to specify.

6.3.3 Computational model

• Commandline arguments are:

float: length along x-direction float: length along y-direction

float: length along z-direction (set to zero for 2D)

integer: number of elements in x-direction integer: number of elements in y-direction

integer: number of elements in z-direction (set to zero for 2D)

interger: interpolation order (1: linear; 2: quadratic)

integer: solver type (o: direct; 1: iterative)

Commandline arguments for tests are:

2.0 1.0 0.0 2 1 0 1 0

2.0 1.0 0.0 4 2 0 1 0

2.0 1.0 0.0 8 4 0 1 0

2.0 1.0 0.0 2 1 0 2 0

2.0 1.0 0.0 4 2 0 2 0

2.0 1.0 0.0 8 4 0 2 0

2.0 1.0 0.0 2 1 0 1 1

2.0 1.0 0.0 4 2 0 1 1

```
2.0 1.0 0.0 8 4 0 1 1
2.0 1.0 0.0 2 1 0 2 1
2.0 1.0 0.0 4 2 0 2 1
2.0 1.0 0.0 8 4 0 2 1
2.0 1.0 1.0 2 1 1 1 0
2.0 1.0 1.0 4 2 2 1 0
2.0 1.0 1.0 8 4 4 1 0
2.0 1.0 1.0 2 1 1 2 0
2.0 1.0 1.0 4 2 2 2 0
2.0 1.0 1.0 8 4 4 2 0
2.0 1.0 1.0 2 1 1 1 1
2.0 1.0 1.0 4 2 2 1 1
2.0 1.0 1.0 8 4 4 1 1
2.0 1.0 1.0 2 1 1 2 1
2.0 1.0 1.0 4 2 2 2 1
2.0 1.0 1.0 8 4 4 2 1
```

• Note: Binary uses command line arguments to search for the relevant mesh files.

6.3.4 Result summary

We use CHeart rev. 6292 to produce numerical reference solutions.

Passed tests: 24 / 24

No failed tests.

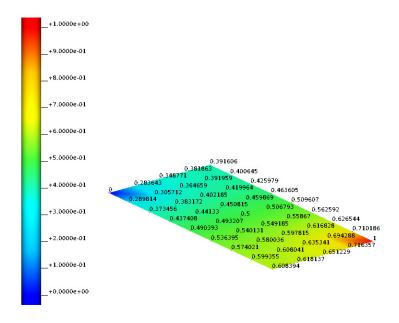


Figure 5: 2D results, iron reference w/ command line arguments [2.0 1.0 0.0 8 4 0 1

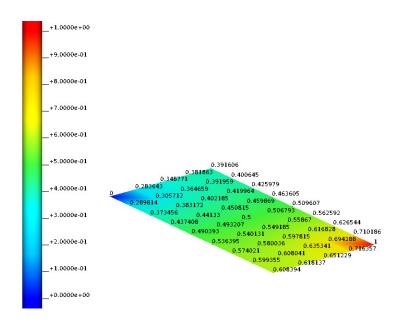


Figure 6: 2D results, current run w/ command line arguments [2.0 1.0 0.0 8 4 0 1 0].

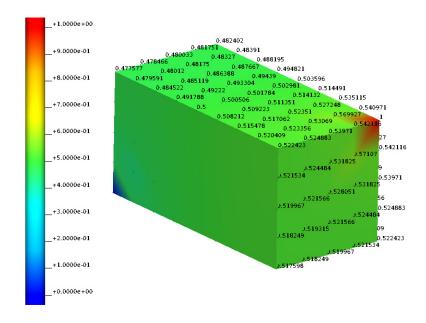


Figure 7: 3D results, iron reference w/ command line arguments [2.0 1.0 1.0 8 4 4 1

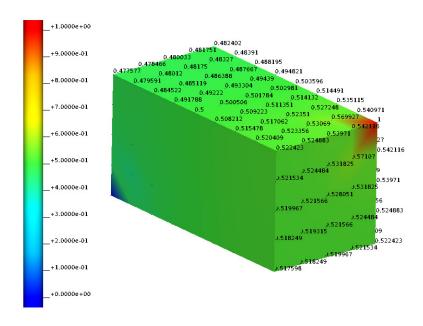


Figure 8: 3D results, current run w/ command line arguments [2.0 1.0 1.0 8 4 4 1 0].

Example uses generated regular meshes and solves a static problem, i.e., applies the boundary conditions in one step.

6.4.1 Mathematical model - 2D

We solve the following scalar equation,

$$\nabla \cdot \nabla \mathbf{u} = \mathbf{0} \qquad \qquad \Omega = [0, 2] \times [0, 1], \tag{14}$$

with boundary conditions

$$u = 15y$$
 $x = 0$, (15)

$$u = 15y$$
 $x = 0,$ (15) $u = 25 - 18y$ $x = 2.$ (16)

No material parameters to specify.

