# Correlation MATH 2441, BCIT

Technical Mathematics for Food Technology

April 19, 2018

#### Instructor Note

I want to change this from emphasis on correlation coefficients and using the critical values on the Pearson correlation coefficient table to doing a proper hypothesis test for the slope  $b_1$  with a null hypothesis  $\beta_1=0$ . This way you can find a confidence interval for  $\beta_1$  and a prediction interval for  $\hat{y}$  (see Devore and Peck's textbook); and the integration with R Statistics is much better. There is also a natural segue to ANOVA with the F-test in R Statistics on linear correlation. Course Outline wants both. It also wants you to do the Kolmogorov-Smirnoff test for normality.

A correlation exists between two variables when the values of one variable are somehow associated with the values of the other variable.

A linear correlation exists between two variables when there is a correlation and the plotted points of paired data result in a pattern that can be approximated by a straight line.

Here is the data for waist (in inches), weight (in pounds), and body fat (in percent) for 20 test subjects.

```
| 33|188|10|| 33|160| 10|| 40|192| 31|| 32|175| 6|
| 40|240|20|| 41|215| 27|| 41|205| 32|| 36|181|21|
| 36|175|22|| 34|159| 12|| 35|173| 21|| 38|200|15|
| 32|168| 9|| 34|146| 10|| 38|187| 25|| 33|159| 6|
| 44|246|38|| 44|219| 28|| 38|188| 30|| 39|196|22|
```



In the previous slide, you can see the data from 20 test subjects. In the following slide, you can see the data from 250 test subjects. It appears that there is a relationship between waist and body fat.





The red line is called the regression line. We will learn how to calculate it later. Here is its equation:

$$b = 1.7w - 42.73 \tag{1}$$

The regression line minimizes the mean square distance of the data points to the line (all other lines have a greater mean square distance from the data points). Have a look at three of the 250 test subjects.

	waist	bf (act)	bf (pred)	error
test subject 1	33.54	12.3	14.29	1.9936
test subject 2	32.68	6.1	12.82	6.7212
test subject 3	34.61	25.3	16.10	-9.1993

It appears that the error is normally distributed (perhaps not quite on the margins).

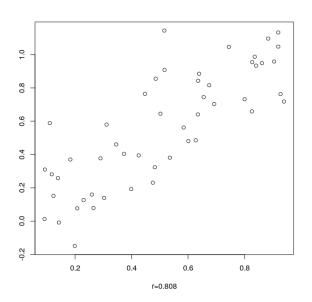


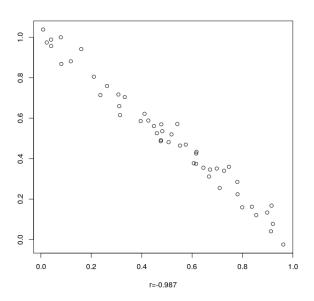




Let's have a look at a few scatterplots. Is there a correlation or not? Is there a linear correlation? The linear correlation coefficient r measures the strength of the linear correlation. It is a sample statistic. The linear correlation coefficient for the population is called  $\varrho$  ("rho" in the Greek alphabet).

The correlation coefficient for the sample of 250 test subjects measuring body fat and waist is r = 0.8236847.









#### Notation

To determine whether there is a linear correlation between two variables, first take note of the following notation.

- n number of pairs of sample data
- \( \) denotes addition of items indicated
- $\sum x$  sum of all x-values
- $\sum x^2$  sum of all  $x^2$ -values
- $(\sum x)^2$  sum of all x-values squared
  - $\sum xy$  sum of all  $x \cdot y$ -values
    - r linear correlation coefficient for sample data
    - $\varrho$  linear correlation coefficient for population of paired data

#### Requirements

Here are the requirements for the procedure that follows.

- The sample of paired (x, y) data is a simple random sample of quantitative data.
- Visual examination of the scatterplot confirms that the points approximate a straight-line pattern.
- Outliers must be removed if they are known to be errors. The procedure is not robust with respect to erroneous outliers.

Requirements 2 and 3 are an intuitive summary of a more stringent requirement: the pairs of (x, y) data must have (or approximate) a bivariate normal distribution, which means that for a fixed value x, the corresponding y-values have a normal distribution, and vice versa. Think of the deviation of the actual y-value from a perfectly linear corresponding y-value as a normally distributed error.

## Calculating r

Here is a simple formula for r that is difficult to calculate. Let  $z_x$  be the z-score of an individual x-value and  $z_y$  be the z-score of an individual y-value. Then

$$r = \frac{\sum (z_x z_y)}{n - 1} \tag{2}$$

Here is a more difficult formula that makes calculation much easier.

$$r = \frac{n\left(\sum xy\right) - \left(\sum x\right)\left(\sum y\right)}{\sqrt{n\left(\sum x^2\right) - \left(\sum x\right)^2}\sqrt{n\left(\sum y^2\right) - \left(\sum y\right)^2}}$$
(3)

#### Calculating r Example

Here are the data for females, shoe prints, and heights.

```
+----+
| 24.8|165.1 | | | 28.1|179.1|
+----+
| 28.6|166.4 | | | 27.6|175.9|
+----+
1 25.4 177.8 11 26.5 1166.4 1
+----+
| 26.7|167.6 | | | 26.5|167.6|
+----+
| 26.7|168.3 | | | 28.4|162.6|
+----+
| 27.9|165.7 | | | 26.5|167.6|
+----+
| 27.9|165.1 | | | 26.0|165.1|
+----+
| 28.9|165.1 | | | 27.0|172.7|
+----+
| 27.9|165.1 | | | 25.1|157.5|
+----+
| 25.9|152.4 | | | 27.9|167.6|
+----+
 25.4|162.6 | | |
+----+
```

#### Calculating r Example

Now calculate the following . . .

