

# Classical Guitar Intonation and Compensation: The Well-Tempered Guitar

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## Abstract

Inspired by the pioneering work of Greg Byers in 1996, we build an intuitive model of classical guitar intonation that includes the effects of the resonant length of the fretted string, linear mass density, tension, and bending stiffness. We begin by deriving an expression for the vibration frequencies of a stiff string using boundary conditions that are pinned at the saddle but clamped at the fret. We adopt logarithmic frequency differences based on “cents” that decouple these physical effects, and then we introduce Taylor series expansions that exhibit clearly the origins of frequency shifts of fretted notes from the corresponding Twelve-Tone Equal Temperament (12-TET) values. Although we have postponed careful measurements of the changes in frequency of open strings arising from small changes in length, we propose a simple experimental method that any interested guitarist can use to estimate these parameters for their own guitars and their favorite string sets. Based on these results, we employ an RMS frequency error method to select values of saddle and nut setbacks that map fretted frequencies — for a particular string set on a particular guitar — almost perfectly onto their 12-TET targets. This exercise allow us to discuss a general approach to tempering an “off-the-shelf” guitar to further reduce the tonal errors inherent in any fretted musical instrument.

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## 1 Introduction and Background

The relationship between mathematics and music is Discuss initial [1] and ongoing [2] work by G. Byers, and recent studies of steel guitar strings [3]. General references on the physics of sound, music, and musical instruments are [4, 5].

Fundamental frequency of a string [6]:

$$f_0 = \frac{1}{2L_0} \sqrt{\frac{T_0}{\mu_0}}, \quad (1)$$

where  $L_0$  is the length of the free (unfretted) string from the saddle to the nut,  $T_0$  is the tension in the free string, and  $\mu_0 \equiv M/L_0$  is the linear mass density of a free string of mass  $M$ .

Throughout this work, we will use *cents* to describe small differences in pitch [7]. One cent is one one-hundredth of a Twelve-Tone Equal Temperament (12-TET) half step, so that there are 1200 cents per octave. Using this approach, the difference in pitch between frequencies  $f_1$  and  $f_2$  is defined as

$$\Delta\nu \equiv 1200 \log_2 \left( \frac{f_2}{f_1} \right). \quad (2)$$

We define  $f \equiv (f_1 + f_2)/2$  and  $\Delta f \equiv f_2 - f_1$ . Then

$$\Delta\nu = 1200 \log_2 \left( \frac{f + \Delta f/2}{f - \Delta f/2} \right) \approx \frac{1200}{\ln 2} \frac{\Delta f}{f}, \quad (3)$$

where the last approximation applies when  $\Delta f \ll f$ . An experienced guitar player can distinguish beat notes with a difference frequency of  $\Delta f \approx 1$  Hz, which corresponds to 8 cents at  $A_2$  ( $f = 220$  Hz) or 5 cents at  $E_4$  ( $f = 329.63$  Hz).

We present the basics of our model of classical guitar strings in Section 2. We begin with a new expression for the allowed vibration frequencies of a stiff string, derived in Appendix A under the assumption that the boundary conditions are not symmetric. We then include a discussion of the four contributions to frequency shifts and errors of non-ideal strings: changes in the resonant length of the fretted string; a decrease in the linear mass density and an increase in the tension of the string; and the mechanical stiffness of the resonating string. Our goal is to simplify the equations through Taylor series expansions to allow an intuitive picture of the

string’s behavior to emerge. We offer an empirical reason to doubt the need for a complicated model of string fretting, and we explore this argument in greater detail in Appendix B. In Section 3, we suggest a simple experiment to estimate the response of the string’s tension to the change in length caused by fretting, and we demonstrate the idea using a normal-tension string set on an Alhambra 8P guitar (as well as other string sets in Appendix D). Then, in Section 4, we use these estimates to demonstrate a straightforward analytic approach to compensating the errors in a guitar string, relying on a method — described in Appendix C — to minimize the root-mean-squared (RMS) frequency deviation at each fret. Finally, we discuss a collaboration of guitar manufacturer and musician to temper the guitar using harmonic tuning and optimize it for a particular piece.

This document – as well as the Python computer code needed to reproduce the figures – is available at GitHub [8].

## 2 Simple Model of Guitar Intonation

The starting point for prior efforts to understand guitar intonation and compensation [1, 3] is a formula for  $f_m$ , the transverse vibration frequency harmonic  $m$  of a stiff string, originally published by Morse in 1936 [9]:

$$f_m = \frac{m}{2L} \sqrt{\frac{T}{\mu}} \left[ 1 + 2B + 4 \left( 1 + \frac{\pi^2 m^2}{8} \right) B^2 \right]. \quad (4)$$

Here  $L$  is the length of the string,  $T$  and  $\mu$  are its tension and the linear mass density, respectively, and  $B$  is a small “bending stiffness” coefficient to capture the relevant mechanical properties of the string. For a homogeneous string with a cylindrical cross section,  $B$  is given by

$$B \equiv \sqrt{\frac{\pi \rho^4 E}{4 T L^2}}, \quad (5)$$

where  $\rho$  is the radius of the string and  $E$  is Young’s modulus (or the modulus of elasticity). But it’s unlikely that Eq. (4) accurately describes the resonant frequencies of a nylon string on a classical guitar, because it assumes that the string is “clamped” at both ends, so that a particular set of symmetric boundary conditions must be applied to the partial differential equation (PDE) describing transverse vibrations of the string. We believe that this assumption is correct for the end of the string held at either the nut or the fret, but that the string is “pinned” (and not clamped) at the saddle. In Appendix A, we solve the PDE using these non-symmetric boundary conditions, and find

$$f_m = \frac{m}{2L} \sqrt{\frac{T}{\mu}} \left[ 1 + B + \left( 1 + \frac{1}{2} m^2 \pi^2 \right) B^2 \right]. \quad (6)$$

Note that this expression is valid only when  $B \ll 1$ . For a typical nylon guitar string with  $E \approx 5$  GPa,  $T \approx 60$  N,  $\rho \approx 0.5$  mm, and  $L \approx 650$  mm, we have  $B \approx 3 \times 10^{-3}$ . (In this case, the quadratic term in  $B$  is only 2% as large as the linear term, and can generally be neglected. We will include it in our analysis below only for completeness.) We’ll use Eq. (6) with some caution, because the physics of nylon strings (particularly the wound base strings) are quite complicated [10].

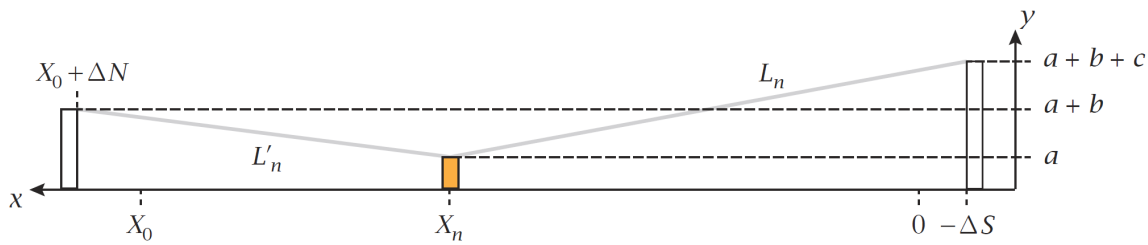


Figure 1: A simple (side-view) schematic of the classical guitar used in this model. The scale length of the guitar is  $X_0$ , but we allow the edges of both the saddle and the nut to be set back an additional distance  $\Delta S$  and  $\Delta N$ , respectively. The location on the  $x$ -axis of the center of the  $n^{\text{th}}$  fret is  $X_n$ . (Note that the  $x$ -axis is directed toward the left in this figure.) In the  $y$  direction,  $y = 0$  is taken as the surface of the fingerboard; therefore the height of each fret above the fingerboard is  $a$ , the height of the nut is  $a + b$ , and the height of the saddle is  $a + b + c$ .  $L_n$  is the *resonant length* of the string from the saddle to the center of fret  $n$ , and  $L'_n$  is the length of the string from the fret to the nut.

Our model is based on the schematic of the guitar shown in Fig. 1. The scale length of the guitar is  $X_0$ , but we allow the edges of both the saddle and the nut to be set back an additional distance  $\Delta S$  and  $\Delta N$ , respectively. The location on the  $x$ -axis of the center of the  $n^{\text{th}}$  fret is  $X_n$ . In the  $y$  direction,  $y = 0$  is taken as the surface of the fingerboard; the height of each fret is  $a$ , the height of the nut is  $a + b$ , and the height of the saddle is  $a + b + c$ .  $L_n$  is the *resonant length* of the string from the saddle to the center of fret  $n$ , and  $L'_n$  is the length of the string from the fret to the nut. The total length of the string is defined as  $\mathcal{L}_n \equiv L_n + L'_n$ .

Previous studies of guitar intonation and compensation have chosen to include the apparent increase in length of the string caused by both the fretting depth and the shape of the fretted string under the finger [1, 3]. As the string is initially pressed to the fret, the total length  $\mathcal{L}_n$  increases and causes the tension in the string — which is pinned at the saddle and clamped at the nut — to increase. As the string is pressed further, does the additional deformation of the string increase its tension (throughout the resonant length  $L_n$ )? There are at least two purely empirical reasons to doubt this hypothesis. First, we can mark a string (with a fine-point felt pen) above a particular fret and then observe the mark with a magnifying glass. As the string is pressed all the way to the finger board, the mark does not move perceptibly — it has become *clamped* on the fret. Second, we can use either our ears or a simple tool to measure frequencies [11] to listen for a shift as we use different fingers and vary the fretted depth of a string. The apparent modulation is far less than would be obtained by classical vibrato ( $\pm 15$  cents), so we assume that once the string is minimally fretted the length(s) can be regarded as fixed. (If this were not the case, then fretting by different people or with different fingers, at a single string or with a barre, would cause additional, varying frequency shifts that would be audible and difficult to compensate.) We discuss this issue in more detail in Appendix B.

