# Diagnosis, Fault-tolerant and Robust Control for a Torsional Control System

Mandatory assignment in DTU course 31320

# Part A

Mogens Blanke, Dimitrios Papageorgiou Version 1.a February, 2020 Table 1: Revision history

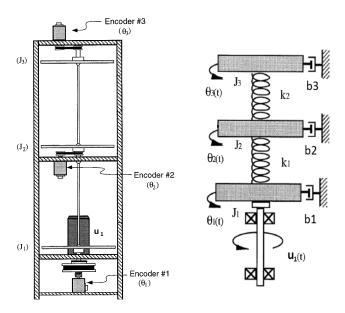
version	date	description	changes
1.a	11.02.2020	new	all pages new
1.b	17.02.2020	added $Q2-Q5$	p. 3 - 4
1.c	27.02.2020	added $Q6-Q7$	p. 5
1.d	02.03.2020	added Q8	p. 6
1.e	08.03.2020	added Q9	p. 6 - 7

# Assignment part A - 2020

#### Introduction

This exercise presents a model of the ECP M205a system. It is a three-mass system that comprises three identical disks, connected in parallel via a flexible low-damped shaft. The system is equipped with three incremental position encoders (one for each disk) and one actuator, i.e. a motor applying torques to the bottom disk.

The control goal is to ensure that either of the disks tracks a specified motion profile. The system considered is sketched in Figure 1. The variables are explained in Table 2.



The normal behaviours of the systems are described by the following constraints:

Table 2: List of variables

variable	$\mathbf{unit}$	description	
$ heta_1$	$\operatorname{rad}$	angular position of bottom disk	
$\omega_1$	$\rm rads^{-1}$	angular velocity of bottom disk	
$ heta_2$	$\operatorname{rad}$	angular position of middle disk	
$\omega_2$	$\rm rads^{-1}$	angular velocity of middle disk	
$\theta_3$	$\operatorname{rad}$	angular position of top disk	
$\omega_3$	$\rm rads^{-1}$	angular velocity of top disk	
u	Nm	torque command for the bottom disk	
$y_1$	$\operatorname{rad}$	measured angular position of bottom disk	
$y_2$	$\operatorname{rad}$	measured angular position of middle disk	
$y_3$	$\operatorname{rad}$	measured angular position of top disk	

$$c_{1}: 0 = \dot{\theta}_{1} - \omega_{1}$$

$$c_{2}: 0 = J_{1}\dot{\omega}_{1} - u + b_{1}\omega_{1} + k_{1}(\theta_{1} - \theta_{2}) + d$$

$$c_{3}: 0 = \dot{\theta}_{2} - \omega_{2}$$

$$c_{4}: 0 = J_{2}\dot{\omega}_{2} + b_{2}\omega_{2} + k_{1}(\theta_{2} - \theta_{1}) + k_{2}(\theta_{2} - \theta_{3})$$

$$c_{5}: 0 = \dot{\theta}_{3} - \omega_{3}$$

$$c_{6}: 0 = J_{3}\dot{\omega}_{3} + b_{3}\omega_{3} + k_{2}(\theta_{3} - \theta_{2})$$

$$d_{7}: 0 = \dot{\theta}_{1} - \frac{d\theta_{1}}{dt}$$

$$d_{8}: 0 = \dot{\omega}_{1} - \frac{d\omega_{1}}{dt}$$

$$d_{9}: 0 = \dot{\theta}_{2} - \frac{d\theta_{2}}{dt}$$

$$d_{10}: 0 = \dot{\omega}_{2} - \frac{d\theta_{3}}{dt}$$

$$d_{11}: 0 = \dot{\theta}_{3} - \frac{d\theta_{3}}{dt}$$

$$d_{12}: 0 = \dot{\omega}_{3} - \frac{d\omega_{3}}{dt}$$

$$m_{13}: 0 = y_{1} - \theta_{1}$$

$$m_{14}: 0 = y_{2} - \theta_{2}$$

$$m_{15}: 0 = y_{3} - \theta_{3}$$

where  $d \triangleq T_C(\omega_1)$  is a function of the bottom disk angular velocity and represents the unknown Coulomb friction torque on that disk. The control input saturates at 2 Nm, i.e.  $u_1 \in [-2,2]$  Nm. The parameters in the forgoing constraints are listed in Table 3.