6.4.2 Mathematical model - 3D

We solve the following scalar equation,

$$\nabla \cdot \nabla \mathbf{u} = 0 \qquad \qquad \Omega = [0, 2] \times [0, 1] \times [0, 1], \tag{17}$$

with boundary conditions

$$u = 15y$$
 $x = 0$, (18)

$$u = 25 - 18y$$
 $x = 2$. (19)

No material parameters to specify.

6.4.3 Computational model

• Commandline arguments are:

float: length along x-direction float: length along y-direction

float: length along z-direction (set to zero for 2D)

integer: number of elements in x-direction integer: number of elements in y-direction

integer: number of elements in z-direction (set to zero for 2D)

interger: interpolation order (1: linear; 2: quadratic)

integer: solver type (o: direct; 1: iterative)

Commandline arguments for tests are:

2.0 1.0 0.0 2 1 0 1 0

2.0 1.0 0.0 4 2 0 1 0

2.0 1.0 0.0 8 4 0 1 0

2.0 1.0 0.0 2 1 0 2 0

2.0 1.0 0.0 4 2 0 2 0

2.0 1.0 0.0 8 4 0 2 0

2.0 1.0 0.0 2 1 0 1 1

2.0 1.0 0.0 4 2 0 1 1

6.4.4 Result summary

We use CHeart rev. 6292 to produce numerical reference solutions.

Passed tests: 24 / 24

No failed tests.

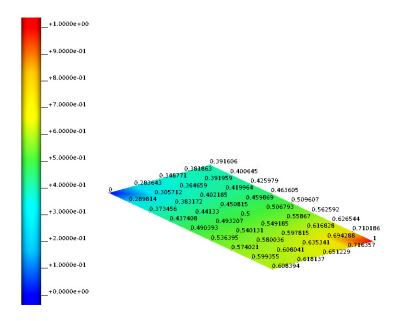


Figure 9: 2D results, iron reference w/ command line arguments [2.0 1.0 0.0 8 4 0 1 0].

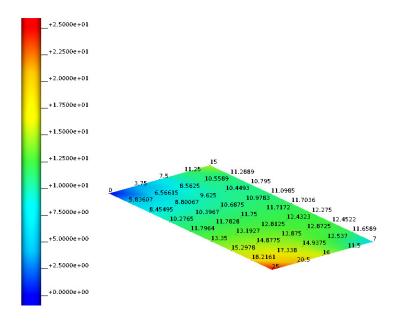


Figure 10: 2D results, current run w/ command line arguments [2.0 1.0 0.0 8 4 0 1 $\,$ o].

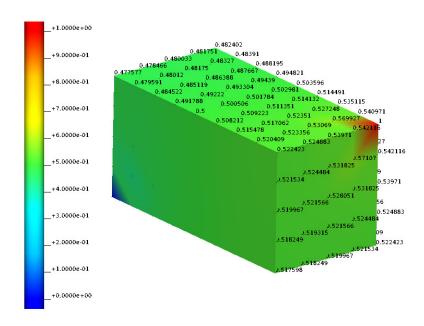


Figure 11: 3D results, iron reference w/ command line arguments [2.0 1.0 1.0 8 4 4 10].

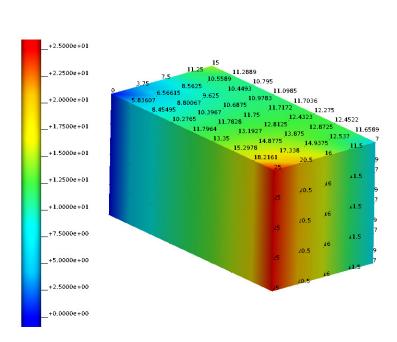


Figure 12: 3D results, current run w/ command line arguments [2.0 1.0 1.0 8 4 4 1 o].

6.5 Example-0003 [COMPILES]

Example uses generated regular meshes and solves a static problem, i.e., applies the boundary conditions in one step.

6.5.1 Mathematical model - 2D

We solve the following scalar equation,

$$\nabla \cdot \nabla u = 0 \qquad \qquad \Omega = [0, 2] \times [0, 1], \tag{20}$$

with boundary conditions

$$u = 15y x = 0, (21)$$

$$u=15y \hspace{1cm} x=0, \hspace{1cm} (21)$$

$$\vartheta_{\pi}u=25-18y \hspace{1cm} x=2. \hspace{1cm} (22)$$

No material parameters to specify.