We start with the form of the fundamental frequency of a fretted string given by Eq. (6) with  $m = 1$ , and apply it to the frequency of a string pressed just behind the  $n^{\text{th}}$  fret:

$$f_n = \frac{1}{2L_n} \sqrt{\frac{T_n}{\mu_n}} \left[ 1 + B_n + \left( 1 + \frac{\pi^2}{2} \right) B_n^2 \right], \quad (7)$$

where  $T_n$  and  $\mu_n$  are the modified tension and the linear mass density of the fretted string,

and

$$B_n \equiv \sqrt{\frac{\pi \rho^4 E}{4 T_n L_n^2}}. \quad (8)$$

We note that  $T_n$  and  $\mu_n$  depend on  $\mathcal{L}_n$ , the *total* length of the fretted string from the saddle to the nut. Ideally, in the 12-TET system [7],

$$f_n = \gamma_n f_0, \quad (12\text{-TET ideal}) \quad (9)$$

where  $f_0$  is the frequency of the open (unfretted) string, and

$$\gamma_n \equiv 2^{n/12}. \quad (10)$$

Therefore, the error interval — the difference between the fundamental frequency of the fretted string and the corresponding perfect 12-TET frequency — expressed in cents is given by

$$\begin{aligned} \Delta v_n &= 1200 \log_2 \left( \frac{f_n}{\gamma_n f_0} \right) \\ &= 1200 \log_2 \left( \frac{L_0}{\gamma_n L_n} \right) + 600 \log_2 \left( \frac{\mu_0}{\mu_n} \right) + 600 \log_2 \left( \frac{T_n}{T_0} \right) \\ &\quad + 1200 \log_2 \left[ \frac{1 + B_n + (1 + \pi^2/2) B_n^2}{1 + B_0 + (1 + \pi^2/2) B_0^2} \right]. \end{aligned} \quad (11)$$

The final form of Eq. (11) makes it clear that — for nylon guitar strings — there are four contributions to intonation:

1. *Resonant Length*: The first term represents the error caused by the increase in the length of the fretted string  $L_n$  compared to the ideal length  $X_n$ , which would be obtained if  $b = c = 0$  and  $\Delta S = \Delta N = 0$ .
2. *Linear Mass Density*: The second term is the error caused by the reduction of the linear mass density of the fretted string. This effect will depend on the *total* length of the string, given by  $\mathcal{L}_n = L_n + L'_n$ .
3. *Tension*: The third term is the error caused by the *increase* of the tension in the string arising from the stress and strain applied to the string by fretting. This effect will also depend on the total length of the string  $\mathcal{L}_n$ .
4. *Bending Stiffness*: The fourth and final term is the error caused by the change in the bending stiffness coefficient caused by decreasing the vibrating length of the string from  $L_0$  to  $L_n$ .

Note that the properties of the logarithm function have *decoupled* these physical effects by converting multiplication into addition. We will discuss each of these sources of error in turn below.

## 2.1 Resonant Length

The length  $L_0$  of the open (unfretted) guitar string can be calculated quickly by referring to Fig. 1. We find:

$$L_0 = \sqrt{(X_0 + \Delta S + \Delta N)^2 + c^2} \approx X_0 + \Delta S + \Delta N + \frac{c^2}{2X_0}, \quad (12)$$

where the approximation arises from Taylor Series that applies when  $c^2 \ll X_0^2$ . Similarly, if  $(b + c)^2 \ll X_0^2$ , the resonant length  $L_n$  is given by

$$L_n = \sqrt{(X_n + \Delta S)^2 + (b + c)^2} \approx X_n + \Delta S + \frac{(b + c)^2}{2X_n}. \quad (13)$$

Then — if the guitar has been manufactured such that  $X_n = X_0/y_n$  — the resonant length error determined by the first term in the last line of Eq. (11) is approximately

$$1200 \log_2 \left( \frac{L_0}{y_n L_n} \right) \approx \frac{1200}{\ln(2)} \left[ \frac{\Delta N - (y_n - 1) \Delta S}{X_0} - \frac{y_n^2 (b + c)^2 - c^2}{2X_0^2} \right] \quad (14)$$

If the guitar is uncompensated, so that  $\Delta S = \Delta N = 0$ , this error is typically less than 0.25 cents. But, with  $\Delta S > 0$  and  $\Delta N < 0$ , we can significantly *increase* the magnitude of this “error” and cause the frequency to shift lower. We’ll see that this is our primary method of compensation.

## 2.2 Linear Mass Density

As discussed above, the linear mass density  $\mu_0$  of an open (unfretted) string is simply the total mass  $M$  of the string clamped between the saddle and the nut divided by the length  $L_0$ . Similarly, the mass density  $\mu_n$  of a string held onto fret  $N$  is  $M/\mathcal{L}_n$ . Therefore

$$\frac{\mu_0}{\mu_n} = \frac{\mathcal{L}_n}{L_0} \equiv 1 + Q_n, \quad (15)$$

where we have followed Byers and defined [1, 3]

$$Q_n \equiv \frac{\mathcal{L}_n - L_0}{L_0}. \quad (16)$$

Since we expect that  $Q_n \ll 1$ , we can approximate the second term in the final line of Eq. (11) as

$$600 \log_2 \left( \frac{\mu_0}{\mu_n} \right) \approx \frac{600}{\ln(2)} Q_n. \quad (17)$$

Referring to Fig. 1, we see that  $\mathcal{L}_n = L_n + L'_n$ , and we calculate  $L'_n$  for  $n \geq 1$  as

$$L'_n = \sqrt{(X_0 - X_n + \Delta N)^2 + b^2} \approx X_0 - X_n + \Delta N + \frac{b^2}{2(X_0 - X_n)}, \quad (18)$$

where the approximation applies when  $b^2 \ll (X_0 - X_n)^2$ . Therefore, using Eq. (13), we have

$$\mathcal{L}_n = L_n + L'_n \approx X_0 + \Delta S + \Delta N + \frac{(b + c)^2}{2X_n} + \frac{b^2}{2(X_0 - X_n)}, \quad (19)$$

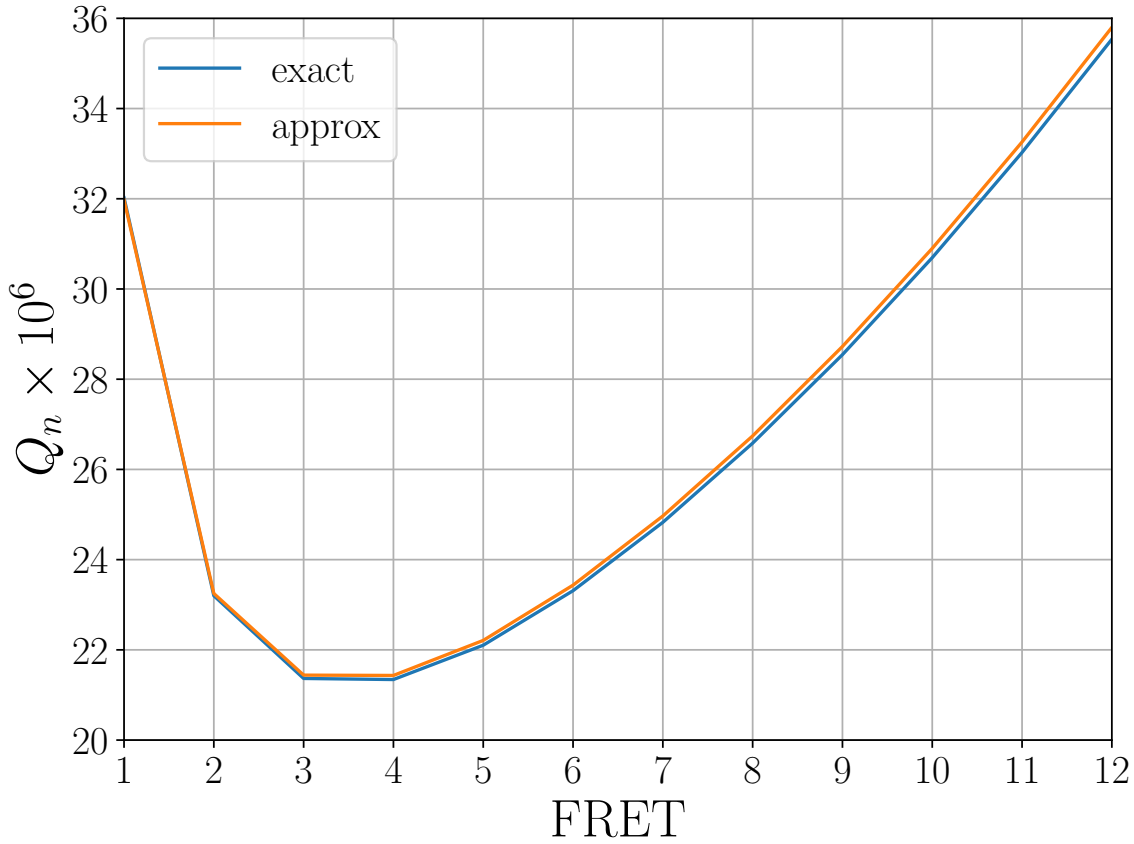


Figure 2: Comparison of the exact expression for the normalized displacement  $Q_n$  as a function of the fret number given by Eq. (16) with the approximate expression given by Eq. (20). For example, at the fifth fret,  $Q_n \approx 22 \times 10^{-6}$ . Here the guitar has  $b = 1.0$  mm,  $c = 3.5$  mm,  $\Delta S = 1.5$  mm,  $\Delta N = -0.25$  mm, and a scale length of 650 mm.

and

$$\begin{aligned}
 Q_n &\approx \frac{1}{2X_0} \left[ \frac{(b+c)^2}{X_n} + \frac{b^2}{X_0 - X_n} - \frac{c^2}{X_0} \right] \\
 &= \frac{\gamma_n}{2X_0^2} \left[ (b+c)^2 + \frac{b^2}{\gamma_n - 1} - \frac{c^2}{\gamma_n} \right].
 \end{aligned} \tag{20}$$

In Fig. 2, we plot a comparison between the exact expression for the normalized displacement  $Q_n$  given by Eq. (16) with the approximate expression given by Eq. (20). Here the guitar has  $b = 1.0$  mm,  $c = 3.5$  mm,  $\Delta S = 1.5$  mm,  $\Delta N = -0.25$  mm, and  $X_0 = 650$  mm. We see that our Taylor series estimate is quite accurate even though it neglects both setbacks, indicating that  $Q_n$  is determined primarily by the values of  $b$  and  $c$ . For the same parameters,  $\Delta v_{12} \approx 0.03$  cents, and will be even smaller for  $n < 12$ . In general, the shift due to linear mass density can be neglected without much loss of accuracy.

### 2.3 Tension

As a guitar string is fretted, its length increases, thereby increasing its tension through linear elastic deformation [12]. We will focus on the response of the string to a longitudinal strain, and

neglect the transverse stress that causes negligible changes in the diameter of the string [10]. In this case, we can write the change in tension of a string experiencing a change in length from  $L$  to  $\mathcal{L}$  as

$$\Delta T = \pi \rho^2 E \frac{\mathcal{L} - L}{L}. \quad (21)$$

Therefore, the tension in a string clamped to fret  $n$  is

$$T_n = T_0 + \Delta T_n = T_0 (1 + \kappa Q_n), \quad (22)$$

where we have used Eq. (16) and defined the dimensionless “string constant”

$$\kappa \equiv \frac{\pi \rho^2 E}{T_0}. \quad (23)$$

In this case, we assume that  $\kappa Q_n \ll 1$ , so that we can approximate the third term in the final line of Eq. (11) as

$$600 \log_2 \left( \frac{T_n}{T_0} \right) \approx \frac{600}{\ln(2)} \kappa Q_n. \quad (24)$$

This frequency shift is larger than that caused by the linear mass density error by a factor of  $\kappa$ .