Table 3: List of parameters

$\operatorname{symbol}$	value	$\operatorname{unit}$	$\operatorname{description}$
$\overline{J_1}$	0.0025	$\mathrm{kgm}^2$	Bottom disk moment of inertia
$J_2$	0.0018	${ m kgm^2}$	Middle disk moment of inertia
$J_3$	0.0018	$\mathrm{kgm}^2$	Top disk moment of inertia
$k_1$	2.7	$Nmrad^{-1}$	Stiffness of the bottom shaft
$k_2$	2.6	${ m Nmrad^{-1}}$	Stiffness of the middle shaft
$b_1$	0.0029	${ m Nmsrad^{-1}}$	Damping/friction on the bottom disk
$b_2$	0.0002	${ m Nmsrad^{-1}}$	Damping/friction on the middle disk
$b_3$	0.00015	$Nmsrad^{-1}$	Damping/friction on the top disk

A Simulink model and a parameter initialisation file have been uploaded to DTU Learn in the *File share/Matlab and Simulink files/Mandatory Assignment Part A* folder for your convenience.

#### Question 1

Make a structural analysis:

- determine a complete matching on the unknown variables,
- find the parity relations in symbolic form,
- investigate other properties you find relevant from a structural analysis,
- reformulate the parity relations to an analytic form, as functions only of known variables and the system parameters.

# Question 2

- Design a set of proper residual generators, ie. residual generators are stable and are causal.
- Implement your residual generators using a Simulink model of the system and demonstrate by simulation that your residuals are insensitive to change of control input.

**Experimental work**: Test the implemented residual generators on the ECP M502a torsional system. Demonstrate their insensitivity to input changes and their fault-detection properties. Comment on the results.

#### Question 3

Write the system in the standard form

$$\dot{x} = Ax + Bu + E_x d$$

$$y = Cx + Du + E_u d$$
(1)

and determine the matrices  $A, B, C, D, E_x$  and  $E_y$ .

## Question 4

Calculate the transfer function matrices  $H_{yu}(s)$ ,  $H_{yd}(s)$  in the standard expression from the textbook,

$$y(s) = H_{yu}(s)u(s) + H_{yd}(s)d(s)$$
(2)

Determine a set of residual generators using a left nullspace design in the frequency domain. Implement the designed residual generators in Matlab/Simulink.

**Experimental work**: Test the implemented residual generators on the ECP M502a torsional system. Demonstrate their insensitivity to input changes and their fault-detection properties. Comment on the results.

**Hints:** For this task it is useful to find a basis for the left nullspace by using the Matlab symbolic toolbox in defining the various transfer functions (e.g. syms s; G = 1/(s + 1)). You may find the following functions useful:

- simplify simplifies symbolic expression,
- expand expands symbolic expression,
- numden extracts enumerator and denominator of symbolic fraction,
- sym2poly converts symbolic polynomial to numeric,
- minreal gives a minimal realization of a transfer function,
- zpk expresses a transfer function as a zero-pole-gain product.

### Question 5

Faults are possible on any of the sensors or at the actuator. Model these as additive faults and determine the transfer function  $H_{rf}(s)$  from faults to residuals in your LTI design. Investigate strong and weak detectability of the faults. What would change in terms of fault detectability if the Coulomb friction function  $T_C(\omega_1)$  were known?

#### Question 6

The sensors have measurement noise. The noise of individual sensors is uncorrelated, i.e.

$$\begin{bmatrix} y_1 \\ y_2 \\ y_3 \end{bmatrix} \sim \mathcal{N} \left( \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}, \begin{bmatrix} \sigma_1^2 & 0 & 0 \\ 0 & \sigma_2^2 & 0 \\ 0 & 0 & \sigma_3^2 \end{bmatrix} \right)$$
 (3)

with  $\sigma_1 = \sigma_2 = \sigma_3 = 10^{-2} \text{ rad.}$ 

Find the discrete-time version of the following residual generator using Matlab c2d with the 'tustin' option and sampling period  $T_s = 0.004$  sec.