6.5.2 Mathematical model - 3D

We solve the following scalar equation,

$$\nabla \cdot \nabla \mathbf{u} = 0 \qquad \qquad \Omega = [0, 2] \times [0, 1] \times [0, 1], \tag{23}$$

with boundary conditions

$$u = 15y$$
 $x = 0$, (24)

$$\partial_n u = 25 - 18y$$
 $x = 2.$
(25)

No material parameters to specify.

6.5.3 Computational model

• Commandline arguments are:

float: length along x-direction float: length along y-direction

float: length along z-direction (set to zero for 2D)

integer: number of elements in x-direction integer: number of elements in y-direction

integer: number of elements in z-direction (set to zero for 2D)

interger: interpolation order (1: linear; 2: quadratic)

integer: solver type (o: direct; 1: iterative)

Commandline arguments for tests are:

2.0 1.0 0.0 2 1 0 1 1 2.0 1.0 0.0 4 2 0 1 1

- Iron $|_{-2} = 44.2627$

- Iron $|_{2} = 118.047$

| CHeart

| CHeart

```
2.0 1.0 0.0 8 4 0 1 1
2.0 1.0 0.0 2 1 0 2 1
2.0 1.0 0.0 4 2 0 2 1
2.0 1.0 0.0 8 4 0 2 1
2.0 1.0 1.0 2 1 1 1 0
2.0 1.0 1.0 4 2 2 1 0
2.0 1.0 1.0 8 4 4 1 0
2.0 1.0 1.0 2 1 1 2 0
2.0 1.0 1.0 4 2 2 2 0
2.0 1.0 1.0 8 4 4 2 0
2.0 1.0 1.0 2 1 1 1 1
2.0 1.0 1.0 4 2 2 1 1
2.0 1.0 1.0 8 4 4 1 1
2.0 1.0 1.0 2 1 1 2 1
2.0 1.0 1.0 4 2 2 2 1
2.0 1.0 1.0 8 4 4 2 1
```

6.5.4 Result summary

We use CHeart rev. 6292 to produce numerical reference solutions.

current_run/l2x1x0_n2x1x0_i1_s0/Example.part0.exnode

current_run/l2x1x1_n8x4x4_i2_s1/Example.part0.exnode

Passed tests: 0 / 24

Failed tests:

```
current_run/l2x1x0_n4x2x0_i1_s0/Example.part0.exnode
                                                              | CHeart
                                                                          - Iron |_2 = 37.2776
current_run/l2x1x0_n8x4x0_i1_s0/Example.part0.exnode
                                                              | CHeart
                                                                          - Iron |_{-2} = 32.2165
current_run/l2x1x0_n2x1x0_i2_s0/Example.part0.exnode
                                                                          - Iron |_{2} = 27.3358
                                                                CHeart
current_run/l2x1x0_n4x2x0_i2_s0/Example.part0.exnode
                                                                CHeart
                                                                          - Iron |_{-2} = 22.1869
current_run/l2x1x0_n8x4x0_i2_s0/Example.part0.exnode
                                                              | CHeart
                                                                          - Iron |_{2} = 19.7449
current_run/l2x1x0_n2x1x0_i1_s1/Example.part0.exnode
                                                              | CHeart
                                                                          - Iron |_{-2} = 44.2627
current_run/l2x1x0_n4x2x0_i1_s1/Example.part0.exnode
                                                                          - Iron |_{2} = 37.2776
                                                                CHeart
current_run/l2x1x0_n8x4x0_i1_s1/Example.part0.exnode
                                                                CHeart
                                                                          - Iron |_{-2} = 32.2165
                                                                          - Iron |_{2} = 27.3358
current_run/l2x1x0_n2x1x0_i2_s1/Example.part0.exnode
                                                              | CHeart
                                                                          - Iron |_{-2} = 22.1869
current_run/l2x1x0_n4x2x0_i2_s1/Example.part0.exnode
                                                              | CHeart
                                                                          - Iron |_{2} = 19.7449
current_run/l2x1x0_n8x4x0_i2_s1/Example.part0.exnode
                                                                CHeart
current_run/l2x1x1_n2x1x1_i1_s0/Example.part0.exnode
                                                                CHeart
                                                                          - Iron |_{-2} = 124.749
current_run/l2x1x1_n4x2x2_i1_s0/Example.part0.exnode
                                                                          - Iron |_{2} = 128.672
                                                              | CHeart
current_run/l2x1x1_n8x4x4_i1_s0/Example.part0.exnode
                                                                          - Iron |_{-2} = 143.606
                                                              | CHeart
                                                                          - Iron |_{2} = 94.2619
current_run/l2x1x1_n2x1x1_i2_s0/Example.part0.exnode
                                                                CHeart
current_run/l2x1x1_n4x2x2_i2_s0/Example.part0.exnode
                                                                CHeart
                                                                          - Iron |_{-2} = 98.7606
                                                                          - Iron |_{-2} = 118.047
current_run/l2x1x1_n8x4x4_i2_s0/Example.part0.exnode
                                                              | CHeart
current_run/l2x1x1_n2x1x1_i1_s1/Example.part0.exnode
                                                              | CHeart
                                                                          - Iron |_{-2} = 124.749
\verb|current_run/l2x1x1_n4x2x2_i1_s1/Example.part0.exnode|\\
                                                                CHeart
                                                                          - Iron |_{2} = 128.672
current_run/l2x1x1_n8x4x4_i1_s1/Example.part0.exnode
                                                                CHeart
                                                                          - Iron |_{-2} = 143.606
current_run/l2x1x1_n2x1x1_i2_s1/Example.part0.exnode
                                                                CHeart
                                                                          - Iron |_{2} = 94.2619
                                                                          - Iron |_{-2} = 98.7606
current_run/l2x1x1_n4x2x2_i2_s1/Example.part0.exnode
                                                              | CHeart
```