$\sum X$	565.7	$\sum y$	3503.3
$\sum x^2$	15268.45	$\sum y^2$	585173.7
$(\sum x)^2$	320016.5	$(\sum y)^2$	12273111
$\sum xy$	94404.95		

... and fill in the formula

$$r = \frac{21 \cdot 94404.95 - 565.7 \cdot 3503.3}{\sqrt{21 \cdot 15268.45 - 320016.5}\sqrt{21 \cdot 585173.7 - 12273111}}$$
 (4)

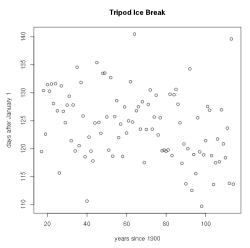
There are many opportunities here to make an error. It is better to use statistics software. In R Statistics, for example, the relevant command is cor(x,y). The result, in either case, is r = 0.22122.

### Hypothesis Testing for Correlation

Use the critical values for the Pearson Correlation Coefficient r to determine whether there is a correlation between the two variables or not. In the case of female shoe prints and heights, n=20, and therefore, at a significance level  $\alpha=0.05$ , the critical value is r=0.444. The null hypothesis is  $\varrho=0$ .

Since our test statistic is only  $r^* = 0.221$ , we fail to reject the null hypothesis that there is no correlation. There is not enough evidence to show that there is a linear correlation (remember to check the requirements first).

**Example 1: Nenana Tripod Ice Break.** Have a look at http://www.nenanaakiceclassic.com/. Is there a correlation? (Might it support the theory that the Earth is warming?)



- Step 1 The null hypothesis is  $\varrho=0$ . The alternative hypothesis is  $\varrho<0$  (the Earth is warming, therefore the tripod will break up the ice earlier in the year the more recently we measure). We will test the null hypothesis at a significance level of  $\alpha=0.01$ .
- Step 2 The test statistic is r = -0.3130899 (calculated using R Statistics).
- Step 3 The critical value of the Pearson Correlation Coefficient r is approximately 0.256 at  $\alpha=0.01$  and n=98 (consult the table).

Decision: reject the null hypothesis. The data supports the hypothesis that there is a linear correlation between years after 1900 and the days after January 1 when the tripod breaks the ice (assuming that the data have a bivariate normal distribution and a linear rather than some other correlation).

Here is how you can do the hypothesis testing in R Statistics. Let y be the years after 1900 and d be the days after January 1 when the tripod breaks the ice. Try the command  $\operatorname{summary}(\operatorname{lm}(\operatorname{d} y))$ . The output is on the next slide. Notice the p-value. It clearly suggests that we should reject  $H_0$ .

#### Residuals:

```
Min 1Q Median 3Q Max -15.2035 -3.6805 -0.2056 4.0684 18.7533
```

#### Coefficients:

```
Estimate Std. Error t value Pr(>|t|)
(Intercept) 128.58108    1.50954    85.18    <2e-16 ***
y         -0.06834    0.02116    -3.23    0.0017 **
```

```
Signif. codes: 0 *** 0.001 ** 0.01 * 0.05 . 0.1
```

Residual standard error: 5.925 on 96 degrees of freedom Multiple R-squared: 0.09803, Adjusted R-squared: 0.08863 F-statistic: 10.43 on 1 and 96 DF, p-value: 0.001695

Let's have a closer look at the summary on the last slide. The residuals are the errors of our predictions using the regression line. For each x-value (independent variable), there is a y-value (dependent variable) and a  $\hat{y}$ -value (prediction using the regression line. The residual is  $\hat{y} - y$  (in R Statistics, the residuals are in z[[3]] for z<-summary(lm(d y))). The residual standard deviation  $s_e$  is a measure how much the data scatters along the regression line:

$$s_{e} = \sqrt{\frac{\sum (\hat{y} - y)^{2}}{n - 2}} \tag{5}$$

The residual standard deviation for the Nenana data is large, 5.925 days, because even if you know the regression line it's hard to predict the date when the ice will be broken in a particular year.

 $s_e$  is one measure of the relationship between x-values and y-values. The correlation coefficient r is another one. In the R summary it is called "Multiple R-squared" and equals  $r^2$ . The reason why it is squared is because one could say that the correlation accounts for  $r^2$  of the variation in the y-values. In the Nenana example, which year it is accounts for 9.8% of the variation in the number of days it takes for the ice to break.

Some statisticians prefer "Adjusted R-squared" which penalizes larger numbers of parameters.

A theorem in statistics tells us that

$$\frac{b_1 - \beta_1}{\frac{s_e}{s_x \sqrt{n-1}}}\tag{6}$$

is distributed according to a t-distribution with degree of freedom df = n - 2.

 $s_x$  is the standard deviation of the x-values.  $s_e$  is the residual standard deviation.  $b_1$  is the slope of the regression line calculated from the sample;  $\beta_1$  is the slope of the regression line hypothesized for the population.

