

1. (a) Forward Euler: $y_{n+1} = y_n + h \times f(y_n, t_n)$

$$\text{Therefore } T(y_n, t_n) = y_n + h f(y_n, t_n)$$

$$g_n = \frac{\partial T(y_n, t_n)}{\partial y_n} = 1 + h \frac{\partial f(y_n, t_n)}{\partial y_n}$$

Depending on the form of $f(y_n, t_n)$ we have several cases:

\Rightarrow i) Decay-type problems with $\frac{\partial f}{\partial y} < 0$

$$g_n = 1 - h \left| \frac{\partial f}{\partial y_n} \right|,$$

and for stability

$$\begin{aligned} |g_n| < 1 &\Rightarrow 0 < 1 - h \left| \frac{\partial f(y_n, t_n)}{\partial y_n} \right| < 1 \\ &\Rightarrow h < \frac{2}{\left| \frac{\partial f(y_n, t_n)}{\partial y_n} \right|}, \end{aligned}$$

which means Forward Euler is conditionally stable.

ii) Growth-problems, $\frac{\partial f}{\partial y} > 0$

$g_n = 1 + h \frac{\partial f}{\partial y} > 1$, therefore it's unconditionally unstable.

iii) The function f is complex valued. $\frac{dy}{dt} = -i w y$

$$g_n = 1 - i w h \Rightarrow |g_n|^2 = 1 + h^2 w^2 > 1$$

hence instability for oscillatory case.

For given equation $f(y, t) = -y^2 - t^4$

$\frac{\partial f}{\partial y} = -2y$ if $y > 0$ then $\frac{\partial f}{\partial y} < 0$

Hence it's decay-type problem. And we find forward Euler is conditional stable with step size $h < \frac{2}{1 - y_n - t_n^4}$; But if $y < 0$, $\frac{\partial f}{\partial y} > 0$ is a growth type problem which implies unstable.

(b) (i) given Rk2: $y_{n+1} = y_n + h [a_1 f(y_n, t_n) + a_2 f(y_n + a_3 h f(y_n, t_n), t_n + a_4 h)]$ ①

do Taylor expansion with $f(y_n + a_3 h f(y_n, t_n), t_n + a_4 h)$:

$f(y_n + a_3 h f(y_n, t_n), t_n + a_4 h)$

$$= f(y_n, t_n) + a_3 h f(y_n, t_n) \frac{\partial f(y_n, t_n)}{\partial y_n} + a_4 h \times \frac{\partial f(y_n, t_n)}{\partial t_n}$$

$$+ \frac{1}{2} [a_3^2 h^2 f^2(y_n, t_n) \frac{\partial^2 f}{\partial y^2} + 2a_3 h f(y_n, t_n) a_4 h \times \frac{\partial^2 f}{\partial t \partial y} + a_4^2 h^2 \frac{\partial^2 f}{\partial t^2}] + O(h^3)$$

And we substitute it back to equation ① and do arrangement:

~~y_{n+1}~~

replace y_n with $y(t_n)$

$$\begin{aligned} y(t_{n+1}) &= y(t_n) + h a_1 f(y(t_n), t_n) + h a_2 f(y(t_n), t_n) + h^2 a_2 a_3 f(y(t_n), t_n) \frac{\partial f}{\partial y} + h^2 a_3 a_4 \frac{\partial f}{\partial t} \\ &+ \frac{h^3}{2} a_2 a_3^2 f^2 \frac{\partial^2 f}{\partial y^2} + h^3 a_2 a_3 a_4 f \frac{\partial^2 f}{\partial t \partial y} + \frac{h^3}{2} a_2 a_4^2 \frac{\partial^2 f}{\partial t^2} + O(h^4) \end{aligned}$$

$$= y(t_n) + h (a_1 + a_2) f(y(t_n), t_n) + \frac{1}{2} h^2 (2a_2 a_3 f \cdot \frac{\partial f}{\partial y} + 2a_2 a_4 \frac{\partial f}{\partial t})$$

$$+ \frac{1}{6} h^3 (3a_2 a_3^2 f^2 \frac{\partial^2 f}{\partial y^2} + 6a_2 a_3 a_4 f \frac{\partial^2 f}{\partial t \partial y} + 3a_2 a_4^2 \frac{\partial^2 f}{\partial t^2}) + O(h^4)$$