Figure 13: 2D results, iron reference w/ command line arguments [2.0 1.0 0.0 8 4 0 10].

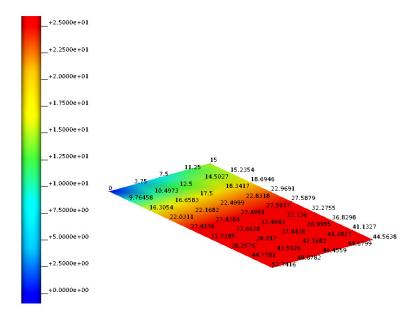


Figure 14: 2D results, current run w/ command line arguments [2.0 1.0 0.0 8 4 0 1 $\,$ o].

Figure 15: 3D results, iron reference w/ command line arguments [2.0 1.0 1.0 8 4 4 10].

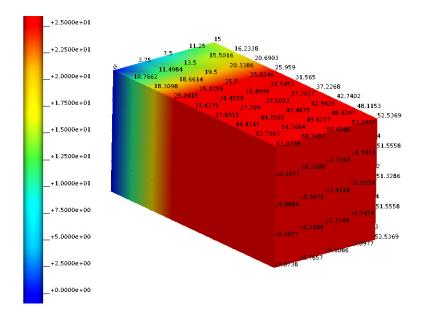


Figure 16: 3D results, current run w/ command line arguments [2.0 1.0 1.0 8 4 4 1 $\,$ o].

6.6 Example-0004 [VALIDATED]

Example uses generated regular meshes and solves a static problem, i.e., applies the boundary conditions in one step.

6.6.1 Mathematical model - 2D

We solve the following scalar equation,

$$\nabla \cdot \nabla u = 0 \qquad \qquad \Omega = [0, 2] \times [0, 1], \tag{26}$$

with boundary conditions

$$u = 2.0e^{x} \cdot \cos(y)$$
 on $\partial\Omega$. (27)

No material parameters to specify.

6.6.2 Computational model

• Commandline arguments are:

integer: number of elements in x-direction integer: number of elements in y-direction

integer: number of elements in z-direction (set to zero for 2D)

interger: interpolation order (1: linear; 2: quadratic)

integer: solver type (o: direct; 1: iterative)

• Commandline arguments for tests are:

42010

84010

21020

42020

84020

42011

84011

21021

42021

84021

100 50 0 1 0 (not tested yet..)

100 50 0 2 0 (not tested yet..)

100 50 0 1 1 (not tested yet..)

100 50 0 2 1 (not tested yet..)

6.6.3 Result summary

We use CHeart rev. 6292 to produce numerical reference solutions.

Passed tests: 10 / 10

No failed tests.

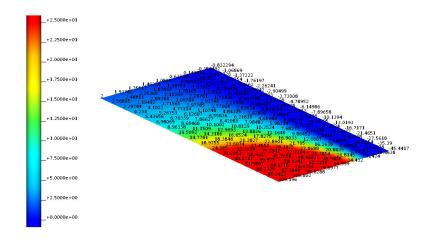


Figure 17: 2D results, iron reference w/ command line arguments [8 4 0 2 0].

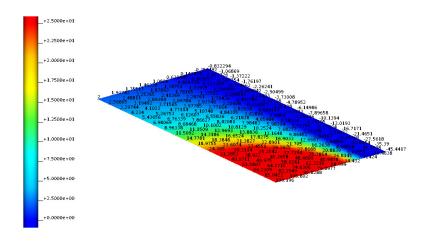


Figure 18: 2D results, current run w/ command line arguments [8 4 0 2 0].

6.7 Example-0011 [RUNS]

Example uses generated regular meshes and solves a static problem, i.e., applies the boundary conditions in one step.