The R summary tells us that the slope of the regression line for the sample is  $b_1=-0.06834$  and the p-value for the hypothesis that  $\beta_1=0$  is 0.0017 (two-tailed) (you can check this by looking at the t-distribution with degree of freedom df=96 and the result of the formula on the last slide, which is  $t^*=-3.23$ ). We reject the hypothesis that  $\beta_1=0$ , which is similar to rejecting the hypothesis that r=0. It is usually not interesting to investigate the hypothesis that the y-intercept is zero.

Here is yet another hypothesis test whether there is a linear correlation or not. A relatively complicated formula gives us the F-statistic of the regression analysis. The F-distribution (named after Ronald Fisher) looks similar to the chi-squared distribution. It has two degrees of freedom. In R Statistics, qf (0.95,5,2) gives you the F-statistic for which 95% of the area under the curve is to the left of the F-statistic, with degrees of freedom 5 and 2. pf (19.29641,5,2) is the reverse procedure which gives you the area under the curve to the left of the F-statistic 19.29641. We will meet this distribution again when we cover ANOVA.

#### Hypothesis Testing for Correlation Exercise

**Exercise 1:** The table below lists measured amounts of redshift and the distances (billions of light-years) to randomly selected clusters of galaxies. Is there sufficient evidence to conclude that there is a linear correlation between amounts of redshift and distances to clusters of galaxies?

+	++
Redshift	Distance
0.0233	0.32
0.0539	0.75
0.0718	1.00
0.0395	0.55
0.0438	0.61
0.0103	0.14

#### The Regression Line

To find the regression line  $\hat{y} = b_0 + b_1 x$ , use the following formula for the slope  $b_1$  and the y-intercept  $b_0$ :

$$b_1 = \frac{n\left(\sum xy\right) - \left(\sum x\right)\left(\sum y\right)}{n\left(\sum x^2\right) - \left(\sum x\right)^2} \tag{7}$$

$$b_0 = \frac{\left(\sum y\right)\left(\sum x^2\right) - \left(\sum x\right)\left(\sum xy\right)}{n\left(\sum x^2\right) - \left(\sum x\right)^2} \tag{8}$$

You may wonder where these equations come from. They identify the line equation which best fits the data using the least squares method. The least squares method identifies the line that best fits the data by measuring the distance that each data point is away from the line, squaring it, and then adding all of those numbers. The line that scores lowest on this fitness test is the regression line.

#### Regression Line Example

**Example 2: Galaxy Distances.** It is clear in the hypothesis test that there is a linear correlation between redshift and galaxy distances, even with a small sample size. What is the regression line? How could we predict the distance of a galaxy, knowing its redshift?

$$b_0 = -0.004396 b_1 = 13.999899$$
 (9)

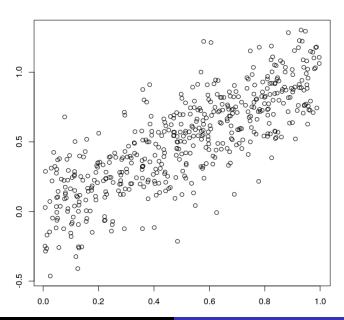
Each thousandth unit of redshift adds fourteen million light-years to the distance.

In R Statistics, you can create a scatterplot of data sets x and y using the command plot(x,y). Adding the command  $abline(lm(y\sim x), col="red")$  will add the regression line to the plot (in red colour).  $lm(y\sim x)$  will give you both the y-intercept and the slope of the regression line.

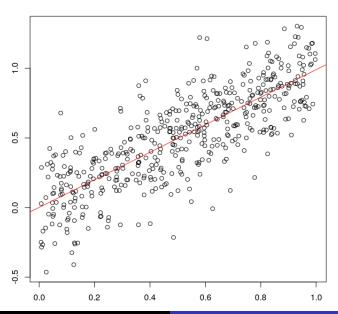
#### Regression Line Example

Here is some R Statistics code:

## Regression Line Example



# Regression Line Example



**Exercise 2:** Consider the data on the next slide. These are the results for two successive term tests (the names are randomly made up by a computer program, but the grades are real). Answer the following questions:

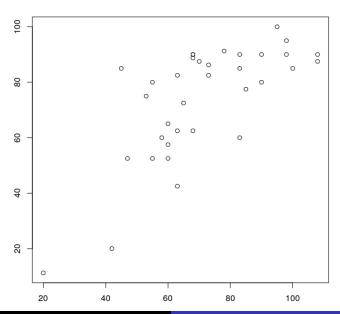
- ① Is there a linear correlation between the first and the second term test? Answer the question for a significance level of  $\alpha=0.05$ . If you were doing this problem with a significance level  $\alpha=0.01$ , what would be the decision and what type of error (type I or type II) would it make less likely compared to using the higher significance level?
- What is the equation of the regression line?
- If William Jones (again, fake name but real grade) had a score of 85 on the first term test, what score is the point estimate for the second term test given the linear correlation? His true score for the second term test was 77.