Comparing it with Taylor expansion:

$$y(t_{n+1}) = y(t_n + h) = y(t_n) + h f(y(t_n), t_n) + \frac{1}{2} h^2 y''(t_n) + \frac{1}{6} h^3 y'''(t_n) + O(h^4)$$

Hence, $\frac{dy}{dt} = y'$ $y'' = \frac{\partial f}{\partial t} + f \frac{\partial f}{\partial y}$

$$y''' = \frac{\partial^2 f}{\partial t^2} + 2 \times \frac{\partial^2 f}{\partial t \partial y} \times f + \frac{\partial^2 f}{\partial y^2} \times f^2 + \frac{\partial f}{\partial t} \cdot \frac{\partial f}{\partial y} + \left(\frac{\partial f}{\partial y}\right)^2 \cdot f$$

Hence the Taylor expansion becomes:

$$\begin{aligned} y(t_{n+1}) &= y(t_n) + h f(y(t_n), t_n) + \frac{1}{2} h^2 \left(\frac{\partial f}{\partial t} + f \frac{\partial f}{\partial y} \right) \\ &\quad + \frac{1}{6} h^3 \left(\frac{\partial^2 f}{\partial t^2} + f \cdot \frac{\partial^2 f}{\partial t \partial y} + 2f^2 \frac{\partial^2 f}{\partial y^2} + \frac{\partial^2 f}{\partial t \partial y} + \left(\frac{\partial f}{\partial y}\right)^2 f \right) + O(h^4) \end{aligned}$$

We can conclude that the condition on constants a_i :

$$i.e. a_1 + a_2 = 1, 2a_2 a_3 = 1, 2a_3 a_4 = 1$$

And For the form of LTE, it can be given: $LTE = M h^3 + O(h^4)$

~~$LTE = \text{Taylor expansion} - y(t_n)$~~

$$= \frac{1}{6} h^3 \left[(1 - 3a_2 a_3^2) f \frac{\partial^2 f}{\partial y^2} + (2 - 6a_2 a_3 a_4) f \frac{\partial^2 f}{\partial t \partial y} + (1 - 3a_2 a_4^2) \frac{\partial^2 f}{\partial t^2} \right]$$

We substitute conditions found in constant: $+ \frac{\partial^2 f}{\partial t \partial y} + \left(\frac{\partial f}{\partial y}\right)^2 f] + O(h^4)$

$$LTE = \frac{1}{6} h^3 \left[(1 - \frac{3}{2} a_3) f \frac{\partial^2 f}{\partial y^2} + (2 - 3a_3) f \frac{\partial^2 f}{\partial t \partial y} + (1 - \frac{3}{2} a_3) \frac{\partial^2 f}{\partial t^2} + \frac{\partial^2 f}{\partial t \partial y} + \left(\frac{\partial f}{\partial y}\right)^2 f \right] + O(h^4)$$

We conclude $M = \left[(1 - \frac{3}{2} a_3) f \frac{\partial^2 f}{\partial y^2} + (2 - 3a_3) f \frac{\partial^2 f}{\partial t \partial y} + (1 - \frac{3}{2} a_3) \frac{\partial^2 f}{\partial t^2} + \frac{\partial^2 f}{\partial t \partial y} + \left(\frac{\partial f}{\partial y}\right)^2 f \right] \times \frac{1}{6}$

(ii) when $f = y^P$ we need select value of a_3 to let $M = 0$.

$$\text{let } a_3 = \frac{2}{3} \text{ and } \frac{\partial f}{\partial y} = P \times y^{P-1} \quad \frac{\partial^2 f}{\partial y \partial t} = P(P-1) y^{P-2} \cdot \frac{dy}{dt}$$

$$\text{then } M = \frac{1}{6} \left[P(P-1) y^{P-2} \frac{dy}{dt} + (P \times y^{P-1})^2 \cdot y^P \right]$$

2. (a) Using a leap-frog approximation for t and central approximation for x :

For equation $U_t + U_{xxx} = 0$ we write:

$$\frac{U_{n,m+1} - U_{n,m-1}}{2\Delta t} + \frac{U_{n+2,m-2} - 2U_{n+1,m} + U_{n,m}}{(\Delta x)^2} - \frac{U_{n,m} - 2U_{n-1,m} + U_{n-2,m}}{(\Delta x)^2} = 0$$

By re-arrangement:

$U_{n,m+1} = U_{n,m-1} - \frac{\Delta t}{(\Delta x)^3} (U_{n+2,m} - 2U_{n+1,m} + 2U_{n-1,m} - U_{n-2,m})$ which is consistent with finite-difference scheme.