$$r(s) = \frac{N_{y_1}(s)}{D(s)}y_1(s) + \frac{N_{y_2}(s)}{D(s)}y_2(s) + \frac{N_{y_3}(s)}{D(s)}y_3(s)$$
(4)

where

$$N_{y_1}(s) = 1.1004 \cdot 10^4$$

$$N_{y_2}(s) = -(7.2199s^2 + 0.6478s + 2.1008 \cdot 10^4)$$

$$N_{y_3}(s) = 1.0003 \cdot 10^4$$

$$D(s) = s^2 + 87.9646s + 3947.8$$

Determine the fault magnitude you could detect on sensor  $y_2$  with a CUSUM algorithm subject to the condition that a fault should be detected within 500 samples, sampling period is  $T_s=0.004$  sec. The time between false alarms should be 3 months or better.

**Experimental work**: Test your CUSUM detector on the ECP M502a torsional system. You can use the 2-sided CUSUM simulink block provided on the course's page. Comment on the results.

# Question 7

Design and implement in Simulink a GLR detector that can detect a sudden offset fault of unknown magnitude in sensor  $y_2$ . For a fault of magnitude  $f_2 = -0.025$  rad determine a threshold h that will give a false alarm probability  $P_F = 0.01$  and the window size M that will give you a probability of missed detection  $P_M = 0.01$  or lower.

**Experimental work**: Test your GLR detector on the ECP M502a torsional system. Demonstrate its robustness properties with respect to false alarms. Comment on the results.

**Hint:** You can use the "Matlab function" block in Simulunk from the "user-defined functions" library.

#### Question 8

Discretize the system with sampling period  $T_s = 4$  ms and design a full state-feedback DLQR that ensures that the top disk tracks a given step change  $\theta_{ref}$  in its position. The resulting closed loop system should have the following form

$$x(k+1) = (F - GK_c)x(k) + GK_cC_{ref}\theta_{ref} + E_xd$$
(5)

$$y(k) = Cx(k) + E_y d (6)$$

with  $F \in \mathbb{R}^{6 \times 6}$ ,  $G \in \mathbb{R}^{6 \times 1}$  being the discretized system matrices and  $C_{ref}$  is a scaling matrix for the scalar reference signal defined as

$$C_{ref} = (C_3(I - F + GK_c)^{-1}GK_c)^+$$
  
 $C_3 = \begin{bmatrix} 0 & 0 & 0 & 1 & 0 \end{bmatrix},$ 

where  $X^+$  denotes the pseudoinverse of a matrix X.

For the design of the DLQR set d=0 and choose the weighting matrices as following:

Implement the controller in Simulink and simulate the closed-loop system for step-wise reference,  $\theta_{ref} = \frac{\pi}{2}$  rad.

Hint: All the states are available for feedback.

#### Question 9

An additive sensor fault  $f_m=0.025$  rad suddenly corrupts the middle disk position measurement after  $t_{f,m}=15$  s, such that

$$y_2^f(t) = y_2(t) + f_m(t) , t \ge t_{f,m} ,$$

where the superscript "f" denotes the corrupted measurement signal. Simulate the effect of the fault and design a virtual sensor to recover from it. Assume that once the fault is detected, the sensor is discarded (C loses a row). Implement the virtual sensor and add it to the existing fault tolerant scheme in Simulink. Simulate the closed-loop system for the same reference and comment on the tracking performance and the outputs of the residuals.

Experimental work: Test the implemented virtual sensor on the ECP M502a torsional system. Use a decision function to enable the virtual sensor whenever

a fault in  $y_2$  is detected. Comment on the quality of the reconstructed measurements and the tracking performance of the closed-loop system in the presence of a fault on  $y_2$ .

#### Practical notes

- The deadline for the report is Wednesday March 18, 2020, at 23:55 hours.
- Please note that max. 20 pages are allowed for part A, excluding front matter. Any pages in excess of 20 (excluding front matter) will be discarded.
- Layout must be reasonable: A4 paper, 20mm margins and font size 11pt.
- The report need be delivered in electronic form, as a .pdf file, via the DTULearn assignment system. Only pdf files are accepted.
- Group-work is encouraged (max 2 persons in one group).
- Please do write your name(s) and student number(s) at the front page and as running head on each page of your report. In addition, do not forget page numbers.