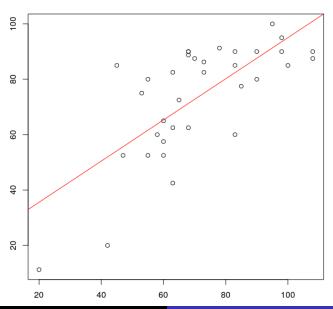
Nancy Rogge	83	60	Arnold Murray	73	82
Elizabeth Rushing	98	95	Ann Coburn	60	52
Katy Nunez	68	62	Kim Lazzari	63	62
Michael Preuss	68	90	Valentina Martinez	68	88
Edna Phipps	68	90	Eric Mumford	78	91
George Thompson	45	85	Alyssa Warner	98	90
James Newman	42	20	Kevin Ellis	65	72
Nathan Stowman	108	90	Susan Ervin	90	80
Kimberly Gaitor	83	90	Albert Gutierrez	55	52
Leland Garner	60	65	Robin Calderon	95	100
Bryan Veilleux	53	75	Jennifer Blackburn	60	57
Mary Watts	73	86	Doris Larkin	83	85
Jerry Brown	58	60	James Miller	63	42
Jacob Ludwick	47	52	Gregory Myklebust	70	87
Wayne Vega	100	85	Rita Swinton	90	90
Kathryn Wilson	55	80	Barbara Richardson	63	82
Tony Bateman	20	11	Ora Tidmore	108	87

$\sum x$	2496	$\sum y$	2580
$\sum x^2$	191344	$\sum y^2$	204700
$(\sum x)^2$	6230016	$(\sum y)^2$	6656400
$\sum xy$	193904	n	34

The solution for the linear correlation coefficient is r = 0.7122366.

The solution for the *y*-intercept and slope of the regression line is  $b_0 = 20.7350$  and  $b_1 = 0.7429$ . The point estimate for William Jones' grade is 83.88.





Costs listed below are repair costs (in dollars) for cars crashed at 6 mi/h in full-front crash tests and the same cars crashed at 6 mi/h in full-rear crash tests (based on data from the Insurance Institute for Highway Safety). The cars are the Toyota Camry, Mazda 6, Volvo S40, Saturn Aura, Subaru Legacy, Hyundai Sonata, and Honda Accord. Is there sufficient evidence to conclude that there is a linear correlation between the repair costs from full-front crashes and full-rear crashes?

Front	936	978	2252	1032	3911	4312	3469
Rear	1480	1202	802	3191	1122	739	2767

Listed below are systolic blood pressure measurements (in mm Hg) obtained from the same woman (based on data from "Consistency of Blood Pressure Differences Between the Left and Right Arms," by Eguchi et al., Archives of Internal Medicine, Vol. 167). Is there sufficient evidence to conclude that there is a linear correlation between right and left arm systolic blood pressure measurements?

Right Arm	102	101	94	79	79	
Left Arm	175	169	182	146	144	

One classic application of correlation involves the association between the temperature and the number of times a cricket chirps in a minute. Listed below are the numbers of chirps in one minute and the corresponding temperatures in °F (based on data from "The Song of Insects" by George W. Pierce, Harvard University Press). Is there sufficient evidence to conclude that there is a linear correlation between the number of chirps in one minute and the temperature?

Chirps	882	1188	1104	864	1200	1032	960	900
°F	69.7	93.3	84.3	76.3	88 6	82.6	71.6	79.6

Lemons and Car Crashes. Find the best predicted crash fatality rate for a year in which there are 500 metric tons of lemon imports.

Lemon Imports	230	265	358	480	530
Crash Fatality Rate	15.9	15.7	15.4	15.3	14.9

Altitude and Temperature. At 6327 ft (or 6.327 thousand feet), Mario Triola, the author of many of these exercises, recorded the temperature. Find the best predicted temperature at that altitude. How does the result compare to the actual recorded value of 48°F?

Altitude	3	10	14	22	28	31	33
Temperature	57	37	24	-5	-30	-41	-54

If the regression line slope for a sample of size n is  $b_1$ , then a confidence interval for the regression line slope  $\beta_1$  of the population is (the confidence level being  $1-\alpha$ )

$$b_1 - E < \beta_1 < b_1 + E \tag{10}$$

with

$$E = t_{\frac{\alpha}{2}} \frac{s_e \sqrt{\sum x^2}}{\sqrt{n} \left(\sum x^2 - \frac{(\sum x)^2}{n}\right)}$$
 (11)

The degree of freedom for  $t_{\frac{\alpha}{2}}$  is n-2.

The data on the next slide shows observations of the Old Faithful geyser in the USA Yellowstone National Park. There are two observation variables in the data set. The first one, called eruptions, is the duration of the geyser eruptions. The second one, called waiting, is the length of waiting period until the next eruption (all in minutes). It turns out there is a correlation between the two variables. The data is available on R Statistics in the dataframe called faithful.