Let $U_{n,m+1} = U(x+\Delta x, t+\Delta t)$

then $U(x, t-\Delta t) - U(x, t+\Delta t) = \frac{\Delta t}{(\Delta x)^3} [U(x+2\Delta x, t) - 2U(x+\Delta x, t) + 2U(x-\Delta x, t) - U(x-2\Delta x, t)]$

$$\text{RHS} = \frac{\Delta t}{(\Delta x)^3} \left[U + 2\Delta x U_x + 2\Delta x^2 U_{xx} + \frac{8}{6} \Delta x^3 U_{xxx} + \frac{16}{24} \Delta x^4 U_{xxxx} \right. \\ \left. - 2(U + \Delta x U_x + \frac{(\Delta x)^2}{2} U_{xx} + \frac{(\Delta x)^3}{6} U_{xxx} + \frac{(\Delta x)^4}{24} U_{xxxx}) \right. \\ \left. + 2(U - \Delta x U_x + \frac{\Delta x^2}{2} U_{xx} + \frac{5\Delta x^3}{6} U_{xxx} + \frac{\Delta x^4}{24} U_{xxxx}) \right. \\ \left. - (U - 2\Delta x U_x + 2\Delta x^2 U_{xx} - \frac{8}{6} \Delta x^3 U_{xxx} + \frac{16}{24} \Delta x^4 U_{xxxx}) \right. \\ \left. + O(\Delta x^5) \right]$$

$$\text{so } U(x, t-\Delta t) = -2\Delta t U_{xxx} - \Delta t O(\Delta x) + U - \Delta t U_x + \frac{(\Delta t)^2}{2} U_{xx} - \frac{\Delta t^3}{6} U_{xxx} + O(\Delta t^4)$$

To calculate the LTR, at $O(\Delta t) = U_t + U_{xxx} = 0$ and $O(\Delta t^3)$ is omitted
hence $\text{LTR} = O(\Delta t^3) + O(\Delta t + \Delta x)$.

(b) For von Neumann Stability set $U_{n,m} = \lambda^m e^{ikn}$, $C = \frac{\Delta t}{(\Delta x)^2}$
rewrite formula:

$$\lambda^{m+1} e^{ikn} = \lambda^{m+1} e^{ikn} - C(\lambda^m e^{ik(n+1)}) \\ \lambda = \frac{1}{\lambda} - C[(e^{ik} - e^{-ik}) - 2(e^{ik} - e^{-ik})] \Rightarrow \lambda^m e^{ik(n+1)} + 2\lambda^m e^{ik(n-1)} - \lambda^m e^{ik(n-2)} \\ \lambda - \frac{1}{\lambda} + 2ic(\sin 2k - 2\sin k) = 0 \\ \lambda^2 + 2ic(\sin 2k - 2\sin k) \cdot \lambda - 1 = 0.$$

$$\lambda = iC(\sin 2k - 2\sin k) \pm \sqrt{-C^2(2\sin k - \sin 2k)^2 + 1} \\ \text{when } C^2(2\sin k - \sin 2k)^2 > 1, \text{ it will be instability since } |\lambda| > 1 \\ \Rightarrow |C| > \frac{1}{2\sin k - \sin 2k}$$

$$\text{Set } iC(\sin 2k - 2\sin k) = \Delta$$

Therefore, $\lambda^2 = \Delta^2 + 1 > 1$ since $\sin 2k - 2\sin k \in [-\frac{3}{2\sqrt{3}}, \frac{3}{2\sqrt{3}}]$
It's conditionally stable with condition

$$|C| < \frac{1}{\sin 2k - 2\sin k}$$

3. (a) Deriving the approximation:

$$\frac{U_{n,m}^P - U_{n,m}^{P-1}}{\Delta t} + C U_{n,m}^{(P)} = \frac{U_{n+1,m}^P - 2U_{n,m}^P + U_{n-1,m}^P}{(\Delta r)^2} + \frac{1}{r} \frac{U_{n+1,m}^P - U_{n-1,m}^P}{2\Delta r}$$

re-arrange the equation:

$$+ \frac{1}{r^2} \frac{U_{n,m+1}^P - U_{n,m}^P + U_{n,m-1}^P}{(\Delta \theta)^2}$$