## 2.4 Bending Stiffness

Since  $B_n$  is already relatively small, we only need to consider the largest contribution arising from the shortened length of the fretted string compared to that of the open string. We see from Eq. (13) that  $L_n \approx L_0/\gamma_n$ , so from Eq. (8) we have

$$B_n = \sqrt{\frac{\pi \rho^4 E}{4 T_n L_n^2}} \approx \frac{L_0}{L_n} \sqrt{\frac{\pi \rho^4 E}{4 T_0 L_0^2}} = \gamma_n B_0. \quad (25)$$

Therefore, the fourth term in the final line of Eq. (11) can be approximated as

$$1200 \log_2 \left[ \frac{1 + B_n + (1 + \pi^2/2) B_n^2}{1 + B_0 + (1 + \pi^2/2) B_0^2} \right] \approx \frac{1200}{\ln(2)} \left[ (\gamma_n - 1) B_0 + \frac{1}{2} (\gamma_n^2 - 1) (1 + \pi^2) B_0^2 \right]. \quad (26)$$

When  $n = 12$  and  $B_0 = 3 \times 10^{-3}$ , the corresponding shift is approximately 5.5 cents, with the quadratic term contributing about 0.25 cents. Note that (to zero order in  $Q_n$ ) this bending stiffness error does not depend on the tiny changes to the linear mass density or the tension that arises due to string fretting. Instead, it is an intrinsic property of the string.

Incorporating all of these effects — and neglecting the term proportional to  $B_0^2$  — we find that the total frequency shift is given by

$$\Delta \nu_n \approx \frac{1200}{\ln(2)} \left[ (\gamma_n - 1) \left( B_0 - \frac{\Delta S}{X_0} \right) + \frac{\Delta N}{X_0} + \frac{1}{2} \kappa Q_n \right]. \quad (27)$$

In this form, we see that the bending stiffness and the increase in string tension due to fretting sharpen the pitch, but that we can flatten it with a positive saddle setback and negative nut setback. In fact, a simple compensation strategy would be to choose  $\Delta S = B_0 X_0$  to compensate for stiffness, and then select  $\Delta N = -\kappa X_0 \bar{Q}/2$ , where  $\bar{Q}$  is the displacement averaged over a particular set of frets. We’ll rely on a more flexible method for compensation in Section 4, but we’ll obtain results that are similar to those found using this basic approach.



### 3 Experimental Estimate of the String Constant

How do we determine the spring constant  $\kappa$  given by Eq. (23)? Ideally, we could conduct an experiment that measures the change in the frequency of an open string — pinned at one end, and clamped at the other — as we make slight changes to its length [1, 3]. From Eq. (6), the derivative of the fundamental frequency of an open string is

$$\begin{aligned}\frac{df}{dL} &= \frac{f}{L} \left( -1 + \frac{L}{2T} \frac{dT}{dL} - \frac{L}{2\mu} \frac{d\mu}{dL} + \frac{L}{1+B} \frac{dB}{dL} \right) \\ &= \frac{f}{L} \left( -1 + \frac{1}{2} \kappa + \frac{1}{2} - \frac{B}{1+B} \right) \\ &\approx \frac{f}{L} \times \frac{1}{2} (\kappa - 1),\end{aligned}\tag{28}$$

where we have used the analysis in Section 2 to determine that

$$\frac{dT}{dL} = \frac{T}{L} \kappa, \tag{29a}$$

$$\frac{d\mu}{dL} = -\frac{\mu}{L}, \text{ and} \tag{29b}$$

$$\frac{dB}{dL} = -\frac{B}{L}. \tag{29c}$$

$$\tag{29d}$$

Therefore, following Byers [1, 3], we define the parameter  $R$  to be

$$R \equiv \frac{L}{f} \frac{df}{dL} = \frac{1}{2} (\kappa - 1), \tag{30}$$

which gives

$$\kappa = 2R + 1. \tag{31}$$

With this measurement of  $\kappa$ , we can estimate the bending stiffness coefficient by comparing Eq. (23) and Eq. (25), and writing  $B_0$  as

$$B_0 = \sqrt{\kappa} \frac{\rho}{2L_0}. \tag{32}$$

It is relatively easy to estimate the values of  $\kappa$  and  $R$  for any guitar string with the aid of a simple device that can measure frequency shifts in cents [11]. First, we tune the open string to the correct 12-TET frequency. Then, we select a fret  $n$ , and measure the frequency deviation  $\Delta\nu_n$  of the fretted string. If we substitute Eq. (32) into Eq. (27), then we find

$$\alpha \kappa + \beta \sqrt{\kappa} - \xi = 0, \tag{33}$$

where we have included the quadratic bending stiffness term, and defined the coefficients

$$\alpha \equiv \frac{1}{2} \left[ Q_n + (\gamma_n^2 - 1) (1 + \pi^2) \left( \frac{\rho}{2L_0} \right)^2 \right], \tag{34a}$$

$$\beta \equiv (\gamma_n - 1) \frac{\rho}{2L_0}, \text{ and} \tag{34b}$$

$$\xi \equiv \frac{\ln(2)}{1200} \Delta\nu_n + \frac{(\gamma_n - 1) \Delta S - \Delta N}{X_0}. \tag{34c}$$

Equation (33) is quadratic in  $\sqrt{\kappa}$ , with the solution

$$\sqrt{\kappa} = \frac{-\beta + \sqrt{\beta^2 + 4\alpha\xi}}{2\alpha}, \quad (35)$$

where we have chosen the positive root.

We’ve used this approach to estimate  $\kappa$  and  $R$  of different string sets on the Alhambra 8P classical guitar, which has  $X_0 = 650$  mm,  $c = 3.5$  mm,  $\Delta S = 1.5$  mm, and  $\Delta N = 0.0$  mm. At the nut,  $b = 1.0$  mm, but the height of the fret board decreases roughly linearly further toward the saddle, effectively increasing  $b$ . We estimate that  $db/dx \approx -0.0034$ , so that  $b$  has increased to 2.0 mm at the 12<sup>th</sup> fret. We show the specifications of a normal-tension classical string set in Table 1 using metric units<sup>1</sup>. In Table 2, we list the frequency deviation from 12-TET at the 12<sup>th</sup> fret for each string in this set, as well as the corresponding estimates of  $\kappa$ ,  $R$ ,  $E$ , and  $B_0$ , computed from Eq. (35), Eq. (30), Eq. (23), and Eq. (32), respectively. The units used for the elastic modulus are gigapascals (1 GPa =  $10^9$  N/m<sup>2</sup>). Similar measurements and results for other string sets are provided in Appendix D.

Table 1: String specifications for the D’Addario Pro-Arte Nylon Classical Guitar Strings – Normal Tension (EJ45). The corresponding scale length is 650 mm.

String	Note	Radius (mm)	Density ( $\times 10^{-7}$ kg/mm)	Tension (N)
J4501	E <sub>4</sub>	0.36	3.74	68.62
J4502	B <sub>3</sub>	0.41	5.05	52.04
J4503	G <sub>3</sub>	0.51	8.36	54.26
J4504	D <sub>3</sub>	0.37	19.21	69.99
J4505	A <sub>2</sub>	0.44	32.90	67.27
J4506	E <sub>2</sub>	0.55	54.72	62.80

Table 2: Derived physical properties of the D’Addario Pro-Arte Nylon Classical Guitar Strings – Normal Tension (EJ45). The corresponding scale length is 650 mm.

String	$\Delta v_{12}$ (cents)	$R$	$\kappa$	$E$ (GPa)	$B_0$ ( $\times 10^{-3}$ )
J4501	3	28.3	57.5	9.9	2.1
J4502	2	20.3	41.5	4.1	2.0
J4503	10	55.0	110.9	7.3	4.1
J4504	0	12.3	25.6	4.2	1.4
J4505	2	18.8	38.5	4.2	2.1
J4506	4	23.4	47.9	3.2	2.9

## 4 Classical Guitar Compensation

Using the data and results presented in Table 2, we can explore different approaches to compensating guitar strings for bending stiffness and string tension perturbations. For example,

<sup>1</sup>Note that the correct unit of force in the metric system is Newtons (N), rather than kilograms, which is a unit of mass.

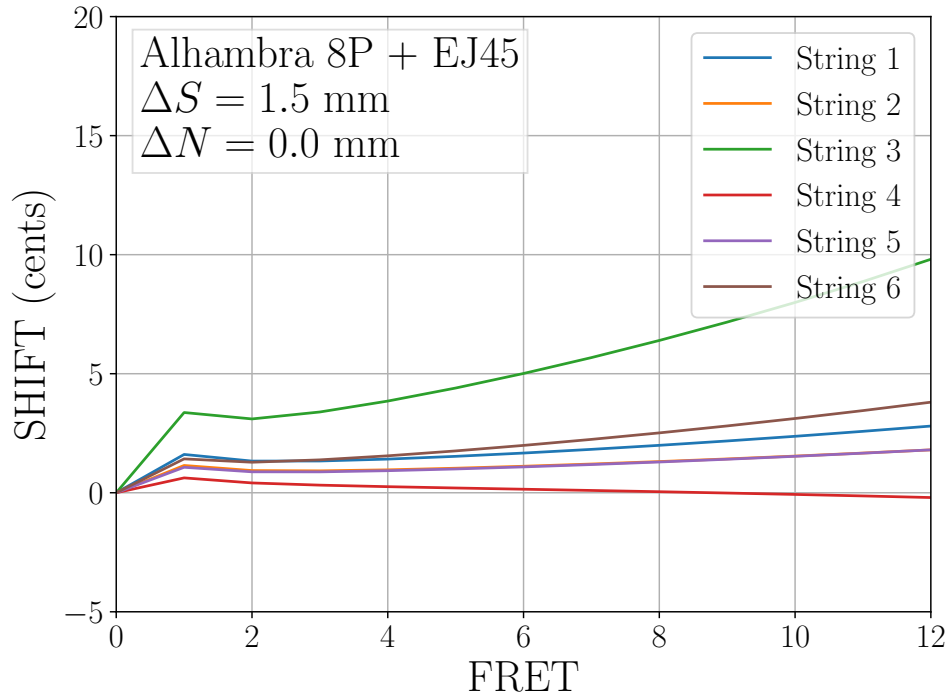
in Fig. 3a, we plot the frequency deviation (in cents) from ideal 12-TET for each string at each of the first 12 frets of an Alhambra 8P classical guitar, assuming that the open string has been perfectly tuned to the correct frequency. Recall that the Alhambra 8P is manufactured with a saddle setback of 1.5 mm, presumably to offset the effects of bending stiffness in the strings. For comparison, in Fig. 3b, we plot the same deviations for the case where  $\Delta S = 0$ , which increases the error of each string at the 12<sup>th</sup> fret by 3 – 4 cents. Recall from Section 2 that we could crudely predict the values of the saddle and setbacks by inspecting Eq. (27). For example, from Table 2, we estimate  $\Delta S \approx B_0 X_0 = 2.7$  mm and  $\Delta N \approx -1.5$  mm for the third (G) string.