1.800         54         2.017         52         4.700         73         4.500         83         4.933         86         2.083         57         1.783         46         2.3           3.333         74         1.867         48         4.033         82         4.050         81         2.033         53         4.583         77         4.367         77         4.1           2.283         62         4.833         80         1.967         56         1.867         47         3.733         79         3.333         68         3.850         84         2.3           4.533         85         1.833         59         4.500         79         4.700         84         4.233         81         4.167         81         1.933         49         4.90           2.883         55         4.783         90         4.000         71         1.783         52         2.233         60         4.333         81         4.500         83         2.99           4.700         88         4.350         80         1.983         62         4.850         86         4.533         82         4.500         83         2.90           4.350																	
3.333       74       1.867       48       4.033       82       4.050       81       2.033       53       4.583       77       4.367       77       4.12         2.283       62       4.833       80       1.967       56       1.867       47       3.733       79       3.333       68       3.850       84       2.33         4.533       85       1.833       59       4.500       79       4.700       84       4.233       81       4.167       81       1.933       49       4.90         2.883       55       4.783       90       4.000       71       1.783       52       2.233       60       4.333       81       4.500       83       2.99         4.700       88       4.350       80       1.983       62       4.850       86       4.533       82       4.500       73       2.383       71       4.5         3.600       85       1.883       58       5.067       76       3.683       81       4.817       77       2.417       50       4.700       80       3.8         1.950       51       1.567       84       2.017       60       4.733       75		3.600	79	3.833	74	2.067	65	2.100	49	1.883	51	1.917	49	4.600	78	3.950	79
2.283       62       4.833       80       1.967       56       1.867       47       3.733       79       3.333       68       3.850       84       2.3         4.533       85       1.833       59       4.500       79       4.700       84       4.233       81       4.167       81       1.933       49       4.93         2.883       55       4.783       90       4.000       71       1.783       52       2.233       60       4.333       81       4.500       83       2.96         4.700       88       4.350       80       1.983       62       4.850       86       4.533       82       4.500       73       2.383       71       4.53         3.600       85       1.883       58       5.067       76       3.683       81       4.817       77       2.417       50       4.700       80       3.83         1.950       51       4.567       78       2.300       59       1.983       59       4.167       74       3.833       75       4.33         1.833       54       4.533       73       3.883       76       4.900       89       4.633       80 <td></td> <td>1.800</td> <td>54</td> <td>2.017</td> <td>52</td> <td>4.700</td> <td>73</td> <td>4.500</td> <td>83</td> <td>4.933</td> <td>86</td> <td>2.083</td> <td>57</td> <td>1.783</td> <td>46</td> <td>2.333</td> <td>64</td>		1.800	54	2.017	52	4.700	73	4.500	83	4.933	86	2.083	57	1.783	46	2.333	64
4.533         85         1.833         59         4.500         79         4.700         84         4.233         81         4.167         81         1.933         49         4.99           2.883         55         4.783         90         4.000         71         1.783         52         2.233         60         4.333         81         4.500         83         2.99           4.700         88         4.350         80         1.983         62         4.850         86         4.533         82         4.500         73         2.383         71         4.53           3.600         85         1.883         58         5.067         76         3.683         81         4.817         77         2.417         50         4.700         80         3.83           1.950         51         4.567         84         2.017         60         4.733         75         4.333         76         4.000         89         4.633         80         1.883         55         3.417         64         2.1           3.917         84         4.331         83         3.600         83         4.417         79         2.017         49         4.583		3.333	74	1.867	48	4.033	82	4.050	81	2.033	53	4.583	77	4.367	77	4.150	75
2.883 55 4.783 90 4.000 71 1.783 52 2.233 60 4.333 81 4.500 83 2.99 4.700 88 4.350 80 1.983 62 4.850 86 4.533 82 4.500 73 2.383 71 4.50 3.600 85 1.883 58 5.067 76 3.683 81 4.817 77 2.417 50 4.700 80 3.83 1.950 51 4.567 84 2.017 60 4.733 75 4.333 76 4.000 85 1.867 49 2.03 4.350 85 1.750 58 4.567 78 2.300 59 1.983 59 4.167 74 3.833 75 4.33 1.833 54 4.533 73 3.883 76 4.900 89 4.633 80 1.883 55 3.417 64 2.13 3.917 84 3.317 83 3.600 83 4.417 79 2.017 49 4.583 77 4.233 76 4.33 4.200 78 3.833 64 4.133 75 1.700 59 5.100 96 4.250 83 2.400 53 2.20 1.750 47 2.100 53 4.333 82 4.633 81 1.800 53 3.767 83 4.800 94 4.47 4.700 83 4.633 82 4.100 70 2.317 50 5.033 77 2.033 51 2.000 55 3.55 2.167 52 2.000 59 2.633 65 4.600 85 4.000 77 4.433 78 4.150 76 4.55 1.750 62 4.800 75 4.067 73 1.817 59 2.400 65 4.083 84 1.867 50 4.11 4.800 84 4.716 90 4.933 88 4.417 87 4.600 81 1.833 46 4.267 82 3.8 1.600 52 1.833 54 3.950 76 2.617 53 3.567 71 4.417 83 1.750 54 3.9 4.250 79 4.833 80 4.517 80 4.067 69 4.000 70 2.183 55 4.483 75 4.41 1.800 51 1.733 54 2.167 48 4.250 77 4.500 81 4.800 81 4.000 78 2.00 1.750 47 4.883 83 4.000 86 1.967 56 4.083 93 1.833 57 4.117 79 4.21 3.450 78 3.717 71 2.200 60 4.600 88 1.800 53 4.800 76 4.087 78 4.57 3.450 78 3.717 71 2.200 60 4.600 88 1.800 53 4.800 76 4.087 78 4.57 3.450 78 3.717 71 2.200 60 4.600 88 1.800 53 4.800 76 4.087 78 4.57		2.283	62	4.833	80	1.967	56	1.867	47	3.733	79	3.333	68	3.850	84	2.350	47
4.700         88         4.350         80         1.983         62         4.850         86         4.533         82         4.500         73         2.383         71         4.55           3.600         85         1.883         58         5.067         76         3.683         81         4.817         77         2.417         50         4.700         80         3.83           1.950         51         4.567         84         2.017         60         4.733         75         4.333         76         4.000         85         1.867         49         2.03           4.350         85         1.750         58         4.567         78         2.300         59         1.983         59         4.167         74         3.833         75         4.33           1.833         54         4.533         73         3.883         76         4.900         89         4.633         80         1.883         55         3.417         64         2.1           3.917         84         3.317         83         3.600         83         4.417         79         2.017         49         4.583         77         4.233         76         4.33		4.533	85	1.833	59	4.500	79	4.700	84	4.233	81	4.167	81	1.933	49	4.933	86