(b) set $U_{n,m}^P = \lambda^P e^{i(\alpha_n + \beta_m)}$

and re-arrange

$$\left(\frac{1}{\Delta t} + C + \frac{2}{(\Delta r)^2} + \frac{2}{r^2(\Delta \theta)^2} \right) \cdot U_{n,m}^P = \frac{1}{\Delta t} U_{n,m}^{P-1} + \left[\frac{1}{(\Delta r)^2} + \frac{1}{2r\Delta r} \right] U_{n+1,m}^P \\ + \left(\frac{1}{(\Delta r)^2} - \frac{1}{2r\Delta r} \right) U_{n-1,m}^P \\ + \frac{1}{r^2(\Delta \theta)^2} U_{n,m+1}^P + \frac{1}{r^2(\Delta \theta)^2} U_{n,m-1}^P$$

(b) set $U_{n,m}^P = \lambda^P e^{i(\alpha_n + \beta_m)}$

The equation becomes:

$$\left[\frac{1}{\Delta t} + C + \frac{2}{(\Delta r)^2} + \frac{2}{r^2(\Delta \theta)^2} \right] \cdot \lambda^P e^{i(\alpha_n + \beta_m)} = \frac{1}{\Delta t} \lambda^{P-1} e^{i(\alpha_n + \beta_m)} + \left[\frac{1}{(\Delta r)^2} + \frac{1}{2r\Delta r} \right] \lambda^P e^{i(\alpha_{n+1} + \beta_m)} \\ + \left[\frac{1}{(\Delta r)^2} - \frac{1}{2r\Delta r} \right] \lambda^P e^{i(\alpha_{n-1} + \beta_m)} \\ + \frac{1}{r^2(\Delta \theta)^2} \lambda^P e^{i(\alpha_n + \beta_{m+1})} + \frac{1}{r^2(\Delta \theta)^2} \lambda^P e^{i(\alpha_n + \beta_{m-1})}$$

$$\frac{1}{\Delta t} + C + \frac{2}{(\Delta r)^2} + \frac{2}{r^2(\Delta \theta)^2} = \frac{1}{\Delta t} \lambda^{-1} + \left[\frac{1}{(\Delta r)^2} + \frac{1}{2r\Delta r} \right] e^{i\alpha} + \left[\frac{1}{(\Delta r)^2} - \frac{1}{2r\Delta r} \right] e^{-i\alpha} \\ + \frac{1}{r^2(\Delta \theta)^2} e^{i\beta} + \frac{1}{r^2(\Delta \theta)^2} e^{-i\beta} \\ = \frac{1}{\Delta t} \frac{1}{\lambda} + \frac{1}{(\Delta r)^2} [e^{i\alpha} + e^{-i\alpha}] + \frac{1}{2r\Delta r} [e^{i\alpha} - e^{-i\alpha}] + \frac{1}{r^2(\Delta \theta)^2} [e^{i\beta} + e^{-i\beta}] \\ = \frac{1}{\Delta t} \frac{1}{\lambda} + \frac{2}{(\Delta r)^2} \cos\alpha + \frac{2}{r\Delta r} \sin\alpha + \frac{2}{r^2(\Delta \theta)^2} \cos\beta$$

$$\Rightarrow \frac{1}{\lambda} = \Delta t \left[\frac{4\sin^2(\frac{\alpha}{2})}{(\Delta r)^2} - \frac{i \sin\alpha}{r\Delta r} + \frac{4\sin^2(\frac{\beta}{2})}{r^2(\Delta \theta)^2} + \frac{1}{\Delta t} + C \right]$$

$$\text{let } m = \frac{4\sin^2(\frac{\alpha}{2})}{(\Delta r)^2} + \frac{4\sin^2(\frac{\beta}{2})}{r^2(\Delta \theta)^2} + \frac{1}{\Delta t} + C, n = -\frac{i \sin\alpha}{r\Delta r}$$

$$\text{then } \frac{1}{\lambda} = m + ni$$

$$\text{the magnitude of } |\lambda|^2 = \sqrt{m^2 + n^2}$$

The system is conditionally stable with condition $\frac{1}{m^2 + n^2} < 1$

(c)

$$4. (a) \frac{d}{dx} (AE + \frac{du}{dx}) + q = 0 \text{ where } q = \rho g A.$$