6.7.1 Mathematical model - 2D

We solve the following scalar equation,

$$\nabla \cdot [\sigma \nabla u] = 0 \qquad \qquad \Omega = [0, 2] \times [0, 1], \tag{28}$$

with boundary conditions

$$u = 0 x = y = 0, (29)$$

$$u = 1$$
 $x = 2, y = 1.$ (30)

The conductivity tensor is defined as,

$$\sigma(x,t) = \sigma = I. \tag{31}$$

6.7.2 Mathematical model - 3D

We solve the following scalar equation,

$$\nabla \cdot [\sigma \nabla u] = 0 \qquad \qquad \Omega = [0, 2] \times [0, 1] \times [0, 1], \tag{32}$$

with boundary conditions

$$u = 0$$
 $x = y = z = 0,$ (33)

$$u = 1$$
 $x = 2, y = z = 1.$ (34)

The conductivity tensor is defined as,

$$\sigma(x,t) = \sigma = I. \tag{35}$$

6.7.3 Computational model

• Commandline arguments are:

float: length along x-direction float: length along y-direction

float: length along z-direction (set to zero for 2D)

integer: number of elements in x-direction integer: number of elements in y-direction

integer: number of elements in z-direction (set to zero for 2D)

integer: interpolation order (1: linear; 2: quadratic)

integer: solver type (o: direct; 1: iterative)

float: σ_{11} float: σ_{22}

float: σ_{33} (ignored for 2D)

• Commandline arguments for tests are:

6.7.4 Result summary

We use CHeart rev. 6292 to produce numerical reference solutions.

Passed tests: 24 / 24

No failed tests.

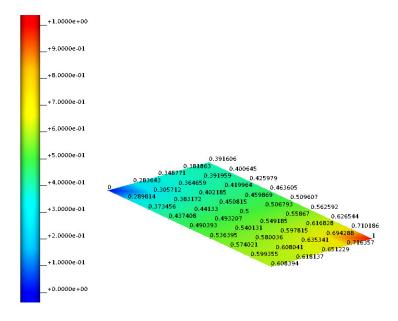


Figure 19: 2D results, iron reference w/ command line arguments [2.0 1.0 0.0 8 4 0 1011].

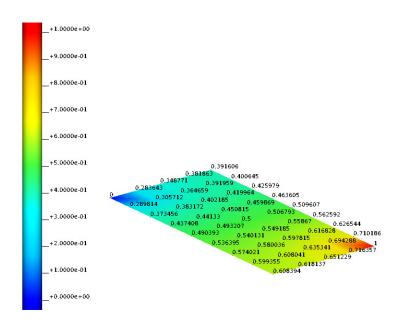


Figure 20: 2D results, current run w/ command line arguments [2.0 1.0 0.0 8 4 0 1 0 1 1].

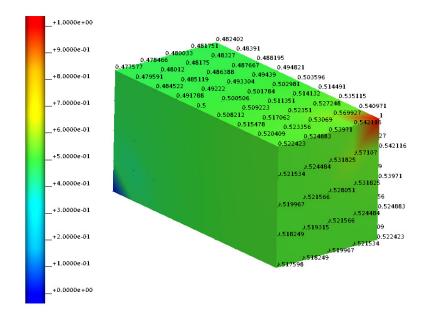


Figure 21: 3D results, iron reference w/ command line arguments [2.0 1.0 1.0 8 4 4 10111].

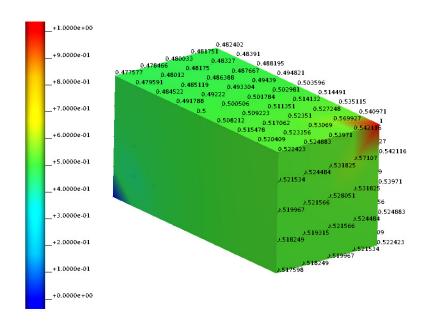


Figure 22: 3D results, current run w/ command line arguments [2.0 1.0 1.0 8 4 4 1 0 1 1 1].