3.600         85         1.883         58         5.067         76         3.683         81         4.817         77         2.417         50         4.700         80         3.83           1.950         51         4.567         84         2.017         60         4.733         75         4.333         76         4.000         85         1.867         49         2.00           4.350         85         1.750         58         4.567         78         2.300         59         1.983         59         4.167         74         3.833         75         4.3           1.833         54         4.533         73         3.883         76         4.900         89         4.633         80         1.883         55         3.417         64         2.1           3.917         84         3.317         83         3.600         83         4.417         79         2.017         49         4.583         77         4.233         76         4.33           4.200         78         3.833         64         4.133         75         1.700         59         5.100         96         4.250         83         4.800         94         4.44		2.883	55	4.783	90	4.000	71	1.783	52	2.233	60	4.333	81	4.500	83	2.900	63
1.950         51         4.567         84         2.017         60         4.733         75         4.333         76         4.000         85         1.867         49         2.00           4.350         85         1.750         58         4.567         78         2.300         59         1.983         59         4.167         74         3.833         75         4.3           1.833         54         4.533         73         3.883         76         4.900         89         4.633         80         1.883         55         3.417         64         2.1           3.917         84         3.317         83         3.600         83         4.417         79         2.017         49         4.583         77         4.233         76         4.3           4.200         78         3.833         64         4.133         75         1.700         59         5.100         96         4.250         83         2.400         53         2.20           1.750         47         2.100         53         4.333         82         4.633         81         1.800         53         3.767         83         4.800         94         4.44     <		4.700	88	4.350	80	1.983	62	4.850	86	4.533	82	4.500	73	2.383	71	4.583	85
4.350         85         1.750         58         4.567         78         2.300         59         1.983         59         4.167         74         3.833         75         4.31           1.833         54         4.533         73         3.883         76         4.900         89         4.633         80         1.883         55         3.417         64         2.12           3.917         84         3.317         83         3.600         83         4.417         79         2.017         49         4.583         77         4.233         76         4.33           4.200         78         3.833         64         4.133         75         1.700         59         5.100         96         4.250         83         2.400         53         2.20           1.750         47         2.100         53         4.333         82         4.633         81         1.800         53         3.767         83         4.800         94         4.44           4.700         83         4.633         82         4.100         70         2.317         50         5.033         77         2.033         51         2.000         55         3.5		3.600	85	1.883	58	5.067	76	3.683	81	4.817	77	2.417	50	4.700	80	3.833	82
1.833       54       4.533       73       3.883       76       4.900       89       4.633       80       1.883       55       3.417       64       2.1         3.917       84       3.317       83       3.600       83       4.417       79       2.017       49       4.583       77       4.233       76       4.3         4.200       78       3.833       64       4.133       75       1.700       59       5.100       96       4.250       83       2.400       53       2.20         1.750       47       2.100       53       4.333       82       4.633       81       1.800       53       3.767       83       4.800       94       4.44         4.700       83       4.633       82       4.100       70       2.317       50       5.033       77       2.033       51       2.000       55       3.5         2.167       52       2.000       59       2.633       65       4.600       85       4.000       77       4.433       78       4.150       76       4.5         1.750       62       4.800       75       4.067       73       1.817       59		1.950	51	4.567	84	2.017	60	4.733	75	4.333	76	4.000	85	1.867	49	2.083	57
3.917       84       3.317       83       3.600       83       4.417       79       2.017       49       4.583       77       4.233       76       4.33         4.200       78       3.833       64       4.133       75       1.700       59       5.100       96       4.250       83       2.400       53       2.20         1.750       47       2.100       53       4.333       82       4.633       81       1.800       53       3.767       83       4.800       94       4.44         4.700       83       4.633       82       4.100       70       2.317       50       5.033       77       2.033       51       2.000       55       3.50         2.167       52       2.000       59       2.633       65       4.600       85       4.000       77       4.433       78       4.150       76       4.50         1.750       62       4.800       75       4.067       73       1.817       59       2.400       65       4.083       84       1.867       50       4.1         4.800       84       4.716       90       4.933       88       4.417       87 <td></td> <td>4.350</td> <td>85</td> <td>1.750</td> <td>58</td> <td>4.567</td> <td>78</td> <td>2.300</td> <td>59</td> <td>1.983</td> <td>59</td> <td>4.167</td> <td>74</td> <td>3.833</td> <td>75</td> <td>4.367</td> <td>82</td>		4.350	85	1.750	58	4.567	78	2.300	59	1.983	59	4.167	74	3.833	75	4.367	82
4.200       78       3.833       64       4.133       75       1.700       59       5.100       96       4.250       83       2.400       53       2.20         1.750       47       2.100       53       4.333       82       4.633       81       1.800       53       3.767       83       4.800       94       4.44         4.700       83       4.633       82       4.100       70       2.317       50       5.033       77       2.033       51       2.000       55       3.50         2.167       52       2.000       59       2.633       65       4.600       85       4.000       77       4.433       78       4.150       76       4.50         1.750       62       4.800       75       4.067       73       1.817       59       2.400       65       4.083       84       1.867       50       4.1         4.800       84       4.716       90       4.933       88       4.417       87       4.600       81       1.833       46       4.267       82       3.8         1.600       52       1.833       54       3.950       76       2.617       53		1.833	54	4.533	73	3.883	76	4.900	89	4.633	80	1.883	55	3.417	64	2.133	67
1.750       47       2.100       53       4.333       82       4.633       81       1.800       53       3.767       83       4.800       94       4.44         4.700       83       4.633       82       4.100       70       2.317       50       5.033       77       2.033       51       2.000       55       3.50         2.167       52       2.000       59       2.633       65       4.600       85       4.000       77       4.433       78       4.150       76       4.50         1.750       62       4.800       75       4.067       73       1.817       59       2.400       65       4.083       84       1.867       50       4.1         4.800       84       4.716       90       4.933       88       4.417       87       4.600       81       1.833       46       4.267       82       3.8         1.600       52       1.833       54       3.950       76       2.617       53       3.567       71       4.417       83       1.750       54       3.9         4.250       79       4.833       80       4.517       80       4.067       69		3.917	84	3.317	83	3.600	83	4.417	79	2.017	49	4.583	77	4.233	76	4.350	74