$$\int_0^L \left(\frac{du}{dx} \cdot \frac{du}{dx} \cdot AE + \rho g A \right) \cdot v dx = 0 \text{ where } v \text{ is the test function.}$$

$$\text{That means } \int_0^L u_{xx} AE v dx + \int_0^L \rho g A v dx = 0$$

$$\int_0^L AE v du' + \int_0^L \rho g A v dx = 0$$

$$AEV \cdot \frac{du}{dx} \Big|_0^L - \int_0^L AE \frac{dv}{dx} \cdot \frac{du}{dx} dx + \int_0^L \rho g A V dx = 0$$

$$\text{And } AEV \cdot \frac{du}{dx} \Big|_0^L = 0 \text{ is given by boundary condition } u(0) = 0, F(L) = 0, \text{ where } F = AE \cdot \frac{du}{dx}$$

$$\text{Hence Eq} \Rightarrow \int_0^L \rho g A V dx - \int_0^L AE \frac{dv}{dx} \frac{du}{dx} dx = 0$$

(b) FE equation for a single 2-node element

$$N_1 = 1 - \frac{x}{L}, N_2 = \frac{x}{L}$$

$$\text{And the stiffness matrix } k_{ij} = \int_0^L \frac{dN_i}{dx} AE \frac{dN_j}{dx} dx$$

$$k_{11} = \int_0^L \frac{dN_1}{dx} AE \frac{dN_1}{dx} dx = \int_0^L \left(-\frac{1}{L}\right) AE \left(-\frac{1}{L}\right) dx = \frac{1}{L^2} AE x \Big|_0^L = \frac{1}{L} AE$$

$$k_{12} = \int_0^L \frac{dN_1}{dx} AE \frac{dN_2}{dx} dx = \int_0^L \left(-\frac{1}{L}\right) AE \left(\frac{1}{L}\right) dx = -\frac{1}{L} AE$$

$$\Rightarrow K = \frac{1}{L} AE \begin{pmatrix} 1 & -1 \\ -1 & 1 \end{pmatrix}$$

$$\text{And the load vector } f_{ei} = \int_0^L q N_i dx$$

$$f_{e1} = \int_0^L q \left(1 - \frac{x}{L}\right) dx = \frac{q}{2} L, f_{e2} = \int_0^L q \frac{x}{L} dx = \frac{q}{2} L$$

$$f_{el} = \frac{q}{2} L \begin{pmatrix} 1 \\ 1 \end{pmatrix}$$

$$f_{bi} = -N_i F \Big|_0^L \Rightarrow f_{b1} = -F(0), f_{b2} = 0 \quad \therefore f_b = \begin{pmatrix} -F(0) \\ 0 \end{pmatrix}$$

Hence the FE equation becomes

$$\frac{1}{L} AE \begin{pmatrix} 1 & -1 \\ -1 & 1 \end{pmatrix} \begin{pmatrix} u_1 \\ u_2 \end{pmatrix} = \frac{q}{2} L \begin{pmatrix} 1 \\ 1 \end{pmatrix} + \begin{pmatrix} -F(0) \\ 0 \end{pmatrix}$$

with the condition $u(0) = 0, F(L) = 0$

$$\frac{1}{L} AE u_2 = \frac{q}{2} L \Rightarrow u_2 = \frac{qL^2}{2AE}$$

$$\frac{1}{L} AE u_2 = F(0) - \frac{q}{2} L \Rightarrow F(0) = qL$$

$$\Rightarrow u(x) = \sum N_i(x) u_i = \frac{qL}{2AE} x$$

(C) 2-node elements:

$$K = \frac{AE}{L} \begin{bmatrix} 1 & -1 & \dots & 0 \\ -1 & 2 & -1 & \dots \\ 0 & -1 & 2 & -1 & \dots \\ \vdots & \vdots & \vdots & \ddots \\ 0 & \vdots & \vdots & \vdots & 1 \end{bmatrix}, \quad F = \left[u_1 + \frac{qL}{n}, \frac{qL}{n}, \dots, \frac{qL}{n}, \frac{qL}{2n} \right]^T \text{ with length } (n+1).$$