7 LINEAR ELASTICITY

7.1 Equation in general form

$$\partial_{tt} \mathbf{u} + \nabla \cdot \mathbf{\sigma}(\mathbf{u}, \mathbf{t}) = \mathbf{f}(\mathbf{u}, \mathbf{t}) \tag{36}$$

7.2.1 Mathematical model

We solve the following equation (both 2D and 3D domains are considered),

$$\nabla \cdot \sigma(\mathbf{u}, \mathbf{t}) = 0$$
 $\Omega = [0, 160] \times [0, 120] \times [0, 120], \mathbf{t} \in [0, 5],$ (37)

with time step size $\Delta_t = 1$ and $\mathbf{u} = [u_x, u_y]$ in 2D $\mathbf{u} = [u_x, u_y, u_z]$ in 3D. The boundary conditions in 2D are given by

$$u_x = u_y = 0 \qquad \qquad x = y = 0, \tag{38}$$

$$u_x = 16$$
 $x = 160$, (39)

and in 3D by

$$u_x = u_y = u_z = 0$$
 $x = y = z = 0$, (40)

$$u_x = 16$$
 $x = 160$. (41)

The material parameters are

$$E = 10000MPa,$$
 (42)

$$v = 0.3, \tag{43}$$

$$\rho = 5 \times 10^{-9} \text{tonne.mm}^3. \tag{44}$$

7.2.2 Computational model

• Commandline arguments are:

float: length along x-direction

float: length along y-direction

float: length along z-direction (set to zero for 2D)

integer: number of elements in x-direction integer: number of elements in y-direction

integer: number of elements in z-direction (set to zero for 2D)

integer: interpolation order (1: linear; 2: quadratic)

integer: solver type (o: direct; 1: iterative)

float: elastic modulus float: Poisson ratio

float: displacement percentage load

• Command line arguments for tests are:

160 120 0 8 6 0 1 0 10000 0.3 0.05

160 120 0 16 12 0 1 0 10000 0.3 0.05

160 120 0 32 24 0 1 0 10000 0.3 0.05

160 120 120 8 6 6 1 0 10000 0.3 0.05

160 120 120 16 12 12 1 0 10000 0.3 0.05

160 120 120 32 24 24 1 0 10000 0.3 0.05

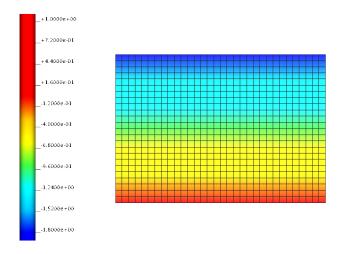


Figure 23: Results, iron 2D fine mesh.

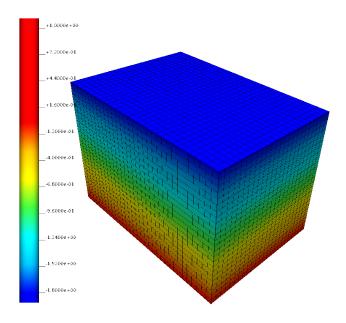


Figure 24: Results, iron 3D fine mesh.

7.2.3 Results

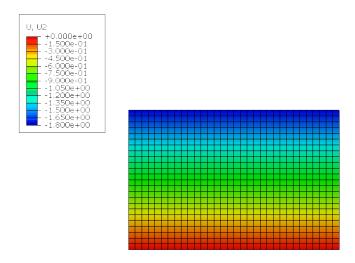
Validation 7.2.4

The iron results are compared to those from Abaqus (version 2017). The figures below show selected results from the validation simulations carried out in Abaqus and provide a qualitative validation. A quantitative validation was carried out by comparing the horizontal displacement $\boldsymbol{u}_{\boldsymbol{y}}$ along

the free-edge (y = 120 for 2D and y = z = 120 for 3D) and computing the L2-norm according to

$$L_{2}\text{-norm} = \sum_{i=1}^{N} \sqrt{\left(u_{y,\text{abaqus}}^{i} - u_{y,\text{iron}}^{i}\right)^{2}}, \tag{45}$$

where N is the total number of nodes along the free-edge. The results over the mesh refinements are given in Table 2.



```
ODB: 2D_UNIAX_ELASTIC_elem_5_160x120mm_intp_1_DIRECT.odb Abaqus/Standard 3DEXPERIENCE
Step: Load, Load.
Pricement 5: Step Time = 5.000
Primary Var: U, U2
Deformed Var: U Deformation Scale Factor: +2.000e+00
```

Figure 25: Results, Abaqus 2D fine mesh.

Dimension	Mesh	L_2 -norm	
2D	Coarse	5.322×10^{-16}	
2D	Medium	1.559×10^{-15}	
2D	Fine	2.900×10^{-15}	
3D	Coarse	3.071×10^{-17}	
3D	Medium	2.125×10^{-17}	
3D	Fine	2.924×10^{-17}	

Table 2: Quantiative error between Abaqus 2017 and iron simulations for linear elastic uniaxial extenions

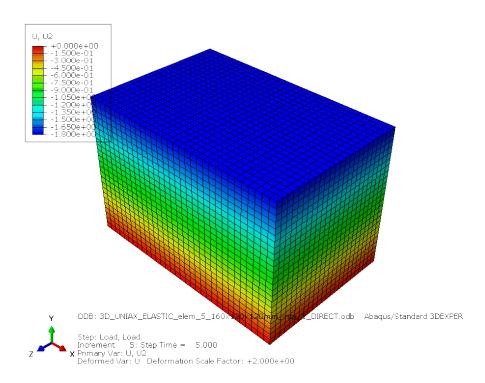


Figure 26: Results, abaqus 3D fine mesh.