Instead of this simple approach, we adopt the method described in Appendix C and adjust the setbacks to minimize the root-mean-squared average of the frequency deviations for each string. This mean (over the first 12 frets) can be computed by squaring the frequency deviations shown in Fig. 3b, averaging those values, and then taking the square root of the result. The setbacks we obtain are listed in Table 3, and the corresponding frequency deviations — obtained with different setbacks for every string — are shown in Fig. 4a (assuming that all other aspects of the Alhambra 8P remain unchanged). Note that the saddle setbacks tend to be larger — and the nut setbacks smaller — than the simple estimates that we made above. This is easily understood by examining Eq. (27): the portion of  $\Delta S$  that exceeds  $B_0 X_0$  scales with  $\gamma_n - 1$ , and helps to compensate for tension errors as  $n$  increases.

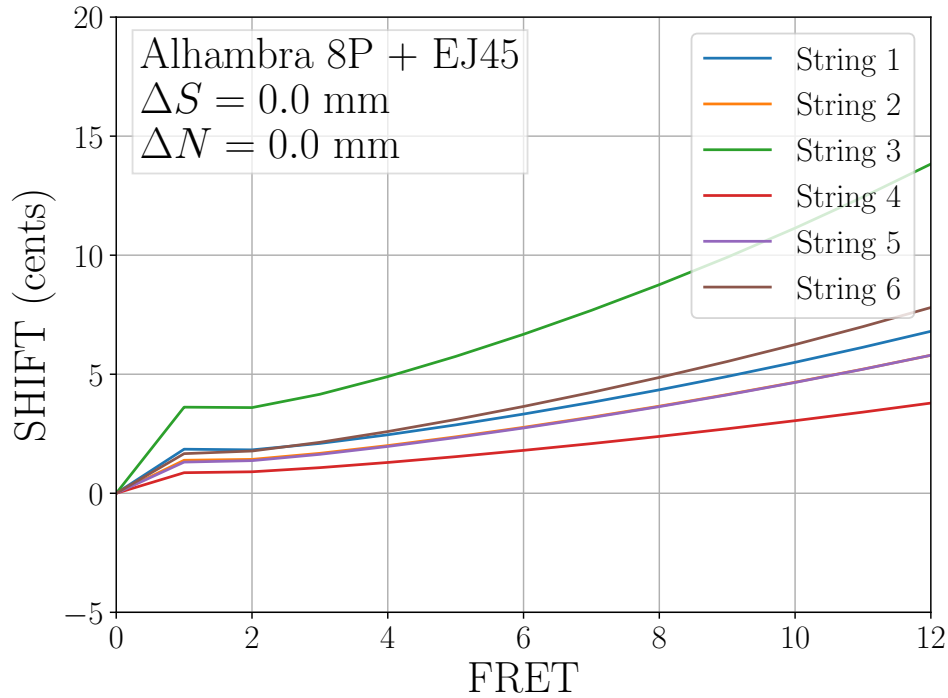
Table 3: Predicted setbacks for the D’Addario Pro-Arte Nylon Classical Guitar Strings – Normal Tension (EJ45) on the Alhambra 8P classical guitar.

String	$\Delta S$ (mm)	$\Delta N$ (mm)	$\overline{\Delta v_{\text{rms}}}$ (cents)
J4501	2.16	-0.43	0.18
J4502	1.92	-0.31	0.15
J4503	4.36	-0.82	0.31
J4504	1.30	-0.19	0.13
J4505	1.94	-0.28	0.15
J4506	2.62	-0.35	0.16

We close this section with a few comments. First, all of the compensated frequency deviation plots presented in this version of our work are theoretical; in the future, we will present experimental results to determine the efficacy of this compensation approach. Second, it is nontrivial to manufacture a guitar with different setbacks for each string [1], and it is unlikely that the exact values listed in Table 3 are applicable to other string sets. We have measured frequency deviations at the 12<sup>th</sup> fret for three other string sets, and in Appendix D we have reproduced the compensation procedure for them. There is enough variation in the setbacks across all strings that it would be difficult to find values that could work well for all string sets. Finally, it is possible to simply take the mean setbacks over the all strings in a particular set, and then use these mean values for all strings. We illustrate this approach in Fig. 4b; the frequency deviations are not as small as in Fig. 4a, but they are generally less than 5 cents. In the next section, we discuss a method to temper the guitar to reduce these errors further.

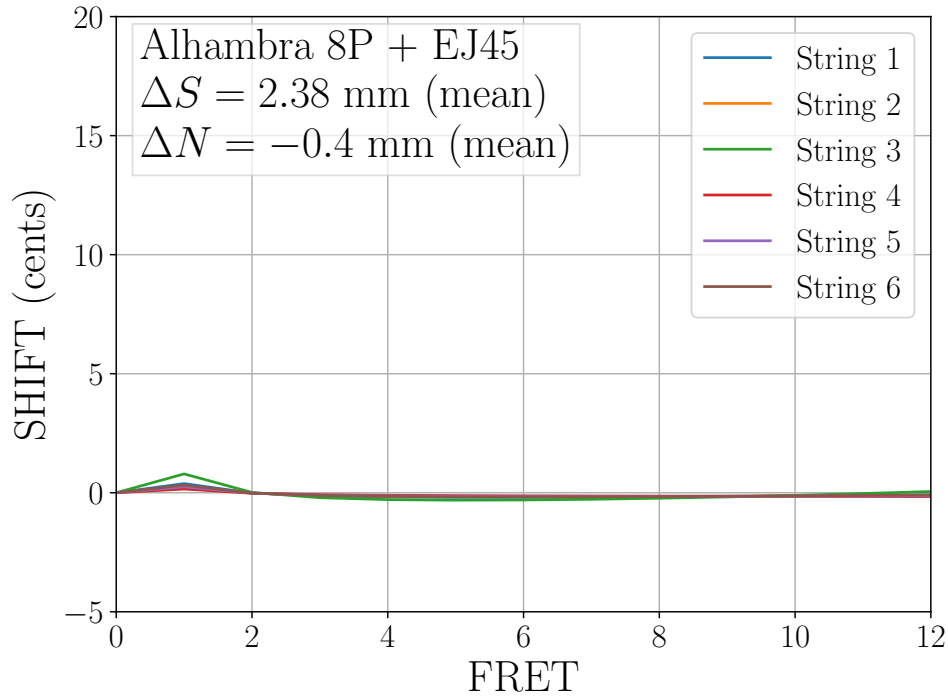


(a) Factory guitar

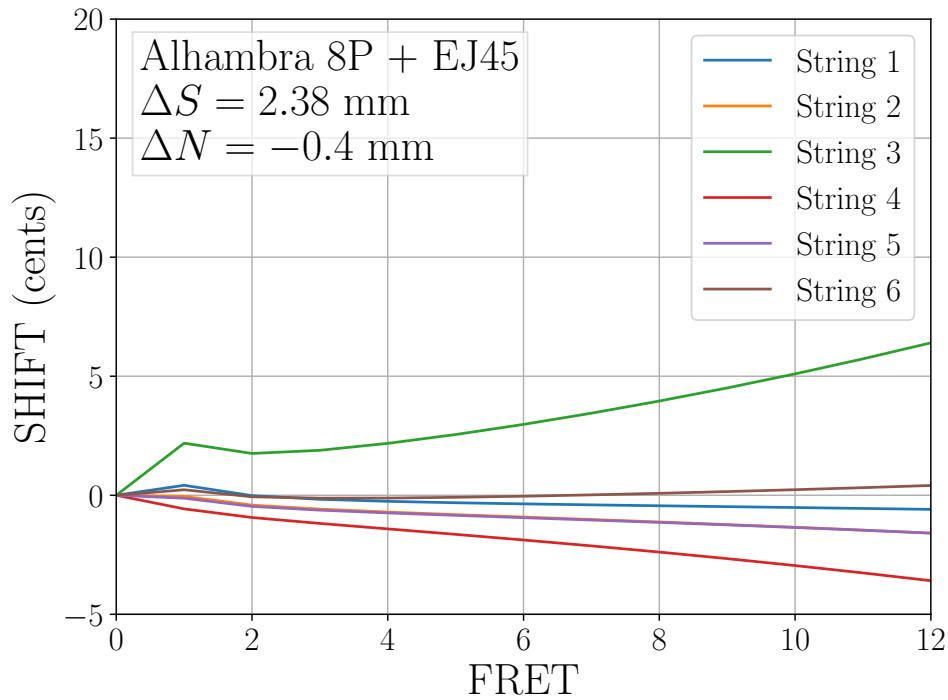


(b) Uncompensated

Figure 3: Frequency shifts (in cents) for an Alhambra 8P guitar with normal tension nylon strings (D'Addario EJ45). In (a), we show the deviations of the guitar as manufactured in the factory, completely consistent with our measurements. In (b), we show the same 12-TET errors that would arise if  $\Delta S = 0$  for the same guitar.



(a) Full compensation



(b) Mean compensation

Figure 4: Frequency shifts (in cents) for an “Alhambra 8P” guitar with normal tension nylon strings (D’Addario EJ45). Instead of the factory setbacks, in (a) we use the individual values for each string that are listed in Table 3. In (b), we set  $\Delta S$  and  $\Delta N$  to the mean of the corresponding column in that table.

## 5 Tempering the Classical Guitar

Temperament: A compromise between the acoustic purity of theoretically exact intervals, and the harmonic discrepancies arising from their practical employment.

— Dr. Theo. Baker [13]

In Fig. 5a, the Alhambra 8P factory guitar with normal tension strings tuned to 12-TET shows the third string having the greatest error in tuning across the fretboard. Tuning the factory guitar to 12-TET exacts a perfect-fifth in the third string while playing a C major chord in first position. This results in the third string being too sharp for the other common chords of E major (G#), A major and D major (A), particularly when the guitar is played at a higher fret position. One way to reduce this error is by lowering the pitch of the third string below 12-TET with an electronic tuner. Another more comprehensive system is to tune all the strings harmonically to the fifth string, which lowers the third string by 7 cents as well as tempering the remaining strings.

In this particular case, the “Harmonic Tuning Method” can be followed using these steps:

1. Begin by tuning the fifth string to  $A_2 = 110$  Hz, resulting in a fifth-fret harmonic of  $A_4 = 440$  Hz. (This can also be tuned by ear using an  $A_4$  tuning fork).
2. Tune that harmonic to the seventh fret harmonic of the fourth string, which is also  $A_4 = 440$  Hz.
3. Tune the seventh fret harmonic on the fifth string (330 Hz, or 0.37 Hz sharper than 12-TET  $E_4$ ) to the fifth-fret harmonic of the sixth string.
4. The seventh fret harmonic on the fifth string can tune the remaining fretted strings: the ninth fret on the third string, the fifth fret on the second string, and the open first string.

Table 4: Harmonic tuning methodology based on  $A_4$  and  $E_4$ . The asterisk indicates a harmonic with a null at the designated fret.