In equation $K \cdot f = F$ where $f = [u_1, u_2, \dots, u_{n+1}]^T$
then write in equation form:

$$\frac{AE}{L} (2u_2 - u_3) = \frac{qL}{n}$$

$$\frac{AE}{L} (-u_{n+1} + 2u_n - u_{n+1}) = \frac{qL}{n}$$

$$\frac{AE}{L} (-u_n + u_{n+1}) = \frac{qL}{2n}$$

when $n = L$, we could get $\begin{cases} \frac{2AE}{L} (-u_2 + u_3) = \frac{qL}{4} + F(0) \\ \frac{AE}{L} (+) u_2 - u_3 = \frac{qL}{2} \\ \frac{AE}{L} (-u_3 + u_3) = \frac{qL}{4} \end{cases}$

Solving for u_2 and u_3 $\begin{cases} 2u_2 - u_3 = \frac{qL^2}{2AE} \\ -u_2 + u_3 = \frac{qL^2}{4AE} \end{cases} \Rightarrow \begin{cases} u_2 = \frac{3qL^2}{8AE} \\ u_3 = \frac{qL^2}{2AE} \end{cases}$

$$\text{Thus } u = [0, \frac{3qL^2}{8AE}, \frac{qL^2}{2AE}]$$

$$F(0) = -qL$$

(d) The last term would be $\frac{qL}{2n} + M$.

5. (a) $\iint \left(-\frac{\partial^2 u}{\partial x^2} - \frac{\partial^2 u}{\partial y^2} \right) - g(x, y) v \, dx \, dy = 0$, v is the test function.

$$\Rightarrow \iint \left(-\frac{\partial u}{\partial x} \cdot \frac{\partial v}{\partial x} - \frac{\partial u}{\partial y} \frac{\partial v}{\partial y} \right) \, dx \, dy + \int_T \left(\frac{\partial u}{\partial x} n_x + \frac{\partial u}{\partial y} n_y \right) v \, ds - \iint g(x, y) v \, dx \, dy = 0$$

then $\iint \left(\frac{\partial u}{\partial x} \frac{\partial v}{\partial x} + \frac{\partial u}{\partial y} \frac{\partial v}{\partial y} + g(x, y) v \right) \, dx \, dy - \int_0^4 \frac{\partial u}{\partial n} \, dy = 0$

(b) FE equation: $Ku = f_f + f_b$ where

Stiffness matrix: $K_{ij} = \iint \left(\frac{\partial N_i}{\partial x} \frac{\partial N_j}{\partial x} + \frac{\partial N_i}{\partial y} \frac{\partial N_j}{\partial y} \right) \, dx \, dy$

Load vector: $f_{ei} = \iint g N_i \, dx \, dy$ where N_i are shape functions.

$$N_1 = \frac{1}{4}(\xi-1)(\eta-1), \quad N_2 = -\frac{1}{4}(\xi+1)(\eta-1)$$

$$N_3 = \frac{1}{4}(\xi+1)(\eta+1), \quad N_4 = -\frac{1}{4}(\xi-1)(\eta+1)$$

Since $(x_1, y_1) = (0, 0)$, $(x_2, y_2) = (2, 0)$, $(x_3, y_3) = (4, 4)$, $(x_4, y_4) = (2, 4)$

then $x = N_1 x_1 + N_2 x_2 + N_3 x_3 + \cancel{N_4} x_4$

$$= 2N_2 + 4N_3 + 2N_4$$

$$= -\frac{1}{2}(\xi+1)(\eta-1) + (\xi+1)(\eta+1) - \frac{1}{2}(\xi-1)(\eta+1) = \xi + \eta + 2$$

$$y = N_1 y_1 + N_2 y_2 + N_3 y_3 + N_4 y_4$$

$$= 4N_3 + 4N_4$$

$$= 2\eta + 2$$

Jacobian: $J = \begin{pmatrix} \frac{\partial x}{\partial \xi} & \frac{\partial x}{\partial \eta} \\ \frac{\partial y}{\partial \xi} & \frac{\partial y}{\partial \eta} \end{pmatrix} = \begin{pmatrix} 1 & 1 \\ 0 & 2 \end{pmatrix}$

Since $\det(J) = 2 \neq 0$ we could have inverse matrix $J^{-1} = \begin{pmatrix} 1 & -\frac{1}{2} \\ 0 & \frac{1}{2} \end{pmatrix}$