7.3.1 Mathematical model

We solve the following equation (both 2D and 3D domains are considered),

$$\nabla \cdot \mathbf{\sigma}(\mathbf{u}, \mathbf{t}) = \mathbf{0}$$
 $\Omega = [0, 160] \times [0, 120] \times [0, 120], \mathbf{t} \in [0, 5],$ (46)

with time step size $\Delta_t = 1$ and $\mathbf{u} = [u_x, u_y]$ in 2D $\mathbf{u} = [u_x, u_y, u_z]$ in 3D. The boundary conditions in 2D are given by

$$u_{x} = u_{y} = 0 \qquad \qquad y = 0, \tag{47}$$

$$u_y = 8$$
 $x = 160,$ (48)

and in 3D by

$$u_x = u_z = 0 x = 0, (49)$$

$$u_{\mathbf{u}} = 0 \qquad \qquad \mathbf{y} = \mathbf{0}, \tag{50}$$

$$u_x = 160$$
 $x = 160$, (51)

$$u_y = 8$$
 $x = 160.$ (52)

The material parameters are

$$E = 10000MPa,$$
 (53)

$$v = 0.3,$$
 (54)

$$\rho = 5 \times 10^{-9} \text{tonne.mm}^3. \tag{55}$$

7.3.2 Computational model

• Commandline arguments are:

float: length along x-direction float: length along y-direction

float: length along z-direction (set to zero for 2D)

integer: number of elements in x-direction integer: number of elements in y-direction

integer: number of elements in z-direction (set to zero for 2D)

integer: interpolation order (1: linear; 2: quadratic)

integer: solver type (o: direct; 1: iterative)

float: elastic modulus float: Poisson ratio

float: displacement percentage load

• Command line arguments for tests are:

160 120 0 8 6 0 1 0 10000 0.3 0.05

160 120 0 16 12 0 1 0 10000 0.3 0.05

160 120 0 32 24 0 1 0 10000 0.3 0.05

160 120 120 8 6 6 1 0 10000 0.3 0.05

160 120 120 16 12 12 1 0 10000 0.3 0.05

160 120 120 32 24 24 1 0 10000 0.3 0.05

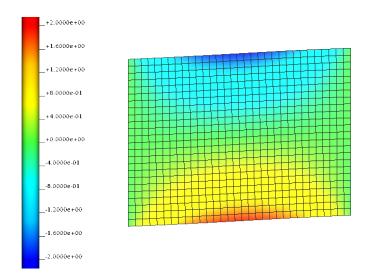


Figure 27: Results, iron 2D fine mesh.

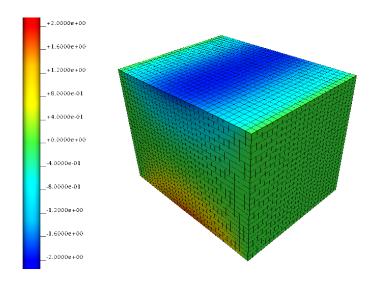


Figure 28: Results, iron 3D fine mesh.

Results 7.3.3

Validation 7.3.4

The iron results are compared to those from Abaqus (version 2017). The figures below show selected results from the validation simulations carried out in Abaqus and provide a qualitative validation. A quantitative validation was carried out by comparing the horizontal displacement u_x along the free-edge (y = 120 for 2D and y = z = 120 for 3D) and computing the L2-norm according to

$$L_{2}\text{-norm} = \sum_{i=1}^{N} \sqrt{\left(u_{y,\text{abaqus}}^{i} - u_{y,\text{iron}}^{i}\right)^{2}}, \tag{56}$$

where N is the total number of nodes along the free-edge. The results over the mesh refinements are given in Table 2.

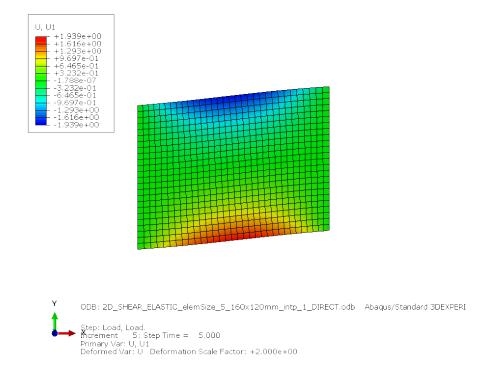


Figure 29: Results, Abaqus 2D fine mesh.