Reference String/Fret	Target String/Fret
$A^*/5$ ( $A_4$ )	$D^*/7$
$A^*/7$ ( $E_4$ )	$E^*/5$
$A^*/7$ ( $E_4$ )	G/9
$A^*/7$ ( $E_4$ )	B/5
$A^*/7$ ( $E_4$ )	E/0

We have summarized these steps in Table 4, and in Figure 5b we show the same guitar tuned in this fashion. Note that other tuning choices can be made depending on the piece being played. For example, the third string could also be tuned at the second fret to  $A_3 = 220$  Hz using the fifth-string harmonic at the 12<sup>th</sup> fret, and/or the first string could be tuned at the fifth fret to  $A_4$  using the fifth-fret harmonic of the fifth string. The flexibility of the harmonic tuning method — and its reliance on only an  $A_4$  tuning fork — is a great asset for the classical guitarist.

In fact, compensation at the factory and harmonic tuning can be combined to allow guitars with a wide variety of string sets to be well-tempered. For example, in Fig. 6a, we plot frequency

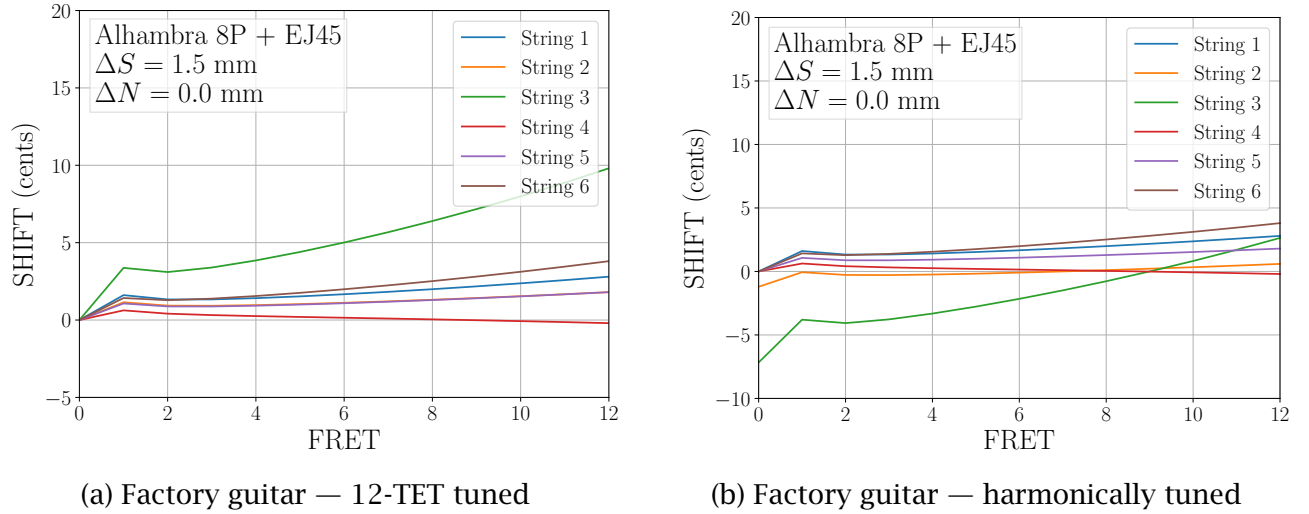


Figure 5: Frequency shift (in cents) for an Alhambra 8P guitar with normal tension nylon strings (D’Addario EJ45). Here we compare (a) the factory guitar tuned to 12-TET with (b) the same guitar harmonically tuned using the approach outlined in Table 4.

shifts (in cents) for an “Alhambra 8P” guitar with normal tension nylon strings (D’Addario EJ45). But, instead of the factory setbacks, we set  $\Delta S$  and  $\Delta N$  to the mean of the corresponding column in Table 3 *neglecting the third string*. This choice results in significant reductions in those setbacks, but the RMS frequency error for the third string is 4.7 cents for 12-TET tuning. In Fig. 6b, we show that the harmonic tuning method described in Table 4 reduces that RMS error to 2.2 cents.

## 6 Conclusion

### A Vibration Frequencies of a Stiff String

Here we outline the calculation of the normal mode frequencies of a vibrating stiff string with non-symmetric boundary conditions. We begin with the wave equation [14]

$$\mu \frac{\partial^2}{\partial t^2} y(x) = T \frac{\partial^2}{\partial x^2} y(x) - E S \mathcal{K}^2 \frac{\partial^4}{\partial x^4} y(x), \quad (36)$$

where  $\mu$  and  $T$  are respectively the linear mass density and the tension of the string,  $E$  is its Young’s modulus (or the modulus of elasticity),  $S$  is the cross-sectional area, and  $\mathcal{K}$  is the radius of gyration of the string. (For a uniform cylindrical string/wire with radius  $\rho$ ,  $S = \pi \rho^2$  and  $\mathcal{K} = \rho/2$ .) If we scale  $x$  by the length  $L$  of the string, and  $t$  by  $1/\omega_0 \equiv (L/\pi)\sqrt{\mu/T}$ , then we obtain the dimensionless wave equation

$$\pi^2 \frac{\partial^2}{\partial t^2} y(x) = \frac{\partial^2}{\partial x^2} y(x) - B^2 \frac{\partial^4}{\partial x^2} y(x), \quad (37)$$

where  $B$  is the “bending stiffness parameter” given by

$$B \equiv \sqrt{\frac{E S \mathcal{K}^2}{L^2 T}}. \quad (38)$$

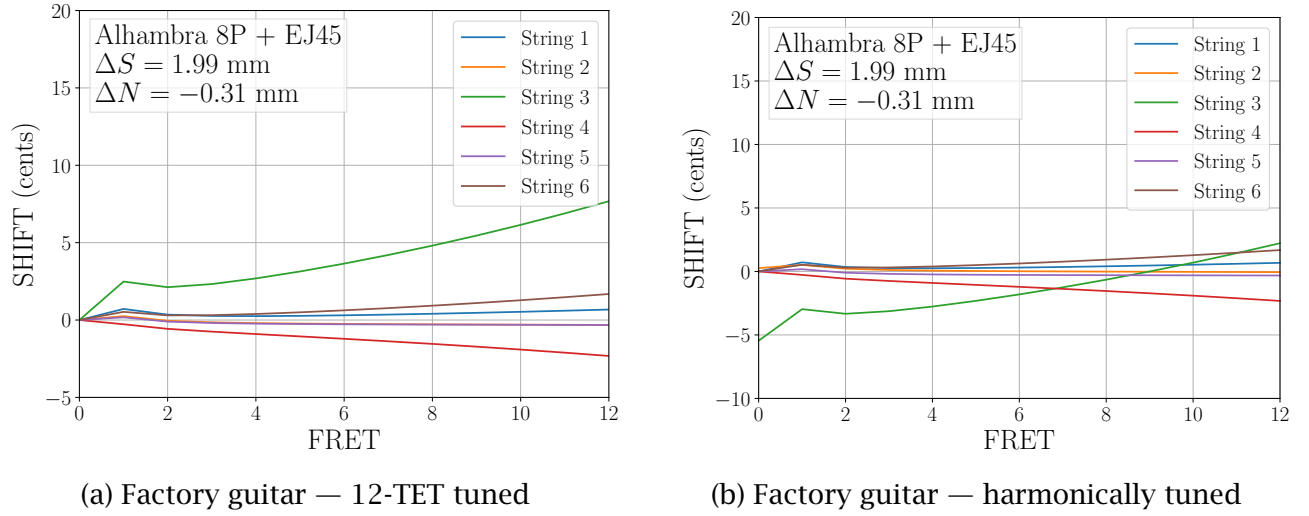


Figure 6: Frequency shifts (in cents) for an “Alhambra 8P” guitar with normal tension nylon strings (D’Addario EJ45). Instead of the factory setbacks, in (a) we set  $\Delta S$  and  $\Delta N$  to the mean of the corresponding column in Table 3 *neglecting the third string*. In (b), we show the same guitar harmonically tuned using the approach outlined in Table 4.

We assume that  $y(x)$  is a sum of terms of the form

$$y(x) = C e^{kx - i\omega t}, \quad (39)$$

requiring that  $k$  and  $\omega$  satisfy the expression

$$B^2 k^4 - k^2 - (\pi \omega)^2 = 0, \quad (40)$$

or

$$k^2 = \frac{1 \pm \sqrt{1 + (2\pi B \omega)^2}}{2B^2}. \quad (41)$$

Therefore, given  $\omega$ , we have four possible choices for  $k$ :  $\pm k_1$ , or  $\pm i k_2$ , where

$$k_1^2 = \frac{\sqrt{1 + (2\pi B \omega)^2} + 1}{2B^2}, \text{ and} \quad (42a)$$

$$k_2^2 = \frac{\sqrt{1 + (2\pi B \omega)^2} - 1}{2B^2}. \quad (42b)$$

The corresponding general solution to Eq. (37) has the form

$$y(x) = e^{-i\omega t} \left( C_1^+ e^{k_1 x} + C_1^- e^{-k_1 x} + C_2^+ e^{ik_2 x} + C_2^- e^{-ik_2 x} \right). \quad (43)$$

As discussed in Section 2, the boundary conditions for the case of a classical guitar string are not symmetric. At  $x = 0$  (the saddle), the string is pinned (but not clamped), so that  $y = 0$  and  $\partial^2 y / \partial x^2 = 0$ . However, at  $x = 1$  (the fret) the string is clamped, so that  $y = 0$  and  $\partial y / \partial x = 0$ . Applying these constraints to Eq. (43), we obtain

$$0 = C_1^+ + C_1^- + C_2^+ + C_2^-, \quad (44a)$$

$$0 = k_1^2 (C_1^+ + C_1^-) - k_2^2 (C_2^+ + C_2^-), \quad (44b)$$

$$0 = C_1^+ e^{k_1} + C_1^- e^{-k_1} + C_2^+ e^{ik_2} + C_2^- e^{-ik_2}, \text{ and} \quad (44c)$$

$$0 = k_1 (C_1^+ e^{k_1} - C_1^- e^{-k_1}) + ik_2 (C_2^+ e^{ik_2} - C_2^- e^{-ik_2}). \quad (44d)$$



Since  $k_1^2 + k_2^2 \neq 0$ , the first two of these equations tell us that  $C_1^- = -C_1^+ \equiv -C_1$ , and  $C_2^- = -C_2^+ \equiv -C_2$ . Therefore, the second two equations become

$$C_1 \sinh(k_1) = -i C_2 \sin(k_2), \text{ and} \quad (45a)$$

$$k_1 C_1 \cosh(k_1) = -i k_2 C_2 \cos(k_2). \quad (45b)$$

Dividing the first of these equations by the second, we find

$$\tan(k_2) = \frac{k_2}{k_1} \tanh k_1. \quad (46)$$

From Eq. (42), we see that  $k_1^2 - k_2^2 = 1/B^2$ , so that

$$k_1 = \frac{1}{B} \sqrt{1 + (B k_2)^2}. \quad (47)$$

In the case of a classical guitar, we expect that  $B \ll 1$ , so  $k_1 \approx 1/B \gg 1$ , and therefore  $\tanh k_1 \rightarrow 1$ . Substituting Eq. (47) into Eq. (46), we obtain

$$\tan(k_2) = \frac{B k_2}{\sqrt{1 + (B k_2)^2}}. \quad (48)$$

We expect that  $B k_2 \ll 1$ , so we assume that  $k_2 = m\pi(1 + \epsilon)$ , where  $m$  is an integer greater than or equal to 1, and  $\epsilon \ll 1$ . Therefore, to second order in  $\epsilon$ , we have  $\tan(k_2) \approx m\pi\epsilon$ , and

$$\epsilon = \frac{B(1 + \epsilon)}{\sqrt{1 + [m\pi B(1 + \epsilon)]^2}}. \quad (49)$$