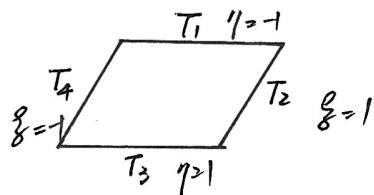
$$(J^T)^{-1} = \begin{pmatrix} 1 & 0 \\ -\frac{1}{2} & \frac{1}{2} \end{pmatrix}$$

$$\begin{aligned} K_{11} &= \iint \left(\frac{\partial N_1}{\partial x}, \frac{\partial N_1}{\partial y} \right) \left(\frac{\partial N_1}{\partial x}, \frac{\partial N_1}{\partial y} \right)^T dx dy \\ &= \iint \left(\frac{\partial N_1}{\partial \xi} \frac{\partial N_1}{\partial \eta} \right) J^{-1} \begin{pmatrix} 1 & 0 \\ 0 & 1 \end{pmatrix} (J^T)^{-1} \begin{pmatrix} \frac{\partial N_1}{\partial \xi} \\ \frac{\partial N_1}{\partial \eta} \end{pmatrix} \det(J) d\xi d\eta \\ &= \int_{-1}^1 \int_{-1}^1 \left[\frac{1}{4}(\xi-1) \frac{1}{4}(\eta-1) \right] \begin{pmatrix} 1 & -\frac{1}{2} \\ 0 & \frac{1}{2} \end{pmatrix} \begin{pmatrix} 1 & 0 \\ 0 & 1 \end{pmatrix} \begin{pmatrix} 1 & 0 \\ -\frac{1}{2} & \frac{1}{2} \end{pmatrix} \begin{pmatrix} \frac{1}{4}(\eta-1) \\ \frac{1}{4}(\xi-1) \end{pmatrix} \times 2 d\xi d\eta \\ &= \frac{1}{32} \int_{-1}^1 \int_{-1}^1 (5\xi^2 + \xi^2 - 2\xi\xi - 2\xi + 4) d\xi d\eta \\ &= \frac{1}{32} \left[\frac{10}{3}\xi^3 + \frac{26}{3}\xi \right]_{-1}^1 = \frac{3}{4} \end{aligned}$$

The Load vector: $f_{1r} = \iint_{-1}^1 g(x, y) N_1 \det(J) d\xi d\eta$.

$$= \int_{-1}^1 \int_{-1}^1 g(\xi + \eta + 2, 2\eta + 2) \frac{1}{4}(\xi-1)(\eta-1) \times 2 d\xi d\eta.$$

(c) The boundary vector for this problem is:



$$\begin{aligned} f_b &= \int_{\Gamma} N_i \frac{\partial N}{\partial n} ds \\ \text{where } ds &= \sqrt{(\partial x/\partial \xi)^2 + (\partial y/\partial \xi)^2} \\ \text{and } dx &= \frac{\partial x}{\partial \xi} d\xi + \frac{\partial x}{\partial \eta} d\eta \\ dy &= \frac{\partial y}{\partial \xi} d\xi + \frac{\partial y}{\partial \eta} d\eta \end{aligned}$$

$$\begin{aligned} \therefore \int_{\Gamma_A} y N_i(\xi, \eta) ds &= \int_{T_2} y(\xi, \eta) N_i(\xi, 1) \sqrt{(\frac{\partial x}{\partial \xi})^2 + (\frac{\partial y}{\partial \xi})^2} d\eta \\ &= \int_{T_2} [(1+\xi)(1+\eta) - (1-\xi)(1+\eta)] N_i \sqrt{5} d\eta. \end{aligned}$$

Therefore $f_{b1} = \int_{-1}^1 (2\eta + 2) N_1(\xi, \eta) \sqrt{5} d\eta = 2\sqrt{5} \int_{-1}^1 (\eta + 1) N_1(\xi, \eta) d\eta = 0$

$$f_{b2} = 2\sqrt{5} \int_{-1}^1 (\eta + 1) N_2 d\eta = \frac{4}{3}\sqrt{5}$$

$$f_{b3} = 2\sqrt{5} \int_{-1}^1 (1+\eta) N_3 d\eta = \frac{8}{3}\sqrt{5}$$

$$f_{b4} = 2\sqrt{5} \int_{-1}^1 (1+\eta) N_4 d\eta = 0$$

(d) The mesh is conforming if it guarantees continuity of solutions across element boundaries.

Yes, it is conforming. Because a mesh of square parent elements are conforming and the isoparametric transformation is continuous.

If additional midside nodes were introduced, it wouldn't be changed. Since the new model with 4 midside nodes is contributed by a group of parallelogram,