4.700       83       4.633       82       4.100       70       2.317       50       5.033       77       2.033       51       2.000       55       3.5         2.167       52       2.000       59       2.633       65       4.600       85       4.000       77       4.433       78       4.150       76       4.5         1.750       62       4.800       75       4.067       73       1.817       59       2.400       65       4.083       84       1.867       50       4.1         4.800       84       4.716       90       4.933       88       4.417       87       4.600       81       1.833       46       4.267       82       3.8         1.600       52       1.833       54       3.950       76       2.617       53       3.567       71       4.417       83       1.750       54       3.9         4.250       79       4.833       80       4.517       80       4.067       69       4.000       70       2.183       55       4.483       75       4.4         1.800       51       1.733       54       2.167       48       4.250       77		4.200	78	3.833	64	4.133	75	1.700	59	5.100	96	4.250	83	2.400	53	2.200	54
2.167       52       2.000       59       2.633       65       4.600       85       4.000       77       4.433       78       4.150       76       4.51         1.750       62       4.800       75       4.067       73       1.817       59       2.400       65       4.083       84       1.867       50       4.12         4.800       84       4.716       90       4.933       88       4.417       87       4.600       81       1.833       46       4.267       82       3.8         1.600       52       1.833       54       3.950       76       2.617       53       3.567       71       4.417       83       1.750       54       3.9         4.250       79       4.833       80       4.517       80       4.067       69       4.000       70       2.183       55       4.483       75       4.4         1.800       51       1.733       54       2.167       48       4.250       77       4.500       81       4.800       81       4.000       78       2.0         1.750       47       4.883       83       4.000       86       1.967       56		1.750	47	2.100	53	4.333	82	4.633	81	1.800	53	3.767	83	4.800	94	4.450	83
1.750     62     4.800     75     4.067     73     1.817     59     2.400     65     4.083     84     1.867     50     4.1       4.800     84     4.716     90     4.933     88     4.417     87     4.600     81     1.833     46     4.267     82     3.8       1.600     52     1.833     54     3.950     76     2.617     53     3.567     71     4.417     83     1.750     54     3.9       4.250     79     4.833     80     4.517     80     4.067     69     4.000     70     2.183     55     4.483     75     4.4       1.800     51     1.733     54     2.167     48     4.250     77     4.500     81     4.800     81     4.000     78     2.0       1.750     47     4.883     83     4.000     86     1.967     56     4.083     93     1.833     57     4.117     79     4.23       3.450     78     3.717     71     2.200     60     4.600     88     1.800     53     4.800     76     4.083     78     4.70       3.067     69     1.667     64     4.233 <td< td=""><td></td><td>4.700</td><td>83</td><td>4.633</td><td>82</td><td>4.100</td><td>70</td><td>2.317</td><td>50</td><td>5.033</td><td>77</td><td>2.033</td><td>51</td><td>2.000</td><td>55</td><td>3.567</td><td>73</td></td<>		4.700	83	4.633	82	4.100	70	2.317	50	5.033	77	2.033	51	2.000	55	3.567	73
4.800     84     4.716     90     4.933     88     4.417     87     4.600     81     1.833     46     4.267     82     3.8       1.600     52     1.833     54     3.950     76     2.617     53     3.567     71     4.417     83     1.750     54     3.9       4.250     79     4.833     80     4.517     80     4.067     69     4.000     70     2.183     55     4.483     75     4.4       1.800     51     1.733     54     2.167     48     4.250     77     4.500     81     4.800     81     4.000     78     2.0       1.750     47     4.883     83     4.000     86     1.967     56     4.083     93     1.833     57     4.117     79     4.2       3.450     78     3.717     71     2.200     60     4.600     88     1.800     53     4.800     76     4.083     78     4.7       3.067     69     1.667     64     4.233     90     3.767     81     3.967     89     4.100     84     4.267     78     4.5		2.167	52	2.000	59	2.633	65	4.600	85	4.000	77	4.433	78	4.150	76	4.500	73
1.600     52     1.833     54     3.950     76     2.617     53     3.567     71     4.417     83     1.750     54     3.9       4.250     79     4.833     80     4.517     80     4.067     69     4.000     70     2.183     55     4.483     75     4.4       1.800     51     1.733     54     2.167     48     4.250     77     4.500     81     4.800     81     4.000     78     2.00       1.750     47     4.883     83     4.000     86     1.967     56     4.083     93     1.833     57     4.117     79     4.22       3.450     78     3.717     71     2.200     60     4.600     88     1.800     53     4.800     76     4.083     78     4.70       3.067     69     1.667     64     4.333     90     3.767     81     3.967     89     4.100     84     4.267     78     4.57		1.750	62	4.800	75	4.067	73	1.817	59	2.400	65	4.083	84	1.867	50	4.150	88
4.250     79     4.833     80     4.517     80     4.067     69     4.000     70     2.183     55     4.483     75     4.4       1.800     51     1.733     54     2.167     48     4.250     77     4.500     81     4.800     81     4.000     78     2.0       1.750     47     4.883     83     4.000     86     1.967     56     4.083     93     1.833     57     4.117     79     4.2       3.450     78     3.717     71     2.200     60     4.600     88     1.800     53     4.800     76     4.083     78     4.7       3.067     69     1.667     64     4.233     90     3.767     81     3.967     89     4.100     84     4.267     78     4.5		4.800	84	4.716	90	4.933	88	4.417	87	4.600	81	1.833	46	4.267	82	3.817	80
1.800     51     1.733     54     2.167     48     4.250     77     4.500     81     4.800     81     4.000     78     2.00       1.750     47     4.883     83     4.000     86     1.967     56     4.083     93     1.833     57     4.117     79     4.2       3.450     78     3.717     71     2.200     60     4.600     88     1.800     53     4.800     76     4.083     78     4.7       3.067     69     1.667     64     4.233     90     3.767     81     3.967     89     4.100     84     4.267     78     4.5		1.600	52	1.833	54	3.950	76	2.617	53	3.567	71	4.417	83	1.750	54	3.917	71
1.750 47 4.883 83 4.000 86 1.967 56 4.083 93 1.833 57 4.117 79 4.20 3.450 78 3.717 71 2.200 60 4.600 88 1.800 53 4.800 76 4.083 78 4.70 3.067 69 1.667 64 4.333 90 3.767 81 3.967 89 4.100 84 4.267 78 4.50		4.250	79	4.833	80	4.517	80	4.067	69	4.000	70	2.183	55	4.483	75	4.450	83
3.450 78 3.717 71 2.200 60 4.600 88 1.800 53 4.800 76 4.083 78 4.70		1.800	51	1.733	54	2.167	48	4.250	77	4.500	81	4.800	81	4.000	78	2.000	56
3 067 69 1 667 64 4 333 90 3 767 81 3 967 89 4 100 84 4 267 78 4 5		1.750	47	4.883	83	4.000	86	1.967	56	4.083	93	1.833	57	4.117	79	4.283	79
		3.450	78	3.717	71	2.200	60	4.600	88	1.800	53	4.800	76	4.083	78	4.767	78
Technical Mathematics for Food Technology Correlation		3.067	60	1 667	64	1 333	٩n	3 767	81	3 967	ឧ၀	4 100	8/	4 267	78	1522	84
	Technical Mathematics for Food Technology							Correla	tion								