The denominator of the right-hand side of this equation has a Taylor expansion given by  $1 - \frac{1}{2} [m\pi B(1 + \epsilon)]^2$ , indicating that it will not contribute to  $\epsilon$  to second order in  $B$ . Therefore, to this order,

$$\epsilon \approx \frac{B}{1 - B} \approx B + B^2. \quad (50)$$

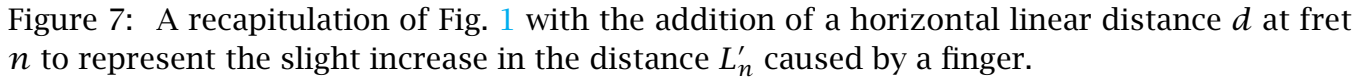
We substitute  $k = \pm i k_2$  into Eq. (40) with  $k_2 = m\pi/(1 - B)$  to obtain

$$\begin{aligned} \omega &= \frac{k_2}{\pi} \sqrt{1 + (B k_2)^2} \\ &= \frac{m}{1 - B} \sqrt{1 + m^2 \pi^2 \left( \frac{B}{1 - B} \right)^2} \\ &\approx m \left[ 1 + B + \left( 1 + \frac{1}{2} m^2 \pi^2 \right) B^2 \right]. \end{aligned} \quad (51)$$

Restoring the time scaling by  $1/\omega_0$ , and defining the frequency (in cycles/second)  $f = \omega/2\pi$ , we finally have

$$f_m = \frac{m}{2L} \sqrt{\frac{T}{\mu}} \left[ 1 + B + \left( 1 + \frac{1}{2} m^2 \pi^2 \right) B^2 \right]. \quad (52)$$

We use this result to build our model in Section 2.

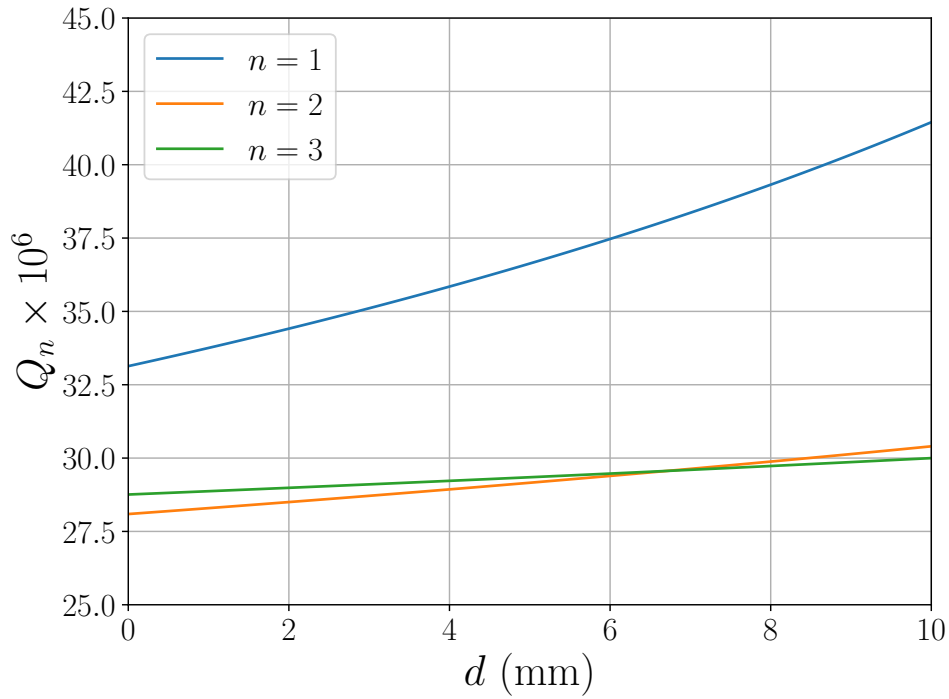
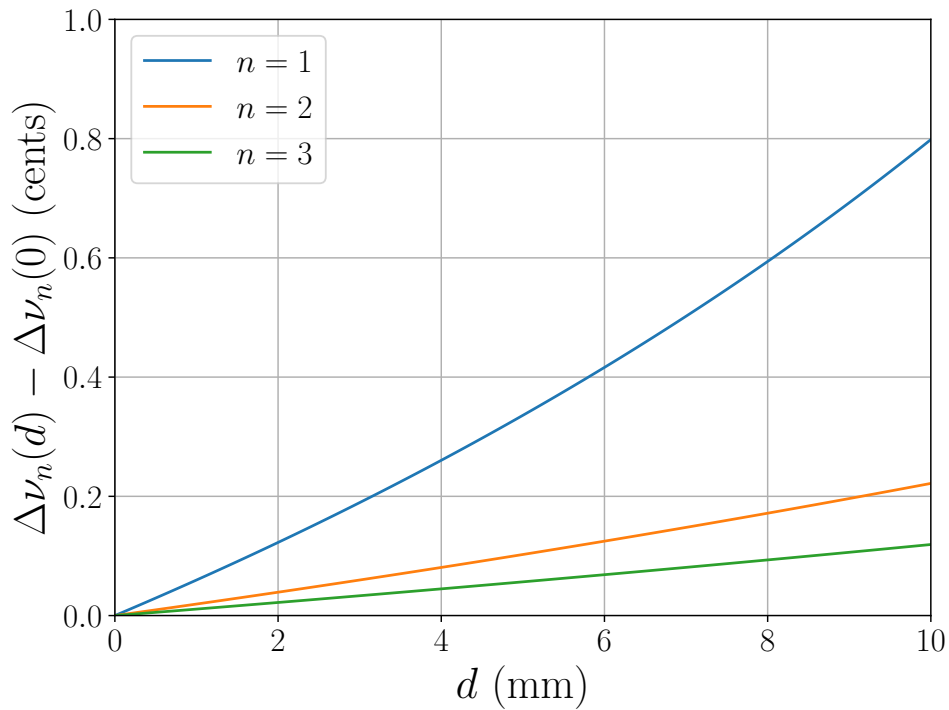


As discussed in Section 2, we have neglected to include a contribution to the incremental change in the length of the fretted string caused by both the depth and the shape of the string under the finger [1, 3]. Here we include this concept in a simple way to determine the effect it could have on the frequency shift due to increased string tension. In Fig. 7, we adopt the schematic of the guitar shown in Fig. 1, but we allow a small, horizontal linear section of string with length  $d$  to represent the action of the finger. In this case, the resonant length  $L_n$  is unaffected, but the remaining string length becomes

Roughly speaking, the act of fretting increases the effective value of  $b^2$  in  $L'_n$  by a factor of  $1 + d/(X_0 - X_n)$ . We can use Eq. (16) to determine the increase in the relative displacement  $Q_n$ .

## C Compensation by Minimizing RMS Error

$$\overline{\Delta v}_{\text{rms}} \equiv \sqrt{\frac{\sum_{n=1}^{n_{\text{max}}} \Delta v_n^2}{n_{\text{max}}}}, \quad (54)$$

(a) Relative displacement  $Q_n$ 

(b) Additional frequency shift of string 3

Figure 8: In (a), we plot the relative displacement  $Q_n$  for the first three frets as a function of the fretting distance parameter  $d$ . Here the guitar has the same parameters as the Alhambra 8P, with normal tension strings. In (b), we show the additional frequency shift of the third string — with  $\kappa = 111$  — as  $d$  increases from 0. For  $n > 3$ , the additional shift is even smaller.

where  $\Delta v_n$  is given by Eq. (27). Here we will vary both  $\Delta S$  and  $\Delta N$  to minimize  $\overline{\Delta v}$ . In this case, it is sufficient to minimize the quantity

$$\chi^2 = \sum_{n=1}^{n_{\max}} \left[ \frac{\ln(2)}{1200} \Delta v_n \right]^2 \quad (55)$$

such that the gradient of  $\chi^2$  with respect to  $\Delta S$  and  $\Delta N$  vanishes. The components of this gradient are

$$\frac{\partial}{\partial \Delta S} \chi^2 = -\frac{2}{X_0} \sum_n (\gamma_n - 1) \left[ (\gamma_n - 1) \left( B_0 - \frac{\Delta S}{X_0} \right) + \frac{\Delta N}{X_0} + \frac{\kappa}{2} Q_n \right], \text{ and} \quad (56a)$$

$$\frac{\partial}{\partial \Delta N} \chi^2 = \frac{2}{X_0} \sum_n \left[ (\gamma_n - 1) \left( B_0 - \frac{\Delta S}{X_0} \right) + \frac{\Delta N}{X_0} + \frac{\kappa}{2} Q_n \right]. \quad (56b)$$

Setting both of these components to zero, we can rewrite them as the matrix equation

$$\begin{bmatrix} \sigma_2 & -\sigma_1 \\ \sigma_1 & -\sigma_0 \end{bmatrix} \begin{bmatrix} \Delta S \\ \Delta N \end{bmatrix} = X_0 \begin{bmatrix} \sigma_2 B_0 + \frac{1}{2} \kappa \overline{Q}_1 \\ \sigma_1 B_0 + \frac{1}{2} \kappa \overline{Q}_0 \end{bmatrix}, \quad (57)$$

where

$$\sigma_k \equiv \sum_{n=1}^{n_{\max}} (\gamma_n - 1)^k, \text{ and} \quad (58)$$

$$\overline{Q}_k \equiv \sum_{n=1}^{n_{\max}} (\gamma_n - 1)^k Q_n. \quad (59)$$

Equation (57) has the straightforward analytic solution

$$\begin{bmatrix} \Delta S \\ \Delta N \end{bmatrix} = \frac{X_0}{\sigma_1^2 - \sigma_0 \sigma_2} \begin{bmatrix} -\sigma_0 & \sigma_1 \\ -\sigma_1 & \sigma_2 \end{bmatrix} \begin{bmatrix} \sigma_2 B_0 + \frac{1}{2} \kappa \overline{Q}_1 \\ \sigma_1 B_0 + \frac{1}{2} \kappa \overline{Q}_0 \end{bmatrix}. \quad (60)$$

For completeness, the corresponding solution when the quadratic stiffness term is included is given by

$$\begin{bmatrix} \Delta S \\ \Delta N \end{bmatrix} = \frac{X_0}{\sigma_1^2 - \sigma_0 \sigma_2} \begin{bmatrix} -\sigma_0 & \sigma_1 \\ -\sigma_1 & \sigma_2 \end{bmatrix} \begin{bmatrix} \sigma_2 B_0 + \frac{1}{2} (1 + \pi^2) (2\sigma_2 + \sigma_3) B_0^2 + \frac{1}{2} \kappa \overline{Q}_1 \\ \sigma_1 B_0 + \frac{1}{2} (1 + \pi^2) (2\sigma_1 + \sigma_2) B_0^2 + \frac{1}{2} \kappa \overline{Q}_0 \end{bmatrix}. \quad (61)$$

The corresponding Hessian matrix for this problem is

$$H = \begin{bmatrix} \frac{\partial^2 \chi^2}{\partial \Delta S^2} & \frac{\partial^2 \chi^2}{\partial \Delta N \partial \Delta S} \\ \frac{\partial^2 \chi^2}{\partial \Delta S \partial \Delta N} & \frac{\partial^2 \chi^2}{\partial \Delta N^2} \end{bmatrix} = \frac{2}{X_0^2} \begin{bmatrix} \sigma_2 & -\sigma_1 \\ -\sigma_1 & \sigma_0 \end{bmatrix}. \quad (62)$$

The Hessian is positive definite if and only if all of its eigenvalues are positive, and in the case of a  $2 \times 2$  real matrix, this holds when the determinant is greater than zero. It is easy to verify numerically (and with some effort algebraically) that  $\text{Det}(H) > 0$  for  $n_{\max} > 1$ . Therefore, the solution for  $\Delta S$  and  $\Delta N$  given by Eq. (60) minimizes the RMS frequency error.