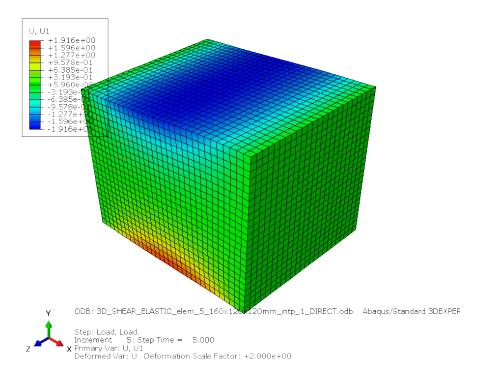


Figure 30: Results, abaqus 3D fine mesh.

Dimension	Mesh	L_2 -norm	
2D	Coarse	6.696×10^{-3}	
2D	Medium	1.273×10^{-3}	
2D	Fine	2.489×10^{-4}	
3D	Coarse	4.234×10^{-4}	
3D	Medium	4.184×10^{-5}	
3D	Fine	3.781×10^{-6}	

Table 3: Quantiative error between Abaqus 2017 and iron simulations for linear elastic shear

8 FINITE ELASTICITY

9 NAVIER-STOKES FLOW

9.1 Equation in general form

$$\partial_{\mathbf{t}}(\rho \mathbf{v}) + \nabla \cdot (\rho \mathbf{v} \otimes \mathbf{v} + p\mathbf{I}) = \rho \mathbf{f}$$
 (57)

g.2 Example-0302-u [COMPILES]

Example uses user-defined simplex meshes in CHeart mesh format with quadratic/linear interpolation for velocity/pressure and solves a dynamic problem.

Setup is the well-known lid-driven cavity problem on the unit square or unit cube in two and three dimensions.

Current issue: does not converge after 30 some time iterations.

9.2.1 Mathematical model - 2D

We solve the incompressible Navier-Stokes equation,

$$\partial_{\mathbf{t}}(\rho \mathbf{v}) + \nabla \cdot (\rho \mathbf{v} \otimes \mathbf{v} + p\mathbf{I}) = \rho \mathbf{f}$$
 $\Omega = [0, 1] \times [0, 1],$ (58)

$$\nabla \cdot \mathbf{v} = 0, \tag{59}$$

with boundary conditions

$$v = 0 x = 0, (60)$$

$$v = 0 x = 1, (61)$$

$$v = 0 y = 0, (62)$$

$$v = [1, 0]^{T}$$
 $y = 1.$ (63)

Density $\rho = 1$, viscosity $\mu = 0.0025$. Thus, Reynolds number Re = 400.

9.2.2 Mathematical model - 3D

We solve the incompressible Navier-Stokes equation,

$$\partial_{\mathbf{t}}(\rho \mathbf{v}) + \nabla \cdot (\rho \mathbf{v} \otimes \mathbf{v} + p\mathbf{I}) = \rho \mathbf{f}$$
 $\Omega = [0, 1] \times [0, 1] \times [0, 1],$ (64)

$$\nabla \cdot \mathbf{v} = 0, \tag{65}$$

with boundary conditions

$$\mathbf{v} = \mathbf{0} \qquad \qquad \mathbf{x} = \mathbf{0}, \tag{66}$$

$$v = 0 x = 1, (67)$$

$$\mathbf{v} = \mathbf{0} \tag{68}$$

$$\mathbf{v} = [1, 0]^{\mathsf{T}} \qquad \qquad \mathbf{y} = 1, \tag{69}$$

$$v = 0 z = 0, (70)$$

$$v = 0 z = 1. (71)$$

Density $\rho = 1$, viscosity $\mu = 0.01$. Thus, Reynolds number Re = 100.

9.2.3 Computational model

• Commandline arguments are:

integer: number of dimensions (2: 2D, 3: 3D integer: mesh refinement level (1, 2, 3, ...)

float: start time float: stop time float: time step size float: density

float: viscosity

integer: solver type (o: direct; 1: iterative)

• Commandline arguments for tests are:

2 1 0.0 0.01 0.001 1.0 0.0025 0

• Note: Binary uses command line arguments to search for the relevant

9.2.4 Result summary

We use CHeart rev. 6292 to produce numerical reference solutions.

10 MONODOMAIN

11 CELLML MODEL

REFERENCES

[1] Chris Bradley, Andy Bowery, Randall Britten, Vincent Budelmann, Oscar Camara, Richard Christie, Andrew Cookson, Alejandro F Frangi, Thiranja Babarenda Gamage, Thomas Heidlauf, et al. Opencmiss: a multi-physics & multi-scale computational infrastructure for the vph/physiome project. Progress in biophysics and molecular biology, 107(1):32-47, 2011.