For the data on the last slide, the residual standard error  $s_e = 5.914$ . The regression line for the sample is

$$\hat{y} = 33.4744 + 10.7296x \tag{12}$$

These numbers were gathered from the R Statistics command summary(lm(faithful[[2]] faithful[[1]])).

The error for the 95% confidence interval is of

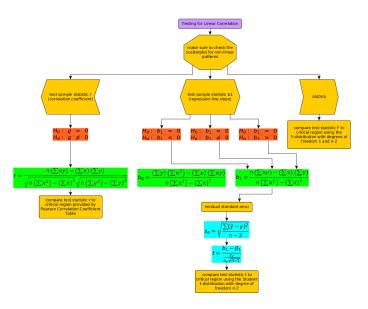
$$E = t_{\frac{\alpha}{2}} \frac{s_{e} \sqrt{\sum x^{2}}}{\sqrt{n} \left(\sum x^{2} - \frac{(\sum x)^{2}}{n}\right)} = 1.968789 \cdot \frac{5.914 \cdot 60.51297}{\sqrt{272} \cdot \left(3661.819 - \frac{899988.1}{272}\right)} = (13)$$

Consequently, the confidence interval

$$b_1 - E < \beta_1 < b_1 + E \tag{14}$$

is (10.60859, 10.85061)

# Flow Chart for Linear Regression Hypothesis Testing



#### End of Lesson

Next Lesson: Goodness of Fit