The setback solution given by Eq. (60) is valid for a single string, and results like those shown in Table 3 and Fig. 4a assume that the guitar is built such that each string — from a particular set of strings — has a unique saddle and nut setback. Suppose that we'd prefer to engineer a

guitar with single, uniform values of both  $\Delta S$  and  $\Delta N$  that provide reasonable compensation across an entire string set (or an ensemble of strings from a variety of manufacturers). In this case, Eq. (54) becomes

$$\overline{\Delta v}_{\text{rms}} \equiv \sqrt{\frac{\sum_{m=1}^{m_{\max}} \sum_{n=1}^{n_{\max}} [\Delta v_n^{(m)}]^2}{m_{\max} n_{\max}}}, \quad (63)$$

where  $m$  labels the strings in the set, and Eq. (27) has been updated to become

$$\Delta v_n^{(m)} \approx \frac{1200}{\ln(2)} \left\{ (\gamma_n - 1) \left[ B_0^{(m)} - \frac{\Delta S}{X_0} \right] + \frac{\Delta N}{X_0} + \frac{1}{2} \kappa^{(m)} Q_n \right\}. \quad (64)$$

If we rigorously follow the same approach that we used to arrive at Eq. (60), in the multi-string case we obtain

$$\begin{bmatrix} \Delta S \\ \Delta N \end{bmatrix} = \begin{bmatrix} \frac{1}{m_{\max}} \sum_{m=1}^{m_{\max}} \Delta S^{(m)} \\ \frac{1}{m_{\max}} \sum_{m=1}^{m_{\max}} \Delta N^{(m)} \end{bmatrix}, \quad (65)$$

where

$$\begin{bmatrix} \Delta S^{(m)} \\ \Delta N^{(m)} \end{bmatrix} = \frac{X_0}{\sigma_1^2 - \sigma_0 \sigma_2} \begin{bmatrix} -\sigma_0 & \sigma_1 \\ -\sigma_1 & \sigma_2 \end{bmatrix} \begin{bmatrix} \sigma_2 B_0^{(m)} + \frac{1}{2} \kappa^{(m)} \overline{Q}_1 \\ \sigma_1 B_0^{(m)} + \frac{1}{2} \kappa^{(m)} \overline{Q}_0 \end{bmatrix}. \quad (66)$$

In other words, we can find the optimum values for both  $\Delta S$  and  $\Delta N$  simply by averaging the corresponding setbacks over a commercially interesting collection of string sets.

## D Other Classical Guitar String Sets

### D.1 Light Tension

Table 5: String specifications for the D’Addario Pro-Arte Nylon Classical Guitar Strings – Light Tension (EJ43). The corresponding scale length is 650 mm.

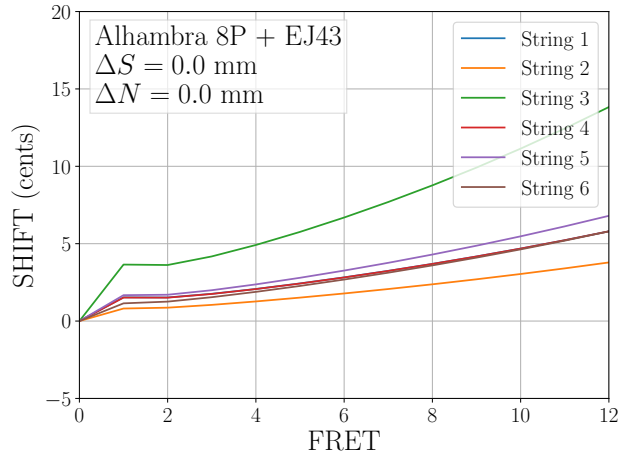
String	Note	Radius (mm)	Density ( $\times 10^{-7}$ kg/mm)	Tension (N)
J4301	E <sub>4</sub>	0.35	3.62	66.39
J4302	B <sub>3</sub>	0.40	4.87	50.24
J4303	G <sub>3</sub>	0.50	8.08	52.48
J4304	D <sub>3</sub>	0.36	18.23	66.41
J4305	A <sub>2</sub>	0.42	27.41	56.06
J4306	E <sub>2</sub>	0.53	51.59	59.21

Table 6: Derived physical properties of the D’Addario Pro-Arte Nylon Classical Guitar Strings – Light Tension (EJ43). The corresponding scale length is 650 mm.

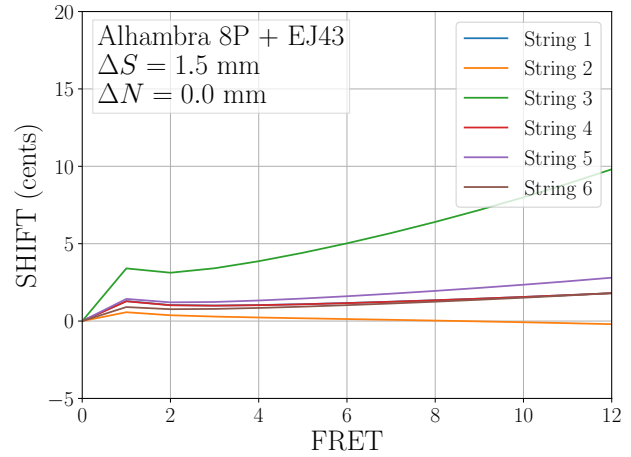
String	$\Delta v_{12}$ (cents)	$R$	$\kappa$	$E$ (GPa)	$B_0$ ( $\times 10^{-3}$ )
J4301	3	23.2	47.3	8.2	1.8
J4302	2	11.2	23.4	2.3	1.5
J4303	10	55.6	112.2	7.4	4.1
J4304	0	22.8	46.7	7.8	1.9
J4305	2	24.8	50.5	5.1	2.3
J4306	4	15.5	32.0	2.1	2.3

Table 7: Predicted setbacks for the D’Addario Pro-Arte Nylon Classical Guitar Strings – Light Tension (EJ43) on the Alhambra 8P classical guitar.

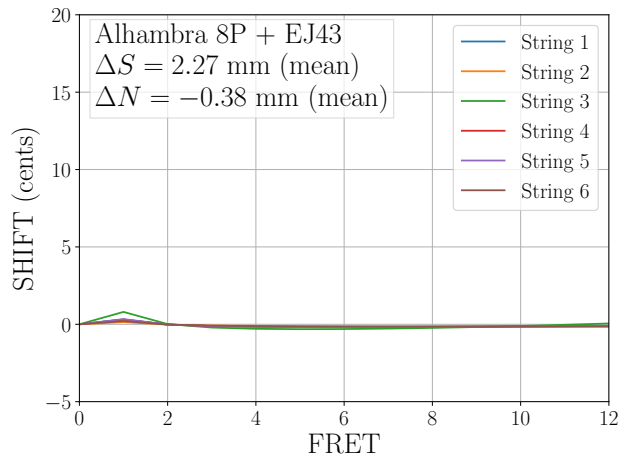
String	$\Delta S$ (mm)	$\Delta N$ (mm)	$\overline{\Delta v}_{\text{rms}}$ (cents)
J4301	1.87	-0.35	0.16
J4302	1.31	-0.17	0.13
J4303	4.35	-0.83	0.31
J4304	1.88	-0.35	0.16
J4305	2.22	-0.37	0.17
J4306	2.00	-0.24	0.14



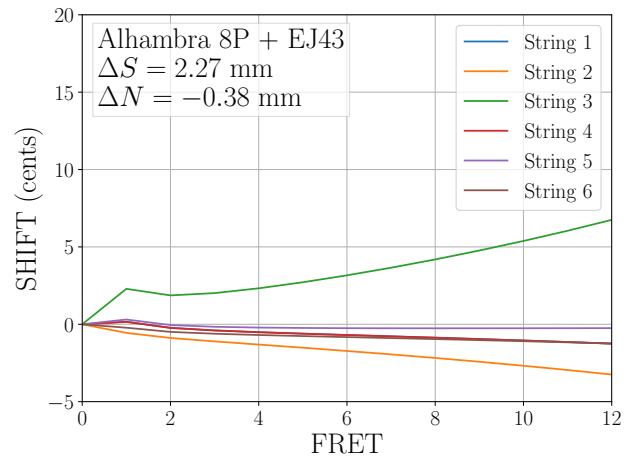
(a) Uncompensated



(b) Factory guitar



(c) Full compensation



(d) Mean compensation

Figure 9: Frequency shift (in cents) for an Alhambra 8P guitar with D'Addario Pro-Arte Nylon Classical Guitar Strings - Light Tension (EJ43). Four different strategies of saddle and nut compensation are illustrated.

## D.2 Hard Tension

Table 8: String specifications for the D'Addario Pro-Arte Nylon Classical Guitar Strings – Hard Tension (EJ46). The corresponding scale length is 650 mm.

String	Note	Radius (mm)	Density ( $\times 10^{-7}$ kg/mm)	Tension (N)
J4601	E <sub>4</sub>	0.36	3.86	70.88
J4602	B <sub>3</sub>	0.42	5.22	53.83
J4603	G <sub>3</sub>	0.52	8.57	55.61
J4604	D <sub>3</sub>	0.38	20.07	73.14
J4605	A <sub>2</sub>	0.46	34.87	71.31
J4606	E <sub>2</sub>	0.56	56.67	65.04

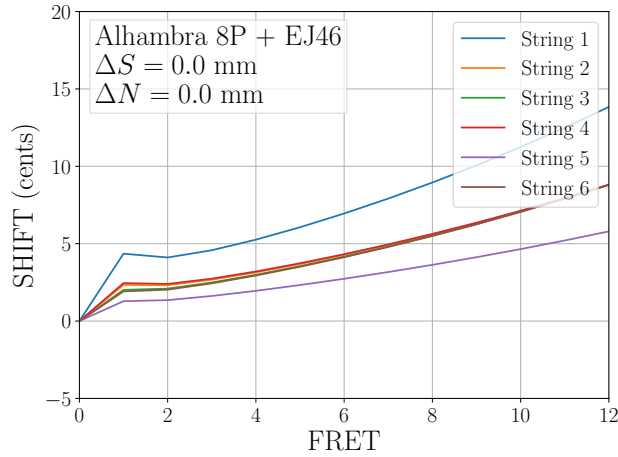
Table 9: Derived physical properties of the D'Addario Pro-Arte Nylon Classical Guitar Strings – Hard Tension (EJ46). The corresponding scale length is 650 mm.

String	$\Delta v_{12}$ (cents)	$R$	$\kappa$	$E$ (GPa)	$B_0$ ( $\times 10^{-3}$ )
J4601	3	69.4	139.8	24.1	3.3
J4602	2	35.4	71.9	7.1	2.7
J4603	10	29.2	59.4	3.9	3.1
J4604	0	37.8	76.6	12.3	2.6
J4605	2	18.2	37.5	4.1	2.2
J4606	4	27.2	55.5	3.7	3.2

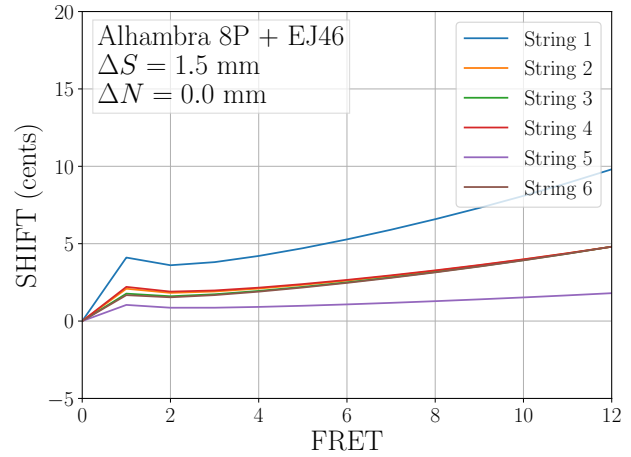
Table 10: Predicted setbacks for the D'Addario Pro-Arte Nylon Classical Guitar Strings – Hard Tension (EJ46) on the Alhambra 8P classical guitar.

String	$\Delta S$ (mm)	$\Delta N$ (mm)	$\overline{\Delta v}_{\text{rms}}$ (cents)
J4601	4.13	-1.04	0.38
J4602	2.80	-0.53	0.21
J4603	2.90	-0.44	0.18
J4604	2.76	-0.57	0.22
J4605	1.95	-0.28	0.15
J4606	2.93	-0.41	0.18

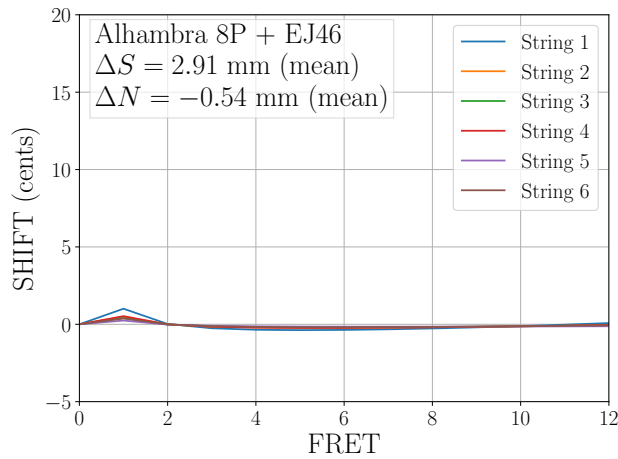




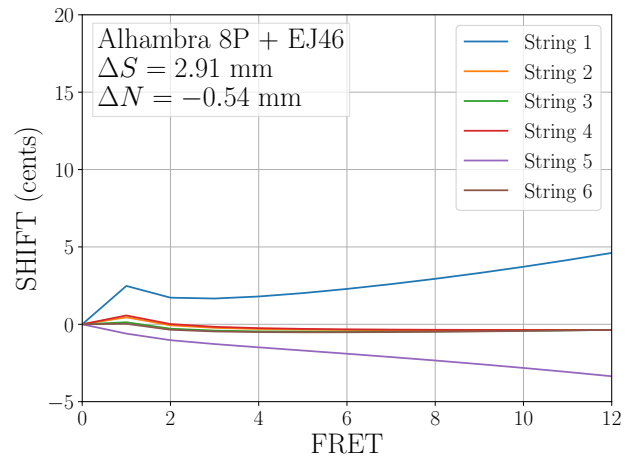
(a) Uncompensated



(b) Factory guitar



(c) Full compensation



(d) Mean compensation

Figure 10: Frequency shift (in cents) for an Alhambra 8P guitar with D'Addario Pro-Arte Nylon Classical Guitar Strings - Hard Tension (EJ46). Four different strategies of saddle and nut compensation are illustrated.

### D.3 Extra Hard Tension

Table 11: String specifications for the D’Addario Pro-Arte Nylon Classical Guitar Strings – Extra Hard Tension (EJ44). The corresponding scale length is 650 mm.

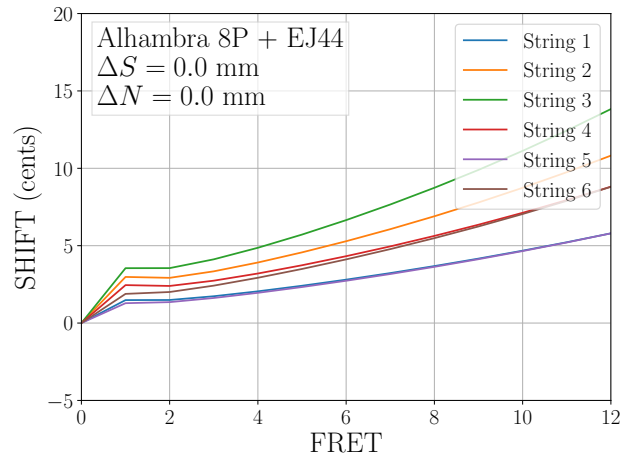
String	Note	Radius (mm)	Density ( $\times 10^{-7}$ kg/mm)	Tension (N)
J4401	E <sub>4</sub>	0.37	4.01	73.57
J4402	B <sub>3</sub>	0.42	5.44	56.07
J4403	G <sub>3</sub>	0.53	8.91	57.86
J4404	D <sub>3</sub>	0.38	20.07	73.14
J4405	A <sub>2</sub>	0.46	34.87	71.31
J4406	E <sub>2</sub>	0.57	61.36	70.42

Table 12: Derived physical properties of the D’Addario Pro-Arte Nylon Classical Guitar Strings – Extra Hard Tension (EJ44). The corresponding scale length is 650 mm.

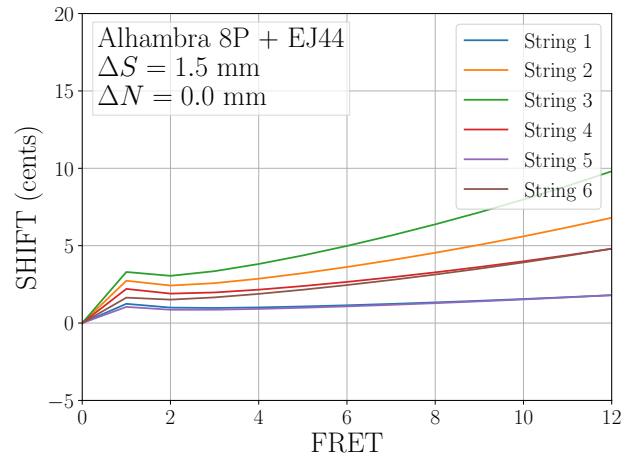
String	$\Delta v_{12}$ (cents)	$R$	$\kappa$	$E$ (GPa)	$B_0$ ( $\times 10^{-3}$ )
J4401	3	22.2	45.4	7.8	1.9
J4402	2	45.9	92.7	9.3	3.1
J4403	10	53.6	108.2	7.1	4.2
J4404	0	37.8	76.6	12.3	2.6
J4405	2	18.2	37.5	4.1	2.2
J4406	4	26.6	54.3	3.7	3.2

Table 13: Predicted setbacks for the D’Addario Pro-Arte Nylon Classical Guitar Strings – Extra Hard Tension (EJ44) on the Alhambra 8P classical guitar.

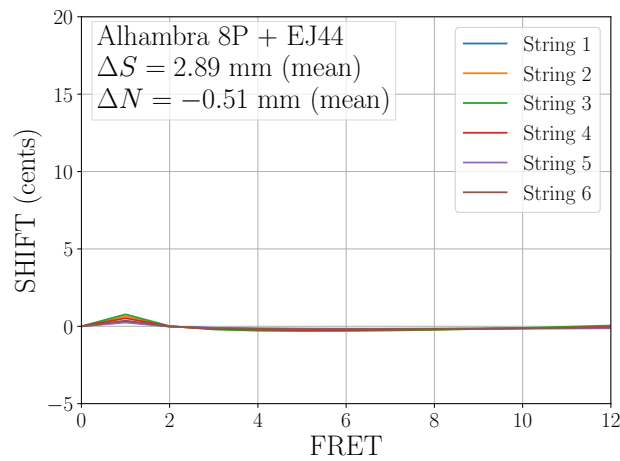
String	$\Delta S$ (mm)	$\Delta N$ (mm)	$\overline{\Delta v}_{\text{rms}}$ (cents)
J4401	1.89	-0.34	0.16
J4402	3.38	-0.69	0.26
J4403	4.39	-0.80	0.30
J4404	2.76	-0.57	0.22
J4405	1.95	-0.28	0.15
J4406	2.94	-0.40	0.17



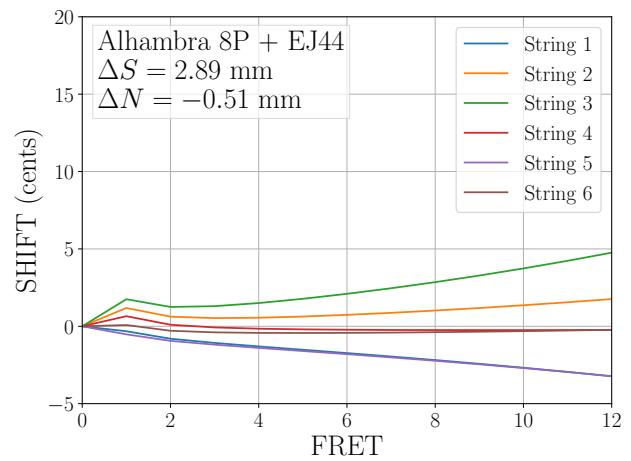
(a) Uncompensated



(b) Factory guitar



(c) Full compensation



(d) Mean compensation

Figure 11: Frequency shift (in cents) for an Alhambra 8P guitar with D'Addario Pro-Arte Nylon Classical Guitar Strings - Extra Hard Tension (EJ44). Four different strategies of saddle and nut compensation are illustrated.

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